



Prevention of Significant Deterioration Air Construction Permit Application

South Shore Energy, LLC, Dairyland Power Cooperative Nemadji River Generation, LLC

Nemadji Trail Energy Center Project No. 101798

Docket Number: 9698-CE-100

Revision 0

December 2021

Prevention of Significant Deterioration Air Construction Permit Application

prepared for

South Shore Energy, LLC,
Dairyland Power Cooperative
Nemadji River Generation, LLC
Nemadji Trail Energy Center
Superior, Wisconsin

Project No. 101798

Revision 0
December 2021

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LIST OF ABBREVIATIONS

Abbreviation Term/Phrase/Name

(NH₄)₂SO₄ ammonium sulfate

°F degrees Fahrenheit

μg/m³ micrograms per cubic meter

% percent

AERMAP AERMOD terrain pre-processor

AERMOD AMS/EPA Regulatory Model

AMS American Meteorological Society

AQRV Air Quality Related Value

AQS Air Quality System

ARM2 Ambient Ratio Method

AVO audio/visual/olfactory

BACT Best Available Control Technology

BPIP-PRIME Building Profile Input Program - Plume Rise Model Enhancements

CAA Clean Air Act

CAAA Clean Air Act Amendments

CAIR Clean Air Interstate Rule

CAQT critical air quality threshold

CEM continuous emission monitor

CFR Code of Federal Regulations

CH₄ methane

CI compression ignition

CO carbon monoxide

CO₂ carbon dioxide

CO₂e carbon dioxide equivalent

EMISFACT emission factor

EOR enhanced oil recovery

EPA U.S. Environmental Protection Agency

ESP electrostatic precipitator

FDCP Fugitive Dust Control Plan

FGR flue gas recirculation

FLAG Federal Land Managers' Air Quality Related Values Work Group

FLM Federal Land Managers

ft/s feet per second

g/hp-hr gram per horsepower hour

g/kW-hr gram per kilowatt hour

g/m² grams per square meter

GCP good combustion practices

GEP Good Engineering Practice

GHG greenhouse gas

GWP global warming potential

H₂O water

H₂SO₄ sulfuric acid

HAP Hazardous Air Pollutant

hp horsepower

HRSG heat recovery steam generator

ICE internal combustion engine

IEC International Electrotechnical Commission

kg/GJ kilograms per gigajoule

kPa kilopascal

kV kilovolt

kW kilowatt

LAER Lowest Achievable Emission Rate

lb/hr pounds per hour

lb/lb-mol pound per pound-mole

lb/MMBtu pounds per million British thermal units

lb/MW-hr pound per megawatt hour

lb/VMT pounds per vehicle mile traveled

lb/yr pounds per year

LDAR leak detection and repair

LNB low-NO_x burner

MACT Maximum Achievable Control Technology

MECL minimum emissions compliance load

MERP Modeled Emission Rates for Precursors

mg/L milligrams per liter

mg/m³ milligrams per cubic meter

MMBtu/hr million British thermal units per hour

MW megawatt

N₂O nitrogen oxide

NAAQS National Ambient Air Quality Standards

NAD 83 North American Datum of 1983

NAICS North American Industrial Classification System

NED National Elevation Dataset

NESHAP National Emission Standards for Hazardous Air Pollutants

ng/J nanogram per Joule

NH₃ ammonia

NH₄HSO₄ ammonium bisulfate

NMHC non-methane hydrocarbon

NO₂ nitrogen dioxide

NO_x nitrogen oxides

NPS National Park Service

NSPS New Source Performance Standards

NSR New Source Review

NSRP-3 National Atmospheric Deposition Program

NTEC Nemadji Trail Energy Center

 O_2 oxygen

OLM Ozone Limiting Method

PBL Planetary Boundary Layers

PM particulate matter

PM₁₀ particulate matter less than 10 microns in diameter

PM_{2.5} particulate matter less than 2.5 microns in diameter

ppb parts per billion

ppm parts per million

PRIME Plume Rise Model Enhancements algorithm

PSD Prevention of Significant Deterioration

psia pounds per square inch

PVMRM Plume Volume Molar Ratio Method

Q/D emissions (Q) divided by distance (D) screening procedure for Class I

areas

RACT Reasonable Available Control Technology

RBLC RACT/BACT/LAER Clearinghouse

RICE Reciprocating Internal Combustion Engines

RMP Risk Management Plan

SCR selective catalytic reduction

SF₆ sulfur hexafluoride

SIC Standard Industrial Classification

SNCR selective non-catalytic reduction

SO₂ sulfur dioxide

SO₃ sulfur trioxide

TCEQ Texas Commission on Environmental Quality

tpy tons per year

| <u>Abbreviation</u> | Term/Phrase/Name |
|---------------------|---------------------|
| USFS | U.S. Forest Service |

USFWS U.S. Fish and Wildlife Service

USGS U.S. Geological Survey

UTM Universal Transverse Mercator

VOC volatile organic compound

VMT vehicle miles traveled

WAC Wisconsin Administrative Code

WDNR Wisconsin Department of Natural Resources

1.0 EXECUTIVE SUMMARY

Pursuant to the requirements specified in the Wisconsin Administrative Code (WAC) Chapter NR 405, South Shore Energy, LLC, a subsidiary of ALLETE, Inc., Dairyland Power Cooperative, and Nemadji River Generation, LLC, a subsidiary of Basin Electric Power Cooperative, (collectively the Owners), are submitting this Prevention of Significant Deterioration (PSD) air construction permit application for the proposed construction of a combined-cycle combustion turbine and associated support equipment at the Nemadji Trail Energy Center (NTEC) (Project) (FID 816127840). The Project, approximately 625-megawatts (MW), will be a greenfield site located east of the existing Enbridge Energy Superior Terminal Facility on the banks of the Nemadji River in the City of Superior in Douglas County, Wisconsin.

The Owners have two current Air Pollution Control Construction Permits for this facility. Permit 18-MMC-168 is for the installation of a combined-cycle facility and permit 21-MMC-011 is for the installation of fugitive emissions of air contaminants from piping components and haul road traffic fugitive emissions. The Owners wish to extend the construction permit expiration date so that construction can commence in 2023. As requested by Wisconsin Department of Natural Resources (WDNR), a new comprehensive permit application that includes all previously submitted permit application materials is being submitted to accomplish this permit action. As part of this submittal the Best Available Control Technology (BACT) and air dispersion modeling analysis are being updated to current standards.

This construction permit application is divided into the following sections:

- Part 1 Executive Summary
- Part 2 Project Description
- Part 3 Emissions Estimates (This section provides estimates of emissions associated with the Project.)
- Part 4 Regulatory Review (This section identifies applicable State and Federal air quality regulations.)
- Part 5 –BACT Analysis
- Part 6 Air Dispersion Modeling (This section provides model descriptions and data requirements for the air quality impact assessment as well as interpretation, analysis, and comparison of the modeling results with applicable air quality regulations.)
- Part 7 Additional Impact Analysis (This section addresses other potential air quality-related impacts (i.e., growth, soil, vegetation, and visibility).)

Construction permit application forms required by the WDNR are included in Appendix A of this application.

1.1 Project Equipment

The Project will consist of one H-Class combustion turbine with a heat recovery steam generator (HRSG) with duct burner and one steam turbine in a combined-cycle configuration along with associated support equipment. The Project is expected to be approximately 625 MW. The combustion turbine will be designed to utilize pipeline-quality natural gas and combust fuel oil (ultra-low sulfur diesel) as back-up fuel. In addition to the combustion turbine, an auxiliary boiler, circuit breakers, two natural gas-fired gas heaters (natural gas heater), an emergency diesel fire pump, an emergency diesel generator, fuel oil storage tanks, haul roads, and natural gas and fuel oil piping components will be included as part of the Project.

1.2 Project Emissions

As required pursuant to WAC Chapter NR 405, this permit application contains the following analyses/assessments regarding emissions of regulated pollutants associated with the construction and operation of the Project:

- Evaluation of ambient air quality in the area for each regulated pollutant for which the Project will result in a PSD significant net emissions increase
- Demonstration that emissions increases resulting from the Project will not cause or contribute to an increase in ambient concentrations of pollutants exceeding the remaining available PSD increment and the National Ambient Air Quality Standards (NAAQS)
- Assessment of any adverse impacts on soils, vegetation, visibility, and growth in the area
- A BACT analysis for each PSD-regulated pollutant for which the Project will result in a significant net emissions increase

Potential emissions from the Project are shown in Table 1-1 which includes start-up and shutdown emissions for the combustion turbine and auxiliary equipment emissions. A full description of equipment associated with the Project is provided in Part 2.0 of this application.

| Pollutant | Project Potential Emissions ^a (tons per year) | PSD Significance Level ¹ (tons per year) |
|-------------------------------------|--|---|
| NO_x | 269 | 40 |
| CO | 2,003 | 100 |
| PM | 167 | 25 |
| PM_{10}^{b} | 167 | 15 |
| $PM_{2.5}^{b}$ | 167 | 10 |
| SO_2 | 29 | 40 |
| VOC | 250 | 40 |
| H ₂ SO ₄ mist | 43 | 7 |
| Lead | 0.01 | 0.6 |
| CO ₂ e | 2,739,294 | 75,000 ² |

Table 1-1: Project Potential Emissions and PSD Significance Levels

Source:

- (1) 40 CFR 52.21(b)(23)(i)
- (2) 40 CFR 52.21(b)(49)(iv)(a)
- (a) Numbers in **bold** indicate the PSD significance level is exceeded
- (b) Filterable plus condensable

The Project is an area (minor) source of Hazardous Air Pollutants (HAPs) (less than 25 tons per year of total HAPs and less than 10 tons per year of any single HAP).

1.3 BACT

The updated BACT analysis shows that the BACT determination in the original applications and PSD permit remain valid. The controls and emission limitations have not changed since the permit issuance date.

A "top-down" BACT analysis was performed for each of the pollutants in Table 1-1 that was above its corresponding PSD significance level: nitrogen oxides (NO_x), carbon monoxide (CO), particulate matter (PM)/ particulate matter of 10 microns in diameter or smaller (PM₁₀)/ particulate matter of 2.5 microns in diameter or smaller (PM_{2.5}), volatile organic compounds (VOC), sulfuric acid (H₂SO₄) mist, and greenhouse gases (CO₂e). In addition, WDNR also requires a BACT analysis for opacity.

State-of-the-art pollution control equipment has been selected as BACT for the Project. Emissions of NO_x from the combustion turbine will be controlled by low-NO_x burners. Emissions of NO_x from both the combustion turbine and the duct burner will be controlled with selective catalytic reduction (SCR). Emissions of CO and VOC will be controlled by good combustion practices as well as an oxidation catalyst (also referred to as a CO catalyst). Use of clean fuels and good combustion practices will control

emissions of H₂SO₄ mist and PM/PM₁₀/PM_{2.5}. Greenhouse gas emissions will be controlled with the use of natural gas fuel, monitoring and control of excess air, and efficient turbine design. To minimize the near-stack opacity, the combustion turbine will be controlled through the use clean fuels and good combustion practices. Table 1-2 displays the BACT results.

Table 1-2: Summary of BACT Results - Combustion Turbine

| Pollutant | Fuel | Control | BACT Emissions ^{a,b} | Average |
|-------------------------------------|----------------|--|---|---------------------|
| NOx | Natural gas | Selective catalytic reduction (SCR) and low-NO _x burners | 2 ppm (with or without duct firing) | 24-hour rolling |
| IVOχ | Fuel oil | SCR and water injection | 6 ppm (with or without duct firing) | 24-hour rolling |
| СО | Natural gas | Good combustion practices, oxidation catalyst | 1.5 ppm (with or without duct firing) ^c | 168-hour rolling |
| CO | Fuel oil | Good combustion practices, oxidation catalyst | 1.5 ppm (with or without duct firing) ^c | 168-hour rolling |
| PM/PM ₁₀ / | Natural gas | Combustion controls and low ash fuels | 36.3 lb/hr (with duct firing) 21.8 lb/hr (without duct firing) | NA |
| PM _{2.5} | Fuel oil | Combustion controls and 54.5 lb/br (with duct firing) | | NA |
| VOC | Natural gas | Good combustion practices, oxidation catalyst | 2.7 ppm (with duct firing) 0.6 ppm (without duct firing) | 168-hour rolling |
| VOC | Fuel oil | Good combustion practices, oxidation catalyst | 3.3 ppm (with duct firing) 0.6 ppm (without duct firing) | 168-hour rolling |
| H ₂ SO ₄ mist | Natural gas | Combustion controls and low sulfur fuels | 9.9 lb/hr (with duct firing) 7.8 lb/hr (without duct firing) | NA |
| 1125O4 IIIst | Fuel oil | Combustion controls and low sulfur fuels | 9.3 lb/hr (with duct firing) 7.0 lb/hr (without duct firing) | NA |
| Natura gas | | Use of natural gas as a fuel, monitoring and control of excess air, efficient turbine design, and oxidation catalyst | 850 lb CO ₂ /MW-hr, gross | 12-month rolling |
| Greenhouse gases | Fuel oil | Use of ultra-low sulfur diesel as a fuel, monitoring and control of excess air, efficient turbine design, and oxidation catalyst | 1,180 lb CO ₂ /MW-hr, gross | 12-month rolling |
| Opacity | Both | Low-NO _x burners, SCR, combustion controls, low ash fuels | N/A | N/A |

Source: Construction permit no.: 18-MMC-168

⁽a) ppm = parts per million; lb/hr = pounds per hour; lb/MW-hr = pound per megawatt hour

⁽b) Concentration at 15 percent oxygen while operating at MECL and greater under steady state conditions, unless otherwise noted

⁽c) Natural gas limit valid for 100% load with duct firing down to MECL. Fuel oil limit valid for 100% load with duct firing down to 75% load.

1.4 Air Quality Analysis

The existing air quality in the Douglas County area is designated as attainment or unclassifiable in regard to the NAAQS for all criteria pollutants. An air dispersion modeling analysis was performed for the pollutants subject to PSD to assess potential ambient air quality impacts associated with the Project. The modeling was performed in accordance with approved WDNR and U.S. Environmental Protection Agency (EPA) modeling guidance.

The modeling analysis (included in Part 6.0 of this application) demonstrates that operation of the Project will not cause or contribute to a violation of the NAAQS or PSD increments, as applicable.

1.5 Additional Impacts Analysis

The potential impacts of the proposed Project on visibility, soils, vegetation, and growth are discussed in Part 7.0 of this application. As indicated by the analysis, the addition of the Project will not have a significant impact on visibility, soils, growth, or vegetation in the surrounding area.

2.0 PROJECT DESCRIPTION

Section 2.0 overview: The references to the most current project descriptions for the permitted units are presented in Table 2-1. A 12-cell cooling tower was initially permitted as part of the Project and was removed as part of a permit modification request dated June 5, 2020.

Table 2-1: Project Description References

| Unit ID | Description | Previous Application Reference | December 2021 Submittal Location |
|---------|--|---|-------------------------------------|
| P01 | Combined-Cycle Turbine | 2.0 Project Description December 2018 Submittal | 2.0 Project Description |
| B02 | Auxiliary boiler | 2.0 Project Description December 2018 Submittal | 2.0 Project Description |
| F03 | Circuit breakers | 1.0 Introduction June 2020 Submittal | 2.0 Project Description |
| P04 | Natural gas-fired heater | 2.0 Project Description December 2018 Submittal | 2.0 Project Description |
| P05 | Natural gas-fired heater | 2.0 Project Description December 2018 Submittal | 2.0 Project Description |
| P06 | Emergency diesel fire pump | 2.0 Project Description December 2018 Submittal | 2.0 Project Description |
| P07 | Emergency diesel generator | 2.0 Project Description December 2018 Submittal | 2.0 Project Description |
| T01 | Diesel fuel day tank | 2.0 Project Description December 2018 Submittal | 2.0 Project Description |
| T02 | Diesel fuel generator tank | 2.0 Project Description December 2018 Submittal | 2.0 Project Description |
| Т03 | Diesel fuel fire pump tank | 2.0 Project Description December 2018 Submittal | 2.0 Project Description |
| F01 | Haul roads | 2.0 Project Description January 2021 Submittal | 2.0 Project Description |
| F02 | Natural gas and fuel oil piping components | 2.0 Project Description January 2021 Submittal | 2.0 Project Description |
| | Project location | Appendix B – Figure B-1 January 2021 Submittal | Appendix B – Figure B-1 |
| | Site plot plan | Appendix B – Figure B-2 January 2021 Submittal | Appendix B – Figure B-2 |

The Project will be located east of the existing Enbridge Energy Superior Terminal Facility on the banks of the Nemadji River in the City of Superior in Douglas County, Wisconsin. The Project location and site plot plan are shown in Figures B-1 and B-2 (Appendix B). Douglas County is currently designated as an attainment/unclassified area for all criteria pollutants in 40 Code of Federal Regulations (CFR) Part 81.

2.1 Turbine (P01) and Emission Controls

The Project will use H-Class combined-cycle turbine technology to generate electricity. The duct burner will combust natural gas and heat the exhaust gas from the combustion turbine within the HRSG. The combustion turbine is proposed to be permitted to operate year-round with no hourly restrictions in combined-cycle mode when combusting natural gas.

The combustion turbine will combust fuel oil when natural gas is unavailable due to limited availability and/or curtailment. Fuel oil, when combusted, will be limited to 11.0 million gallons per year of fuel oil.

To control emissions of NO_x, the combustion turbine will be equipped with low-NO_x burners. In addition, SCR will be added in the HRSG to further reduce NO_x emissions. To minimize emissions of sulfur dioxide (SO₂), H₂SO₄ mist, and PM/PM₁₀/PM_{2.5}, the combustion turbine will be controlled by using clean fuels and good combustion practices. Emissions of CO and VOC will be controlled by using an oxidation catalyst and good combustion practices. Greenhouse gas emissions will be controlled with the use of natural gas or ultra-low sulfur diesel fuel, monitoring, control of excess air, efficient turbine design, and use of an oxidation catalyst.

2.2 Auxiliary Boiler (B02)

A 100 million British thermal units per hour (MMBtu/hr) natural gas-fired auxiliary boiler will be constructed to support the operations of the Project and will be permitted for 8,760 hours of operation per year. The auxiliary boiler will be designed with ultra-low NO_x burners, flue gas recirculation (FGR), and oxidation catalyst.

2.3 Sulfur Hexafluoride (SF₆) Containing Equipment (F03)

The following SF₆-containing circuit breaker equipment is proposed:

- Three 345-kilovolt (kV) circuit breakers are proposed for the substation.
- Two 19-kV (estimate) low-side generator circuit breakers will be located in the plant before the step-up transformers that feed the onsite switchyard.

Note that the Project will include six disconnect switches at each substation site; however, the switches are open air type switches and do not contain SF₆.

2.4 Natural Gas Heaters (P04 and P05)

Two natural gas-fired heaters will be used to heat the natural gas prior to combustion in the turbine. Both heaters will be permitted for unlimited operation. The gas heaters will be designed with low-NO_x burners.

2.5 Emergency Diesel Fire Pump (P06)

An emergency diesel fire pump will be built to support the Project in case of a fire. The emergency diesel fire pump will have a maximum power output of 282 horsepower (hp) and will be fired solely by ultralow sulfur diesel. The Owners propose to operate the emergency diesel fire pump for up to 500 hours annually for testing and maintenance purposes, and therefore supports a limit on routine hours of operation of the emergency diesel fire pump.

2.6 Emergency Diesel Generator (P07)

An emergency diesel generator will be built to support the Project's combustion turbine in case of a power interruption. The emergency diesel generator will have a maximum power output of 1,490 hp (1,112 kilowatt [kW]) and will be fired solely by ultra-low sulfur diesel. The Owners propose to operate the emergency diesel generator for up to 500 hours annually for testing and maintenance purposes, and therefore supports a limit on routine hours of operation of the emergency diesel generator.

2.7 Diesel Storage Tanks (T01, T02, and T03)

The project will include three diesel storage tanks: one 180,000-gallon tank, one 1,700-gallon tank, and one 350-gallon tank. These tanks will store diesel fuel for the combustion turbine, emergency diesel generator, and emergency diesel fire pump.

2.8 Haul Road Traffic Fugitives (F01)

Miscellaneous supplies associated with facility operation will be transported to and from the site via trucks. Up to 520 trucks per year are expected for delivery or removal. Some examples of activities associated with facility operation are as follows, but not limited to, aqueous ammonia for emissions control and water treatment and fuel oil for emergency equipment.

To mitigate onsite road emissions from these deliveries, NTEC will pave the primary facility roads. Both fuel oil and natural gas to the combustion turbine and duct burner will be delivered to the site via pipeline and not by truck delivery.

2.9 Natural Gas and Fuel Oil Fugitives (F02)

The proposed project will include natural gas piping components from the natural gas line that will enter the project site to provide gas for the combustion turbine, duct burner, natural gas heaters and auxiliary boiler. These natural gas piping components are potential sources of methane and VOC emissions due to emissions from valves, flanges, sampling connections and relief valves.

The proposed project will also include fuel oil piping components from the fuel oil line that will enter the project site to provide fuel oil for the combustion turbine and duct burner, as well as the emergency diesel fire pump and emergency diesel generator. These fuel oil piping components are potential sources of methane and VOC emissions due to emissions from valves, flanges, sampling connections and relief valves.

3.0 EMISSIONS ESTIMATES

Section 3.0 overview: The references to the most current emissions estimates write-up sections for the permitted units are presented in Table 3-1. Overall potential emissions from the Project are shown in Table 1-1 of this application. The emissions calculations for each permitted unit are presented in Appendix C and capture all project updates that have occurred throughout the permitting process. Updates to the previously submitted emissions calculations in Appendix C and in Table 3-4 and Table 3-5 in this section are the result of project updates and post application submittal actions.

Table 3-1: Emissions Estimates References

| Unit ID | Description | Previous Application Reference | December 2021 Submittal Location |
|---------|--|---|-------------------------------------|
| P01 | Combined-Cycle Turbine | 3.0 Emissions Estimates December 2018 Submittal | 3.0 Emissions Estimates |
| B02 | Auxiliary boiler | 3.0 Emissions Estimates December 2018 Submittal | 3.0 Emissions Estimates |
| F03 | Circuit breakers | 1.0 Introduction June 2020 Submittal | 3.0 Emissions Estimates |
| P04 | Natural gas-fired heater | 3.0 Emissions Estimates December 2018 Submittal | 3.0 Emissions Estimates |
| P05 | Natural gas-fired heater | 3.0 Emissions Estimates December 2018 Submittal | 3.0 Emissions Estimates |
| P06 | Emergency diesel fire pump | 3.0 Emissions Estimates December 2018 Submittal | 3.0 Emissions Estimates |
| P07 | Emergency diesel generator | 3.0 Emissions Estimates December 2018 Submittal | 3.0 Emissions Estimates |
| T01 | Diesel fuel day tank | 3.0 Emissions Estimates December 2018 Submittal | 3.0 Emissions Estimates |
| T02 | Diesel fuel generator tank | 3.0 Emissions Estimates December 2018 Submittal | 3.0 Emissions Estimates |
| Т03 | Diesel fuel fire pump tank | 3.0 Emissions Estimates December 2018 Submittal | 3.0 Emissions Estimates |
| F01 | Haul roads | 3.0 Emissions Estimates January 2021 Submittal | 3.0 Emissions Estimates |
| F02 | Natural gas and fuel oil piping components | 3.0 Emissions Estimates January 2021 Submittal | 3.0 Emissions Estimates |

Emissions of air contaminants will result from the combustion of natural gas and fuel oil in the combustion turbine and natural gas in the duct burner. There will also be emissions of air contaminants generated from the auxiliary equipment: an auxiliary boiler, circuit breakers, two natural gas heaters, an emergency diesel fire pump, an emergency diesel generator, fuel oil storage tanks, haul roads, and natural gas and fuel oil piping components.

Process flow diagrams for the combustion turbine process and auxiliary equipment are located in Appendix A. Each emission point's control device descriptions, control efficiencies, and procedures for estimating emissions is discussed in detail in the sections below. Tables summarizing the emissions estimates are included in Appendix C.

3.1 Combustion Turbine (P01)

The following sections summarize the combustion turbine hours of operation, emissions estimates for various operating loads when combusting natural gas and fuel oil, and start-up/shutdown operation.

3.1.1 Combustion Turbine Hours of Operation

The following conservative assumptions were applied to seven combustion turbine operating scenarios to determine maximum potential annual emissions as shown in Table 3-2.

| | Scenario | | | | | | |
|--|----------|---|---|---|---|---|---|
| Type of Operation | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| Natural gas with duct firing | X | X | X | | | X | X |
| Natural gas (normal operation) | | | | X | X | | |
| Natural gas start-up/shutdown | | X | X | X | X | | X |
| Fuel oil with duct firing ^a | | | | | | X | X |
| Fuel oil (normal operation) ^a | | | X | | X | | |
| Fuel oil start-un/shutdowna | | | Y | | Y | Y | Y |

Table 3-2: Combustion Turbine Operating Cases for Maximum Potential Annual Emissions

Start-up and shutdown emissions were based on the start-up and shutdown profiles for the combined-cycle combustion turbine and the number of start-up and shutdown events per year for each fuel. The Owners are requesting the following start-up and shutdown limits:

- An hours per year limit on start-up and shutdown (1,525 hours per year for start-up and shutdown, combined) for natural gas operation
- 42 start-ups and 42 shutdowns per year for fuel oil operation.

3.1.2 Combustion Turbine Operation Emissions

Emissions from the combustion turbine are dependent on ambient temperature conditions and the turbine's operating load, which can vary from 33 to 100 percent. To account for representative seasonal climatic variations, potential emissions from the proposed combustion turbine were analyzed at the

⁽a) Fuel oil, when combusted, will be limited to 11.0 million gallons per year of fuel oil.

minimum emissions compliance load (MECL) (designated as "low"), 75, and 100 percent load conditions for ambient temperatures ranging from negative (-)34.3 degrees Fahrenheit (°F) to 95.5°F. The projected emissions were based on data provided by the combustion turbine manufacturer and/or from AP-42 emission factors. Detailed calculations of the combustion turbine's emissions are provided in Appendix C of this application.

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For purposes of emission calculations and modeling, the MECL ranges from 33 to 50 percent load, depending on ambient conditions, and was grouped as "low" load. When grouping, the worst-case parameters were chosen (highest emission rate, lowest temperature, lowest flow rate).

Based on the above assumptions, the maximum expected hourly emission rates for normal operation (excluding start-up and shutdown) for the combustion turbine are shown in Table 3-3.

| | • | • | | |
|--|------------------------------------|-----------------------------|------------------------------|-----------------------|
| | Natural Gas with Duct Firing | Natural Gas 100% Load | Fuel Oil with Duct Firing | Fuel Oil 100% Load |
| Pollutant | | pounds | per hour | |
| NO_x | 33.5 | 26.5 | 72.7 | 51.6 |
| CO | 15.3 | 12.1 | 11.1 | 7.8 |
| PM/PM ₁₀ /PM _{2.5} | 36.3 | 21.8 | 54.5 | 39.4 |
| SO_2 | 6.4 | 5.1 | 6.1 | 4.6 |
| VOC | 15.5 | 2.8 | 14.1 | 1.8 |
| H ₂ SO ₄ mist | 9.9 | 7.8 | 9.3 | 7.0 |
| Lead | | | 0.04 | 0.04 |
| CO ₂ e | 592,127 | 469,787 | 947,846 | 819,965 |

Table 3-3: Maximum Expected Hourly Combustion Turbine Emission Rates

3.1.3 Combustion Turbine Start-Up and Shutdown Emissions Calculation Method

The combustion turbine emissions are based on 1,525 hours per year for start-up and shutdown, combined, for natural gas operation. Potential start-up and shutdown emissions were based on a start-up profile and conservatively assumed that there will be a combination of cold starts, warm starts, hot-fast starts, and shutdown on natural gas. There will also be up to 42 start-ups and 42 shutdown events per year on fuel oil. One start-up/shutdown event is equivalent to one start-up plus one shutdown.

Potential start-up and shutdown emissions for natural gas and fuel oil combustion are shown in Table 3-4 and Table 3-5, respectively. Detailed calculations of the potential start-up and shutdown emissions are provided in Appendix C.

Table 3-4: Potential Natural Gas Turbine Start-up and Shutdown Emissions

| Pollutant | Sta | art-up Emissio | Shutdown Emissions | Start-up and Shutdown Emissions ^a | |
|-------------------------------------|---------------|------------------|-----------------------|--|---------------|
| | lb/cold start | lb/warm start | lb/hot-fast start | lb/shutdown | tons per year |
| NO_x | 335.0 | 233.0 | 111.0 | 59.0 | 108.3 |
| СО | 11,066 | 6,495 | 779.0 | 463.0 | 1,369 |
| $PM/PM_{10}/PM_{2.5}$ | 43.6 | 29.1 | 16.3 | 10.9 | 16.6 |
| SO_2 | 10.2 | 6.8 | 3.8 | 2.6 | 3.9 |
| VOC | 950.0 | 558.0 | 67.0 | 40.0 | 117.8 |
| H ₂ SO ₄ mist | 15.6 | 10.4 | 5.9 | 3.9 | 6.0 |
| Lead | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| CO ₂ e | 939,573 | 626,382 | 352,340 | 234,893 | 358,212 |

⁽a) Emissions are based on 1,525 hours per year for start-up and shutdown, combined, for natural gas operation.

Table 3-5: Potential Fuel Oil Turbine Start-up and Shutdown Emissions

| Pollutant | Start-up Shutdown Emissions Emissions | | Start-up and Shutdown Emissions ^a | |
|--|--|-------------|--|--|
| | lb/start | lb/shutdown | tons per year | |
| NO_x | 860.0 | 108.0 | 20.3 | |
| СО | 25,846 | 1,227 | 568.5 | |
| PM/PM ₁₀ /PM _{2.5} | 78.9 | 19.7 | 2.1 | |
| SO_2 | 9.2 | 2.3 | 0.2 | |
| VOC | 2,951 | 122.0 | 64.5 | |
| H ₂ SO ₄ mist | 14.0 | 3.5 | 0.4 | |
| Lead | 0.08 | 0.02 | 0.002 | |
| CO ₂ e | 1,639,929 | 409,982 | 43,048 | |

⁽a) Emissions are based on 42 start-ups and 42 shutdowns

3.2 HAP Emissions

The Project is an area source of HAPs (*i.e.*, less than 25 tons per year of total HAPs and less than 10 tons per year of any single HAP). HAP emission calculations and a summary of HAP emissions are included in Appendix C.

3.3 Auxiliary Boiler Emissions (B02)

One 100 MMBtu/hr auxiliary boiler will be installed at the facility to be used while the combustion turbine is operating. The boiler will be fired with natural gas. The auxiliary boiler will be limited to annual operations of 8,760 hours. Emissions for this unit were estimated based on AP-42 emission factors and vendor data. Greenhouse gas emissions were estimated based on the emission factors in 40 CFR Part 98. Detailed calculations are provided in Appendix C.

3.4 SF₆ Containing Equipment (F03)

Annual potential to emit emissions of SF₆ from the circuit breakers were based on maximum leakage rate of 0.5 percent per year, the amount of SF₆ in each size of circuit breaker, and the global warming potential (GWP). Project potential emissions of CO₂e leakage from all proposed circuit breakers combined are estimated to be 120 tons per year. A detailed report of the SF₆ emissions is provided in Appendix C of this application.

3.5 Natural Gas Heaters Emissions (P04 and P05)

Two 10.0 MMBtu/hr natural gas-fired heaters will be installed at the facility to heat the natural gas prior to being combusted in the combustion turbine. As a worst-case estimate, it is assumed that annual operations will be 8,760 hours per year for each heater. Emissions for the gas heaters were estimated based on AP-42 emission factors. Greenhouse gas emissions were estimated based on the emission factors in 40 CFR Part 98. Detailed calculations are provided in Appendix C.

3.6 Emergency Diesel Fire Pump Emissions (P06)

One 282-hp diesel fire pump will be installed for emergency power use at the facility. The fire pump will be fired with ultra-low sulfur diesel. Emissions for the emergency diesel fire pump were estimated assuming an annual testing and maintenance schedule of 500 hours. Emissions for this unit were estimated based on New Source Performance Standards (NSPS) limits and AP-42 emission factors. Greenhouse gas emissions were estimated based on the emission factors in 40 CFR Part 98. Detailed calculations of diesel fire pump emissions are provided in Appendix C.

3.7 Emergency Diesel Generator Emissions (P07)

One 1,490 hp (1,112 kW) diesel generator will be installed for emergency power use at the facility; the generator will be fired with ultra-low sulfur diesel. Emissions for the emergency diesel generator were estimated assuming an annual testing and maintenance schedule of 500 hours. Emissions for this unit were estimated based on NSPS limits and AP-42 emission factors. Greenhouse gas emissions were

estimated based on the emission factors in 40 CFR Part 98. Detailed calculations of diesel generator emissions are provided in Appendix C.

3.8 Diesel Storage Tanks Calculation Method (T01, T02, and T03)

The project will include three diesel storage tanks: one 180,000-gallon tank, one 1,700-gallon tank, and one 350-gallon tank. Emissions from loading and breathing losses were estimated for the storage tanks using the EPA TANKS emission software. A detailed report of the fuel oil storage tank emissions is provided in Appendix C.

3.9 Haul Road Traffic Fugitives Calculation Method (F01)

Emissions from haul roads due to traffic were estimated using the paved roads, size-specific emission calculation equation below:

$$E = k * (sL)^{0.91} 0.91 * (W)^{1.02}$$

Where:

E = pounds per vehicle miles traveled (lb/VMT)

sL = silt loading grams per square meter (g/m²) = 2.4 g/m²

W = mean vehicle weight (tons)

k = constant (AP-42 Table 13.2-1.1)

The mean vehicle weight is calculated by averaging the loaded and unloaded vehicle weights. The "ubiquitous baseline" of 0.6 g/m² was selected from the less than 500 average daily traffic category in AP-42 Table 13.2.1-2; and the ubiquitous winter baseline multiplier during months with frozen precipitation (x4) was applied to this value to obtain a silt loading value of 2.4 g/m² for all paved roads.

For paved roads, vehicle miles traveled (VMT) is calculated as follows:

 $VMT = length \ of \ path \ haul \ road \ vehicle \ travels * maximum \ trips \ (hourly \ or \ annual)$

Whether a vehicle travels the haul road twice (back and forth) or once (when traveling in a loop) was accounted for when calculating the miles traveled for each haul road route. Detailed calculations of haul road emissions are provided in Appendix C.

3.10 Natural Gas and Fuel Oil Fugitives Calculation Method (F02)

Fugitive emissions will come from small leaks in equipment connections throughout the facility. The estimated number of connectors, flanges, open ended lines, pump seals and valves were determined from engineering plans for the facility. The emissions were then estimated using the 1995 Protocol for

Equipment Leak Emission Estimates- EPA-453/R-95-017. The emissions estimates for fuel oil fugitives is "total organics" which includes non-VOCs such as methane and ethane and is assumed to be VOCs for the purposes of this application. The emissions estimates for natural gas VOC fugitive emissions was calculated using the minimum methane content. Further, to determine natural gas CO₂e fugitive emissions the maximum methane content was used. Detailed calculations of natural gas and fuel oil fugitives are provided in Appendix C.

4.0 REGULATORY REVIEW

Overview: The references to the most current regulatory review sections for the permitted units are presented in Table 4-1. Specific post-application regulatory updates are also referenced.

Table 4-1: Regulatory Review References

| Unit ID | Description | Previous Application Reference | December 2021 Submittal Location |
|-------------|--|---|---|
| P01 | Combined-Cycle Turbine | 4.0 Regulatory Review December 2018 Submittal | 4.0 Regulatory Review |
| B02 | Auxiliary boiler | 4.0 Regulatory Review December 2018 Submittal | 4.0 Regulatory Review |
| F03 | Circuit breakers | Appendix A - Form 4530-132 June 2020 Submittal | 4.0 Regulatory Review |
| P04 | Natural gas-fired heater | 4.0 Regulatory Review December 2018 Submittal | 4.0 Regulatory Review |
| P05 | Natural gas-fired heater | 4.0 Regulatory Review December 2018 Submittal | 4.0 Regulatory Review |
| P06 | Emergency diesel fire pump | 4.0 Regulatory Review December 2018 Submittal | 4.0 Regulatory Review |
| P07 | Emergency diesel generator | 4.0 Regulatory Review December 2018 Submittal | 4.0 Regulatory Review |
| T01 | Diesel fuel day tank | 4.0 Regulatory Review December 2018 Submittal | 4.0 Regulatory Review |
| T02 | Diesel fuel generator tank | 4.0 Regulatory Review December 2018 Submittal | 4.0 Regulatory Review |
| Т03 | Diesel fuel fire pump tank | 4.0 Regulatory Review December 2018 Submittal | 4.0 Regulatory Review |
| F01 | Haul roads | 4.0 Regulatory Review January 2021 Submittal | 4.0 Regulatory Review |
| F02 | Natural gas and fuel oil piping components | 4.0 Regulatory Review January 2021 Submittal | 4.0 Regulatory Review |
| All units | Chapter NR 445 Analysis | Data request response letter to WDNR February 23, 2021 | Section 4.4.20 |
| P06 and P07 | Subpart IIII | Post application NTEC Response #01 | Additional language incorporated into Section 4.2.5 |
| HRSG | Subpart KKKK | Post application NTEC Response #09 | Additional language incorporated into Section 4.2.6 |

The Project is subject to various Federal and State air regulations. Part 4 contains a discussion of applicable Federal and WAC provisions. Where applicable, reference to general limitations is provided when there is no specific requirement that applies to an emission source.

In certain instances, there may be multiple applicable regulatory requirements that identify differing levels of emission limitations. For instance, where a BACT emission limitation is established for a specific pollutant and a NSPS regulation is also applicable, the BACT limitation may be more stringent than an applicable NSPS emission limitation for the same pollutant. In these situations, it is understood that compliance with the most restrictive requirement would demonstrate compliance with other less stringent requirements.

4.1 PSD Regulations

PSD review applies to a physical change of a major stationary source located in an area designated as attainment or unclassified that would result in a significant emissions increase of a regulated New Source Review (NSR) pollutant and a significant net emissions increase of that pollutant pursuant to WAC Chapter NR 405. PSD review consists of the following:

- A BACT analysis
- An air quality analysis
- An analysis of additional impacts on visibility, soils, vegetation, and growth

Three criteria were evaluated to determine PSD applicability to the Project (EPA, 1990):

- Whether the Project is sufficiently large (in terms of its emissions) to be a "major stationary source" or "major modification"
- Whether the source is in an area designated as "attainment" or "unclassified"
- Whether the Project would result in a "significant emissions increase" or a "significant net emissions increase" of a "regulated NSR pollutant" as defined by s. NR 405.02(27)(a)

Regulated NSR pollutants in Wisconsin include NO_x, SO₂, CO, PM, PM₁₀, PM_{2.5}, VOC, CO₂e, hydrogen sulfide, H₂SO₄ mist, fluorides, and lead. The definition of a "major stationary source" is given in s. NR 405. The Project is included in the 26 source categories specified in the PSD regulations as major stationary sources if the potential emissions of a regulated NSR pollutant exceed 100 tons per year (because the HRSG generates steam). The Project has the potential to emit regulated NSR pollutants in excess of 100 tons per year; therefore, the Project meets the "major stationary source" classification for a number of regulated NSR pollutants. Thus, the Project meets the first criterion for PSD applicability.

The Project is in an attainment/unclassified area for all criteria pollutants; thus, it meets the second criterion for PSD applicability.

The maximum potential emissions from the Project are listed in Table 1-1, which include start-up and shutdown emissions from the combustion turbine. The Project would result in a "significant emission increase" for the following regulated NSR pollutants: NO_x, CO, VOC, PM/PM₁₀/PM_{2.5}, H₂SO₄ mist, and CO₂e. Thus, the Project meets the third and final criterion for PSD applicability.

The PSD regulations in s. NR 405 require the following issues be addressed:

- Determination of BACT on a case-by-case basis, taking into account costs as well as energy, environmental, and economic impacts;
- Demonstration that the increase in emissions would not cause or contribute to an exceedance of the NAAQS or PSD increment;
- Analysis of the impairment, if any, to visibility, soils, vegetation, and growth.

Section 5.0 contains the BACT analyses for the regulated NSR pollutants.

4.2 New Source Performance Standards

Per 40 CFR Part 60 and s. NR 440 WAC, the Project is subject to NSPS. Relevant NSPS standards are listed below, and if applicable, a description of how the Owners plan to meet the standards.

4.2.1 Subpart Db - Not Applicable

HRSGs and duct burners regulated under Subpart KKKK are exempt from the requirements of 40 CFR Part 60 Subparts Da, Db, and Dc.

4.2.2 Subpart Dc

NSPS 40 CFR Part 60, Subpart Dc applies to Small Industrial-Commercial-Institutional Steam Generating Units between the sizes of 10 MMBtu/hr and 100 MMBtu/hr. This rule applies to the auxiliary boiler (100 MMBtu/hr) and the two gas heaters (10 MMBtu/hr, each). Since the auxiliary boiler and gas heaters combust natural gas, the Owners will keep records of the sulfur content of the natural gas as certified by the supplier or test data and record the daily usage of natural gas in the auxiliary boiler and natural gas heaters. For gas-fired units of this size, there are no emissions limits provided in the rule. The Owners will comply with the record keeping and reporting requirements of the rule.

4.2.3 Subpart GG - Not Applicable

Stationary combustion turbines constructed after February 18, 2005, that are subject to NSPS 40 CFR Part 60, Subpart KKKK are exempt from the requirements of Subpart GG. Section 4.2.6, below, covers Subpart KKKK.

4.2.4 Subpart Kb - Not Applicable

NSPS 40 CFR Part 60, Subpart Kb applies to each storage vessel with a capacity greater than or equal to 75 cubic meters used to store volatile organic liquids for which construction, reconstruction, or modification is commenced after July 23, 1984. Two of the diesel storage tanks will have a capacity less than 75 cubic meters; therefore, the 1,700-gallon and 350-gallon storage tanks will not be subject to Subpart Kb.

This subpart applies to storage vessels with a capacity greater than or equal to 151 cubic meters (39,890 gallons) storing a liquid with a maximum true vapor pressure greater than 3.5 kilopascals (kPa) (0.5 pounds per square inch [psia]). The 180,000-gallon tank diesel storage tank that will be installed as part of the Project is greater than 151 cubic meters (39,890 gallons); however, the tank will not be subject to Subpart Kb as its vapor pressure is less than 3.5 kPa.

4.2.5 Subpart IIII

NSPS 40 CFR Part 60, Subpart IIII applies to stationary compression ignition (CI) internal combustion engines (ICE) and the manufacturers or owners and operators of these engines as follows:

- 1. **Manufacturers** of stationary CI ICE with a displacement of less than 30 liters per cylinder where the model year is 2007 or later for non-fire pump engines and the model year listed or later model years for fire pump engines (2008 or 2011)
- 2. **Owners and operators** of stationary CI ICE that commenced construction after July 11, 2005, where the CI ICE are manufactured after April 1, 2006 (non-fire pump engines), or manufactured as a National Fire Protection Agency fire pump engine after July 1, 2006

For purposes of this application, Subpart IIII is assumed to be applicable to the emergency fire pump and the emergency diesel generator. Both engines will meet the definition of "emergency stationary internal combustion engine" under this subpart as follows:

- There is no time limit on the use of emergency stationary ICE in emergency situations.
- The engine may be operated for a maximum of 100 hours per calendar year for testing and maintenance, except as indicated, below.
- 50 hours of the 100 hours per calendar year allocated may be used for non-emergency situations.

Further, both engines will be 2009 model year or later.

Based on the size (horsepower) and use (emergency) and assuming the Owners purchase a certified model year 2009 or later CI ICE with a displacement that will less than 10 liters per cylinder, the emergency fire pump will be certified in accordance with the limits in 40 CFR 60.4202(d). As the emergency fire pump will be between 175 and 300 hp, the limits are as follows:

- 4.0 gram per kilowatt hour (g/kW-hr) (3.0 gram per horsepower hour [g/hp-hr]) for non-methane hydrocarbons (NMHC) plus NO_x
- 3.5 g/kW-hr (2.6 g/hp-hr) for CO
- 0.20 g/kW-hr (0.15 g/hp-hr) for PM

Based on the size (horsepower) and use (emergency) and assuming the Owners purchase a certified model year 2007 or later CI ICE with a displacement that will less than 10 liters per cylinder, the emergency generator will be certified in accordance with the limits in 40 CFR 60.4202(a)(2), which refer to the limits in 40 CFR 89.112. As the emergency generator will be greater than 560 kW and manufactured after 2006, Table 1 of 40 CFR 60.89.112(a) indicates the following applicable emission standards [subject to the same being included in a family emission limit in an averaging, banking, and trading program for which the emission standards in Table 2 of 40 CFR 89.112(d) are applicable]:

- 6.4 g/kW-hr (4.8 g/hp-hr) for NMHC plus NO_x
- 3.5 g/kW-hr (2.6 g/hp-hr) for CO
- 0.20 g/kW-hr (0.15 g/hp-hr) for PM

The emergency generator will also be subject to the exhaust opacity limits in 40 CFR 89.113, with single-cylinder engines, propulsion marine diesel engines, and constant speed engines being exempt from these limits:

- 20 percent during the acceleration mode
- 15 percent during the lugging mode
- 50 percent during the peaks in either the acceleration or lugging modes

Compliance with this subpart will be shown by purchasing an engine certified to meet the applicable emission standards for the model year and maximum engine power depending on the date of purchase. The Owners will install emergency diesel engines that are certified to meet the applicable emission standards based on the date that the unit will be installed.

Pursuant to 40 CFR 60.4207(b), owners and operators of CI ICE subject to Subpart IIII with a displacement of less than 10 liters per cylinder that use diesel fuel must purchase diesel fuel that meets the requirements of 40 CFR 80.510(b) for non-road diesel fuel. This rule will be applicable to the emergency diesel engine, since the proposed emergency diesel engine will have a displacement of less than 10 liters per cylinder. As stated in 40 CFR 80.510(b), non-road diesel fuel must be limited to 15 parts per million (ppm) maximum sulfur content. The cetane index is limited to a minimum of 40 and the maximum aromatic content is limited to 35 volume percent.

The Owners will be subject to the applicable requirements of this rule for the emergency fire pump and emergency generator. The Owners intend to limit maintenance and readiness testing to 100 hours to meet the definition of emergency for 40 CFR 60, Subpart IIII. The emergency equipment potential to emit emissions were calculated using 500 hours per year per EPA guidance. The EPA believes that 500 hours per year is an appropriate default assumption for estimating the number of hours that emergency equipment could be expected to operate under worst-case conditions.

4.2.6 Subpart KKKK

NSPS 40 CFR Part 60, Subpart KKKK is applicable to all stationary combustion turbines that commenced construction, modification, or reconstruction after February 18, 2005, and have a heat input equal to or greater than 10.7 gigajoules per hour (10 MMBtu/hr), based on the higher heating value of fuel.

Per 40 CFR 40b(i), if the combustion turbine is subject to Subpart KKKK, then the associated HRSG is exempt from the requirements of 40 CFR Part 60 Subparts Da, Db, and Dc. Per 40 CFR 60.4305(a), since the combustion turbine is greater than 10 MMBtu/hr and will be constructed after February 18, 2005, the combustion turbine is subject to Subpart KKKK. The HRSG associated with the turbine meets the applicability requirements of 40 CFR 60, Subpart KKKK.

Pursuant to 40 CFR Section 60.4320(a) and Table 1 to Subpart KKKK, the NSPS NO_x applicable combustion turbine limit for natural gas combustion, is 15 ppm at 15 percent oxygen or 54 nanogram per Joule (ng/J) of useful output (0.43 pound per megawatt hour [lb/MW-hr]), when burning more than 50 percent natural gas (60.4325).

When combusting more than 50 percent fuel oil, the limit for NO_x is 42 ppm at 15 percent oxygen or 160 ng/J of useful output (1.3 lb/MW-hr).

During operations when ambient temperatures are less than 0 °F or when the turbine is operating at less than 75 percent load, the NO_x emission standard is 96 ppm at 15 percent oxygen or 590 ng/J of useful output (4.7 lb/MWh). This applies when combusting either natural gas or fuel oil. All MW readings are in gross MW. The higher emission standard applies for the hour if at any point in the hour the unit was subject to the higher standard.

In accordance with Subpart KKKK, the Owners would demonstrate compliance with the NO_x emission limit by conducting performance testing pursuant to Section 60.4340(a), or alternatively, by installing, calibrating, maintaining, and operating a continuous monitoring system (i.e., continuous emission monitor (CEM) or continuous parameter monitor) in accordance with Section 60.4340(b).

For operating periods during which multiple emissions standards apply, the applicable standard is the average of the applicable standards during each hour per §60.4380(b)(3). For combined cycle units, the limits are calculated from hourly average emission rates to assess excess emissions on a 30-unit operating day rolling average basis, as described in § 60.4380(b)(1).

The Owners expect to have a NO_x emission rate of 2 ppm at 15 percent oxygen for natural gas combustion and 6 ppm for fuel oil combustion with the use of SCR.

The NSPS SO₂ limit for the turbine is 0.90 lb/MW-hr gross output, **or** the facility must limit fuel so that any fuel combusted contains total potential sulfur emissions equal to or less than 0.060 lb SO₂/MMBtu heat input. Emissions of SO₂ will be well below 0.90 lb/MW-hr for both fuel oil and natural gas operation; therefore, per 40 CFR Section 60.4365(a), the Owners will keep on record the fuel quality characteristics of the natural gas and fuel oil from the suppliers and fuel analysis records.

4.2.7 Subpart TTTT

NSPS 40 CFR Part 60, Subpart TTTT, Standards of Performance for Greenhouse Gas Emissions for Electric Utility Generating Units regulates carbon dioxide (CO₂) emissions from electric generating units under the NSPS (Clean Air Act 111b regulations). The standards apply to any steam generating unit, integrated gasification combined-cycle, or combustion turbine that commenced construction after January 18, 2014, or reconstruction or modification after June 18, 2014, that has a base load rating greater than 250 MMBtu/hr of fossil fuel and serves a generator capable of selling greater than 25 MW of electricity to a utility power distribution system.

The combustion turbine will be subject to NSPS Subpart TTTT. The standard provides a limit for natural gas-fired combined-cycle combustion turbines. A natural gas-fired combined-cycle turbine is limited to

450 kilograms of CO₂ per megawatt-hour of gross energy output (1,000 pounds CO₂ per MW-hour [lb CO₂/MW-hr]) on a 12-operating month rolling average basis. An alternative to meeting the gross energy output the Owners can petition to comply with the alternate net energy output standard, 470 kilograms of CO₂ per megawatt-hour of net energy output (1,030 lb/MW-hr) on a 12-operating month rolling average basis. These limits are based on an assumed operation of 90 percent natural gas in a 12-month period. The combined-cycle combustion turbine will comply with the limit in NSPS Subpart TTTT.

If the turbine combusts 90 percent or less natural gas, in accordance with Table 2 of Subpart TTTT, the limit becomes 50 kilograms CO₂ per gigajoule (kg/GJ) to 69 kg/GJ of heat input (120 to 160 pounds per million British thermal units [lb/MMBtu]) as determined by the procedures in 40 CFR Section 60.5525.

4.3 National Emission Standards for Hazardous Air Pollutants and Maximum Achievable Control Technology

National Emission Standards for Hazardous Air Pollutants (NESHAP) are contained in 40 CFR Part 63 (adopted by reference in s. NR 445). NESHAP are emissions standards set by the EPA for specific source categories. The NESHAP require the maximum degree of emission reduction of certain HAP emissions that the EPA determines to be achievable, which is known as the maximum achievable control technology (MACT) standards.

The following MACT standards are relevant to the Project.

4.3.1 Subpart YYYY - Not Applicable

EPA promulgated MACT standards for new stationary combustion turbines on March 5, 2004. These standards apply to stationary combustion turbines for which construction commenced after January 14, 2003. On April 7, 2004, however, EPA proposed to remove gas-fired units from the combustion turbine source category regulated by NSPS 40 CFR 63, Subpart YYYY. In the interim, EPA has stayed the applicability of Subpart YYYY requirements for gas-fired combustion turbines.

This regulation applies only to combustion turbines at facilities that are major sources of HAPs. The Project will be an area source of HAPs; therefore, the Project is not subject to this regulation.

4.3.2 Subpart ZZZZ

The Reciprocating Internal Combustion Engines (RICE) MACT (40 Part 63, Subpart ZZZZ) is applicable to stationary RICE located at major or area sources of HAP emissions. Both the emergency generator and emergency fire pump will be a new source located at an area source per 40 CFR 63.6590(c)(1). Therefore, the emergency generator will comply with the requirements of Subpart ZZZZ by meeting the

requirements of 40 CFR Part 60 Subpart IIII pursuant to 40 CFR 63.6590(c)(1) and the fire pump will comply with the requirements of Subpart ZZZZ by meeting the requirements of NSPS Subpart IIII pursuant to 40 CFR 63.6590(c)(1).

4.3.3 Subpart JJJJJJ – Not applicable

40 CFR Part 60, Subpart JJJJJJ applies to industrial, commercial, or institutional boilers and process heaters located at an area source of HAPs. According to the subpart definitions, the two gas-fired heaters and auxiliary boiler fall under the definition of gas-fired boiler. Per 63.11195(e), gas-fired boilers are not subject to Subpart JJJJJJ.

4.4 Wisconsin Air Quality Standards and Regulations

This section describes the regulations which apply to the Project, according to the WAC.

4.4.1 s. NR 404 Ambient Air Quality

Ambient air quality standards applicable to the entire state are listed in s. NR 404. The Owners will comply with all applicable state standards.

4.4.2 s. NR 405 - PSD Review

Under the 1977 Clean Air Act Amendments (CAAA), BACT and other PSD requirements apply both to emissions of criteria pollutants and to emissions of certain non-criteria pollutants that are regulated under Section 111 (NSPS) and Section 112 (NESHAP) of the Act. However, in Section 112(b)(6) of the 1990 CAAA, Congress specifically excluded the HAPs listed in Section 112(b)(1) from the PSD requirements. EPA clarified this exclusion in a March 11, 1991 memo by stating that:

...the following pollutants, which have been regulated under PSD, are now exempt from federal PSD applicability:

- arsenic
- beryllium
- radionuclides (including radon

- asbestos
- hydrogen sulfide
- and polonium)

- benzene
- mercury
- vinyl chloride

However, Wisconsin still includes hydrogen sulfide as a PSD pollutant listed in Table A of s. NR 405.02 (27)(a). As such, PSD review of this pollutant is a state-only requirement. This Project will be subject to PSD for several pollutants. Part 5 of this application contains the BACT analyses. Part 6 contains the air dispersion modeling analyses and Part 7 contains the additional impacts analysis.

4.4.3 s. NR 406 – Construction Permits

The purpose of this section is 1) to establish permit and permit review requirements and permit duration for construction permits and 2) to define types of stationary sources that are exempt from the requirement to obtain a construction permit. This permit application is intended to satisfy the construction permit application requirements to obtain a permit.

4.4.4 s. NR 407 – Operation Permits

For new sources that require a construction permit, the initial filing date is the date that the construction permit is filed (NR 407.04(1)(b)). However, because of the nature of this project, and because multiple vendor selections have yet to be made, there is not enough data to complete the operation permit application at this time. The Project will complete the application for a Title V operating permit after start-up of the facility.

4.4.5 s. NR 410 – Air Permit, Emission, and Inspection Fees

This section describes the fees necessary for submitting a permit to WDNR for processing. The Project has included the necessary permit fees as indicated in s. NR 410.03.

4.4.6 s. NR 415 - Control of Particulate Emissions

This section applies to all air contaminant sources which emit particulate matter and to their owners and operators. The general limitations (s. NR 415.03) contained in this regulation state, "No person may cause, allow or permit particulate matter to be emitted into the ambient air which substantially contributes to exceeding of an air standard, or creates air pollution."

NR 415.04 addresses fugitive dust and states, "No person may cause, allow or permit any materials to be handled, transported or stored without taking precautions to prevent particulate matter from becoming airborne. Nor may a person allow a structure, a parking lot, or a road to be used, constructed, altered, repaired, sand blasted or demolished without taking such precautions...Such precautions shall include, but not be limited to...[t]he paving or maintenance of roadway areas so as not to create air pollution."

All roads will be paved, thus meeting the requirements of this rule.

Section NR 415.05 more specifically provides: "No person may cause, allow or permit the emission of particulate matter to the ambient air from any indirect heat exchanger, power or heating plant, fuel-burning installation or pulp recovery furnace with maximum heat input more than one million Btu per hour in excess of one of the listed limitations."

The limits applicable to the Project are as follows:

- The auxiliary boiler, two gas heaters, fire pump, and diesel generator are all limited to 0.15 lb PM/MMBtu per NR 415.06(2)(a)
- The combustion turbine is limited to 0.10 lb PM/MMBtu per NR 415.06(2)(c)

4.4.7 s. NR 417 – Control of Sulfur Emissions

This chapter applies to all air contaminant sources which emit SO₂ or other sulfur compounds and to their owners and operators. Section NR 417.03 provides: "No person may cause, allow or permit emission of sulfur or sulfur compounds into the ambient air which substantially contribute to the exceeding of an air standard or cause air pollution." However, there are no specific limits for natural gas-fired and ultra-low sulfur fuel oil-fired equipment.

4.4.8 s. NR 419 – Control of Organic Compound Emissions

This chapter applies to all air contaminant sources which emit organic compounds and to their owners and operators. "No person may cause, allow or permit organic compound emissions into the ambient air which substantially contribute to the exceeding of an air standard or cause air pollution," s. NR 419.03(1). However, there are no specific limits for any new equipment for this Project.

4.4.9 s. NR 420 – Control of Organic Compound Emissions from Petroleum and Gasoline Sources

This regulation lists the storage, recordkeeping, and maintenance requirements for organic compound storage tanks larger than 40,000 gallons. However, the 180,000-gallon storage tank at the facility will be exempt from the rules in this section under NR 420.03(1)(a) – exemption for storage vessels being used for number 2 through number 6 fuel oils.

4.4.10 s. NR 426 – Control of Carbon Monoxide Emissions

This regulation restricts any source from emitting CO in quantities or amounts that cause or contribute to an exceedance of air quality standards or cause air pollution. The air dispersion modeling performed as part of this application and detailed in Part 6 of this report demonstrates that this facility will not cause or contribute to a violation of any CO air quality standards.

4.4.11 s. NR 427 - Control of Lead Emissions

This chapter applies to all air contaminant sources which emit lead and to their owners and operators. However, no specific limits apply to the equipment for this Project.

4.4.12 s. NR 428 – Control of Nitrogen Compound Emissions

This chapter applies to all air contaminant sources which emit nitrogen compounds and to their owners and operators. However, no specific limits apply to the equipment for this Project.

4.4.13 s. NR 429 – Malodorous Emissions and Open Burning

This regulation is intended to restrict offensive odors in the ambient air and the burning of refuse, except under certain conditions, and would apply to the facility.

4.4.14 s. NR 431 – Control of Visible Emissions

No person may cause, allow, or permit emissions into the ambient air from any direct or portable source in excess of one of the limits specified in this chapter. The combustion turbine, auxiliary boiler, two gas heaters, fire pump, and diesel generator are limited to 20 percent opacity. Where the presence of uncombined water is the only reason for failure to meet the requirements of this chapter, such failure is not a violation of this chapter.

4.4.15 s. NR 432 – Allocation of Clean Air Interstate Rule NO_x Allowances.

This rule adopts the federal Clean Air Interstate Rule (CAIR) into the state rules. To address interstate transport of pollutants, it contains state regulations regarding NO_x reductions from major electric generating units in Wisconsin. Please note, this rule has been replaced by the Cross-State Air Pollution Rule.

4.4.16 s. NR 436 - Emission Prohibition, Exceptions, Delayed Compliance Orders and Variances

This requirement prohibits emissions into the ambient air in excess of limitations set under s. NR 400 through 499. As indicated within this application, emission limits for the Project will be at least as stringent as those established under ss. NR 400 through 499. However, the WDNR may grant exceptions to the emission limits pursuant to WDNR-approved plans.

4.4.17 s. NR 438 - Air Contaminant Emission Inventory Reporting Requirements

The WDNR has established specific requirements applicable to all air contaminant sources to demonstrate compliance with permit requirements. This application incorporates these requirements, and the Project will be subject to these requirements as they are included in the construction and operating permits. The Owners would submit an Emissions Inventory Report annually to the WDNR, along with necessary emission fees.

4.4.18 s. NR 439 - Reporting, Recordkeeping, Testing, Inspection and **Determination of Compliance Requirements**

The WDNR has established specific requirements applicable to emission sources to demonstrate compliance with permit requirements. This application incorporates these requirements, and the Project will be subject to these requirements as they are included in the construction and operating permits.

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s. NR 440 - Standards of Performance for New Stationary Sources 4.4.19

Wisconsin has incorporated some of the NSPS listed in 40 CFR Part 60 into the state regulations. This is a review of those regulations with respect to the Project. Although the State of Wisconsin has adopted the federal NSPS, the Wisconsin rules may not be updated as soon as the federal rules. Where this is the case, the more restrictive federal standards apply. Applicable NSPS are addressed above in Section 4.2.

4.4.20 s. NR 445 - Control of Hazardous Pollutants

Sources that combust a group 1 virgin fossil fuel are exempt from NR 445 requirements per 445.07(5)(a). Accordingly, no NR 445.07 analysis is included for the following Project emission sources:

- EU01 Combustion Turbine (Stack S01)
- EU02 Auxiliary Boiler (Stack S02)
- EU04 Natural Gas Heater #1 (Stack S04)
- EU05 Natural Gas Heater #2 (Stack S05)
- EU06 Emergency Diesel Fire Pump (Stack S06)
- EU07 Emergency Diesel Generator (Stack S07)

The following emission units do not emit any pollutants that are regulated under NR 445:

- F03 SF6 Circuit Breakers
- F01 Haul Road Fugitives

The following emission units emit pollutants that are regulated under NR 445:

- Process P01, Stack S01, Control C01a SCR
- EU08 Diesel Tank (Stack S08)
- EU09 Diesel Generator Tank (Stack S09)
- EU10 Diesel Fire Pump Tank (Stack S10)
- F02 Natural Gas and Fuel Oil Piping Components

The total non-exempt potential emissions of HAPs from the Project are summarized in Appendix C for the most significant state HAPs emitted from the Project.

The exhausts from the tanks are considered to be obstructed for the purposes of NR 445 because the breathing vents for these storage tanks are not powered exhausts. As such, the potential HAP emissions resulting from these emission units have been multiplied by a factor of 4. For conservativeness, each non-exempt HAP was assumed to be equal to the full estimated breathing and loading VOC losses from the EPA TANKS emission software (emissions were not speciated).

The natural gas and fuel oil piping components are considered fugitive emissions and have been multiplied by a factor of 4.

The total non-exempt potential emissions of HAPs from the Project are summarized in Appendix C. The table also lists the thresholds for each HAP for each stack height category. When comparing the total non-exempt potential emission rate for each HAP to the corresponding NR 445 threshold values, the threshold values will not be exceeded for any of the listed HAPs, except for the ammonia 24-hour average.

The SCR will have a maximum ammonia slip level of 10 ppm which yields an emission rate of 62.0 pounds per hour (lb/hr) (543,120 pounds per year [lb/yr]). The NR 445 threshold for a stack greater than 75 feet in height is 28.2 lb/hr and 612,587 lb/yr; therefore, dispersion modeling is required for the 24-hr average. The 24-hour ambient air standard in NR 445 for ammonia is 418 micrograms per cubic meter (μ g/m³). The resultant modeled concentrations are shown in Table 4-2 and show compliance with the ambient air standard.

Table 4-2: NR 445 Air Dispersion Modeling Results for 24-hour Ammonia Concentration

| | Maximum Modeled Impact | NR 445 Air Quality Standard |
|-----------|---------------------------|--------------------------------|
| Pollutant | micrograms per cubic | meter (µg/m³) |
| Ammonia | 16.5 | 418 |

Based upon this analysis, the Project will be in compliance with the requirements of NR 445.

4.5 Chemical Accident Prevention

40 CFR Part 68, Accidental Release Prevention Provisions, under Clean Air Act (CAA) Section 112(r), Prevention of Accidental Releases, establishes a general duty for owners and operators of stationary sources who produce, process, handle, or store any of a number of regulated substances, to prevent and

mitigate accidental releases of these substances by preparing detailed risk assessments and implementing a number of safety procedures through the preparation of a risk management plan (RMP).

The specific requirements of the RMP for affected facilities are established in 40 CFR Part 68, Accidental Release Prevention Provisions. These regulations require the owner or operator of an affected source to prepare and implement an RMP to detect and prevent or minimize accidental releases of regulated substances, and to provide a prompt emergency response to any such release to protect human health and the environment.

Affected facilities are those stationary sources that store, use, or handle any of the 140 listed hazardous chemicals or flammable/explosive substances in amounts greater than the listed threshold quantities. This list of regulated substances includes commonly stored liquid phases of gases such as ammonia, which the Project may store at quantities near or above the threshold levels for use in conjunction with the SCR for NO_x control on the combustion turbine. If a facility stores aqueous ammonia of concentrations of 20 percent or greater an RMP is required for the facility's storage, use, and handling of ammonia.

Aqueous ammonia (19 percent solution) will be delivered to the site via a truck with an unloading pump then stored in a bulk 35,000-gallon storage tank. The Project's SCR would use 19 percent concentration aqueous ammonia, therefore, an RMP is **not required** for the facility's storage, use, and handling of ammonia.

5.0 BEST AVAILABLE CONTROL TECHNOLOGY ANALYSIS

S. NR 405, WAC requires the application of BACT for each regulated NSR pollutant for which a significant net emissions increase will be realized as a result of the Project. As indicated in Part 1, the Project will result in significant emission increases of NO_x, CO, PM₁₀, PM_{2.5}, VOC, H₂SO₄ mist, and CO₂e for combined-cycle operation. These pollutants will be subject to PSD review. Additionally, WDNR requires a BACT for opacity. Therefore, a BACT analysis was performed for each of these regulated NSR pollutants.

The Project will consist of one H-Class combustion turbine with a HRSG and one steam turbine in a combined-cycle configuration and associated support equipment. The combustion turbine will be designed to utilize pipeline-quality natural gas and combust fuel oil (ultra-low sulfur diesel) as back-up fuel. In addition to the combustion turbine, an auxiliary boiler, circuit breakers, two natural gas-fired gas heaters (natural gas heater), an emergency diesel fire pump, an emergency diesel generator, fuel oil storage tanks, haul roads, and natural gas and fuel oil piping components will be included as part of the Project. This Part describes the BACT analysis for all new equipment proposed for the Project.

The BACT analysis was performed using the "top-down" approach, which is described in this Part. A summary of the BACT emission limits and the associated control technologies for the combined-cycle combustion turbine are shown in Table 5-1. BACT emission limits and associated control technologies for the auxiliary equipment are listed in Table 5-2.

Table 5-1: Summary of BACT Results: Combined-Cycle Operation

| Pollutant | Fuel | Control | BACT Emissions ^{a,b} | Average |
|-------------------------------------|----------------|--|---|---------------------|
| Natural gas | | Selective catalytic reduction (SCR) and low-NO _x burners | 2 ppm (with or without duct firing) | 24-hour rolling |
| Fuel oil | Fuel oil | SCR and water injection | 6 ppm (with or without duct firing) | 24-hour rolling |
| СО | Natural gas | Good combustion practices, oxidation catalyst | 1.5 ppm (with or without duct firing) ^c | 168-hour rolling |
| | Fuel oil | Good combustion practices, oxidation catalyst | 1.5 ppm (with or without duct firing) ^c | 168-hour rolling |
| PM/PM ₁₀ / | Natural gas | Combustion controls and low ash fuels | 36.3 lb/hr (with duct firing) 21.8 lb/hr (without duct firing) | NA |
| PM _{2.5} | Fuel oil | Combustion controls and low ash fuels | 54.5 lb/hr (with duct firing) 39.4 lb/hr (without duct firing) | NA |
| VOC | Natural gas | Good combustion practices, oxidation catalyst | 2.7 ppm (with duct firing) 0.6 ppm (without duct firing) | 168-hour rolling |
| | Fuel oil | Good combustion practices, oxidation catalyst | 3.3 ppm (with duct firing) 0.6 ppm (without duct firing) | 168-hour rolling |
| H ₂ SO ₄ mist | Natural gas | Combustion controls and low sulfur fuels | 9.9 lb/hr (with duct firing) 7.8 lb/hr (without duct firing) | NA |
| 1125O4 IIIIst | Fuel oil | Combustion controls and low sulfur fuels | 9.3 lb/hr (with duct firing) 7.0 lb/hr (without duct firing) | NA |
| Caranhana | Natural gas | Use of natural gas as a fuel, monitoring and control of excess air, efficient turbine design, and oxidation catalyst | 850 lb CO ₂ /MW-hr, gross | 12-month rolling |
| Greenhouse gases | Fuel oil | Use of ultra-low sulfur diesel as a fuel, monitoring and control of excess air, efficient turbine design, and oxidation catalyst | 1,180 lb CO ₂ /MW-hr, gross | 12-month rolling |
| Opacity | Both | Low-NO _x burners, SCR, combustion controls, low ash fuels | N/A | N/A |

Source: Construction permit no.: 18-MMC-168

⁽a) ppm = parts per million; lb/hr = pounds per hour; lb/MW-hr = pound per megawatt hour

⁽b) Concentration at 15 percent oxygen while operating at MECL and greater under steady state conditions, unless otherwise noted

⁽c) Natural gas limit valid for 100% load with duct firing down to MECL. Fuel oil limit valid for 100% load with duct firing down to 75% load.

Table 5-2: Summary of BACT Results: Auxiliary Equipment

| Equipment | Pollutant | Control ^a | BACT Emission Rate ^a |
|---|--|--|---------------------------------|
| | NO _x | Ultra-LNB/GCP/clean fuels/FGR | 0.011 lb/MMBtu |
| | СО | Oxidation Catalyst/GCP/clean fuels | 0.0037 lb/MMBtu |
| A '1' 1 '1 DO2 | $PM/PM_{10}/PM_{2.5}$ | GCP/clean fuels | 0.01 lb/MMBtu |
| Auxiliary boiler - B02 | VOC | Oxidation Catalyst/GCP/clean fuels | 0.0027 lb/MMBtu |
| | H ₂ SO ₄ mist | GCP/clean fuels | 0.01 lb/hr |
| | Greenhouse gases (CO ₂ e) | GCP/clean fuels | 160 lb/MMBtu |
| | Opacity | GCP/clean fuels | N/A |
| Circuit Breaker – F03 | SF ₆ | Leak monitoring | <0.5% loss rate |
| | NO _x | LNB/GCP/clean fuels | 0.049 lb/MMBtu |
| | CO | GCP/clean fuels | 0.08 lb/MMBtu |
| N. I. I. DOA I | PM/PM ₁₀ /PM _{2.5} | GCP/clean fuels | 0.01 lb/MMBtu |
| Natural gas heaters -P04 and P05 (each) | VOC | GCP/clean fuels | 0.005 lb/MMBtu |
| ros (each) | H ₂ SO ₄ mist | GCP/clean fuels | NA |
| | Greenhouse gases (CO ₂ e) | GCP/clean fuels | NA |
| | Opacity | GCP/clean fuels | N/A |
| | NO_x | GCP/clean fuels | 3.0 g/hp-hr |
| | CO | GCP/clean fuels | 2.6 g/hp-hr |
| E | $PM/PM_{10}/PM_{2.5}$ | GCP/clean fuels | 0.15 g/hp-hr |
| Emergency diesel fire pump – P06 | VOC | GCP/clean fuels | 1.1 g/hp-hr |
| 100 | H ₂ SO ₄ mist | GCP/clean fuels | NA |
| | Greenhouse gases (CO ₂ e) | GCP/clean fuels | NA |
| | Opacity | GCP/clean fuels | N/A |
| | NO_x | GCP/clean fuels | 4.8 g/hp-hr |
| | СО | GCP/clean fuels | 2.6 g/hp-hr |
| Emanage ov diagal conceptor | PM/PM ₁₀ /PM _{2.5} | GCP/clean fuels | 0.15 g/hp-hr |
| Emergency diesel generator – P07 | VOC | GCP/clean fuels | 0.32 g/hp-hr |
| | H ₂ SO ₄ mist | GCP/clean fuels | NA |
| | Greenhouse gases (CO ₂ e) | GCP/clean fuels | NA |
| | Opacity | GCP/clean fuels | NA |
| Diesel tanks – T01, T02, T03 | VOC | Fixed roof tank | NA |
| Haul Roads – F01 | PM/PM ₁₀ /PM _{2.5} | Haul roads | Fugitive Dust Control Plan |
| Natural gas and fuel oil | GHG | Fuel Piping | LDAR program - instrument |
| piping components – F02 | VOC | Fuel Piping | monitoring |

Source: Construction permit no.: 18-MMC-168 and 21-MMC-011

(a) FGR = flue gas recirculation; LNB = low- NO_x burners; GCP = good combustion practices; lb/MMBtu = pound per million British thermal units; tpy = tons per year; g/hp-hr = gram per horsepower hour

BACT is an emission limitation based on the maximum degree of reduction which the WDNR determines is achievable, on a case-by-case basis, taking into account energy, environmental, and economic impacts and other costs.

The WDNR has directed by policy that the BACT be determined using a "top-down" process. The "top-down" process was outlined in a December 1, 1987, memorandum from the EPA Assistant Administrator for Air and Radiation.

While there is no legal requirement to perform the BACT analysis utilizing a specific criteria or process, the WDNR follows the EPA-developed guidance that establishes a five-step "top-down" BACT process/methodology (EPA, 1990).

For purposes of this PSD application, the Owners have prepared this BACT analysis consistent with EPA's top down approach, which consists of the following steps:

Step 1 – Identify all potential control technologies

Step 2 – Determine technical feasibility (of potential technologies)

Step 3 – Rank control technologies by control effectiveness

Step 4 – Evaluate most effective controls and document results

Step 5 – Select BACT

Each of these steps is discussed in further detail below.

Step 1 – Identify all potential control technologies. The first step in a "top-down" analysis is to identify, for all applicable emission units, all "available" control options. Available control options are defined as those air pollution control technologies or techniques that have a practical potential for application to the emissions unit and the regulated pollutant under evaluation and have been demonstrated in practice. Air pollution control technologies and techniques include the application of production processes or available methods, systems, and techniques, including innovative fuel combustion techniques and add-on controls.

<u>Step 2 – Determine technical feasibility (of potential options)</u>. In the second step, the technical feasibility of the control options identified in Step 1 is evaluated with respect to source-specific factors. A demonstration of technical infeasibility should be documented and should show, based on physical, chemical, and engineering principles, that technical difficulties would preclude the successful use of the control option on the emissions unit under review. Technically infeasible control options are then eliminated from further consideration in the BACT analysis.

<u>Step 3 – Rank control technologies by control effectiveness</u>. All remaining control alternatives not eliminated in Step 2 are ranked and then listed in order of overall control effectiveness for the pollutant under review, with the most effective control alternative at the top. A list should be prepared for each pollutant and for each emissions unit (or grouping of similar units) subject to a BACT analysis.

Step 4 – Evaluate most effective controls and document results. After the identification of available and technically feasible control technology options, the energy, environmental, and economic impacts are taken into account, in this Step. For each control option an objective evaluation of each impact is presented. Both beneficial and adverse impacts should be discussed and, where possible, quantified. If the Owners accept the top alternative in the listing as BACT, the Owners proceed to consider whether impacts of unregulated air pollutants or impacts in other media would justify selection of an alternative control option. If there are no outstanding issues regarding collateral environmental impacts, the analysis ends, and the results proposed as BACT. If the top candidate is shown to be inappropriate, due to energy, environmental, or economic impacts, the rationale for this finding is documented and the next level of control is analyzed.

<u>Step 5 – Select BACT</u>. The final BACT determination is presented in this Step.

Greenhouse Gas BACT Process

Based on EPA Greenhouse Gas Guidance (EPA, 2011), the Greenhouse BACT process is similar to the five Steps summarized above. Steps 1 and 2 identify potential control strategies and then eliminate technologically infeasible options. Step 3 ranks the remaining technically feasible control technologies. Step 4 evaluates the most effective control technologies from an environmental, energy, and economic perspective. And finally, Step 5 selects the most appropriate BACT.

The BACT analysis for the Project is also based on the following concepts:

- Emission limits are defined on a "case-by-case" analysis that considers site specific factors
- Emission limits must be "achievable" on a long-term, day in and day out, basis
- The technology must be available and feasible for a specific project
- BACT does not redefine the facility as proposed (including fuels)

There is no prescriptive approach to performing a case-by-case control technology and emission limit analysis. PSD permitting authorities determine emission limits on a case-by-case basis. These case-by-case determinations must consider source-specific and site-specific characteristics. This is not a "cookie-

cutter" approach and there is no single right answer to determining the appropriate emission limits for a specific source or for a specific pollutant.

The WDNR is not required to set any emission limit at the most stringent level that has been demonstrated by a facility using similar emissions control technology. Similarly, an emission limit does not need to be set at the most stringent emission limit found in another permit. Rather, the WDNR has the authority and is required to evaluate and determine the correct emissions limits and control technologies for a project based on project-specific factors, including location. The case-by-case process does not require that each subsequent determination identify emission limitations that are equal to or more stringent than the previous determination.

Further, in establishing the emission limits, the BACT must confirm that emission limits are achievable by the specific facility that is subject to the emission limits: (1) over the life of the facility; and (2) during all operating conditions, not just ideal conditions. The use of a safety factor or margin is well-established in the air permitting context to appropriately account for the uncertainty and operational variability that will occur over the life of a facility. This safety factor must be sufficient to allow permit holders to comply on a continuous basis. Emission limits should not be based on the lowest emissions rate or highest control efficiency ever documented by a similar facility for a short-term period. The emission limits must account for a full range of operating conditions and the inherent variability of complex fuel combustion and air pollution control systems.

To be considered in the permitting process, a control technology must be commercially available (i.e., it must be offered for sale on a commercial scale through commercial channels). Permittees are not required to explore research and development projects to determine whether a specific technology is suitable. In addition, to be considered feasible technology for purposes of inclusion in an analysis, a particular technology must have been previously demonstrated, on a long-term basis, at commercial scale. In fact, even 2-3 years of operating history on a commercial scale has been determined to be insufficient to demonstrate that a particular technology is feasible.

The air permit process cannot redefine the source. The Owners have defined the "proposed facility," including the goals, objectives, purpose and basic design. Requiring alteration as to the type of power generating unit and/or range of fuels to be used would redefine the source.

Fuels can be an inherent part of a project design. In such cases, the air permitting process cannot be used to require a fuel other than the fuels proposed by the Owners. As Congress explained, "the Administrator may consider the use of clean fuels to meet BACT requirements if a permit applicant proposes to meet

such requirements by using clean fuel. <u>In no case is the Administrator compelled to require the mandatory use of clean fuels by a permit applicant</u>." (emphasis added). S. Rep. No. 101-228 at 338 (1989).

The first step in the "top-down" BACT process is the identification of potentially available control technologies. One of the ways to identify available control technologies is to review previous BACT determinations for similar sources. EPA's RACT/BACT/LAER Clearinghouse (RBLC) database was reviewed to identify recent BACT determinations for similar projects. This database is maintained on EPA's Technology Transfer Network website at www.epa.gov/ttn/catc. Advanced queries of the database were conducted to identify control technology determinations for sources similar to the proposed combined-cycle combustion turbine and applicable auxiliary equipment. The queries are summarized in Table 5-3, below. The results of the RBLC query can be found in Appendix D.

Initial Look-up Addendum Equipment **Process Type Lookup Code Dates Look Up Dates** Combined-Cycle Combustion 15.210 – Natural gas combustion October 2008 to November 2018 Turbine October 2018 to October 2021 15.220 – Fuel oil combustion P01 **Auxiliary Boiler** October 2008 to November 2018 13.310 – Natural Gas October 2018 P02 to October 2021 Circuit Breakers 99.999 – Other Miscellaneous January 2010 to February 2020 F03 Sources January 2020 to October 2021 Natural gas heaters October 2008 to November 2018 13.310 – Natural Gas P04 and P05 October 2018 to October 2021 Emergency diesel fire pump October 2008 to November 2018 17.210 – Fuel Oil P06 October 2018 to October 2021 Emergency diesel generator October 2008 to November 2018 17.110 – Fuel Oil P07 October 2018 to October 2021 Haul Roads February 2020 January 2010 to 99.410 – Paved Roads F01 January 2020 to October 2021 64.002 – Equipment Leaks Natural gas and fuel oil January 2010 to February 2020 50.007 – Petroleum Refining piping component January 2020 to October 2021 Equipment Leaks/Fugitive F02 **Emissions**

Table 5-3: RBLC Query Information

To identify previous control technology determinations for comparable sources, queries were run using the "standard search" in which the RBLC database was searched using the following parameters:

- Draft Determinations and RBLC Permits issued during or after the dates presented in Table 5-3
- Standard Industrial Classification (SIC) code of 4911 for electrical generation plants

- North American Industrial Classification System (NAICS) code for a combustion turbine electrical generation plant 221112 which includes all types of fossil fuel electrical generation plants.
- SIC codes for auxiliary equipment, as applicable

The NAICS and SIC codes are the most appropriate codes to search in the advanced search option of the RBLC. The SIC and NAICS are systems of source classification developed for the purpose of differentiating industrial types. The SIC and the NAICS systems are used in many EPA documents to differentiate types of industries. It is appropriate to use these codes as the match criteria in queries of the RBLC database since other facilities that use similar turbines will likely have similar characteristics. After the NAICS and SIC codes were identified and queries run, combustion turbines that were not similar (e.g., digester gas-fired, fuel oil-fired, cogeneration units, boilers, etc.) were eliminated from the search. Information on turbine emissions was sorted from the remaining combustion turbine listing. A discussion of control options identified in the RBLC database is included in each subsection. When the combustion turbine results were found in a search, results for the various auxiliary equipment were also available in the search results as well. Therefore, complete RBLC searches were done for all BACT-eligible equipment.

In some cases, the RBLC listings are not clearly categorized and cover both simple- and combined-cycle installations. Also, it should be noted that all RBLC listings in California represent Lowest Achievable Emission Rate (LAER); although they are often listed as BACT, BACT and LAER are essentially the same in California. LAER is a much more stringent requirement than BACT and involves application of control technology regardless of cost. This is not the case for the proposed Project, which is subject only to BACT.

5.1 BACT for Nitrogen Oxides - Combined-Cycle Combustion Turbine (P01)

Previously submitted BACT Sections and updated references to the nitrogen oxides BACT section for the combined-cycle combustion turbine are presented in Table 5-4. The updated combined-cycle combustion turbine nitrogen oxides BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

December 2021 **Previous Application Reference** Description **Submittal Location 5.0 BACT** BACT Analysis Steps 1 to 5 **5.0 BACT** December 2018 Submittal Table D-1a (natural gas), Table D-1a (natural gas), Table D-1b (fuel oil) Table D-1b (fuel oil) Appendix D, December 2018 Submittal Appendix D **RBLC** Table D-1a Addendum (natural gas Table D-1b Addendum (fuel oil) Appendix D

Table 5-4: Combustion Turbine Nitrogen Oxides BACT Analysis References

The following sections outline the top-down steps for NO_x emissions from the combustion turbine.

5.1.1 Step 1. Identify All Potential Control Strategies

NO_x is primarily formed in combustion processes in two ways:

- 1. The combination of elemental nitrogen with oxygen in the combustion air within the high temperature environment of the combustor (thermal NO_x)
- 2. The oxidation of nitrogen contained in the fuel (fuel NO_x)

Natural gas contains negligible amounts of fuel-bound nitrogen, although some molecular nitrogen is present. Therefore, it is assumed that essentially all NO_x emissions from the combustion turbine will originate as thermal NO_x . The rate of formation of thermal NO_x is a function of residence time and free oxygen and is exponential with peak flame temperature.

The combustion turbine will be subject to NO_x limits per NSPS Subpart KKKK and thus the BACT determination and resulting emission limits must be at least as stringent as the NSPS. During combined-cycle operation, the duct burners in the HRSGs will contribute to NO_x emissions. Part 4 identifies the applicable Subpart KKKK limits for the combustion turbine and duct burners.

Control of NO_x emissions from combustion turbines is generally aimed at either the prevention of NO_x formation or the capture and oxidation of post-combustion NO_x. Since the rate of formation of thermal NO_x is a function of residence time and free oxygen, and is exponential with peak flame temperature, "front-end" control techniques are aimed at controlling one or more of these variables. These controls include the XONONTM system and low-NO_x burners. The XONONTM system uses a catalyst to keep the system temperatures lower while low-NO_x burners offer a staged combustion process, resulting in a lower

peak flame temperature. Water injection reduces the combustion temperature, thereby reducing the formation of NO_x .

Other control methods utilize add-on control equipment to remove NO_x from the exhaust gas stream after its formation. The most common control techniques involve the injection of ammonia into the gas stream to reduce the NO_x to molecular nitrogen and water. Ammonia can either be injected into the system without the use of a catalyst (selective non-catalytic reduction [SNCR]) or with the use of a catalyst (SCR). Finally, EM_xTM (formerly SCONO_xTM), a multi-pollutant control technology, relies upon a catalyst similar to SCR to reduce NO_x emissions but does so without injecting ammonia into the exhaust gas stream.

The output from the RBLC search provided in Appendix D shows that a variety of emission limits and control technologies have been applied to combustion turbines for natural gas and fuel oil combustion. The most stringent limits found during a review of EPA's database were for facilities located in ozone non-attainment areas. These facilities were required to meet such low emission limits since they were subject to LAER requirements.

Typical BACT determinations for combined-cycle units that are located in attainment areas were in the 2 to 15 ppm range using low-NO_x burners, water injection, SCR, or a combination of these technologies. The lower emission rates listed utilize SCR.

5.1.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling NO_x emissions are evaluated for technical feasibility in the following sections.

5.1.2.1 XONON™ System

The XONONTM system controls NO_x emissions by preventing their formation. The key to the XONONTM system is the utilization of a chemical process versus a flame to combust fuel, thus limiting temperature and NO_x formation. The XONONTM system is an integral part of the combustor. The fuel and air that are supplied to the combustor are thoroughly mixed before entering the catalyst. The catalyst is responsible for combusting the fuel to release its energy. Due to the low catalyst operating temperatures, the nitrogen molecules are not involved in the reaction chemistry; they pass through the catalyst unchanged, thereby eliminating NO_x formation. The XONONTM system does have the same high outlet temperature, and some NO_x is formed in the post-combustion process. However, use of the technology has limited NO_x emissions to less than 2.5 ppm.

Currently, the XONONTM system has not had wide-scale application. It has been demonstrated on a 1.5-MW unit in California, with the unit operating in a base load capacity (24 hours a day, 7 days a week). Tests are underway to apply this technology to other types and sizes of turbines; however, testing data is currently unavailable. As the combustion turbine is expected to experience repeated start-ups and shutdowns, it is unclear how the changing load conditions would affect the XONONTM system. As this is a large combined-cycle project, and the XONONTM system has yet to demonstrate applicability for such units, the XONONTM system has been deemed technically infeasible for this Project.

5.1.2.2 EM_xTM System (formerly SCONO_xTM)

The EM_xTM system (formerly SCONO_xTM) uses a single catalyst to remove NO_x emissions from combustion exhaust gas by oxidizing nitric oxide to nitrogen dioxide (NO₂) and then absorbing the NO₂ onto a catalytic surface using a potassium carbonate absorber coating. The potassium carbonate coating reacts with NO₂ to form potassium nitrites and nitrates, which are deposited onto the catalyst surface. The optimal temperature window for operation of the EM_xTM catalyst ranges from 300 °F to 700 °F. EM_xTM does not use ammonia. Therefore, there are no ammonia emissions from this technology.

When all of the potassium carbonate absorber coating has been converted to nitrogen compounds, NO_x can no longer be absorbed and the catalyst must be regenerated. Regeneration is accomplished by passing a dilute hydrogen reducing gas across the surface of the catalyst in the absence of oxygen. Hydrogen in the gas reacts with the nitrites and nitrates to form water and nitrogen. CO₂ in the gas reacts with the potassium nitrite and nitrates to form potassium carbonate, which is the absorbing surface coating on the catalyst. The regeneration gas is produced by reacting natural gas with a carrier gas (such as steam) over a steam-reforming catalyst.

The demonstrated application for EM_xTM is currently limited to combined-cycle combustion turbines under approximately 50 MW in size. The EM_xTM system has not been demonstrated on any type of combustion source other than a combustion turbine. There are technical differences between the proposed combustion turbine versus those few sources where this technology has been demonstrated in practice. In addition, this is a large combined-cycle project, and the EM_x system has yet to demonstrate applicability for such units. Therefore, the EM_x system has not been demonstrated to function efficiently on large combined-cycle combustion turbines and is not technically feasible. (Environmental Resource Management, 2014).

Therefore, EM_xTM is technically infeasible for this Project.

5.1.2.3 Selective Non-Catalytic Reduction

SNCR is a post-combustion NO_x control technology in which a reagent (ammonia or urea) is injected into the exhaust gases to react chemically with NO_x, forming nitrogen and water. The success of this process in reducing NO_x emissions is highly dependent on the ability to uniformly mix the reagent into the flue gas at a zone in the exhaust stream at which the flue gas temperature is within a narrow range, typically from 1,700°F to 2,000°F. To achieve the necessary mixing and reaction, the residence time of the flue gas within this temperature window should be at least 0.5 to 1.0 seconds. The consequences of operating outside the optimum temperature range are severe. Outside the upper end of the temperature range, the reagent will be converted to NO_x. Below the lower end of the temperature range, the reagent will not react with the NO_x and the ammonia slip concentrations (ammonia discharge from the stack) will be very high. The flue gases from the HRSG have an exhaust temperature of approximately 200°F. Even strategically placing the ammonia injection further upstream would probably result only in peak temperatures of around 1,300°F. Such a low temperature would require that additional fuel be combusted at some point in order to raise the temperature to the levels that SNCR will operate. Combustion of the additional fuel would not only increase the NO_x emissions, but also all other criteria pollutants, especially CO. In addition, the added fuel used to raise the exhaust gas temperature will increase the annual operating costs for the facility.

SNCR has not been applied to any combustion turbines according to the RBLC database. Because of the comparatively low exhaust temperatures, fuel and energy requirements, environmental implications and economic considerations; SNCR is considered to be technically infeasible for the combustion turbine and duct burner under consideration for this Project.

5.1.2.4 Selective Catalytic Reduction

SCR is a post-combustion technology that employs ammonia in the presence of a catalyst to convert NO_x to nitrogen and water. The function of the catalyst is to lower the activation energy of the NO_x decomposition reaction. Technical factors related to this technology include the catalyst reactor design, optimum operating temperature, sulfur content of the fuel, de-activation due to aging, ammonia slip emissions, and the design of the ammonia injection system.

SCR represents state-of-the-art control for combined-cycle back end gas turbine NO_x removal. SCR technology is being permitted as LAER and BACT for combined-cycle turbines at 2 to 5 ppm NO_x. Conventional SCR uses a metal honeycomb or "foil" catalyst support structure and requires an HRSG to drop flue gas temperatures to less than 600°F.

The Project's turbine will operate with the exhaust gases reaching temperatures over 1,100°F prior to entering the HRSG. Duct burner firing and passage of the flue gasses through the HRSG will lower the temperature of the gas stream to approximately 200°F. By placing the catalyst bed at the correct strategic point within the HRSG, an SCR could effectively operate and reduce NO_x emissions. A disadvantage of this system is that particles from the catalyst may become entrained in the exhaust stream and contribute to increased particulate matter emissions. In addition, ammonia slip reacts with the sulfur in the fuel creating ammonia bisulfates that become particulate matter. SCR can be applied to the combined-cycle turbine and duct burner and is considered technically feasible.

5.1.2.5 Low-NO_x Burners

Lean premixed combustors are currently available from most turbine manufacturers. This technology seeks to reduce combustion temperatures, thereby reducing NO_x formation. In a conventional combustor, the air and fuel are introduced at an approximately stoichiometric ratio and air/fuel mixing occurs at the flame-front where diffusion of fuel and air reaches the combustible limit. A lean premixed combustor design premixes the fuel and air prior to combustion. Premixing results in a homogenous air/fuel mixture, which minimizes localized fuel-rich pockets that produce elevated combustion temperatures and higher NO_x emissions. A lean air-to-fuel ratio approaching the lean flammability limit is maintained, and the excess air serves as a heat sink to lower combustion temperatures, which lowers NO_x formation. A pilot flame is used to maintain combustion stability in this fuel-lean environment.

Controlled NO_x emission guarantees using low-NO_x burners range from 5 to 25 ppm for turbines 20 MW or greater but vary considerably from vendor to vendor without duct firing. With duct firing, these values vary depending on the size of the duct burners. Low-NO_x burners are currently available for these turbines and duct burners and are a technically feasible control option for this Project for natural gas combustion.

5.1.2.6 Water or Steam Injection

Steam and water injection work to increase the thermal mass by dilution and thereby reduce peak temperatures in the flame zone. With water injection, there is an additional benefit of absorbing the latent heat of vaporization from the flame zone. Water or steam is typically injected at a water-to-fuel ratio of less than one.

Water or steam injection is usually accompanied by an efficiency penalty (typically 2 to 3 percent), but there is an increase in power output (typically 5 to 6 percent) due to the increased mass flow required to maintain turbine inlet temperature at manufacturer's specifications. Both CO and VOC emissions are

increased by water injection depending on the amount of water that is injected. Water injection is generally used for fuel oil combustion because it is difficult to aerosolize the fuel oil for air/fuel mixing or is used on aeroderivative combustion turbines. Water/steam injection is available for the combined-cycle turbine and duct burner under consideration for this Project and is therefore considered technically feasible for fuel oil combustion.

5.1.2.7 Summary of the Technically Feasible Control Options

Technically feasible NO_x control options for the combined-cycle combustion turbine are summarized in Table 5-5. The expected performance has been determined considering the performance of existing systems, vendor guarantees, permitted emission limits, and the design requirements for the combustion turbine.

Table 5-5: Summary of Technically Feasible NO_x Control Technologies for Combined-Cycle Combustion Turbines

| Con | trol System | Expected Performance (ppm) | Technical Feasibility | Comments |
|---------------------|---------------------------------------|--|--------------------------|---|
| Combustion controls | Low-NO _x burners | 35 (natural gas) | Feasible | Standard on combustion turbines for natural gas operation. |
| | Water injection | 42 (fuel oil) | Feasible | Used only during fuel oil operation. |
| | XONONTM | N/A | Not feasible | Testing is still underway. Only used on a 1.5 MW unit not operating continuously. |
| Post | $\mathrm{EM_{x}^{TM}}$ | N/A | Not feasible | For units less than 50 MW in size |
| combustion controls | Selective non- catalytic reduction | N/A | Not feasible | Exhaust temperature is too low. |
| | Selective catalytic reduction | 2 (natural gas with or without duct firing) 6 (fuel oil with or without duct firing) | Feasible | 2 ppm is the lowest achievable emission rate with SCR on natural gas. Catalyst will be fouled on fuel oil. |

5.1.3 Step 3. Rank the Technically Feasible Control Technologies

Add-on controls may be used for natural gas and fuel oil combustion in the turbine. The combustion turbines under consideration come with low-NO_x burners and water injection as part of their standard packages; therefore, low-NO_x burners and water injection are used as the baseline for the proposed combustion turbine.

The technically feasible NO_x control technologies for the combustion turbine are ranked by control effectiveness in Table 5-6.

| Control Technology | Reduction (%) | Controlled Emission Level (ppm) ^a |
|-------------------------------|--------------------------------|--|
| Selective catalytic reduction | 94-85% | 2 ppm (natural gas) 6 ppm (fuel oil) |
| Low-NO _x burners | N/A (baseline for natural gas) | 35 ppm |
| Water injection | N/A (baseline for fuel oil) | 42 ppm |

Table 5-6: Ranking of Technically Feasible NO_x Control Technologies for Combined-Cycle Combustion Turbines

5.1.4 Step 4. Evaluate the Most Effective Controls

Recent BACT determinations have indicated a level of 2 to 15 ppm for NO_x emissions from combined-cycle units that are fired with natural gas (Appendix D). The combustion turbines under consideration are able to achieve 2 ppm while combusting natural gas and 6 ppm while combusting fuel oil on a long-term basis with SCR.

The Project's combined-cycle unit will have an SCR system located in the HRSG, along with low-NO_x burners and water injection which are standard on duel-fuel combustion turbines. The SCR vendors have indicated that 2 ppm is the lowest emission rate achievable with or without the duct burners operating for natural gas combustion. The SCR system will therefore be able to meet 2 ppm for all loads down to MECL, including when duct firing while combusting natural gas and 6 ppm while combusting fuel oil with and without duct firing. Because SCR represents the most effective control and has been selected as BACT, an economic feasibility determination is not required, per 40 CFR 52.21. The energy and environmental considerations for the selected BACT are discussed below for informational purposes.

⁽a) Emission rate for 100% load to MECL with and without duct firing.

SCR is selected as BACT for control of NO_x emissions from the proposed combined-cycle combustion turbine, along with low- NO_x burners (natural gas combustion) and water injection (fuel oil combustion).

5.1.4.1 Selective Catalytic Reduction

Energy Impacts

An SCR system results in a loss of energy due to the pressure drop across the SCR catalyst. To compensate for the energy loss in the SCR system, additional natural gas combustion is required to maintain the net energy output, which also results in additional air pollutant emissions.

Environmental Impacts

SCR systems consist of an ammonia injection system and a catalytic reactor. Urea can be decomposed in an external reactor to form ammonia for use in a SCR. Unreacted ammonia may escape through to the exhaust gas. This is commonly called "ammonia slip." It is estimated that ammonia slip from an SCR on a unit this size could be 10 ppm and may be considered to be an environmental impact. The ammonia that is released may also react with other pollutants in the exhaust stream to create fine particulates in the form of ammonium salts. In addition, the storing of the ammonia on-site is another environmental and safety concern. SCR catalysts must also be replaced on a routine basis. In some cases, these catalysts may be classified as a hazardous waste. This typically requires either returning the material to the manufacturer for recycling and reuse or disposal in designated landfills.

5.1.4.2 Low-NO_x Burners

Energy Impacts

Low-NO_x burners are usually accompanied by an efficiency penalty (typically 2 to 3 percent) and an increase in power output (typically 5 to 6 percent). The increase in power output results from the increase in mass flow required to maintain turbine inlet temperature at manufacturer's specifications. Because there is a power increase, no energy impacts are associated with low-NO_x burners.

Environmental Impacts

The low-NO_x burner system may increase CO and VOC emissions on a lb/hr basis; however, the potential increase in CO and VOC emissions does not outweigh the advantages of decreased NO_x emissions to reduce health effects.

Economic Impacts

The turbine manufacturer currently installs low-NO_x burners as standard equipment on natural gas-fired combustion turbines. With the low-NO_x burners, these turbines may achieve NO_x emission rates of 35

ppm at full load. Since the low-NO_x burners are considered standard equipment on the turbine, there is no annualized cost of the control.

5.1.4.3 Water Injection

Energy Impacts

Water injection, used during fuel oil operation only, is also usually accompanied by an efficiency penalty (typically 2 to 3 percent) and an increase in power output (typically 5 to 6 percent). No huge energy impacts are associated with water injection.

Environmental Impacts

Water injection does use water, a natural resource, to control NO_x emissions. However, at the very few operating hours that are requested in this permit, the water use should be very minimal.

5.1.5 Step 5. Proposed NO_x BACT Determination

The BACT recommended for control of NO_x emissions from the combined-cycle combustion turbine is low-NO_x burners and water injection with SCR. These controls will meet a NO_x emission limit of 2 ppm at 15 percent oxygen during steady state conditions for all loads down to MECL with and without duct firing for natural gas combustion and 6 ppm at 15 percent oxygen during steady state conditions for all loads down to MECL with and without duct firing for fuel oil combustion. Compliance will be determined with NO_x CEMs on a 24-hour rolling average, excluding start-up and shutdown.

5.2 BACT for Carbon Monoxide – Combined-Cycle Combustion Turbine (P01)

Previously submitted BACT Sections and updated references to the carbon monoxide BACT section for the combined-cycle combustion turbine is presented in Table 5-7. The updated combined-cycle combustion turbine carbon monoxide BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

| Description | Previous Application Reference | December 2021 Submittal Location |
|----------------------------|-------------------------------------|-------------------------------------|
| BACT Analysis Steps 1 to 5 | 5.0 BACT December 2018 Submittal | 5.0 BACT |
| | Table D-1a (natural gas), | Table D-1a (natural gas), |
| | Table D-1b (fuel oil) | Table D-1b (fuel oil) |
| RBLC | Appendix D, December 2018 Submittal | Appendix D |
| KBLC | | |

Table 5-7: Combustion Turbine Carbon Monoxide BACT Analysis References

Table D-1a Addendum (natural gas), Table D-1b Addendum (fuel oil) Appendix D The following sections outline the top-down steps for CO emissions from combustion turbines.

5.2.1 Step 1. Identify Potential Control Strategies

CO is a product resulting from incomplete combustion. Control of CO is typically accomplished by providing adequate fuel residence time and a high temperature in the combustion zone to complete combustion. These control factors, however, also tend to result in increased emissions of NO_x. Conversely, a lower NO_x emission rate achieved through flame temperature control (by water injection or dry lean pre-mix) can result in higher levels of CO emissions. A compromise is usually established where the flame temperature reduction is set to achieve the lowest NO_x emission rate possible while keeping CO emissions to an acceptable level.

CO emissions from combustion turbines are a function of oxygen availability (excess air), flame temperature, residence time at flame temperature, combustion zone design, and turbulence. Post-combustion control involves the use of catalytic oxidation; front-end control involves controlling the combustion process to suppress CO formation.

The technologies identified for reducing CO emissions from the Project's turbine are the EM_x^{TM} system, an oxidation catalyst, and combustion controls. The standard technology for reducing CO emissions is to maintain "good combustion" through proper control and monitoring of the combustion process.

A survey of the RBLC database (Appendix D) indicated that most new combined-cycle turbines in attainment areas have been required to install add-on controls to control CO emissions from combined-cycle turbines. CO emissions from natural gas-fired combined-cycle turbines ranged from 0.9 to 25 ppm. H-class combustion turbines in combined-cycle mode have been permitted from 0.9 ppm to 5 ppm in most cases, based on the information that is available in the RBLC and from other sources that describe the class of turbines installed at the various locations. The lowest Siemens H-class permitted unit is 2.0 ppm.

5.2.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling CO emissions are evaluated for technical feasibility in the following sections.

5.2.2.1 EM_xTM System

The EM_x^{TM} system was described in the BACT analysis for NO_x . The EM_x^{TM} system simultaneously oxidizes CO to CO_2 , NO to NO_2 , and then absorbs NO_2 onto the surface of a catalyst using a potassium carbonate absorber coating. VOCs are also removed by the catalyst system. The system does not use

ammonia and operates most effectively at temperatures ranging from 300°F to 700°F. Operation of EM_x^{TM} requires natural gas, water, steam, electricity, and ambient air. Steam and reformed natural gas are used periodically to regenerate the catalyst bed and are an integral part of the process. Because EM_x^{TM} does not use ammonia there are no ammonia emissions from this technology.

Regeneration of the catalyst is accomplished by passing a dilute hydrogen reducing gas across the surface of the catalyst in the absence of oxygen. Hydrogen in the gas reacts with the nitrites and nitrates to form water and nitrogen. CO₂ in the gas reacts with the potassium nitrite and nitrates to form potassium carbonate, which is the absorbing surface coating on the catalyst. The regeneration gas is produced by reacting natural gas with a carrier gas (such as steam) over a steam-reforming catalyst.

The demonstrated application for EM_xTM is currently limited to combined-cycle combustion turbines under approximately 50 MW in size. The EM_xTM system has not been demonstrated on any type of combustion source other than a combustion turbine. There are technical differences between the proposed combustion turbine versus those few sources where this technology has been demonstrated in practice. These significant technical differences preclude a determination that the EM_xTM system has been demonstrated to function efficiently on sources that are similar to the proposed furnaces and boilers (Environmental Resource Management, 2014).

Therefore, the EM_x^{TM} system is considered a technically infeasible method of controlling CO emissions from the proposed combined-cycle combustion turbine and duct burner.

5.2.2.2 Oxidation Catalyst

Oxidation catalysts are a post-combustion technology which does not rely on the introduction of additional chemicals, such as ammonia with SCR, for a reaction to occur. The oxidation of CO to CO₂ utilizes excess air present in the turbine exhaust; the activation energy required for the reaction to proceed is lowered in the presence of a catalyst. Products of combustion are introduced into a catalytic bed, with the optimum temperature range for these systems being between 700°F and 1,100°F. At higher temperatures, catalyst sintering may occur, potentially causing permanent damage to the catalyst. The addition of a catalyst bed onto the turbine exhaust will create a pressure drop, resulting in back pressure to the turbine. This has the effect of reducing the efficiency of the turbine and the power generating capabilities. It is expected that the catalyst will be placed in the exhaust train (HRSG) where the temperature will be optimal for the catalytic reaction.

The use of an oxidation catalyst is considered to be a technically feasible method of controlling CO emissions from the proposed combined-cycle combustion turbine and duct burner.

5.2.2.3 Combustion Control

"Good combustion practices" include operational and incinerator design elements to control the amount and distribution of excess air in the flue gas to confirm that there is enough oxygen present for complete combustion. Such control practices applied to the proposed turbine can achieve CO emission levels of 4 ppm for the combustion turbine at 100 percent load.

Good combustion practices are considered to be a technically feasible method of controlling CO emissions from the proposed combined-cycle combustion turbine and duct burner.

5.2.2.4 Summary of the Technically Feasible Control Options

The technical feasibility of the CO control options for the proposed combined-cycle combustion turbine is summarized in Table 5-8. The expected performance has been determined considering the performance of existing systems, vendor guarantees, permitted emission limits, and the design requirements for the turbines.

Table 5-8: Summary of Technically Feasible CO Control Technologies for Combined-Cycle Combustion Turbines

| Control System | | Expected Performance (ppm) ^a | Technical Feasibility | Comments |
|-----------------|--------------------|---|--------------------------|---|
| Combusti | on controls | 4 (natural gas) 10 (fuel oil) | Feasible | Standard on turbines. Not an add- on control |
| Post combustion | Oxidation catalyst | 1.5 (natural gas) 1.5 (fuel oil) | Feasible | Produces CO ₂ emissions |
| controls | EM_{x}^{TM} | N/A | Not feasible | For units less than 50 MW in size |

⁽a) Natural gas limit valid for 100% load with duct firing down to MECL. Fuel oil limit valid for 100% load with duct firing down to 75% load.

5.2.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible CO control technologies for the combustion turbine are ranked by control effectiveness in Table 5-9.

| Control Technology | Reduction (%) | Controlled Emission Level (ppm) ^a |
|--------------------|---------------------------|--|
| Oxidation catalyst | 50-80% | 1.5 (natural gas) 1.5 (fuel oil) |
| Combustion control | Not applicable (baseline) | 4 (natural gas) 10 (fuel oil) |

Table 5-9: Ranking of Technically Feasible CO Control Technologies for Combined-Cycle Combustion Turbines

5.2.4 Step 4. Evaluate the Most Effective Control Technologies

Operating the proposed combined-cycle combustion turbine with good combustion practices will achieve 1.5 ppm at 15 percent oxygen on a long-term basis for 100 percent load with duct firing down to MECL for natural gas combustion and 1.5 ppm at 15 percent oxygen for 100 percent load with duct firing down to 75 percent load for fuel oil combustion. The next step is to review each of the technically feasible control options for environmental, energy, and economic impacts.

5.2.4.1 Oxidation Catalyst

Energy Impacts

The addition of a catalyst bed onto the turbine exhaust for the oxidation catalyst will create a pressure drop, resulting in back pressure to the turbine. This has the effect of reducing the efficiency of the turbine and the power generating capabilities.

Environmental Impacts

The oxidation catalyst oxidizes CO to CO₂ which is released to the atmosphere. CO₂ is a greenhouse gas that may be contributing to global warming and is now a regulated pollutant. Increasing CO₂ emissions could have a negative impact on the atmosphere. However, the oxidation catalyst will also reduce the amount of methane (CH₄) (also a greenhouse gas). Considering both greenhouse gases, the net effect is an overall decrease in greenhouse gas emissions on a CO₂e basis.

As with all controls that utilize catalysts for removal of pollutants, the catalyst must be disposed of after it is spent. The catalyst may be considered hazardous waste and require special treatment or disposal; even if it is not hazardous, it adds to the already full landfills.

Economic Impacts

The Owners have selected the highest control available for CO emissions; therefore, no economic analysis is necessary.

⁽a) Natural gas limit valid for 100% load with duct firing down to MECL. Fuel oil limit valid for 100% load with duct firing down to 75% load.

The impacts listed above do not outweigh the health benefits of controlling CO emissions with the use of an oxidation catalyst.

An oxidation catalyst along with good combustion practices was selected as BACT for control of CO emissions from the combined-cycle combustion turbine.

5.2.5 Step 5. Proposed CO BACT Determination

The BACT recommended for control of CO emissions from the proposed combustion turbine is good combustion practices and the use of an oxidation catalyst. These controls will meet a CO emission limit of 1.5 ppm at 15 percent oxygen during steady state conditions for all loads down to MECL with and without duct firing for natural gas combustion and 1.5 ppm at 15 percent oxygen for 75 percent to 100 percent load with and without duct firing for fuel oil combustion. These proposed limits are on a 168-hour rolling average.

5.3 BACT for Particulate Matter – Combined-Cycle Combustion Turbine (P01)

Previously submitted BACT Sections and updated references to the particulate matter BACT section for the combined-cycle combustion turbine is presented in Table 5-10. The updated combined-cycle combustion turbine particulate matter BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

| Description | Previous Application Reference | December 2021 Submittal Location |
|----------------------------|---|--|
| BACT Analysis Steps 1 to 5 | 5.0 BACT December 2018 Submittal | 5.0 BACT |
| RBLC | Table D-1a (natural gas), Table D-1b (fuel oil) Appendix D, December 2018 Submittal | Table D-1a (natural gas), Table D-1b (fuel oil) Appendix D |
| | | Table D-1a Addendum (natural gas), Table D-1b Addendum (fuel oil) Appendix D |

Table 5-10: Combustion Turbine Particulate Matter BACT Analysis References

The following sections outline the top-down steps for particulate matter emissions from combustion turbines.

5.3.1 Step 1. Identify Potential Control Strategies

Particulate (PM/PM₁₀/PM_{2.5}) emissions from natural gas combustion sources consist of inert contaminants in natural gas, of sulfates from fuel sulfur or mercaptans used as odorants, of dust drawn in from the

ambient air, and particles of carbon and hydrocarbons resulting from incomplete combustion. Therefore, units firing fuels with low ash content and high combustion efficiency exhibit correspondingly low particulate emissions.

A contributor to PM/PM₁₀/PM_{2.5} emissions in combined-cycle turbines with SCR is the ammonium sulfates that are produced when NO₂ and ammonia react with sulfur in the fuel. Sulfur is present in all fuels, including natural gas and fuel oil proposed for this Project. Because of the sulfur, ammonium sulfates can form, as illustrated by the following equations:

$$2NH_3 + SO_3 + H_2O \rightarrow (NH_4)_2 HSO_4$$

$$NH_3 + SO_3 + H_2O \rightarrow NH_4 HSO_4$$

Ammonium sulfates are also formed when the ammonia content of the flue gas exceeds that of the sulfur trioxide (SO₃); the amount of ammonium bisulfate then can increase as the ammonia slip increases. Other variables are velocity/temperature profiles, oxygen levels, water content, cycling, presence of an oxidation catalyst or duct burner, ammonia/SO₃ ratios, etc. Therefore, it is expected that combustion turbines with SCR will have higher particulate emissions than those without SCR.

Post-combustion controls, such as electrostatic precipitators (ESPs) or baghouses, have never been applied to commercial gas-fired turbines. Available control strategies include the use of low ash fuel, such as natural gas, and combustion controls. BACT emission rates vary in the RBLC database with rates being listed as 0.0012 to 0.044 lb/MMBtu and 4.4 to 43 lb/hr for natural gas and 0.0168 to 0.0368 lb/MMBtu and 34.3 to 72 lb/hr for fuel oil. As stated previously, these emission rates vary due to many reasons.

5.3.2 Step 2. Identify Technically Feasible Control Technologies

Particulate control devices are not typically installed on gas turbines. Post-combustion controls, such as ESPs or baghouses, have never been applied to commercial gas-fired turbines. Therefore, the use of ESPs and baghouse filters are both considered technically infeasible, and do not represent an available control technology.

In the absence of add-on controls, the most effective control method demonstrated for combustion turbines is the use of low ash fuel, such as natural gas, and combustion controls. This was confirmed by a survey of the RBLC database (Appendix D) which showed no add-on PM/PM₁₀/PM_{2.5} control

technologies for combined-cycle combustion turbine units. Proper combustion control and the firing of fuels with negligible or zero ash content (such as natural gas) is the predominant control method listed.

5.3.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible $PM/PM_{10}/PM_{2.5}$ control technologies for the combustion turbine are ranked by control effectiveness in Table 5-11.

Table 5-11: Ranking of Technically Feasible PM/PM₁₀/PM_{2.5} Control Technologies for Combined-Cycle Combustion Turbine

| Control Technology | Reduction (%) | Controlled Emission Level (lb/hr) ^a |
|-------------------------------------|---------------------------------|---|
| Low ash fuel and combustion control | Not applicable (baseline) | 36.3 lb/hr (natural gas with duct firing) 21.8 lb/hr (natural gas) 54.5 lb/hr (fuel oil with duct firing) 39.4 lb/hr (fuel oil) |

⁽a) Emission rate for 100% load to MECL with and without duct firing.

5.3.4 Step 4. Evaluate the Most Effective Control Technologies

No energy, environmental, or economic impacts are associated with combustion controls; the use of low ash fuel is not an add-on control device.

5.3.5 Step 5. Proposed PM/PM₁₀/PM_{2.5} BACT Determination

The use of low ash fuels and good combustion control represents BACT for PM/PM₁₀/PM_{2.5} control in the proposed combined-cycle combustion turbine. These operational controls will limit PM/PM₁₀/PM_{2.5} emissions, including duct burner emissions, to the levels shown in Table 5-11, above, depending on fuel and operating condition for combined-cycle operation.

This limit includes front and back half PM/PM₁₀/PM_{2.5} emissions, takes into account emissions from the ammonium sulfate produced from sulfur and ammonia slip that could be emitted as PM/PM₁₀/PM_{2.5}, and includes the duct burner emissions that will be emitted out of the turbine stack.

5.4 BACT for Volatile Organic Compounds – Combined-Cycle Combustion Turbine

Previously submitted BACT Sections and updated references to the VOC BACT section for the combined-cycle combustion turbine is presented in Table 5-12. The updated combined-cycle combustion turbine VOC BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

December 2021 **Previous Application Reference** Description **Submittal Location 5.0 BACT** BACT Analysis Steps 1 to 5 **5.0 BACT** December 2018 Submittal Table D-1a (natural gas), Table D-1a (natural gas), Table D-1b (fuel oil) Table D-1b (fuel oil) Appendix D Appendix D, December 2018 Submittal **RBLC** Table D-1a Addendum (natural gas), Table D-1b Addendum (fuel oil) Appendix D

Table 5-12: Combustion Turbine Sulfuric Acid Mist BACT Analysis References

The following sections outline the top-down steps for VOC emissions from combustion turbines.

5.4.1 Step 1. Identify Potential Control Strategies

Like CO, VOC is a product resulting from incomplete combustion. VOC emissions occur when a portion of the natural gas fuel remains unburned or is only partially burned during the combustion process. With natural gas, some organics are unreacted trace constituents of the gas, while others may be products of the heavier hydrocarbon constituents. Partially burned hydrocarbons result from poor air-to-fuel mixing prior to, or during, combustion or incorrect air-to-fuel ratios in the combustion turbine.

The technologies identified for reducing VOC emissions from combined-cycle combustion turbines are the same as identified for CO control: the multi-pollutant control system, an oxidation catalyst (also referred to as a CO catalyst), and combustion controls. The standard technology for reducing VOC emissions is to maintain "good combustion" through proper control and monitoring of the combustion process through the air-to-fuel ratio. In addition, since most of the BACT determinations for CO for combined-cycle combustion turbines also include an oxidation catalyst, determinations for VOC emissions often include an oxidation catalyst along with good combustion practices. A survey of the RBLC database (Appendix D) indicates that combustion controls is the most prevalent BACT control along with oxidation catalysts listed as LAER and BACT for VOC. VOC emissions from the permitted facilities ranged from 0.3 ppm to 5 ppm for natural gas-fired combustion turbines and 2 ppm to 3.6 ppm for fuel-oil combustion.

5.4.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling VOC emissions are evaluated for technical feasibility in the following sections.

5.4.2.1 EM_x™ System

The EM_xTM system was described in the BACT analysis for NO_x (Section 5.1.2.2). It is also applicable for controlling VOC and can reduce emissions by up to 20 percent. The system does not use ammonia and operates most effectively at temperatures ranging from 300°F to 700°F. Operation of EM_xTM requires natural gas, water, steam, electricity, and ambient air. Steam and reformed natural gas are used periodically to regenerate the catalyst bed and are an integral part of the process. Because EM_xTM does not use ammonia, there are no ammonia emissions from this technology.

Regeneration of the catalyst is accomplished by passing a dilute hydrogen reducing gas across the surface of the catalyst in the absence of oxygen. Hydrogen in the gas reacts with the nitrites and nitrates to form water and nitrogen. CO₂ in the gas reacts with the potassium nitrite and nitrates to form potassium carbonate, which is the absorbing surface coating on the catalyst. The regeneration gas is produced by reacting natural gas with a carrier gas (such as steam) over a steam-reforming catalyst.

The demonstrated application for EM_xTM is currently limited to combined-cycle combustion turbines under approximately 50 MW in size. The EM_xTM system has not been demonstrated on any type of combustion source other than a combustion turbine. There are technical differences between the proposed combustion turbine versus those few sources where this technology has been demonstrated in practice. These significant technical differences preclude a determination that the EM_xTM system has been demonstrated to function efficiently on sources that are similar to the proposed furnaces and boilers (Environmental Resource Management, 2014).

Therefore, the EM_x^{TM} system is considered a technically infeasible method of controlling VOC emissions from the proposed combined-cycle combustion turbines and duct burners.

5.4.2.2 Oxidation Catalyst

As discussed in Section 5.2.2.2, oxidation catalysts are a post-combustion technology that do not rely on the introduction of additional chemicals, such as ammonia or urea with SCR, for a reaction to occur. The catalyst beds that reduce CO also promote the oxidation of VOC, thereby reducing the VOC emissions out the stack. Such systems typically achieve a maximum of 35 to 40 percent removal of VOC, as opposed to the much higher efficiencies achieved for CO reduction.

The use of an oxidation catalyst for VOC control is considered to be technically feasible for the combined-cycle combustion turbine.

5.4.2.3 Combustion Control

"Good combustion practices" include operational and design elements to control the amount and distribution of excess air in the flue gas to confirm that there is enough oxygen present for complete combustion (controlling the air-to-fuel ratio). Such control practices applied to the proposed turbine can achieve VOC emission levels of approximately 1 ppm when combusting natural gas or fuel oil without an oxidation catalyst for all loads down to MECL.

Good combustion practices are a technically feasible method of controlling VOC emissions from the proposed combustion turbine.

5.4.2.4 Summary of the Technically Feasible Control Options

The technical feasibility of the VOC control options for the proposed combustion turbine is summarized in Table 5-13. The expected performance has been determined considering the performance of existing systems, vendor guarantees, permitted emission limits, and the design requirements for the turbine.

Table 5-13: Summary of Technically Feasible VOC Control Technologies for Combined-Cycle Combustion Turbines

| Control System | | Expected Performance (ppm) | Technical Feasibility | Comments |
|---------------------|---------------------------------|--|--------------------------|--|
| Combustion controls | | 1 ppm (natural gas without duct firing) 1 ppm (fuel oil without duct firing) | Feasible | Standard on the proposed combustion turbine. Not an add-on control |
| Post combustion | | | Feasible | Produces CO ₂ emissions. |
| controls | $\mathrm{EM_{x}}^{\mathrm{TM}}$ | N/A | Not feasible | For units less than 50 MW in size |

5.4.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible VOC control technologies for the proposed combined-cycle combustion turbine are ranked by control effectiveness in Table 5-14.

| Control Reduction Technology (%) | | Controlled Emission Level (ppm) ^a |
|----------------------------------|---------------------------|---|
| Oxidation catalyst | 35-40% | 2.7 ppm (natural gas with duct firing) 0.6 ppm (natural gas) 3.3 ppm (fuel oil with duct firing) 0.6 ppm (fuel oil) |
| Combustion control | Not applicable (baseline) | 4.1 ppm (natural gas with duct firing) 1 ppm (natural gas) 5.6 ppm (fuel oil with duct firing) 1 ppm (fuel oil) |

Table 5-14: Ranking of Technically Feasible VOC Control Technologies for Combined-Cycle Combustion Turbines

5.4.4 Step 4. Evaluate the Most Effective Control Technologies

The next step is to review each of the technically feasible control options for environmental, energy, and economic impacts.

5.4.4.1 Oxidation Catalyst

Energy Impacts

The addition of a catalyst bed onto the turbine exhaust for the oxidation catalyst will create additional pressure drop, resulting in increased back pressure to the turbine. This has the effect of reducing the efficiency of the turbine and the power generating capabilities.

Environmental Impacts

The oxidation catalyst oxidizes CO and VOC to CO₂ which is released to the atmosphere. CO₂ is a greenhouse gas that may be contributing to global warming. Increasing CO₂ emissions could have a negative impact on the atmosphere.

In addition, as with all controls that utilize catalysts for pollutant removal, the catalyst must be disposed of after it is spent. The catalyst may be considered hazardous waste and require special treatment or disposal; even if it is not hazardous, it adds to the existing landfills.

Economic Impacts

The Owners have selected the highest control available for VOC emissions; therefore, no economic analysis is necessary.

⁽a) Emission rate for 100% load to MECL with and without duct firing.

5.4.4.2 Combustion Control

No energy, environmental, or economic impacts are associated with combustion controls.

5.4.5 Step 5. Proposed VOC BACT Determination

The BACT recommended for control of VOC emissions from the proposed combustion turbine is the use of good combustion practices with the added control of an oxidation catalyst. These controls will meet a VOC natural gas combustion emission limit of 2.7 ppm at 15 percent oxygen and 0.6 ppm at 15 percent oxygen with and without duct firing, respectively for all steady state loads down to MECL. The controls will also meet a VOC fuel oil limit of 3.3 ppm at 15 percent oxygen and 0.6 ppm at 15 percent oxygen, with and without duct firing, respectively for all steady state loads down to MECL. These emission rates represent the lowest emission rate achievable for VOC emissions with an oxidation catalyst for this turbine. Compliance will be determined on a 168-hour rolling average.

An oxidation catalyst along with good combustion practices was selected as BACT for VOC emissions from the proposed combined-cycle combustion turbine for both fuel oil and natural gas combustion.

5.5 BACT for Sulfuric Acid Mist – Combined-Cycle Combustion Turbine

Previously submitted BACT Sections and updated references to the sulfuric acid mist BACT section for the combined-cycle combustion turbine is presented in Table 5-15. The updated combined-cycle combustion turbine sulfuric acid mist BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

December 2021 Description **Previous Application Reference Submittal Location 5.0 BACT** BACT Analysis Steps 1 to 5 **5.0 BACT** December 2018 Submittal Table D-1a (natural gas), Table D-1a (natural gas), Table D-1b (fuel oil) Table D-1b (fuel oil) Appendix D Appendix D, December 2018 Submittal **RBLC** Table D-1a Addendum (natural gas). Table D-1b Addendum (fuel oil) Appendix D

Table 5-15: Combustion Turbine Sulfuric Acid Mist BACT Analysis References

The following sections outline the top-down steps for H₂SO₄ mist emissions from combustion turbines.

5.5.1 Step 1. Identify Potential Control Strategies

The majority of the fuel sulfur combusted in the combustion turbine leaves the boiler as SO₂. During combustion, a small percentage of the fuel sulfur is further oxidized from SO₂ to SO₃. As the temperature of the flue gas decreases as it passes through the HRSG and pollution control systems, this SO₃ may combine with water vapor present in the exhaust gas path to form sulfuric acid vapor.

When the flue gas temperature drops below the acid dew point, sulfuric acid vapor further condenses into an aerosol, forming H₂SO₄ mist. H₂SO₄ mist may also be a component of condensable particulate matter, with particle sizes in the sub-micron size.

Very limited data is available on the quantity of SO₂ that will be converted to SO₃ through the entire combustion turbine/HRSG/SCR/oxidation catalyst. Vanadium is the component in SCR catalyst and is believed to catalyze the oxidation of SO₂ to SO₃ in the exhaust train when present in the fuel. No information on the amount of SO₂ that is oxidizes to SO₃ is available for oxidation catalyst. Therefore, the H₂SO₄ emission estimate assumes 100 percent conversion of SO₂ to SO₃ and 100 percent conversion of SO₃ to H₂SO₄, since no guarantees exist, and very little data is available for this combustion turbine with back-end controls. The combustion turbine will combust natural gas with sulfur content up to 0.5 grains per standard cubic foot on a 12-month rolling average, and fuel oil that will be less than or equal to 15 ppm sulfur (ultra-low sulfur fuel oil).

5.5.2 Step 2. Identify Technically Feasible Control Technologies

As with SO₂, there are no add-on controls available for H₂SO₄ mist from combustion turbines. In the absence of add-on controls, the most effective control method demonstrated for combustion turbines is the use of low sulfur fuel, such as natural gas and ultra-low sulfur fuel oil, and combustion controls. Proper combustion control and the firing of fuels with very low sulfur content is the only known control method available. This was confirmed by a survey of the RBLC database (Appendix D).

5.5.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible H₂SO₄ mist control technologies for the combustion turbine are ranked by control effectiveness in Table 5-16.

| Table 5-16: Ranking of Technically Feasible H₂SO₄ |
|--|
| Control Technologies for Combined-Cycle Combustion Turbines |

| Control Technology | Reduction (%) | Controlled Emission Level (lb/hr) ^a |
|--|---------------------------|---|
| Low sulfur fuel and combustion control | Not applicable (baseline) | 9.9 lb/hr (natural gas with duct firing) 7.8 lb/hr (natural gas) 9.3 lb/hr (fuel oil with duct firing) 7.0 lb/hr (fuel oil) |

⁽a) Emission rate for 100% load to MECL with and without duct firing.

5.5.4 Step 4. Evaluate the Most Effective Control Technologies

There are no energy, environmental, or economic impacts associated with combustion controls; the use of low sulfur fuel and combustion control is not an add-on control device.

5.5.5 Step 5. Proposed H₂SO₄ Mist BACT Determination

The use of low sulfur fuel and good combustion control represents BACT for H₂SO₄ mist control in the proposed combined-cycle combustion turbine. These operational controls will limit H₂SO₄ mist emissions, including duct burner emissions, to the levels shown in Table 5-16, above, depending on fuel and operating condition for combined-cycle operation.

5.6 BACT for Greenhouse Gases – Combined-Cycle Combustion Turbine (P01)

Previously submitted BACT Sections and updated references to the greenhouse gases BACT section for the combined-cycle combustion turbine is presented in Table 5-17. The updated combined cycle combustion turbine greenhouse gas BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

Table 5-17: Combustion Turbine Greenhouse Gases BACT Analysis References

| Description | Previous Application Reference | December 2021 Submittal Location |
|----------------------------|--|--|
| BACT Analysis Steps 1 to 5 | 5.0 BACT December 2018 Submittal | 5.0 BACT |
| RBLC | Table D-1a (natural gas), Table D-1b (fuel oil) Appendix D December 2018 Submittal | Table D-1a (natural gas), Table D-1b (fuel oil) Appendix D |
| | | Table D-1a Addendum (natural gas), Table D-1b Addendum (fuel oil) Appendix D |

The following sections outline the top-down steps for greenhouse gas (GHG) emissions from combustion turbines.

5.6.1 Step 1. Identify All Potential Control Strategies

For the proposed combined-cycle combustion turbine, the CO₂e emissions are due to CO₂, CH₄, and nitrogen oxide (N₂O) emissions. The GWP of CH₄ and N₂O emissions are normalized to the warming potential of carbon dioxide (as CO₂e) by multiplying the CH₄ emissions by 25 and the N₂O emissions by 298. Despite the higher warming potentials of CH₄ and N₂O compared to CO₂, it is expected that CO₂ emissions will still account for over 99 percent of the CO₂e GWP for this unit, based on published emission factors for natural gas-fired turbines.

There are two broad strategies for reducing CO₂ emissions from stationary combustion processes such as combustion turbines. The first is to minimize the production of CO₂ through the use of low-carbon fuels and through aggressive energy-efficient design. The use of gaseous fuels, such as natural gas, reduces the production of CO₂ during the combustion process relative to burning solid fuels (e.g., coal or coke) and liquid fuels (e.g., distillate or residual oils). Additionally, a highly efficient operation requires less fuel for process heat, which directly impacts the amount of CO₂ produced. Establishing an aggressive basis for energy recovery and facility efficiency will reduce CO₂ production and the costs to recover it.

The second strategy for CO₂ emission reduction is carbon capture and sequestration. The inherent design of the combustion turbines produces a dilute CO₂ stream for potential capture.

The CO₂ emissions from combustion turbines can theoretically be captured through pre-combustion methods or through post-combustion methods. In the pre-combustion approach, oxygen instead of air is used to combust the fuel and a concentrated CO₂ exhaust gas is generated. This approach significantly reduces the capital and energy cost of removing CO₂ from conventional combustion processes using air as an oxygen source, but it incurs significant capital and energy costs associated with separating oxygen from the air.

Post-combustion methods are applied to conventional combustion techniques using air and carbon-containing fuels in order to isolate CO₂ from the combustion exhaust gases. Because the air used for combustion contains nearly 80 percent nitrogen, the CO₂ concentration in the exhaust gases is only 5 to 20 percent depending on the amount of excess air and the carbon content of the fuel.

5.6.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling GHG emissions are evaluated for technical feasibility in the following sections.

5.6.2.1 Fuel Selection

Fuel selection has a significant impact on GHG formation.

5.6.2.1.1 Low-Carbon Fuels

Numerous fuels are available for use. As Table 5-18 shows, combustion of natural gas yields 40 to 50 percent less CO₂ than does combustion of coal and petroleum coke and approximately 30 percent less CO₂ than does combustion of residual oil. Accordingly, the preferential burning of a low-carbon gaseous fuel in the proposed combustion turbine is an extremely effective CO₂ control technique. This control technique is technically feasible for the combustion turbine and duct burner and is an inherent part of the Project's design.

Table 5-18: CO₂ Emission Factors

| Fuel | kilograms CO₂ per MMBtu |
|---------------------------|-------------------------|
| Petroleum coke | 113.67 |
| Coal (anthracite) | 103.69 |
| Distillate fuel oil No. 2 | 73.96 |
| Natural gas | 53.06 |

Source: Title 40 CFR Part 98: Table C-1 to Subpart C of Part 98 -

Default CO₂ Emission Factors and Types of Fuel

5.6.2.1.2 Combustion of Biogenic Sources

The proposed combustion turbine has not been designed to accommodate fibrous biomass, such as woody biomass, which is the most likely biomass available in sufficient quantities for the unit from the surrounding area. For both regulatory and technical feasibility issues, biogenic sources are not a feasible option since they are not part of the original design.

5.6.2.2 Energy Efficiency

The evaluation of energy efficiency, continuous excess air monitoring and control and the selection of efficient turbine design, are discussed below.

5.6.2.2.1 Continuous Excess Air Monitoring and Control

Excessive amounts of combustion air in turbines results in energy-inefficient operation because more fuel combustion is required in order to heat the excess air to combustion temperatures. This inefficiency can be alleviated using state-of-the-art instrumentation for monitoring and controlling the excess air levels in the combustion process, which reduces the heat input by minimizing the amount of combustion air needed for safe and efficient combustion. Additionally, lowering excess air levels, while maintaining good combustion, reduces not only CO₂ emissions but also NO_x emissions. The combustion turbine will be equipped with oxygen monitors as part of the CEM system.

5.6.2.2.2 Selection of Efficient Turbine Design

Energy efficiency reduces CO₂ emissions by maximizing the operation of the combustion turbine, thereby reducing the amount of fuel burned per megawatt-hr produced.

Combustion control optimization and energy efficient equipment is a main control strategy for emissions of greenhouse gases. The combustion turbine design that is under consideration for this Project is highly efficient. Energy efficiency is technically and economically feasible. Potential options that may increase efficiency include the following:

- Airfoil-shaped compressor rotor blades designed to increase compressor efficiency
- 13 stage high efficiency compressor design with modulating inlet guide vanes and inter-stage air extraction for cooling and sealing air
- Fuel gas heating via HRSG feedwater to improve turbine efficiency while maintaining constant firing temperature
- Inlet air filtration system utilizing high efficiency media filters to remove combustion air contaminants
- On and off-line compressor water wash capability to remove deposits and other contaminants from compressor blades to maintain and improve compressor efficiency
- Low-NO_x combustor for improved performance, enhanced operability, and lower emissions
- Extended turndown for increased spinning reserve capability and lower fuel costs
- Advanced hot gas path components with 3D airfoil shapes, improved materials, improved sealing, more effective cooling to achieve increased turbine efficiency
- Higher firing temperatures to increase turbine performance and overall turbine efficiency

5.6.2.3 Add-on Control Devices

Another method of GHG control is an add-on control device.

5.6.2.3.1 Catalytic Oxidation

N₂O emissions are reduced by passing the combustion gases over a catalyst, converting N₂O to nitrogen plus oxygen. Similarly, VOC emissions, such as CH₄, may be converted from CH₄ to CO₂ plus water. For the same reasons given above in the discussion for CO BACT controls, **catalytic oxidation is technically feasible for the control of GHG emissions from the proposed combined-cycle combustion turbine.**

5.6.2.3.2 Thermal Oxidation

Several types of thermal oxidation technology are available. All these technologies oxidize CH₄ to CO₂ and water, by raising the temperature of the treated gas stream to approximately 1,600°F for approximately one to two seconds. Given sufficient mixing, this residence time and temperature is capable of achieving at least a 98 percent reduction in CH₄ emissions for these processes.

Secondary pollutants, however, are produced by thermal oxidation, including NO_x and CO from the combustion of natural gas used to heat the process stream. Thermal oxidation technologies also may employ some form of heat recovery, either recuperative or regenerative, to reduce economic, environmental and energy costs. In the case of a combustion turbine, it is expected that approximately 20 lb/hr of CH₄ will be produced at full load (with an exhaust flow rate of approximately 1,000,000 million standard cubic feet per minute). The exhaust gas stream is thus both high volume and very dilute in CH₄, so it would need to be concentrated to the point that the CH₄ would be capable of combustion. Also, additional CO₂ would be produced due to the need for combusting natural gas to heat the CH₄ to the oxidation point. This would reduce the overall effectiveness in reducing CO₂e emissions due to CH₄ because additional CO₂ would be produced as a result of combusting the CH₄. Therefore, thermal oxidation is technically infeasible for the control of GHG emissions from the proposed combined-cycle combustion turbine.

5.6.2.4 Carbon Capture and Sequestration

Carbon capture and sequestration is a general term which is used for approaches that capture and separate CO₂ from an exhaust stream, and then store it in a place which will keep it from the atmosphere for a long time. The two general categories of CO₂ capture are: pre-combustion CO₂ capture and post-combustion CO₂ capture.

5.6.2.4.1 Pre-Combustion CO₂ Capture

Pre-combustion CO₂ capture is used in gasification plants, where the CO₂ is captured from the syngas prior to combustion in the turbine, where it is relatively concentrated in the gas stream. This facility is not

a gasification plant; therefore, pre-combustion capture is technically infeasible for the control of CO₂ emissions from the proposed combined-cycle combustion turbine.

5.6.2.4.2 Post-Combustion CO₂ Capture

Post-combustion CO₂ capture is used for units such as pulverized coal plants. In these units, the flue gas concentration of CO₂ runs between 10-15 percent by volume and is released at atmospheric pressure. This results in a high actual volume of gas to be treated. Trace impurities in the airflow tend to reduce the effectiveness of the CO₂-adsorbing process and compressing the captured CO₂ from atmospheric pressure to pipeline pressure represents a large parasitic load. The currently available process is costly and energy intensive, so research is being done on ways to increase the solvent capture efficiency and reduce the cost. These approaches include investigating the use of alternative solvents, solid sorbents or membranes. Of these potentially more efficient approaches, most are currently at laboratory/bench scale, so are not technically feasible. Pilot scale processes are starting to be placed in service, such as a 48 MW slipstream project at Brindisi, Italy, started in March 2011, which is limited to capturing less than 10,000 tons of CO₂ per year. A larger 235-MW slipstream project for the 1,300 MW Mountaineer Power Plant near New Haven, West Virginia was built with technology that used chilled ammonia to trap CO₂. The pilot project removed up to 300,000 metric tons of CO₂; however, the project was abandoned due to diminishing Federal and State support for clean coal technology. No commercially available post-combustion CO₂ capture systems are known to have been installed at large power plant other than pilot-scale demonstration projects. Therefore, post-combustion capture is technically infeasible for the control of CO₂ emissions from the proposed combined-cycle combustion turbine.

5.6.2.5 CO₂ Sequestration

CO₂ sequestration involves transporting CO₂ to a suitable geologic location where it can be injected as a supercritical fluid into deep, underground rock formations for permanent storage. Identifying a suitable site within an economically-viable distance from the Project site will require site-specific quantitative risk assessment. Four trapping methods are known: mineral trapping, physical adsorption, hydrodynamic trapping, and solubility trapping.

5.6.2.5.1 Mineral Trapping

The mineral trapping method traps CO₂ by undergoing a chemical reaction with various minerals, resulting in the formation of a carbonate mineral. This process can be rapid or very slow, depending on the chemistry of the rock and water at the site. Mineral trapping is expected to result in the most stable, permanent form of geological CO₂ sequestration. Experiments have shown that basalt formations can rapidly transform injected CO₂ into carbonate minerals, beginning precipitation in a few months' time and

completing conversion within 100 years or less, depending on depth of injection. Sandstone formations low in carbonates may also be suitable candidates, depending on the mineral contents of the formations. These methods have been demonstrated only on a laboratory scale; therefore, mineral trapping is **not** technically feasible for the proposed combined-cycle combustion turbine.

5.6.2.5.2 Physical Adsorption

The physical adsorption process traps CO₂ molecules are trapped in micropore wall surfaces of coal organic matter or organic rich shales. The hydrostatic pressure in the formation controls the adsorption process. The injection of CO₂ can also result in driving off CH₄ for collection by other wells, helping the economics. Wisconsin has coal beds in the mid-northeast part of the state (Northeast Wisconsin Shelf and Arkoma Basin). There is a commercial coal belt that contains coal beds greater than or equal to 10 inches thick. The coal beds that are greater than or equal to 14 inches thick are mineable by underground methods. Coal mining in Wisconsin has been steadily decreasing since 1981. Some coal beds in the US are being tested for CO₂ storage/ CH₄ recovery, but this is currently at a pilot phase. Defining the depths and lateral distribution of coal strata that might be suitable for this approach has not been done, due to the significant depths required for CO₂ sequestration. Significant research and exploration efforts would be required to determine whether such coal beds even actually occur at the required depths beneath western Wisconsin. Use of coal beds in Wisconsin would require much further study to locate a suitable site for sequestration, and since the results of pilot phase testing of this technique are not known, these factors combined render the use of coal beds **not technically feasible for the proposed combined-cycle combustion turbine**.

5.6.2.5.3 Hydrodynamic Trapping

With hydrodynamic trapping, the pore space of a salt-water aquifer takes the injected CO₂, in a geologic setting where the aquifer is capped by an impermeable rock layer to trap the CO₂ well below the near-surface environment. For storage purposes, the aquifer should be saline enough to be non-potable, and deep enough (over 2,700 feet) to confirm that the pressure is sufficient to keep the compressed CO₂ in a supercritical liquid phase. Since the sedimentary bedrock strata in the site vicinity are over 10,000 feet thick, the possibility exists that geologically suitable strata exist somewhere within these layered rock formations. However, in the absence of oil and gas exploratory test holes, the locations, depths, and character of such strata are not known, and would have to be discovered and defined by extensive exploratory drilling and testing. As the state of Wisconsin is unlikely to apply for primacy for the Class VI regulations (governing injection wells), EPA rules that require a minimum of 10,000 milligrams per liter (mg/L) total dissolved solids to qualify as saline enough to be suitable for injection will probably apply. Discovering locations which exceed 10,000 mg/L would require significant exploration and test

wells to characterize the site and determine the aquifer suitability. At these depths, defining suitable geologic would be rendered costly and problematic. Multiple oil and gas fields exist in the region, but a serious limitation to feasibility in an existing oil or gas field is the great likelihood of significant numbers of "penetrations" (old, either documented or undocumented wells and test holes that may or may not be adequately plugged and abandoned). Also, the additional surface infrastructure that would be needed to inject CO₂ would be massive, problematic, and likely infeasible. Pilot-scale projects injecting CO₂ into saline aquifers are underway in Illinois and Texas at depths of over 6,000 feet and these are the closest known sites that have been initially characterized for potential long-term sequestration, but the studies are in their early stages. Therefore, hydrodynamic trapping is **technically infeasible for the control of CO₂ emissions from the proposed combined-cycle combustion turbine** at this time.

5.6.2.5.4 Solubility Trapping

With solubility trapping, the CO₂ dissolves in the water or forms carbonic acid, becoming slightly heavier and, theoretically, sinking to the bottom of the aquifer. Solubility trapping also occurs during CO₂ flooding for enhanced oil recovery (EOR). In this case, the CO₂ dissolves into the oil, and is trapped by the immobile, non-recoverable oil. CO₂ flooding has been used for years for EOR, resulting in some existing injection infrastructure at oil fields (using both solubility trapping and hydrodynamic trapping), although the sequestration effects were not originally monitored, and the volumes injected for such operations are minuscule. However, oil fields have stored crude oil and natural gas for millions of years, and the geologic conditions that trap oil and gas are also the conditions suitable for CO2 storage. If the CO₂ is used for EOR, the cost of transporting it to the oil field may be partially offset. Since the sedimentary bedrock strata in the site vicinity are over 10,000 feet thick, the possibility exists that oil and gas fields involving geologically suitable strata exist somewhere within these layered rock formations within the region. However, defining suitable geologic conditions in an existing oil or gas field, including the locations, depths, and character of such strata would have to be defined by extensive exploratory drilling and testing. Multiple oil and gas fields exist in the region, however, as was the case with hydrodynamic trapping, there is a likelihood of undocumented penetrations. Also, additional surface infrastructure that would be needed to inject CO₂ would be massive, problematic, and likely infeasible. Therefore, solubility trapping is technically infeasible for the control of CO₂ emissions from the proposed combined-cycle combustion turbine at this time.

5.6.2.5.5 Summary of CO₂ Sequestration

To summarize, existing CO₂ capture technologies have not been applied at large power plants, as the economic costs are prohibitive, and while more efficient approaches are being investigated, none have currently been developed past the pilot-stage. A published cost estimate for a 235-MW slipstream pilot

project in West Virginia is \$668 million, so scaling that linearly to a size capable of handling the approximate 625-net MW capacity of this project would be over \$1.8 billion. Potential carbon sequestration sites may exist in Wisconsin, but the technologies to use them are mostly still in the pilotscale phase of development, and the Owners would need to do much more investigation in order to discover where the sites are, if any, and characterize them enough to demonstrate the long-term viability of the locations. Defining suitable geologic conditions in an existing oil or gas field, including the locations, depths, and character of suitable strata, and defining penetrations (potentially leaky wells and test holes, some of which are likely to exist but are undocumented) into the geological traps comprising existing oil and gas fields, would have to be defined by extensive exploratory drilling and testing. One of the closest known existing sites for sequestration is the Williston Basin in the Dakotas, approximately 350 miles from the plant. The cost to construct a pipeline as determined from a similar project (Iowa Power & Light Ottumwa – Iowa Department of Natural Resources project 11-219) to this project's site would be approximately \$1.4 million/mile of pipeline, or about \$700 million. The capital cost estimated for this comparable project was nearly \$2.1 billion for capture equipment and pipeline construction alone prior to any costs for gas compression, additional injection and monitoring wells necessary to handle the volume of CO₂ produced, pipeline right-of-way, operation and maintenance costs, etc. As can be seen from the above discussion, the qualitative cost estimate of capture and sequestration is quite high, the technological effectiveness for the capture equipment for a unit of this size has not been demonstrated in practice yet, and there is uncertainty as to whether locations capable of storing the large amounts of CO₂ that would be produced per year exist within a closer radius of the plant. These considerations are sufficient to eliminate this option without requiring a more detailed site-specific technological or economic analysis.

5.6.2.6 Summary of Technically Feasible Control Technologies

The technical feasibility of the greenhouse gas control options for the proposed combustion turbine is summarized in Table 5-19. The expected performance has been determined considering the performance of existing systems, vendor guarantees, permitted emission limits, and the design requirements for the turbine.

Table 5-19: Summary of Technically Feasible Greenhouse Gas Control Technologies for Combustion Turbine

| Control System | | Technical Feasibility | Comments |
|--------------------|---|--------------------------|--|
| Fuel Selection | Low Carbon Fuels | Feasible | Natural gas has been selected as the primary fuel for this project |
| | Combustion of Biogenic Sources | Not Feasible | |
| Energy | Continuous Excess Air Monitoring and Control | Feasible | Standard for the turbines under consideration |
| Efficiency | Efficient Turbine Design | Feasible | Standard for the turbines under consideration |
| Post Combustion | Catalytic Oxidation | Feasible | Will reduce CH ₄ emissions but create CO ₂ |
| Controls | Thermal Oxidation | Not Feasible | |
| Carbon | Pre-combustion CO ₂ capture | Not Feasible | |
| Capture | Post-combustion CO ₂ capture | Not Feasible | |
| | Mineral Trapping | Not Feasible | |
| Carbon | Physical Adsorption | Not Feasible | |
| Sequestration | Hydrodynamic Trapping | Not Feasible | |
| | Solubility Trapping | Not Feasible | |

5.6.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible control technologies are low-carbon fuel (natural gas), monitoring and control of excess air, efficient turbine design, and catalytic oxidation. The use of low-carbon fuels and aggressive energy-efficient design to reduce CO₂ emissions is inherent in the design of the proposed combustion turbine under consideration and is considered the baseline condition. Table 5-20 presents the ranking of the greenhouse gas technologies deemed feasible for the Project. While these four technologies are "ranked" in order of their presentation, they are more appropriately considered as a suite of measures that would be implemented to allow the Project to generate and consume power in the most efficient manner and thereby achieve BACT for greenhouse gases.

Table 5-20: Greenhouse Gas Control Technology Ranking for the Combustion Turbine

| Technology | Ranking | Applied to Project |
|--|---------|--------------------|
| Combined – Cycle Combustion Turbine (employing efficient, state-of-the-art design) | 1 | Yes |
| Clean Fuel – Natural Gas | 2 | Yes |
| Catalytic Oxidation | 3 | Yes |
| Operational Design – Control of Excess Air | 4 | Yes |

5.6.4 Step 4. Evaluate the Most Effective Control Technologies

The next step is to review each of the technically feasible control options for environmental, energy, and economic impacts.

5.6.4.1 Environmental, Energy, and Economic Feasibility of Control Options

Because the Owners are proposing to utilize all four of the feasible technologies for reducing greenhouse gases from the proposed combustion turbine, no detailed analysis is provided to compare the available control technologies' relative environmental, energy and economic impacts.

5.6.4.2 Oxidation Catalyst

An oxidation catalyst works to reduce CH₄ emissions according the following equation:

$$CH_4 + 2O_2 = CO_2 + 2H_2O$$

Substituting in the molecular weights of CH₄ (16.043 pound per pound mol [lb/lb-mol]) and CO₂ (44.0096 lb/lb-mol), the removal of 1 pound of CH₄ results in the release of 2.7 pounds of CO₂. However, CH₄ has a GWP of 25, whereas the GWP of CO₂ is 1. Substituting in the GWPs, the removal of 1 pound of CH₄ results in a net reduction of 22.3 lb CO₂ as CO₂e.

It is also important to note the increase in CO₂e emissions from the oxidation of CO to CO₂ in accordance with the following reaction:

$$2CO + O_2 = 2CO_2$$

CO₂ will be emitted at a rate of approximately 1.5 pounds per pound of CO. Therefore, it is expected that there will still be a net decrease in CO₂e, even with the additional CO₂ that is produced from the oxidation catalyst with the oxidation of CO and CH₄.

There are no additional negative environmental impacts from the use of an oxidation catalyst, other than those mentioned in Step 4 of the combustion turbine CO BACT.

5.6.5 Step 5. Proposed Greenhouse Gas BACT Determination

BACT for greenhouse gas emissions from the combustion turbine is determined to be the use of natural gas as a fuel, monitoring and control of excess air, efficient turbine design, and an oxidation catalyst. These design options will allow the combustion turbine to not exceed 850 lb CO₂/MW-hr (gross) on a 12-month rolling average basis while combusting natural gas and 1,180 lb CO₂/MW-hr (gross) on 12-month rolling average basis while combusting fuel oil.

5.7 BACT for Start-Up and Shutdown Emissions – Combined-Cycle Combustion Turbine (P01)

Previously submitted BACT Sections and updated references to the BACT analysis sections for the start-up and shutdown emissions for the combined-cycle combustion turbine are presented in Table 5-21. The updated combined cycle combustion turbine start-up and shutdown BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

Table 5-21: Combustion Turbine Start-Up and Shutdown BACT Analysis References

| Description | Previous Application Reference | December 2021 Submittal Location |
|----------------------------|---|---|
| BACT Analysis Steps 1 to 5 | 5.0 BACT December 2018 Submittal | 5.0 BACT |
| DDI C | Table D-1c (startup/shutdown) Appendix D, December 2018 Submittal | Table D-1c (startup/shutdown) Appendix D |
| RBLC | | Table D-1c Addendum (startup/shutdown) Appendix D |

The following sections outline the top-down BACT steps for start-up and shutdown emissions from the combustion turbine.

5.7.1 Step 1. Identify Potential Control Strategies

Criteria pollutants will be emitted during start-up and shutdown of the combustion turbine. Start-up emissions are generally higher for CO, NO_x, and VOC than for normal operation because the SCR and oxidation catalyst cannot fully operate to their full potentials until the exhaust gases reaches the appropriate operating temperature.

The Owners are requesting an hours per year limit on start-up and shutdown (1,525 hours per year for start-up and shutdown, combined) for natural gas operation and 42 start-ups and 42 shutdowns per year for fuel oil operation. Start-up is defined as 0 percent load to MECL and shutdown is defined as MECL to 0 percent load.

5.7.2 Step 2. Identify Technically Feasible Control Technologies

Controls that may be used during normal operation are not available to control start-up and shutdown emissions. SCR and oxidation catalysts require a minimum operating temperature to control emissions (for the catalytic reactions to occur for removal of NO_x and CO). This temperature is not reached until approximately 600 to 650°F. Although this temperature is reached in the HRSG before MECL, the CO and NO_x curves show that these emissions are unstable until around MECL. In addition, the manufacturer will only guarantee emissions down to MECL, indicating that this is where stability in these emissions is reached. To minimize emissions, however, start-up and shutdown shall be limited to 2 hours for start-up and 30 minutes for shutdown.

Therefore, no technically feasible control technologies for start-up and shutdown emissions from the combustion turbine have been identified.

5.7.3 Step 3. Rank the Technically Feasible Control Technologies

Since no technically feasible control technologies for start-up and shutdown emissions have been identified, ranking of such control technologies is not applicable.

5.7.4 Step 4. Evaluate the Most Effective Control Technologies

Since no technically feasible control options for start-up and shutdown emissions have been identified, evaluation of environmental, energy or economic impacts of such control technologies is not applicable.

5.7.5 Step 5. Proposed Start-up and Shutdown BACT Determination

BACT will include limiting combined-cycle operation to 1,525 hours per year for start-up and shutdown, combined, for natural gas operation and 42 start-ups and 42 shutdowns per year for fuel oil operation. Table 5-22 and Table 5-23 displays the BACT emission rates for start-up and shutdown emissions for the combustion turbine for natural gas and fuel oil operation, respectively.

Table 5-22: Combined-Cycle Combustion Turbine Natural Gas Start-up and Shutdown Emissions

| Pollutant | Start-up Emissions | | Shutdown Emissions | Start-up and Shutdown Emissions ^a | |
|-------------------------------------|--------------------|------------------|-----------------------|--|---------------|
| | lb/cold start | lb/warm start | lb/hot-fast start | lb/shutdown | tons per year |
| NO_x | 335.0 | 233.0 | 111.0 | 59.0 | 108.3 |
| СО | 11,066 | 6,495 | 779.0 | 463.0 | 1,369 |
| $PM/PM_{10}/PM_{2.5}$ | 43.6 | 29.1 | 16.3 | 10.9 | 16.6 |
| VOC | 950.0 | 558.0 | 67.0 | 40.0 | 117.8 |
| H ₂ SO ₄ mist | 15.6 | 10.4 | 5.9 | 3.9 | 6.0 |
| CO ₂ e | 939,573 | 626,382 | 352,340 | 234,893 | 358,212 |

⁽a) Emissions are based on 1,525 hours per year for start-up and shutdown, combined, for natural gas operation.

Table 5-23: Combined-Cycle Combustion Turbine Fuel Oil Start-up and Shutdown Emissions

| Pollutant | Start-up Emissions | Shutdown Emissions | Start-up and Shutdown Emissions ^a |
|-------------------------------------|-----------------------|-----------------------|--|
| | lb/start | lb/shutdown | tons per year |
| NO_x | 860.0 | 108.0 | 20.3 |
| CO | 25,846 | 1,227 | 568.5 |
| $PM/PM_{10}/PM_{2.5}$ | 78.9 | 19.7 | 2.1 |
| VOC | 2,951 | 122.0 | 64.5 |
| H ₂ SO ₄ mist | 14.0 | 3.5 | 0.4 |
| CO ₂ e | 1,639,929 | 409,982 | 43,048 |

⁽a) Emissions are based on 42 start-ups and 42 shutdowns per year.

5.8 BACT for Opacity - Combined-Cycle Combustion Turbine (P01)

Previously submitted BACT Sections and updated references to the opacity BACT analysis sections for the combined cycle combustion turbine are presented in Table 5-24. The updated combined cycle combustion turbine opacity BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

December 2021 Description **Previous Application Reference Submittal Location 5.0 BACT** BACT Analysis Steps 1 to 5 **5.0 BACT** December 2018 Submittal Table D-1a (natural gas), Table D-1a (natural gas), Table D-1b (fuel oil) Table D-1b (fuel oil) Appendix D, December 2018 Submittal Appendix D **RBLC** Table D-1a Addendum (natural gas) Table D-1b Addendum (fuel oil) Appendix D

Table 5-24: Combustion Turbine Opacity BACT Analysis References

The following sections outline the top-down BACT steps for opacity emissions from the combustion turbine.

5.8.1 Step 1. Identify Potential Control Strategies

Opacity is not a discrete pollutant and cannot be measured using mass emissions rate criteria (e.g., lb/hr). Therefore, a typical top-down BACT economic analysis that evaluated effectiveness on a \$/ton basis cannot be conducted on opacity. Rather, the opacity BACT determination should focus on pollutants in the flue gas that contribute to opacity. These pollutants include PM, NO_x, SO₂, and H₂SO₄. BACT determinations have been performed for PM, NO_x, and H₂SO₄ for this combined-cycle combustion turbine. Units firing fuels with low ash content and high combustion efficiency exhibit correspondingly low exhaust opacity.

5.8.2 Step 2. Identify Technically Feasible Control Technologies

The Owners have prepared a detailed BACT evaluation for pollutants that potentially contribute to opacity. Based on these BACT evaluations, the Owners have identified the following control technologies as technically feasible: SCR and combustion control for NO_x control; low ash fuel and combustion control for PM control; and low sulfur and good combustion practices for H₂SO₄ mist. These technologies represent BACT for the criteria pollutants and will also minimize opacity.

5.8.3 Step 3. Rank the Technically Feasible Control Technologies

Based on these BACT evaluations, the Owners have ranked the following feasible control technologies for opacity: (1) combustion control, (2) clean fuels. The Owners have determined that the use of low ash fuel and combustion control combine to rank as the top option for opacity control.

5.8.4 Step 4. Evaluate the Most Effective Control Technologies

The energy, environmental, and economic impacts of the feasible control technologies are described in their respective BACT analysis.

5.8.5 Step 5. Proposed Opacity BACT Determination

BACT for exhaust opacity will include the use of combustion control for NO_x control, the use of low ash fuel and combustion control for PM control and the use of low sulfur fuel for H_2SO_4 mist control. The combination of these control technologies represents BACT for opacity.

5.9 BACT for Auxiliary Boiler (B02)

Previously submitted BACT Sections and updated references to the BACT analysis sections for the auxiliary boiler are presented in Table 5-25. Further analysis of the oxidation catalyst performed by the WDNR determined that an oxidation catalyst is economically feasible; therefore, the application text has been updated to reflect this update. The updated auxiliary boiler BACT analysis shows that the BACT determination in the PSD permit remain valid.

| Description | Previous Application Reference | December 2021 Submittal Location |
|----------------------------|--|--|
| BACT Analysis Steps 1 to 5 | 5.0 BACT December 2018 Submittal | 5.0 BACT |
| | Post application NTEC Response #3 | Incorporated throughout Sections 5.9.2 and 5.9.4 |
| DDI G | Table D-2, Appendix D December 2018 Submittal | Table D-2, Appendix D |
| RBLC | | Table D-2 Addendum, Appendix D |
| Economic Tables | Tables E-1a, E-1b, E-2a, E-2b, E-3a, and E-3b, Appendix E, December 2018 Submittal | Appendix E |

Table 5-25: Auxiliary Boiler BACT Analysis References

The auxiliary boiler is rated at 100 MMBtu/hr and is proposed to operate 8,760 hours per year. The RBLC has limited information on BACT conclusions for the auxiliary boiler (Appendix D). The RBLC tables also show high variability for emission rates for each pollutant. For all pollutants, no add-on controls were listed because auxiliary boilers are so small.

5.9.1 BACT for Nitrogen Oxides - Auxiliary Boiler

The following sections outline the top-down steps for NO_x emissions from the auxiliary boiler.

5.9.1.1 Step 1. Identify Potential Control Strategies

SCR, low-NO_x burners, combustion controls, and FGR are listed as BACT in the RBLC for auxiliary boilers. NO_x emissions listed in the RBLC range from 0.0085 to 0.36 lb/MMBtu for similar-sized auxiliary boilers utilizing low-NO_x burners and combustion controls. The RBLC listings for units with SCR range from 0.0032 to 0.015 lb/MMBtu.

5.9.1.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling NO_x emissions are evaluated for technical feasibility in the following sections.

5.9.1.2.1 SCR

The RBLC listed one unit with SCR as BACT for a similarly sized auxiliary boiler (approximately 100 MMBtu/hr). An SCR vendor said that they could provide an SCR for this size boiler. The vendor's removal efficiency for this size unit is 90 percent control of NO_x.

As a result, an SCR system is technically feasible for the auxiliary boiler.

5.9.1.2.2 Low-NO_x Burners

Low-NO_x burners are currently available from most auxiliary boiler manufacturers. This technology seeks to reduce combustion temperatures, thereby reducing NO_x. In a conventional combustor, the air and fuel are introduced at an approximately stoichiometric ratio, and air/fuel mixing occurs at the flame front where diffusion of fuel and air reaches the combustible limit. A lean premixed combustor design premixes the fuel and air prior to combustion. Premixing results in a homogenous air/fuel mixture, which minimizes localized fuel-rich pockets that produce elevated combustion temperatures and higher NO_x emissions. A lean air-to-fuel ratio approaching the lean flammability limit is maintained, and the excess air serves as a heat sink to lower combustion temperatures, which lowers NO_x formation. A pilot flame is used to maintain combustion stability in this fuel-lean environment.

Low- NO_x burners are available on auxiliary boilers and are considered both baseline and technically feasible for the auxiliary boiler.

5.9.1.2.3 Ultra-Low NO_x Burners

Ultra-low NO_x burners are available for purchase on most auxiliary boilers of this size. The ultra-low NO_x burners provide additional control of NO_x emissions through the burning process.

Ultra-low NO_x burners are available on auxiliary boilers and is technically feasible for the auxiliary boiler.

5.9.1.2.4 Combustion Control

"Good combustion practices" include operational and design elements to control the amount and distribution of excess air in the flue gas to confirm that there is enough oxygen present for complete combustion. FGR is included as combustion control for this auxiliary boiler.

As a result, combustion control is considered baseline for the auxiliary boiler and is technically feasible.

5.9.1.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible NO_x control technologies for the 100 MMBtu/hr auxiliary boiler are ranked by control effectiveness in Table 5-26.

Table 5-26. Ranking of NO_x Control Technologies for the Auxiliary Boiler

| Control Technology | Reduction (%) | Controlled Emission Level (lb/MMBtu) |
|--|---------------------------|--------------------------------------|
| SCR | 90 | 0.0036 |
| Ultra-low NO _x burners | 50 | 0.011 |
| Low-NO _x burners, FGR, and combustion control | Not applicable (baseline) | 0.036 |

Source: Based on vendor data

5.9.1.4 Step 4. Evaluate the Most Effective Control Technologies

Each technically feasible control technology was evaluated for energy, environmental, and economic impacts. These impacts are discussed below for each control technology.

5.9.1.4.1 SCR

Energy and Environmental Impacts

Energy and environmental impacts for an SCR system are discussed in Section 5.1.4.1.

Economic Impacts

The capital costs and annualized costs associated with an SCR system for the auxiliary boiler are shown in Appendix E. The total capital investment of installing an SCR system on the auxiliary boiler is approximately \$659,550. On an annual basis, the SCR system would cost almost \$228,620 which results

in a cost per ton of NO_x removed of approximately \$15,264 while removing only 14.2 tons of NO_x per year. Therefore, this cost is considered not economically feasible for the auxiliary boiler.

An SCR is not considered economically feasible and is not proposed as BACT for the auxiliary boiler.

5.9.1.4.2 Ultra-Low-NO_x Burners

Energy and Environmental Impacts

Ultra-low-NO_x burners may decrease efficiency slightly on the auxiliary boiler, however these impacts are not significant.

Economic Impacts

The capital costs and annualized costs associated with installing ultra-low-NO_x burners on the auxiliary boiler are shown in Appendix E. The total capital investment of installing ultra-low-NO_x burners on the auxiliary boiler is approximately \$150,765. On an annual basis, the ultra-low-NO_x burners would cost \$66,868 which results in a cost per ton of NO_x removed of approximately \$5,895 while removing 11.3 tons of NO_x per year. The cost to install ultra-low-NO_x burners is considered economically feasible by the Owners and is therefore considered BACT for the auxiliary boiler.

5.9.1.5 Low-NO_x Burners, FGR, and Combustion Control

Because the low- NO_x burners come standard on most auxiliary boilers and combustion control is accomplished through operation of the auxiliary boiler, there are no incremental energy, environmental, or economic impacts associated with these controls.

5.9.1.6 Steps 5. Proposed BACT for NO_x

Since ultra-low NO_x burners, FGR, and combustion control are considered economically feasible, and SCR is not economically feasible, ultra-low NO_x burners and FGR was selected as BACT for NO_x from the auxiliary boiler at an emission rate of 0.011 lb/MMBtu.

5.9.2 BACT for Carbon Monoxide - Auxiliary Boiler

The following sections outline the top-down steps for CO emissions from the auxiliary boiler.

5.9.2.1 Step 1. Identify Potential Control Strategies

The RBLC does not list add-on controls in the BACT determinations for control of CO emissions from auxiliary boiler. As with the turbine, good combustion control will help control emissions of CO from the auxiliary boiler. An oxidation catalyst system may be available to control CO emissions from the

auxiliary boiler, with one instance of an oxidation catalyst selected as BACT as listed in the RBLC database. Emission limits range from 0.0075 lb/MMBtu to 0.0842 lb/MMBtu.

5.9.2.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling CO emissions are evaluated for technical feasibility in the following sections.

5.9.2.2.1 Oxidation Catalyst System

One control vendor has indicated that an oxidation catalyst system may be used on an auxiliary boiler this size. The oxidation catalyst system is an add-on control that converts CO and VOC to CO₂ by use of a catalyst. Section 5.2.2.2 describes the oxidation catalyst system for gas-fired units. Due to the size of the auxiliary boiler, the exhaust gases do not need to be heated before going to the catalyst.

An oxidation catalyst system is considered technically feasible for the auxiliary boiler; one vendor has provided a quote for this system.

5.9.2.2.2 Combustion Control

"Good combustion practices" include operational and design elements to control the amount and distribution of excess air in the flue gas to confirm that there is enough oxygen present for complete combustion.

Good combustion practices are a technically feasible method of controlling CO emissions from the auxiliary boiler.

5.9.2.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible CO control technologies for the 100 MMBtu/hr auxiliary boiler are ranked by control effectiveness in Table 5-27.

Table 5-27: Ranking of CO Control Technologies for the Auxiliary Boiler

| Control Technology | Reduction (%) | Controlled Emission Level (lb/MMBtu) |
|--------------------|---------------------------|--------------------------------------|
| Oxidation catalyst | 90° | 0.0037 |
| Combustion control | Not applicable (baseline) | 0.037 |

Source: Based on AP-42

⁽a) Control efficiencies were obtained from a vendor based on preliminary design and is consistent with other project oxidation catalyst control efficiencies. See Appendix F for vendor information.

5.9.2.4 Step 4. Evaluate the Most Effective Control Technologies

Technically feasible control technology was evaluated for energy, environmental, and economic impacts.

5.9.2.4.1 Oxidation Catalyst

Energy and Environmental Impacts

Energy and environmental impacts of an oxidation catalyst are discussed in Section 5.2.4.1.

Economic Impacts

The control cost analysis for an oxidation catalyst system for the auxiliary boiler is displayed Appendix E. An oxidation catalyst system for this size unit would require a total capital investment of \$147,225. The annual costs of operating this oxidation catalyst system would be \$80,801. On an annual basis, only 14.6 tons per year of CO along with 1.2 tons per year of VOC would be removed at a cost of \$5,125 per ton of pollutants removed, based on unlimited operation (8,760 hours per year).

The cost is considered economically feasible for an oxidation catalyst system; therefore, an oxidation catalyst for control of CO emissions from the auxiliary boiler is considered as BACT.

5.9.2.5 Step 5. Proposed BACT for CO

Since add-on controls are economically feasible for CO, an oxidation catalyst and combustion control was selected as BACT for CO from the auxiliary boiler at an emission rate of 0.0037 lb/MMBtu.

BACT for CO emissions from the auxiliary boiler is an oxidation catalyst and good combustion practices.

5.9.3 BACT for Particulate Matter - Auxiliary Boiler

The following sections outline the top-down steps for PM/PM₁₀/PM_{2.5} emissions from the auxiliary boiler.

5.9.3.1 Step 1. Identify Potential Control Strategies

The RBLC does not list any control strategies other than good combustion practices and low ash fuel (natural gas). No add-on controls were identified for significant removal of these pollutants from the auxiliary boiler exhaust. The RBLC lists emission rates of 0.005 lb/MMBtu for similar sized auxiliary boilers (approximately 100 MMBtu/hr) up to 0.020 lb/MMBtu.

5.9.3.2 Step 2. Identify Technically Feasible Control Technologies

The only technically feasible control option is combustion control for PM/PM₁₀/PM_{2.5}.

5.9.3.3 Step 3. Rank the Technically Feasible Control Technologies

The only technically feasible control option is combustion control for PM/PM₁₀/PM_{2.5}.

5.9.3.4 Steps 4 and 5. Evaluate the Most Effective Control Technologies and Proposed BACT for PM/PM₁₀/PM_{2.5}

Since add-on controls are not feasible on such a small gas-fired unit, combustion control was selected as BACT for PM/PM₁₀/PM_{2.5} from the auxiliary boiler at an emission rate of 0.01 lb/MMBtu.

5.9.4 BACT for Volatile Organic Compounds - Auxiliary Boiler

The following sections outline the top-down steps for VOC emissions from the auxiliary boiler.

5.9.4.1 Step 1. Identify Potential Control Strategies

The RBLC does not list add-on controls in the BACT determinations for control of VOC emissions from auxiliary boiler. As with the turbine, good combustion control will help control emissions of VOC from the auxiliary boiler. An oxidation catalyst system may be available to control VOC and CO emissions from the auxiliary boiler, with two VOC entries listed as BACT for VOC emissions. Emission rates vary from the various sized auxiliary boiler, but at 100 MMBtu/hr approximate size, the lowest emission limit is 0.005 lb/MMBtu, with good combustion practices.

5.9.4.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling VOC emissions are evaluated for technical feasibility in the following sections.

5.9.4.2.1 Oxidation Catalyst System

One control vendor has indicated that an oxidation catalyst system may be used on an auxiliary boiler this size. The oxidation catalyst system is an add-on control that converts CO and VOC to CO₂ by use of a catalyst. Section 5.4.2.2 describes the oxidation catalyst system for gas-fired units. Due to the size of the auxiliary boiler, the exhaust gases do not need to be heated before going to the catalyst.

An oxidation catalyst system is considered technically feasible for the auxiliary boiler; one vendor has provided a quote for this system.

5.9.4.2.2 Combustion Control

"Good combustion practices" include operational and design elements to control the amount and distribution of excess air in the flue gas to confirm that there is enough oxygen present for complete combustion.

Good combustion practices are a technically feasible method of controlling VOC emissions from the proposed auxiliary boiler.

5.9.4.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible VOC control technologies for the 100 MMBtu/hr auxiliary boiler are ranked by control effectiveness in Table 5-28.

Table 5-28: Ranking of VOC Control Technologies for the Auxiliary Boiler

| Control Technology | Reduction (%) | Controlled Emission Level (lb/MMBtu) |
|--------------------|---------------------------|--------------------------------------|
| Oxidation catalyst | 50 ^a | 0.0027 |
| Combustion control | Not applicable (baseline) | 0.005 |

Source: Based on AP-42

5.9.4.4 Step 4. Evaluate the Most Effective Control Technologies

Technically feasible control technology was evaluated for energy, environmental, and economic impacts.

5.9.4.4.1 Oxidation Catalyst

Energy and Environmental Impacts

Energy and environmental impacts of an oxidation catalyst are discussed in Section 5.4.4.1.

Economic Impacts

The control cost analysis for an oxidation catalyst system for the auxiliary boiler is displayed in Appendix E and are the same as those provided for the CO BACT analysis. An oxidation catalyst system for this size unit would require a total capital investment of \$147,225. The annual costs of operating this oxidation catalyst system would be \$80,801. On an annual basis, only 14.6 tons per year of CO along with 1.2 tons per year of VOC would be removed at a cost of almost \$5,125 per ton of pollutants removed, based on unlimited operation (8,760 hours per year).

The cost is considered economically feasible for an oxidation catalyst system; therefore, an oxidation catalyst for control of VOC emissions from the auxiliary boiler is considered as BACT.

5.9.4.5 Step 5. Proposed BACT for VOC

Since add-on controls are economically feasible for VOC, an oxidation catalyst and combustion control was selected as BACT for VOC from the auxiliary boiler at an emission rate of 0.0027 lb/MMBtu.

⁽a) Control efficiencies were obtained from a vendor based on preliminary design and is consistent with other project oxidation catalyst control efficiencies. See Appendix F for vendor information.

BACT for VOC emissions from the auxiliary boiler is an oxidation catalyst and good combustion practices.

5.9.5 BACT for Sulfuric Acid Mist – Auxiliary Boiler

The following sections outline the top-down steps for H₂SO₄ emissions from the auxiliary boiler.

5.9.5.1 Step 1-5 Identify, Rank and Select BACT

There are no add-on control technologies for controlling H₂SO₄ emissions from an auxiliary boiler. As with the combustion turbine, using low sulfur fuel and controlling combustion is the only technologically feasible control option.

BACT is use of lower sulfur fuel and good combustion practices. This will achieve an emission rate of 0.01 pounds per hour of H₂SO₄ from the auxiliary boiler.

5.9.6 BACT for Greenhouse Gases - Auxiliary Boiler (Steps 1-5)

The auxiliary boiler will be fired exclusively on natural gas, is rated at 100 MMBtu/hr, and will be permitted to be fired a total of 8,760 hours per year. GHG emissions from this unit are estimated to be on the order of 51,289 tons CO₂e per year. The basic GHG BACT reasoning presented for the turbine essentially applies to this boiler as well. The Owners propose that GHG BACT for this boiler will be the following:

- Use of clean fuels (exclusive use of natural gas)
- Requiring the Owners to maintain the unit according to the manufacturer's specifications, and to operate the unit in the most efficient manner possible, i.e. good combustion practices.
- Tune the unit every two years according to the manufacturer's specifications.
- Record the annual hours of operation and annual fuel use and report the GHG emissions annually. The GHG emissions from this unit may be included in the facility-wide annual GHG limit.

5.9.7 BACT for Opacity - Auxiliary Boiler

The following sections outline the top-down steps for opacity emissions from the auxiliary boiler.

5.9.7.1 Step 1. Identify Potential Control Strategies

Opacity is not a discrete pollutant and cannot be measured using mass emissions rate criteria (e.g., lb/hr). Therefore, a typical top-down BACT economic analysis that evaluated effectiveness on a \$/ton basis cannot be conducted on opacity. Rather, the opacity BACT determination should focus on pollutants in the flue gas that contribute to opacity. These pollutants include PM, NO_x, SO₂, and H₂SO₄. BACT

determinations have been done for PM, NO_x and H₂SO₄ for this auxiliary boiler. Units firing fuels with low ash content and high combustion efficiency exhibit correspondingly low exhaust opacity.

5.9.7.2 Step 2. Identify Technically Feasible Control Technologies

The Owners have prepared a detailed BACT evaluation for pollutants that potentially contribute to opacity. Based on these BACT evaluations, the Owners have identified the following control technologies as technically feasible: SCR and combustion control for NO_x control; and low ash, low sulfur fuel and combustion control for PM and H₂SO₄ control. These technologies represent BACT for the criteria pollutants and will also minimize opacity.

5.9.7.3 Step 3. Rank the Technically Feasible Control Technologies

Based on these BACT evaluations, the Owners have ranked the following feasible control technologies for opacity: (1) combustion control, (2) clean fuels. The Owners have determined that the use of low ash, low sulfur fuel and combustion control combine to rank as the top option for opacity control.

5.9.7.4 Step 4. Evaluate the Most Effective Control Technologies

The energy, environmental, and economic impacts of the feasible control technologies are described in their respective BACT analysis.

5.9.7.5 Step 5. Proposed Opacity BACT Determination

BACT for exhaust opacity will include the use of combustion control for NO_x control and the use of low ash, low sulfur fuel and combustion control for PM and H₂SO₄ control. The combination of these control technologies represents BACT for opacity for the auxiliary boiler.

5.10 BACT for Greenhouse Gases (GHG) – SF₆-Containing Circuit Breakers (F03)

Previously submitted BACT Sections, post application submittals, and updated references to the BACT analysis sections for the SF₆-containing circuit breakers are presented in Table 5-29. The updated circuit breaker BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

| Description | Previous Application Reference | December 2021 Submittal Location |
|----------------------------|-------------------------------------|-------------------------------------|
| BACT Analysis Steps 1 to 5 | 5.0 BACT December 2018 Submittal | 5.0 BACT |
| RBLC | Table 2-4 | Table D-7, |
| | December 2018 Submittal | Appendix D |
| | | Table D-7 Addendum, |
| | | Appendix D |
| Evaluation of leakage rate | September 1, 2020 | Appendix F - Additional |
| | letter submittal to WDNR | Information |

Table 5-29: SF6-Containing Circuit Breakers BACT Analysis References

SF₆ is a very potent GHG with a GWP of 22,800, which means that it is 22,800 times more potent as a GHG than CO₂. SF₆ is a gaseous dielectric used in circuit breakers. The Project is expected to have three 345-kV circuit breakers and two 19-kV circuit breakers that will all contain small amounts of SF₆. Leakage is expected to be minimal and is expected to occur only as a result of circuit interruption and at extremely low temperatures.

Emissions of SF₆ from the circuit breakers are shown in Appendix C. Annual potential to emit emissions of SF₆ from the circuit breakers were based on maximum leakage rate of 0.5 percent per year, the amount of SF₆ in each size of circuit breaker, and the GWP. Project potential emissions of CO₂e leakage from all proposed circuit breakers combined are estimated to be 120 tons per year.

The following sections outline the top-down steps for GHG emissions from the SF₆-circuit breakers.

5.10.1 Step 1 and Step 2. Identify Potential Control Strategies and Eliminate Technologically Infeasible Options

The first steps in a top-down BACT analysis are to determine the potential control strategies and then determine if the control strategy is technically feasible for the Project. There are no add-on control technologies for SF₆; only inherent controls are available. The following control strategies have been identified and considered in determining BACT for SF₆ emissions from circuit breakers:

1. Use state-of-the-art SF₆ technology with leak detection systems to limit fugitive emissions.

The use of state-of-the-art gas-filled circuit breakers using SF₆ with leak detection to limit fugitive emissions is the proposed control option. Modern circuit breakers are designed as a totally enclosed-pressure system with far lower potential for SF₆ emissions than older circuit breakers. The current International Electrotechnical Commission (IEC) standards are that new equipment be built to low leakage limits (less than 0.5 percent per year) (Blackman, et al., 2019).

The effectiveness of these leak-tight closed systems is further enhanced by equipping them with an alarm that provides a warning when SF₆ has leaked from the breaker. Therefore, this type of technology is available to limit emissions, is feasible for use, and is the baseline established for this BACT analysis.

2. Substitution of another, non-greenhouse-gas substance for SF₆ such as the use of a different dielectric oil or compressed air (air-blast) circuit breaker as the dielectric material in the breakers.

One alternative to SF₆ would be the use of a dielectric oil or compressed air (air-blast) circuit breakers, which historically were used in high-voltage installations prior to the development of SF₆ breakers. SF₆ has become the predominant insulator and arc quenching substance in circuit breakers today because of its superior capabilities over oil and air-blast circuit breakers. The main drawback to oil and air-blast breakers are that these types of breakers require significantly larger equipment to replicate the same insulating and arc-quenching capabilities of the SF₆ breakers and air-blast breakers can have significant noise impacts to nearby residences. This type of technology is not feasible for use here, however, because oil breakers are no longer available from vendors, other than as used equipment. According to vendors, air-blast breakers are available only for breakers below 69-kV currently, but were also not available for the very small 19-kV circuit breakers also proposed for this Project. Therefore, oil and air-blast breakers are not available control technology for circuit breakers proposed for the Project.

3. Use an emerging technology to replace SF₆ with a material that has similar dielectric and arc-quenching properties, but without the drawbacks of oil and air-blast breakers.

The availability of emerging technology alternatives to SF_6 was researched. According to the most recent report released by the EPA SF_6 Partnership, there is no clear alternative to SF_6 (EPA, 2015). Research and development efforts have been focused on finding substitutions for SF_6 that have comparable insulating and arc quenching properties in high-voltage applications (U.S. Climate Change Technology Program, 2003). Most studies have concluded "there is no replacement gas immediately available to use as an SF_6 substitute" for high-voltage applications (Siemens Industry, Inc., 2013). Therefore, the alternative to use an emerging technology to replace SF_6 is not an available control technology.

Table 5-30 displays the control options and feasibility for SF₆.

Table 5-30. Summary of Potential GHG Control Technologies

| GHG Technology | Evaluation Status |
|---|---------------------------|
| State-of-the-art SF ₆ technology with leak detection systems | Considered and applied |
| Oil/air-blast circuit breakers | Considered (Not Feasible) |
| Use of emerging technology to replace SF ₆ | Considered (Not Feasible) |

5.10.2 Step 3. Rank the Technically Feasible Control Technologies

Table 5-31 presents the ranked technically feasible control options.

Table 5-31. GHG Technology Rankings for Circuit Breaker Equipment Leaks

| Control Technology | Emission Rate (short tons CO₂e/year) | Emissions Reduction (short tons CO₂e/year) |
|---|---|---|
| State-of-the-art SF ₆ technology with leak detection systems | 120 | N/A |

5.10.3 Step 4. Evaluate the Most Effective Control Technologies

The next step is to review each of the technically feasible control options for environmental, energy, and economic impacts.

5.10.3.1 Environmental, Energy, and Economic Feasibility of Control Options

Purchasing leak detection systems for the circuit breakers will come with a cost: however, the costs are not considered not economically feasible for this Project.

Further information was provided to WDNR that confirms the circuit breakers selected are consistent with the best that is presently available and are 'state of the art' and addresses why a 0.1 percent leakage rate is not achievable. This additional information letter submitted to the WDNR on September 1, 2020 is included in Appendix F for reference.

5.10.4 Step 5. GHG BACT Emission Limitation

The proposed BACT for the circuit breakers consists of the following:

- State-of-the-art enclosed-pressure SF₆ circuit breakers with a guaranteed loss rate of 0.5 percent by weight or less by year; and
- Low-pressure detection system with alarm system

A review of the RBLC for circuit breakers containing SF₆ (most of them combined-cycle plants) have a similar or the same BACT determination. As shown in Appendix D, a leak detection rate of 0.5 percent from enclosed pressured design with leak detection alarms is BACT.

5.10.5 Compliance with GHG BACT for Circuit Breakers

Any SF₆ emissions from the circuit breakers will be fugitive emissions. Fugitive emissions are, by their nature, very difficult to monitor directly, as they are not emitted from a discrete emission point.

Therefore, the Owners propose the following compliance demonstrations, recordkeeping and monitoring requirements:

- 1. Follow manufacturer recommendations for maintenance and repair of the affected breakers, with recovery and recycling of SF₆ removed during maintenance procedures.
- 2. Install a low-pressure detection system with an alarm system on each SF₆ circuit breaker to measure pressure changes.
- 3. Create alarms based on the pressure readings in the breakers, so that leaks can be detected before a substantial portion of SF₆ is lost.
- 4. Upon a detectable pressure drop that is 10 percent of the original pressure (accounting for ambient air conditions), perform maintenance on a breaker to fix seals within 20 days of the detection of the pressure drop.
- 5. Keep a log of all detected leaks and maintenance procedures potentially affecting SF₆ emissions from circuit breakers that are part of this Project.
- 6. For a period of at least 5 years, track and maintain records of annual SF₆ leakage amounts due to breakers that are part of this Project. The leakage amounts will be assumed equal to the inventory of SF₆ replaced in the breakers each calendar year.

These proposed work practices are consistent with the BACT determinations identified above.

5.11 BACT for Natural Gas Heaters (P04 and P05)

Previously submitted BACT Sections, post-application submittals, and updated references to the BACT analysis sections for the natural gas heaters are presented in Table 5-32. The updated natural gas heaters BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

December 2021 **Description Previous Application Reference Submittal Location** December 2018 Submittal 5.0 BACT BACT Analysis Steps 1 to 5 Incorporated into Section Post application NTEC Response #15 5.11.1 Table D-4, Appendix D Table D-4. December 2018 Submittal Appendix D **RBLC** Table D-4 Addendum Addendum update Appendix D Tables E-3a, E-3b, E-4a, E-4b Appendix E December 2018 Submittal **Economic Tables** Table 1a & Table 1b Appendix E Post application NTEC Response #15

Table 5-32: Natural Gas Heaters BACT Analysis References

There are two natural gas heaters proposed as part of the Project. The heaters heat natural gas prior to entering the facility and are fired by natural gas, a clean-burning fuel. Each heater is rated at 10.0 MMBtu/hr and is proposed to operate 8,760 hours per year each. The RBLC has limited information on BACT conclusions for heaters (Appendix D). The RBLC tables also show high variability for emission rates for each pollutant. For all pollutants, no add-on controls were listed because gas heaters are so small.

5.11.1 BACT for Nitrogen Oxides - Gas Heaters

The following sections outline the top-down steps for NO_x emissions from the gas heaters.

5.11.1.1 Step 1. Identify Potential Control Strategies

There are no add-on NO_x control techniques available for units of this size. Ultra-low NO_x burners, low- NO_x burners, along with combustion controls, are listed as BACT in the RBLC for the gas heaters. NO_x emissions listed in the RBLC range from 0.013 to 0.2466 lb/MMBtu for similar sized gas heater utilizing low- NO_x burners and combustion controls.

In discussions with vendors, multiple vendors stated that they cannot meet the 0.013 NO_x emission rate with low-NO_x burners. It was determined that the emission rate of 0.013 lb/MMBtu is in line with vendor quotes for ultra-low-NO_x burners.

The natural gas heaters installed for the Project will be equipped with low NO_x burners. Since the vendor has not been selected yet, the natural gas heater NO_x emission factor listed in the application is based on the emission factor listed in AP-42 Section 1.4, Table 1.4-1 for small boilers (<100 MMBtu/hr) controlled

by low NO_x burners. This value is consistent with other BACT units with low NO_x burners listed in the RBLC.

Because there are lower emission limits presented in the RBLC, vendors were contacted to determine what NO_x control options were available for natural gas heaters of this size. Low NO_x burners are standard on these natural gas heaters; however, to achieve the lower NO_x levels reported in the RBLC, the vendors stated that this would require ultra-low NO_x burners. As such, the costs and emission guarantees for ultra-low NO_x burners were obtained from the vendors. As required by a top-down BACT analysis, evaluation of this additional control was completed.

5.11.1.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling NO_x emissions are evaluated for technical feasibility in the following sections.

5.11.1.2.1 SCR

Although the RBLC did not list any add-on control devices as BACT for a gas heater, one SCR vendor said that they could provide an SCR for this size unit. The vendor's removal efficiency for this size unit is 90 percent control of NO_x.

As a result, an SCR system is technically feasible for the gas heaters.

5.11.1.2.2 Low-NO_x Burners

Low-NO_x burners are currently available from most gas heater manufacturers. This technology seeks to reduce combustion temperatures, thereby reducing NO_x. In a conventional combustor, the air and fuel are introduced at an approximately stoichiometric ratio, and air/fuel mixing occurs at the flame front where diffusion of fuel and air reaches the combustible limit. A lean premixed combustor design premixes the fuel and air prior to combustion. Premixing results in a homogenous air/fuel mixture, which minimizes localized fuel-rich pockets that produce elevated combustion temperatures and higher NO_x emissions. A lean air-to-fuel ratio approaching the lean flammability limit is maintained, and the excess air serves as a heat sink to lower combustion temperatures, which lowers NO_x formation. A pilot flame is used to maintain combustion stability in this fuel-lean environment.

Low-NO_x burners are available on the gas heaters and are considered both baseline and technically feasible.

5.11.1.2.3 Ultra-Low-NO_x Burners

Ultra-low-NO_x burners are available on the gas heaters and is considered technically feasible.

5.11.1.2.4 Combustion Control

"Good combustion practices" include operational and design elements to control the amount and distribution of excess air in the flue gas to confirm that there is enough oxygen present for complete combustion.

As a result, combustion control is considered baseline for the gas heaters and is technically feasible.

5.11.1.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible NO_x control technologies for the 10.0 MMBtu/hr gas heaters are ranked by control effectiveness in Table 5-33.

Table 5-33: Ranking of NO_x Control Technologies for the Gas Heaters

Controlled

| Control Technology | Reduction (%) | Controlled Emission Level (lb/MMBtu) |
|--|---------------------------|--|
| SCR | 90 | 0.0049 |
| Ultra-low NO _x burners | 73 | 0.013 |
| Low-NO _x burners and combustion control | Not applicable (baseline) | 0.049 |

5.11.1.4 Step 4. Evaluate the Most Effective Control Technologies

Each technically feasible control technology was evaluated for energy, environmental, and economic impacts. These impacts are discussed below for each control technology.

5.11.1.4.1 SCR

Energy and Environmental Impacts

Energy and environmental impacts for an SCR system are discussed in Section 5.1.4.1.

Economic Impacts

The capital costs and annualized costs associated with an SCR system for each gas heater was evaluated and the analysis is located in Appendix E. The total capital investment of installing an SCR system on the gas heater is approximately \$137,910. On an annual basis, the SCR system would cost approximately \$103,539, which results in a cost per ton of NO_x removed of almost \$53,604 while removing only 1.9 tons

of NO_x per year. Therefore, any control of NO_x by add-on controls would result in costs that would not be economical.

An SCR is not proposed as BACT for the gas heaters because it is not economically feasible.

5.11.1.4.2 Ultra-Low-NO_x Burners and Combustion Control

Energy and Environmental Impacts

Ultra-low NOx burners may decrease efficiency slightly on the natural gas heaters; however, these impacts are not significant.

Economic Impacts

The economic impacts of installing an ultra-low-NO_x burner on the natural gas heaters were evaluated. The capital costs and annualized costs associated with installing ultra-low-NO_x burners on the natural gas heaters are in Appendix E. The total capital investment of installing ultra-low-NO_x burners on each natural gas heater is approximately \$25,990. On an annual basis, the ultra-low-NO_x burners would cost \$22,526 which results in a cost per ton of NO_x removed of approximately \$13,187 while removing only an additional 1.7 tons of NO_x per year over the standard low-NO_x burners. Installing and operating ultra-low-NO_x burners results in costs that are economically infeasible.

5.11.1.4.3 Low-NO_x Burners and Combustion Control

Because the low-NO_x burners come standard on most gas heaters and combustion control is accomplished through operation of the gas heater, there are no incremental energy, environmental, or economic impacts associated with these controls.

5.11.1.5 Step 5. Proposed NO_x Gas Heaters BACT Determination

Low-NO_x burners and combustion control was selected as BACT for the gas heaters; add-on controls are not practical on this small unit since the economic impacts are high. The low-NO_x burners can achieve an emission rate of 0.049 lb/MMBtu during steady state operation.

5.11.2 BACT for Carbon Monoxide – Gas Heaters

The following sections outline the top-down steps for CO emissions from gas heaters.

5.11.2.1 Step 1. Identify Potential Control Strategies

The RBLC does not list add-on controls for gas heater in the BACT determinations for control of CO emissions from gas heaters; however, one control vendor has indicated that an oxidation catalyst system may be used on a gas heater this size. As with the combustion turbines, good combustion control will help

control emissions of CO from the gas heaters. CO emissions listed in the RBLC range from 0.0075 to 0.1108 lb/MMBtu for similar sized gas heater utilizing combustion controls and clean fuels. A majority of the gas heaters listed in the RBLC that are less than 0.08 lb/MMBtu are much larger than the proposed gas heaters for this Project.

5.11.2.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling CO emissions are evaluated for technical feasibility in the following sections.

5.11.2.2.1 Oxidation Catalyst System

One control vendor has indicated that an oxidation catalyst system may be used on a gas heater this size. The oxidation catalyst system is an add-on control that converts CO and VOC to CO₂ by use of an oxidation catalyst. Section 5.2.2.2 describes the oxidation catalyst system for gas-fired units.

An oxidation catalyst system is considered technically feasible for the gas heaters; one vendor has provided a quote for this system.

5.11.2.2.2 Combustion Control

"Good combustion practices" include operational and design elements to control the amount and distribution of excess air in the flue gas to confirm that there is enough oxygen present for complete combustion.

Good combustion practices are a technically feasible method of controlling CO emissions from the gas heaters.

5.11.2.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible CO control technologies for the 10.0 MMBtu/hr gas heaters are ranked by control effectiveness in Table 5-34.

Control TechnologyReduction (%)Controlled Emission Level (lb/MMBtu)Oxidation catalyst900.008Combustion controlNot applicable (baseline)0.08

Table 5-34: Ranking of CO Control Technologies for the Gas Heaters

5.11.2.4 Step 4. Evaluate the Most Effective Control Technologies

Each technically feasible control technology was evaluated for energy, environmental, and economic impacts. These impacts are discussed below for each control technology.

5.11.2.4.1 Oxidation Catalyst

Energy and Environmental Impacts

Energy and environmental impacts of an oxidation catalyst are discussed in Section 5.2.4.1.

Economic Impacts

The control cost analysis for an oxidation catalyst system for the gas heater is displayed in Appendix E. An oxidation catalyst system for this size unit would require a total capital investment of \$33,582. The annual costs of operating this oxidation catalyst system would be \$34,849. On an annual basis, only 3.2 tons per year of CO along with 0.07 tons per year of VOC would be removed at a cost of almost \$10,550 per ton of pollutants removed.

The cost is considered economically infeasible; therefore, an oxidation catalyst for control of CO emissions from the gas heaters is not considered BACT.

5.11.2.5 Step 5. Proposed BACT for CO

Since add-on controls are not feasible on such a small gas-fired unit, combustion control was selected as BACT for CO from the gas heaters at an emission rate of 0.08 lb/MMBtu.

BACT for CO emissions from the gas heaters is good combustion practices.

5.11.3 BACT for Particulate Matter – Gas Heaters

The following sections outline the top-down steps for PM/PM₁₀/PM_{2.5} emissions from gas heaters.

5.11.3.1 Step 1. Identify Potential Control Strategies

The RBLC does not list any control strategies other than good combustion practices and low ash fuel (natural gas). No add-on controls were identified for significant removal of these pollutants from the gas heater exhaust.

5.11.3.2 Step 2. Identify Technically Feasible Control Technologies

The only technically feasible control option is combustion control for PM/PM₁₀/PM_{2.5}.

5.11.3.3 Step 3. Rank the Technically Feasible Control Technologies

The only technically feasible control option is combustion control for PM/PM₁₀/PM_{2.5}.

5.11.3.4 Steps 4 and 5. Evaluate the Most Effective Control Technologies and Proposed BACT for PM/PM₁₀/PM_{2.5}

Since add-on controls are not feasible on such a small gas-fired unit, combustion control was selected as BACT for PM/PM₁₀/PM_{2.5} from the gas heaters at an emission rate of 0.01 lb/MMBtu.

5.11.4 BACT for Volatile Organic Compounds – Gas Heaters

The following sections outline the top-down steps for VOC emissions from gas heaters.

5.11.4.1 Step 1. Identify Potential Control Strategies

The RBLC does not list add-on controls for gas heaters in the BACT determinations for control of VOC emissions; however, one control vendor has indicated that an oxidation catalyst system may be used on a gas heater this size. As with the combustion turbines, good combustion control will help control emissions of VOC from the gas heaters.

5.11.4.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling VOC emissions are evaluated for technical feasibility in the following sections.

5.11.4.2.1 Oxidation Catalyst System

One control vendor has indicated that an oxidation catalyst system may be used on a gas heater this size. The oxidation catalyst system is an add-on control that converts CO and VOC to CO₂ by use of a catalyst. Section 5.4.2.2 describes the oxidation catalyst system for gas-fired units.

An oxidation catalyst system is considered technically feasible for the gas heaters; one vendor has provided a quote for this system.

5.11.4.2.2 Combustion Control

"Good combustion practices" include operational and design elements to control the amount and distribution of excess air in the flue gas to confirm that there is enough oxygen present for complete combustion.

Good combustion practices are a technically feasible method of controlling VOC emissions from the gas heaters.

5.11.4.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible VOC control technologies for the 10.0 MMBtu/hr gas heaters is ranked by control effectiveness in Table 5-35.

Table 5-35: Ranking of VOC Control Technologies for the Gas Heaters

| Control Technology | Reduction (%) | Controlled Emission Level (lb/MMBtu) |
|--------------------|---------------------------|--------------------------------------|
| Oxidation catalyst | 30 | 0.0038 |
| Combustion control | Not applicable (baseline) | 0.005 |

Each technically feasible control technology was evaluated for energy, environmental, and economic impacts. These impacts are discussed below for each control technology.

5.11.4.4 STEP 4. Evaluate the Most Effective Control Technologies

Each technically feasible control technology was evaluated for energy, environmental, and economic impacts. These impacts are discussed below for each control technology.

5.11.4.4.1 Oxidation Catalyst

Energy and Environmental Impacts

Energy and environmental impacts of an oxidation catalyst are discussed in Section 5.4.4.1.

Economic Impacts

The control cost analysis for an oxidation catalyst system for the gas heater is displayed in Appendix E. An oxidation catalyst system for this size unit would require a total capital investment of \$33,582. The annual costs of operating this oxidation catalyst system would be \$34,849. On an annual basis, only 3.2 tons per year of CO along with only 0.07 tons per year of VOC would be removed at a cost of almost \$10,550 per ton of pollutants removed.

The cost is considered economically infeasible; therefore, an oxidation catalyst for control of VOC emissions from the gas heaters is not considered BACT.

5.11.4.5 STEP 5. Proposed BACT for VOC

Since add-on controls are not feasible on such a small gas-fired unit, combustion control was selected as BACT for VOC from the gas heaters at an emission rate of 0.005 lb/MMBtu.

BACT for VOC emissions from the gas heaters is good combustion practices.

5.11.5 BACT for Sulfuric Acid Mist - Gas Heaters

The following sections outline the top-down steps for H₂SO₄ emissions from the gas heaters.

5.11.5.1 Step 1-5 Identify, Rank and Select BACT

There are no add-on control technologies for controlling H₂SO₄ emissions from a gas heater. As with the combustion turbines, using low sulfur fuel and controlling combustion is the only technologically feasible control option.

BACT is use of lower sulfur fuel and good combustion practices. This will achieve an emission rate of 3.9×10^{-3} tons per year of H_2SO_4 from each of the gas heaters.

5.11.6 BACT for Greenhouse Gases – Gas Heaters (Steps 1-5)

The gas heaters as proposed will be fired exclusively on natural gas and used to pre-heat natural gas fuel to facilitate start-up. The units are each rated at approximately 10.0 MMBtu/hr and will be permitted to be fired a total of 8,760 hours per year each. GHG emissions from this unit are estimated to be on the order of 5,129 tons CO₂e per year, each. These GHG emissions are also *de minimis*, when compared to the turbine GHG emissions or the facility total GHG emissions. The basic GHG BACT reasoning presented for the turbines essentially applies to this heater as well. The Owners propose that GHG BACT for these units will be the following:

- Use of clean fuels (exclusive use of natural gas)
- Requiring the Owners to maintain the unit according to the manufacturer's specifications, and to operate the unit in the most efficient manner possible, i.e. good combustion practices
- Tune the unit every two years according to the manufacturer's specifications
- Record the annual hours of operation and annual fuel use and report the GHG emissions annually. The GHG emissions from this unit may be included in the facility-wide annual GHG limit.

5.11.7 BACT for Opacity - Gas Heaters

The following sections outline the top-down steps for opacity emissions from gas heaters.

5.11.7.1 Step 1. Identify Potential Control Strategies

Opacity is not a discrete pollutant and cannot be measured using mass emissions rate criteria (e.g., lb/hr). Therefore, a typical top-down BACT economic analysis that evaluated effectiveness on a \$/ton basis cannot be conducted on opacity. Rather, the opacity BACT determination should focus on pollutants in the flue gas that contribute to opacity. These pollutants include PM, NO_x, SO₂, and H₂SO₄. BACT

determinations have been done for PM, NO_x and H₂SO₄ for the gas heaters. Units firing fuels with low ash content and high combustion efficiency exhibit correspondingly low exhaust opacity.

5.11.7.2 Step 2. Identify Technically Feasible Control Technologies

The Owners have prepared a detailed BACT evaluation for pollutants that potentially contribute to opacity. Based on these BACT evaluations, the Owners have identified the following control technologies as technically feasible: SCR and combustion control for NO_x control; and low ash, low sulfur fuel and combustion control for PM and H₂SO₄ control. These technologies represent BACT for the criteria pollutants and will also minimize opacity.

5.11.7.3 Step 3. Rank the Technically Feasible Control Technologies

Based on these BACT evaluations, the Owners have ranked the following feasible control technologies for opacity: (1) combustion control, (2) clean fuels. The Owners have determined that the use of low ash, low sulfur fuel and combustion control combine to rank as the top option for opacity control.

5.11.7.4 Step 4. Evaluate the Most Effective Control Technologies

The energy, environmental, and economic impacts of the feasible control technologies are described in their respective BACT analysis.

5.11.7.5 Step 5. Proposed Opacity BACT Determination

BACT for exhaust opacity will include the use of combustion control for NO_x control and the use of low ash, low sulfur fuel and combustion control for PM and H₂SO₄ control. The combination of these control technologies represents BACT for opacity for the gas heaters.

5.12 BACT Analysis for Emergency Diesel Fire Pump (P06)

Previously submitted BACT Sections, post application submittals, and updated references to the BACT analysis sections for the emergency diesel fire pump are presented in Table 5-36. The updated emergency diesel fire pump BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

| Description | Previous Application Reference | December 2021 Submittal Location |
|----------------------------|--|-------------------------------------|
| DACT Analysis Stone 1 to 5 | 5.0 BACT December 2018 Submittal | 5.0 BACT |
| BACT Analysis Steps 1 to 5 | Post application NTEC Response #18 | Incorporated into Section 5.12.3 |
| RBLC | Appendix D, Table D-6 December 2018 Submittal | Appendix D, Table D-6 |
| RBLC | | Table D-6 Addendum, Appendix D |
| Economic Tables | Table 1 and Table 2 Post application NTEC Response #11 | Appendix E |

Table 5-36: Emergency Diesel Fire Pump BACT Analysis References

One 282-hp emergency diesel-fired fire pump will be installed for the Project. The emergency diesel fire pump will be limited to 500 hours per year (100 hours per year for testing and maintenance purposes) and will utilize ultra-low sulfur transportation-grade distillate fuel oil, with a sulfur content of no more than 0.0015 weight percent. The emergency diesel fire pump will comply with the applicable NSPS requirements. The RBLC has limited information on BACT conclusions for small engines such as the emergency diesel fire pump (Appendix D). The RBLC tables also show high variability for emission rates for each pollutant. For all pollutants, no add-on controls were listed because the add-on controls were determined to not be economically feasible due to engine size.

BACT can be no less stringent than the NSPS Subpart IIII limits, which are discussed in Section 4.2.5.

5.12.1 BACT for Nitrogen Oxides – Emergency Diesel Fire Pump

The following sections outline the top-down steps for NO_x emissions from the emergency diesel fire pump.

5.12.1.1 Step 1. Identify Potential Control Strategies

For an emergency diesel fire pump that only operates 500 hours per year, there are no controls that are available that would approach being cost effective. In addition, the fuel oil that is combusted would quickly poison and/or foul an SCR catalyst in a short amount of operating time. For the purposes of this BACT analysis, however, it is assumed that an SCR system may be technically feasible.

5.12.1.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling NO_x emissions are evaluated for technical feasibility in the following sections.

5.12.1.2.1 SCR

The RBLC did not list any add-on control devices as BACT for the emergency diesel fire pump; however, an SCR may be available for this size of engine.

As a result, an SCR system is considered technically feasible for the emergency diesel fire pump.

5.12.1.2.2 Combustion Control and Clean Fuels

"Good combustion practices" include operational and design elements to control the amount and distribution of excess air in the flue gas to confirm that there is enough oxygen present for complete combustion.

As a result, combustion control and clean fuels are considered baseline for the emergency diesel fire pump and is technically feasible.

5.12.1.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible NO_x control technologies for the emergency diesel fire pump are ranked by control effectiveness in Table 5-37.

Table 5-37: Ranking of NO_x Control Technologies for the Emergency Diesel Fire Pump

| Control Technology | Reduction (%) | Controlled Emission Level (g/hp-hr) |
|------------------------------------|---------------------------|---|
| SCR | 90 | 0.30 |
| Combustion Control and Clean Fuels | Not applicable (baseline) | 3.0 |

5.12.1.4 Step 4. Evaluate the Most Effective Control Technologies

Each technically feasible control technology was evaluated for energy, environmental, and economic impacts. These impacts are discussed below for each control technology.

5.12.1.4.1 SCR

Energy and Environmental Impacts

Energy and environmental impacts for an SCR system are discussed in Section 5.1.4.1.

Economic Impacts

Because this unit will only operate 500 hours per year, a cost analysis is not needed to show that the cost per ton of NO_x removed would be economically infeasible. The emergency diesel fire pump will only emit 0.47 tons per year of NO_x, based on the annual 500-operating hour limitation.

Therefore, an SCR is not proposed as BACT because it is not economically feasible for the emergency diesel fire pump.

5.12.1.4.2 Combustion Control and Clean Fuels

Combustion control is accomplished through operational control of the engines; therefore, there are no energy, environmental, or economic impacts associated with this control.

5.12.1.5 Step 5. Proposed NO_x Emergency Diesel Fire Pump BACT Determination

Combustion control and clean fuels were selected as BACT for NO_x for the emergency diesel fire pump; add-on controls are not practical on a unit this size, with limited operation, and the economic impacts are high. The emergency diesel fire pump will be able to achieve 3.0 g/hp-hr of NO_x emissions on an ongoing basis.

5.12.2 BACT for Carbon Monoxide – Emergency Diesel Fire Pump

The following sections outline the top-down steps for CO emissions from the emergency diesel fire pump.

5.12.2.1 Step 1. Identify Potential Control Strategies

For an engine that only operates 500 hours per year for testing and maintenance, there are no controls that are available that would even approach being cost effective. In addition, the fuel oil that is combusted would quickly poison and/or foul an oxidation catalyst in a short amount of operating time. For the purposes of this BACT analysis, however it is assumed that an oxidation catalyst may be technically feasible.

5.12.2.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling CO emissions are evaluated for technical feasibility in the following sections.

5.12.2.2.1 Oxidation Catalyst

The RBLC did not list any add-on control devices as BACT for the emergency diesel fire pump; however, an oxidation catalyst may be available for this small engine size.

As a result, an oxidation catalyst system is considered technically feasible for the emergency diesel fire pump.

5.12.2.2.2 Combustion Control

"Good combustion practices" include operational and design elements to control the amount and distribution of excess air in the flue gas to confirm that there is enough oxygen present for complete combustion.

As a result, combustion control is considered baseline for the emergency diesel fire pump and is technically feasible.

5.12.2.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible CO control technologies for the emergency diesel fire pump are ranked by control effectiveness in Table 5-38.

Table 5-38: Ranking of CO Control Technologies for the Emergency Diesel Fire Pump

| Control Technology | Reduction (%) | Controlled Emission Level (g/hp-hr) |
|--------------------|---------------------------|--|
| Oxidation Catalyst | 90 | 0.26 |
| Combustion Control | Not applicable (baseline) | 2.6 |

5.12.2.4 Step 4. Evaluate the Most Effective Control Technologies

Each technically feasible control technology was evaluated for energy, environmental, and economic impacts. These impacts are discussed below for each control technology.

5.12.2.4.1 Oxidation Catalyst

Energy and Environmental Impacts

Energy and environmental impacts for an oxidation catalyst are discussed in Section 5.2.4.1.

Economic Impacts

The control cost analysis for an oxidation catalyst system for the emergency fire pump is shown in Appendix E. An oxidation catalyst system for this size unit would require a total capital investment of \$23,660. The annual costs of operating this oxidation catalyst system would be \$5,838. On an annual basis, only 0.32 tons per year of CO and 0.09 tons per year of VOC would be removed at a total cost of \$14,326 per ton of both pollutants removed, based on limited operation of 500 hours per year.

Keep in mind that normal operation for this unit will be testing and maintenance for less than one hour per week and results costs for the add- on controls would be much, much higher. Even when considering emergency operation for up to 500 hours per year, the cost for adding an oxidation catalyst to the emergency fire pump is considered economically infeasible; therefore, an oxidation catalyst for control of CO and VOC emissions from the emergency fire pump is not considered BACT. Additionally, since the emergency fire pump will typically operate for less than one hour during routine maintenance and testing, the emissions will be uncontrolled since it takes time for the catalyst to warm-up to optimal operating temperature; therefore, an oxidation catalyst is not an effective control technology.

Therefore, an oxidation catalyst is not proposed as BACT because it is not economically feasible for the emergency diesel fire pump.

5.12.2.4.2 Combustion Control

Combustion control is accomplished through operational control of the engine, therefore, there are no energy, environmental, or economic impacts associated with this control.

5.12.2.5 Step 5. Proposed CO Emergency Diesel Fire Pump BACT Determination

Combustion control was selected as BACT for CO for the emergency diesel fire pump; add-on controls are not practical on this small unit with limited operation and economic impacts are high. The emergency diesel fire pump will be able to achieve 2.6 g/hp-hr of CO emissions on an on-going basis.

5.12.3 BACT for Particulate Matter – Emergency Diesel Fire Pump

The following sections outline the top-down steps for particulate matter emissions from the emergency diesel fire pump.

5.12.3.1 Step 1. Identify Potential Control Strategies

The RBLC does not list any control strategies other than good combustion practices and low ash fuel (natural gas) for the emergency diesel fire pump.

A diesel particulate filter was deemed technically infeasible for the fire pump as the National Fire Protection Association, Underwriters Laboratories and Factory Mutual will not allow a particulate filter to be installed on the exhaust stack of a fire pump. This is because it is possible for this filter to become clogged, rendering the diesel engine inoperable.

No add-on controls were identified for significant removal of these pollutants from the engine's exhaust.

5.12.3.2 Step 2. Identify Technically Feasible Control Technologies

The only technically feasible control option is combustion control for PM/PM₁₀/PM_{2.5}.

5.12.3.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible PM/PM₁₀/PM_{2.5} control technologies for the emergency diesel fire pump are ranked by control effectiveness in Table 5-39.

Table 5-39: Ranking of PM/PM₁₀/PM_{2.5} Control Technologies for the Emergency Diesel Fire Pump

| Control Technology | Reduction (%) | Controlled Emission Level (g/hp-hr) |
|------------------------------------|---------------------------|--|
| Combustion Control and Clean Fuels | Not applicable (baseline) | 0.15 |

5.12.3.4 Steps 4 and 5. Evaluate the Most Effective Control Technologies and Proposed BACT for PM/PM₁₀/PM_{2.5}

Since no add-on controls were identified, combustion control with low ash fuel was selected as BACT for $PM/PM_{10}/PM_{2.5}$ at an emission rate of 0.15 g/hp-hr for the emergency diesel fire pump.

5.12.4 BACT for Volatile Organic Compounds – Emergency Diesel Fire Pump

The following sections outline the top-down steps for VOC emissions from the emergency diesel fire pump.

5.12.4.1 Step 1. Identify Potential Control Strategies

For an engine that only operates 500 hours per year for testing and maintenance, there are no controls that are available that would even approach being cost effective. In addition, the fuel oil that is combusted would quickly poison and/or foul the oxidation catalyst in a short amount of operating time. For the purposes of this BACT analysis; however, it is assumed that an oxidation catalyst may be technically feasible.

5.12.4.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling VOC emissions are evaluated for technical feasibility in the following sections.

5.12.4.2.1 Oxidation Catalyst

Although the RBLC did not list any add-on control devices as BACT for the emergency diesel fire pump, an oxidation catalyst may be available for this small engine.

As a result, an oxidation catalyst system is considered technically feasible for the emergency diesel fire pump.

5.12.4.2.2 Combustion Control

"Good combustion practices" include operational and design elements to control the amount and distribution of excess air in the flue gas to confirm that there is enough oxygen present for complete combustion.

As a result, combustion control is considered baseline for the emergency diesel fire pump and is technically feasible.

5.12.4.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible VOC control technologies for the emergency diesel fire pump are ranked by control effectiveness in Table 5-40.

Table 5-40: Ranking of VOC Control Technologies for the Emergency Diesel Fire Pump

| Control Technology | Reduction (%) | Controlled Emission Level (g/hp-hr) |
|--------------------|---------------------------|--|
| Oxidation Catalyst | 20 | 0.91 |
| Combustion Control | Not applicable (baseline) | 1.1 |

5.12.4.4 Step 4. Evaluate the Most Effective Control Technologies

Each technically feasible control technology was evaluated for energy, environmental, and economic impacts. These impacts are discussed below for each control technology.

5.12.4.4.1 Oxidation Catalyst

Energy and Environmental Impacts

Energy and environmental impacts for an oxidation catalyst are discussed in Section 5.4.4.1.

Economic Impacts

The control cost analysis for an oxidation catalyst system for the emergency fire pump is shown in Appendix E. An oxidation catalyst system for this size unit would require a total capital investment of \$23,660. The annual costs of operating this oxidation catalyst system would be \$5,838. On an annual basis, only 0.32 tons per year of CO and 0.09 tons per year of VOC would be removed at a total cost of \$14,326 per ton of both pollutants removed, based on limited operation of 500 hours per year.

Keep in mind that normal operation for this unit will be testing and maintenance for less than one hour per week and results costs for the add- on controls would be much, much higher. Even when considering emergency operation for up to 500 hours per year, the cost for adding an oxidation catalyst to the emergency fire pump is considered economically infeasible; therefore, an oxidation catalyst for control of CO and VOC emissions from the emergency fire pump is not considered BACT. Additionally, since the emergency fire pump will typically operate for less than one hour during routine maintenance and testing, the emissions will be uncontrolled since it takes time for the catalyst to warm-up to optimal operating temperature; therefore, an oxidation catalyst is not an effective control technology.

Therefore, an oxidation catalyst is not proposed as BACT because it is not economically feasible for the emergency diesel fire pump.

5.12.4.4.2 Combustion Control

Combustion control is accomplished through operational control of the engines; therefore, there are no energy, environmental, or economic impacts associated with this control.

5.12.4.5 Step 5. Proposed VOC Emergency Diesel Fire Pump BACT Determination

Combustion control was selected as BACT for VOC for the emergency diesel fire pump; add-on controls are not practical on these small units with limited operation and economic impacts are high. The emergency diesel fire pump will be able to achieve 1.1 g/hp-hr of VOC emissions on an on-going basis.

5.12.5 BACT for Sulfuric Acid Mist – Emergency Diesel Fire Pump

The following sections outline the top-down steps for H₂SO₄ emissions from the emergency diesel fire pump.

5.12.5.1 Step 1-5 Identify, Rank and Select BACT

There are no add-on control technologies for controlling H₂SO₄ emissions from a diesel fire pump. As with the combustion turbine, using low sulfur fuel and controlling combustion is the only technologically feasible control option.

BACT is use of lower sulfur fuel and good combustion practices. This will achieve an emission rate of 0.02 tons per year of H₂SO₄ from the fire pump.

5.12.6 BACT for Greenhouse Gases – Emergency Diesel Fire Pump (Steps 1-5)

The emergency diesel fire pump is proposed to be used for no more than 500 hours per year. The design of the engine is dictated by the manufacturer, not by the end-user. As such, the Project is limited to commercially available options, which include those engines meeting EPA Tier 3 requirements.

Consistent with its rationale for the BACT determination for greenhouse gas emissions from the combustion turbine, BACT for the emergency diesel fire pump involves selection of the most efficient stationary emergency engine that can meet the facility's needs. Total greenhouse gas emissions from the emergency diesel fire pump are estimated at 80 tons CO₂e per year. These greenhouse gas emissions are also *de minimis* when compared to the turbine greenhouse gas emissions.

A Tier 3-certified engine is the most fuel-efficient option for these purposes. Further, because emissions of greenhouse gases are directly correlated to operation of the unit, BACT requires that the engine shall only be operated for maintenance, readiness testing, and during emergencies and other periods authorized by the permitting agency and/or the permit.

Operation of the emergency diesel fire pump will be limited by permit conditions for reliability-and maintenance related activities and the Owners will be required to keep records of the operation of the emergency diesel fire pump and its fuel usage. Therefore, the Owners believe no additional conditions are required to enforce this greenhouse gas BACT determination.

5.12.7 BACT for Opacity – Emergency Diesel Fire Pump

The following sections outline the top-down steps for opacity emissions from the emergency diesel fire pump.

5.12.7.1 Step 1. Identify Potential Control Strategies

Opacity is not a discrete pollutant and cannot be measured using mass emissions rate criteria (e.g., lb/hr). Therefore, a typical top-down BACT economic analysis that evaluated effectiveness on a \$/ton basis

cannot be conducted on opacity. Rather, the opacity BACT determination should focus on pollutants in the flue gas that contribute to opacity. These pollutants include PM, NO_x, SO₂, and H₂SO₄. BACT determinations have been done for PM, NO_x and H₂SO₄ for this emergency diesel fire pump. Units firing fuels with low ash content and high combustion efficiency exhibit correspondingly low exhaust opacity.

5.12.7.2 Step 2. Identify Technically Feasible Control Technologies

The Owners have prepared a detailed BACT evaluation for pollutants that potentially contribute to opacity. Based on these BACT evaluations, the Owners have identified the following control technologies as technically feasible: SCR and combustion control for NO_x control; and low ash, low sulfur fuel and combustion control for PM and H₂SO₄ control. These technologies represent BACT for the criteria pollutants and will also minimize opacity.

5.12.7.3 Step 3. Rank the Technically Feasible Control Technologies

Based on these BACT evaluations, the Owners have ranked the following feasible control technologies for opacity (1) combustion control, (2) clean fuels. The Owners have determined that the use of low ash, low sulfur fuel and combustion control combine to rank as the top option for opacity control.

5.12.7.4 Step 4. Evaluate the Most Effective Control Technologies

The energy, environmental, and economic impacts of the feasible control technologies are described in their respective BACT analysis.

5.12.7.5 Step 5. Proposed Opacity BACT Determination

BACT for exhaust opacity will include the use of combustion control for NO_x control and the use of low ash, low sulfur fuel and combustion control for PM and H_2SO_4 control. The combination of these control technologies represents BACT for opacity.

5.13 BACT Analysis for Emergency Diesel Generator (P07)

Previously submitted BACT Sections, post application submittals, and updated references to the BACT analysis sections for the emergency diesel generator are presented in Table 5-41. The updated emergency diesel generator BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

Table 5-41: Emergency Diesel Generator BACT Analysis References

Provious Application Reference

December

| Description | Previous Application Reference | December 2021 Submittal Location |
|----------------------------|----------------------------------|-------------------------------------|
| BACT Analysis Steps 1 to 5 | 5.0 BACT December 2018 Submittal | 5.0 BACT |

| | Post application NTEC Response #18 | Incorporated into Section 5.13.3 | |
|-----------------|------------------------------------|----------------------------------|--|
| | Appendix D, Table D-5 December | Table D-5 | |
| RBLC | 2018 Submittal | Appendix D | |
| RBLC | | Table D-5 Addendum | |
| | | Appendix D | |
| | Table 3 and Table 4 | Appendix E | |
| Economic Tables | Post application NTEC Response #11 | Appendix E | |
| | Table 2a and Table 2b | Appendix E | |
| | Post application NTEC Response #17 | Appendix E | |

One 1,490 hp (1,112 kW) emergency diesel generator will be installed for the Project. The emergency diesel generator will be limited to 500 hours per year (100 hours per year for testing and maintenance purposes) and will utilize ultra-low sulfur transportation grade distillate fuel oil, with a sulfur content of no more than 0.0015 weight percent. The emergency diesel generator will comply with the applicable NSPS requirements. The RBLC has limited information on BACT conclusions for small engines such as the emergency diesel generator (Appendix D). The RBLC tables also show high variability for emission rates for each pollutant. For all pollutants, no add-on controls were listed because the add-on controls were determined to not be economically feasible due to engine size.

BACT can be no less stringent than the NSPS Subpart IIII limits, which are discussed in Section 4.2.5.

A cost difference between a Tier 2 and Tier 4 engine as well as the associated dollar per ton of controlled emissions was provided at the request of WDNR as part of the post application information requests. The analysis is provided in Appendix E.

5.13.1 BACT for Nitrogen Oxides – Emergency Diesel Generator

The following sections outline the top-down steps for NO_x emissions from the emergency diesel generator.

5.13.1.1 Step 1. Identify Potential Control Strategies

For an emergency diesel generator that only operates 500 hours per year for testing and maintenance, there are no controls that are available that would approach being cost effective. In addition, the fuel oil that is combusted would quickly poison and/or foul an SCR catalyst in a short amount of operating time. For the purposes of this BACT analysis, however it is assumed that an SCR system may be technically feasible.

5.13.1.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling NO_x emissions are evaluated for technical feasibility in the following sections.

5.13.1.2.1 SCR

The RBLC did not list any add-on control devices as BACT for the emergency diesel generator; however, an SCR may be available for this size of engine.

As a result, an SCR system is considered technically feasible for the emergency diesel generator.

5.13.1.2.2 Combustion Control

"Good combustion practices" include operational and design elements to control the amount and distribution of excess air in the flue gas to confirm that there is enough oxygen present for complete combustion.

As a result, combustion control is considered baseline for the emergency diesel generator and is technically feasible.

5.13.1.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible NO_x control technologies for the emergency diesel generator are ranked by control effectiveness in Table 5-42.

Table 5-42: Ranking of NO_x Control Technologies for the Emergency Diesel Generator

| Control Technology | Reduction (%) | Controlled Emission Level (g/hp-hr) |
|-----------------------|---------------------------|---|
| SCR | 90 | 0.48 |
| Combustion Control | Not applicable (baseline) | 4.8 |

5.13.1.4 Step 4. Evaluate the Most Effective Control Technologies

Each technically feasible control technology was evaluated for energy, environmental, and economic impacts. These impacts are discussed below for each control technology.

5.13.1.4.1 SCR

Energy and Environmental Impacts

Energy and environmental impacts for an SCR system are discussed in Section 5.1.4.1.

Economic Impacts

The capital costs and annualized costs associated with an SCR system for the emergency diesel generator is shown in Appendix E. The total capital investment of installing an SCR system on the emergency diesel generator is approximately \$80,866. On an annual basis, the SCR system would cost approximately \$46,681, which results in a cost per ton of NOx removed of almost \$14,592 while removing only 3.3 tons of NOx per year, based on limited operation of 500 hours per year. Therefore, any control of NOx by add-on controls would result in costs that would not be economical, even when considering a maximum emergency use of up to 500 hours per year. In reality, the cost per ton removed will be much less, knowing that this unit will only be tested for up to one hour per week. Additionally, since the emergency diesel generator will typically operate for less than one hour during routine maintenance and testing, the emissions will be uncontrolled since it takes time for the SCR to warm-up to optimal operating temperature; therefore, a SCR is not an effective control technology.

Therefore, an SCR is not proposed as BACT because it is not economically feasible for the emergency diesel generator.

5.13.1.4.2 Combustion Control

Combustion control is accomplished through operational control of the engines; therefore, there are no energy, environmental, or economic impacts associated with this control.

5.13.1.5 Step 5. Proposed NO_x Emergency Diesel Generator BACT Determination

Combustion control was selected as BACT for NO_x for the emergency diesel generator; add-on controls are not practical on a unit this size, with limited operation, and the economic impacts are high. The emergency diesel generator will be able to achieve 4.8 g/hp-hr of NO_x emissions on an on-going basis.

5.13.2 BACT for Carbon Monoxide – Emergency Diesel Generator

The following sections outline the top-down steps for CO emissions from the emergency diesel generator.

5.13.2.1 Step 1. Identify Potential Control Strategies

For an engine that only operates 500 hours per year for testing and maintenance, there are no controls that are available that would even approach being cost effective. In addition, the fuel oil that is combusted would quickly poison and/or foul the oxidation catalyst in a short amount of operating time. For the

purposes of this BACT analysis, however it is assumed that an oxidation catalyst may be technically feasible.

5.13.2.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling CO emissions are evaluated for technical feasibility in the following sections.

5.13.2.2.1 Oxidation Catalyst

The RBLC did not list any add-on control devices as BACT for the emergency diesel generator; however, an oxidation catalyst may be available for this small engine size.

As a result, an oxidation catalyst system is considered technically feasible for the emergency diesel generator.

5.13.2.2.2 Combustion Control

"Good combustion practices" include operational and design elements to control the amount and distribution of excess air in the flue gas to confirm that there is enough oxygen present for complete combustion.

As a result, combustion control is considered baseline for the emergency diesel generator and is technically feasible.

5.13.2.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible CO control technologies for the emergency diesel generator are ranked by control effectiveness in Table 5-43.

Table 5-43: Ranking of CO Control Technologies for the Emergency Diesel Generator

| Control Technology | Reduction (%) | Controlled Emission Level (g/hp-hr) |
|--------------------|---------------------------|--|
| Oxidation Catalyst | 90 | 0.26 |
| Combustion Control | Not applicable (baseline) | 2.6 |

5.13.2.4 Step 4. Evaluate the Most Effective Control Technologies

Each technically feasible control technology was evaluated for energy, environmental, and economic impacts. These impacts are discussed below for each control technology.

5.13.2.4.1 Oxidation Catalyst

Energy and Environmental Impacts

Energy and environmental impacts for an oxidation catalyst are discussed in Section 5.2.4.1.

Economic Impacts

Because the emergency diesel generator only operates for 500 hours per year for testing and maintenance, a cost analysis is not needed to show that the cost per ton of CO removed would be economically infeasible. The emergency diesel generator will only emit 2.15 tons per year of CO, based on the annual 500 operating hour limitation.

Therefore, an oxidation catalyst is not proposed as BACT because it is not economically feasible for the emergency diesel generator.

5.13.2.4.2 Combustion Control

Combustion control is accomplished through operational control of the engine, therefore, there are no energy, environmental, or economic impacts associated with this control.

5.13.2.5 Step 5. Proposed CO Emergency Diesel generator BACT Determination

Combustion control was selected as BACT for CO for the emergency diesel generator; add-on controls are not practical on this small unit with limited operation and economic impacts are high. The emergency diesel generator will be able to achieve 2.6 g/hp-hr of CO emissions on an on-going basis.

5.13.3 BACT for Particulate Matter – Emergency Diesel Generator

The following sections outline the top-down steps for $PM/PM_{10}/PM_{2.5}$ emissions from the emergency diesel generator.

5.13.3.1 Step 1. Identify Potential Control Strategies

The RBLC does not list any control strategies other than good combustion practices and low ash fuel (natural gas) for the emergency diesel generator. Vendors have stated there is no precedent for a particulate filter on an emergency diesel generator; therefore, a diesel particulate filter is considered experimental control technology not viable for the diesel generator.

No add-on controls were identified for significant removal of these pollutants from the engine's exhaust.

5.13.3.2 Step 2. Identify Technically Feasible Control Technologies

The only technically feasible control option is combustion control for PM/PM₁₀/PM_{2.5}.

5.13.3.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible PM/PM₁₀/PM_{2.5} control technologies for the emergency diesel generator are ranked by control effectiveness in Table 5-44.

Table 5-44: Ranking of PM/PM₁₀/PM_{2.5} Control Technologies for the Emergency Diesel Generator

| Control Technology | Reduction (%) | Controlled Emission Level (g/hp-hr) |
|--------------------|---------------------------|--|
| Combustion Control | Not applicable (baseline) | 0.15 |

5.13.3.4 Steps 4 and 5. Evaluate the Most Effective Control Technologies and Proposed BACT for PM/PM₁₀/PM_{2.5}

Since no add-on controls were identified, combustion control with low ash fuel was selected as BACT for $PM/PM_{10}/PM_{2.5}$ at an emission rate of 0.15 g/hp-hr for the emergency diesel generator.

5.13.4 BACT for Volatile Organic Compounds – Emergency Diesel Generator

The following sections outline the top-down steps for VOC emissions from the emergency diesel generator.

5.13.4.1 Step 1. Identify Potential Control Strategies

For an engine that only operates 500 hours per year for testing and maintenance, there are no controls that are available that would even approach being cost effective. In addition, the fuel oil that is combusted would quickly poison and/or foul the oxidation catalyst in a short amount of operating time. For the purposes of this BACT analysis, however it is assumed that an oxidation catalyst may be technically feasible.

5.13.4.2 Step 2. Identify Technically Feasible Control Technologies

The primary methods for controlling VOC emissions are evaluated for technical feasibility in the following sections.

5.13.4.2.1 Oxidation Catalyst

Although the RBLC did not list any add-on control devices as BACT for the emergency diesel generator, an oxidation catalyst may be available for this small engine.

As a result, an oxidation catalyst system is considered technically feasible for the emergency diesel generator.

5.13.4.2.2 Combustion Control

"Good combustion practices" include operational and design elements to control the amount and distribution of excess air in the flue gas to confirm that there is enough oxygen present for complete combustion.

As a result, combustion control is considered baseline for the emergency diesel generator and is technically feasible.

5.13.4.3 Step 3. Rank the Technically Feasible Control Technologies

The technically feasible VOC control technologies for the emergency diesel generator are ranked by control effectiveness in Table 5-45.

Table 5-45: Ranking of VOC Control Technologies for the Emergency Diesel Generator

| Control Technology Reduction (%) | | Controlled Emission Level (g/hp-hr) | |
|----------------------------------|---------------------------|--|--|
| Oxidation Catalyst | 20 | 0.26 | |
| Combustion Control | Not applicable (baseline) | 0.32 | |

5.13.4.4 Step 4. Evaluate the Most Effective Control Technologies

Each technically feasible control technology was evaluated for energy, environmental, and economic impacts. These impacts are discussed below for each control technology.

5.13.4.4.1 Oxidation Catalyst

Energy and Environmental Impacts

Energy and environmental impacts for an oxidation catalyst are discussed in Section 5.4.4.1.

Economic Impacts

Because the emergency diesel generator will only operate 500 hours per year for testing and maintenance, a cost analysis is not needed to show that the cost per ton of VOC removed would not be economically feasible. The emergency diesel generator will only emit 0.26 tons per year of VOC, based on the annual 500 operating hour limitation.

Therefore, an oxidation catalyst is not proposed as BACT because it is not economically feasible for the emergency diesel generator.

5.13.4.4.2 Combustion Control

Combustion control is accomplished through operational control of the engines; therefore, there are no energy, environmental, or economic impacts associated with this control.

5.13.4.5 Step 5. Proposed VOC Emergency Diesel Generator BACT Determination

Combustion control was selected as BACT for VOC for the emergency diesel generator; add-on controls are not practical on these small units with limited operation and economic impacts are high. The emergency diesel generator will be able to achieve 0.32 g/hp-hr of VOC emissions for the generator on an on-going basis.

5.13.5 BACT for Sulfuric Acid Mist – Emergency Diesel Generator

The following sections outline the top-down steps for H₂SO₄ emissions from the emergency diesel generator.

5.13.5.1 Step 1-5 Identify, Rank and Select BACT

There are no add-on control technologies for controlling H_2SO_4 emissions from a diesel generator. As with the combustion turbine, using low sulfur fuel and controlling combustion is the only technologically feasible control option.

BACT is use of lower sulfur fuel and good combustion practices. This will achieve an emission rate of 6.9 x 10⁻⁴ tons per year of H₂SO₄ from the emergency diesel generator.

5.13.6 BACT for Greenhouse Gases – Emergency Diesel Generator (Steps 1-5)

The emergency diesel generator is proposed to be used for no more than 500 hours per year. The design of the engine is dictated by the manufacturer, not by the end-user. As such, the Project is limited to commercially available options, which include those engines meeting EPA Tier 2 requirements.

Consistent with its rationale for the BACT determination for greenhouse gas emissions from the combustion turbine, BACT for the emergency diesel generator involves selection of the most efficient stationary emergency diesel generator that can meet the facility's needs. Total greenhouse gas emissions from the emergency diesel generator are estimated at 841 tons CO₂e per year. These greenhouse gas emissions are also *de minimis* when compared to the turbine greenhouse gas emissions.

A Tier 2-certified engine is the most fuel-efficient option for these purposes. Further, because emissions of greenhouse gases are directly correlated to operation of the unit, BACT requires that the engine shall

only be operated for maintenance, readiness testing, and during emergencies and other periods authorized by the permitting agency and/or the permit.

Because operation of the emergency diesel generator will be limited by permit conditions for reliabilityand maintenance related activities and the Owners will be required to keep records of the operation of the emergency diesel generator and its fuel usage. Therefore, the Owners believe no additional conditions are required to enforce this greenhouse gas BACT determination.

5.13.7 BACT for Opacity – Emergency Diesel Generator

The following sections outline the top-down steps for opacity emissions from the emergency diesel generator.

5.13.7.1 Step 1. Identify Potential Control Strategies

Opacity is not a discrete pollutant and cannot be measured using mass emissions rate criteria (e.g., lb/hr). Therefore, a typical top-down BACT economic analysis that evaluated effectiveness on a \$/ton basis cannot be conducted on opacity. Rather, the opacity BACT determination should focus on pollutants in the flue gas that contribute to opacity. These pollutants include PM, NO_x, SO₂, and H₂SO₄. BACT determinations have been done for PM, NO_x and H₂SO₄ for this emergency diesel generator. Units firing fuels with low ash content and high combustion efficiency exhibit correspondingly low exhaust opacity.

5.13.7.2 Step 2. Identify Technically Feasible Control Technologies

The Owners have prepared a detailed BACT evaluation for pollutants that potentially contribute to opacity. Based on these BACT evaluations, the Owners have identified the following control technologies as technically feasible: SCR and combustion control for NO_x control; and low ash, low sulfur fuel and combustion control for PM and H₂SO₄ control. These technologies represent BACT for the criteria pollutants and will also minimize opacity.

5.13.7.3 Step 3. Rank the Technically Feasible Control Technologies

Based on these BACT evaluations, the Owners have ranked the following feasible control technologies for NO_x: (1) combustion control, (2) clean fuels. The Owners have determined that the use of low ash, low sulfur fuel and combustion control combine to rank as the top option for opacity control.

5.13.7.4 Step 4. Evaluate the Most Effective Control Technologies

The energy, environmental, and economic impacts of the feasible control technologies are described in their respective BACT analysis.

5.13.7.5 Step 5. Proposed Opacity BACT Determination

BACT for exhaust opacity will include the use of combustion control for NO_x control and the use of low ash, low sulfur fuel and combustion control for PM and H₂SO₄ control. The combination of these control technologies represents BACT for opacity.

5.14 BACT for Volatile Organic Compounds – Fuel Oil Storage Tanks (T01, T02, and T03)

Previously submitted BACT Sections and updated references to the BACT analysis sections for the fuel oil storage tanks are presented in Table 5-46. The updated fuel oil storage tank BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

Table 5-46: Fuel Oil BACT Analysis References

| Description | Previous Application Reference | December 2021 Submittal Location |
|----------------------------|---|-------------------------------------|
| BACT Analysis Steps 1 to 5 | ACT Analysis Steps 1 to 5 5.0 BACT December 2018 Submittal | |

The following sections outline the top-down BACT steps for emissions of VOC from the fuel oil storage tanks.

5.14.1 Steps 1, 2, and 3. Identify Potential Feasible Control Strategies and Rank Control Strategies

The Project will include three fuel oil (diesel) storage tanks: 180,000-gallon, 1,700-gallon, and 350-gallon. Diesel fuel has a very low vapor pressure and as such, controls that may be used on high vapor pressure liquids, such as floating roofs, are not as effective at reducing emissions. Fixed roof tanks are proposed for control of emissions from the fuel oil storage tanks.

5.14.2 Steps 4 and 5. Evaluate the Most Effective Control Technologies and Proposed BACT for VOC Emissions

The proposed BACT for the fuel oil storage tanks is the use of fixed roof tanks. Because emissions are extremely low from these sources, this is the only feasible and reasonable control for these small emission sources. Emissions will be less than 0.04 tons per year.

5.15 BACT for Particulate Matter (PM/PM₁₀/PM_{2.5}) – Haul Road Fugitives (F01)

Previously submitted BACT Sections and updated references to the BACT analysis sections for the haul road fugitives are presented in Table 5-47. The updated haul road BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

DescriptionPrevious Application
ReferenceDecember 2021
Submittal LocationBACT Analysis Steps 1 to 55.0 BACT
January 2021 Submittal5.0 BACTAppendix D, Table D-2
January 2021 SubmittalTable D-9, Appendix DTable D-9 Addendum,
Appendix D

Table 5-47: Haul Road Fugitives BACT Analysis References

Haul roads will be located onsite and delivery truck traffic will travel on paved roads. Emissions of particulate matter will be filterable only and speciated into PM, PM₁₀, and PM_{2.5}. However, control technologies will control all sizes of particulate.

5.15.1 Step 1: Identify Potential Control Strategies

In a review of the RBLC, the following control technologies for particulate emissions from roads were identified:

- 1. Chemical dust suppression and surfactant application,
- 2. Watering, sweeping and vacuuming,
- 3. Paving, and
- 4. Traffic and speed restrictions

5.15.2 Step 2: Identify Technically Feasible Control Technologies

All of the options listed, except chemical dust suppression and surfactant application, are potentially applicable control technologies considered technically feasible for the Project. Chemical dust suppression and surfactant application are generally used for unpaved surface and are considered infeasible for this Project as the facility roads will be paved.

5.15.3 Step 3: Rank the Technically Feasible Control Technologies

The third step in the BACT analysis is to rank the remaining control technologies in order of control effectiveness. Table 5-48 provides a listing of PM/PM₁₀/PM_{2.5} control technologies by effectiveness.

Table 5-48: Efficiency Ranking of Particulate Control Technologies for Haul Roads

| Control Technology | Approximate Control Efficiency (percent) | |
|--|---|--|
| Water flushing followed by sweeping of paved roads | up to 96 | |
| Water flushing of paved roads | up to 69 | |
| Vacuum sweeping of paved roads | up to 58 | |
| Paving | | |
| Speed/traffic restrictions | | |

Source: EPA Control of Open Fugitive Dust Sources

5.15.4 Step 4: Evaluate Most Effective Control Technologies

The fourth step in the BACT analysis is to evaluate the most effective control technology based on energy, environmental, and economic impacts. Based on a review of the RBLC, the implementation of a Fugitive Dust Control Plan (FDCP) is considered a control method accepted as BACT for particulate emissions from roads at similar facilities. No specific BACT emission limits associated with the previously mentioned control methods were obtained from the RBLC.

5.15.5 Step 5: Select BACT

The applicants propose to develop, maintain, and implement a FDCP as BACT for the paved roads.

5.16 BACT for Greenhouse Gases (GHG) and VOCs – Natural Gas and Fuel Oil Fugitives (F02)

Previously submitted BACT Sections, post application evaluations, and updated references to the BACT analysis sections for the natural gas and fuel oil fugitives are presented in Table 5-49. The updated natural gas and fuel oil fugitives BACT analysis shows that the BACT determination in the original application and PSD permit remain valid.

Previous Application December 2021 Description Reference **Submittal Location 5.0 BACT 5.0 BACT** January 2021 Submittal Post application BACT BACT Analysis Steps 1 to 5 evaluation on "leak-proof" Incorporated into Section 5.0 piping components **BACT** WDNR Memorandum dated July 8, 2021 Table D-1, Appendix D Table D-8, Appendix D January 2021 Submittal **RBLC** Table D-8 Addendum, Appendix D Appendix E Cost Evaluations Appendix E January 2021 Submittal Cost Analysis **Economic Tables** Post application BACT Appendix E evaluation on "leak-proof"

Table 5-49: Natural Gas and Fuel Oil Fugitives BACT Analysis References

The proposed project will include natural gas piping components from the natural gas line that will enter the Project site to provide gas for the combustion turbine, duct burner, natural gas heaters and auxiliary boiler. These natural gas piping components are potential sources of methane emissions due to emissions from valves, flanges, sampling connections and relief valves.

piping components

The proposed project will also include fuel oil piping components from the fuel oil line that will enter the Project site to provide fuel oil for the combustion turbine and duct burner. The emergency diesel fire pump and emergency diesel generator piping components will also have minimal fugitive emissions. These fuel oil piping components are potential sources of VOC emissions due to emissions from valves, flanges, sampling connections and relief valves.

Methane is not a VOC but is regulated as a GHG with a GWP of 25 when expressed as CO₂e. Evaporative emissions from fuel oil, such as xylene and benzene, are VOCs.

5.16.1 Step 1: Identify Potential Control Strategies

Greenhouse gas emissions (methane) and VOCs may leak out of certain components within the pipeline system, anywhere there is a connection, valve or flange. Per a review of the RBLC database (Appendix D), the following technologies were identified as potential control options for these piping fugitives:

- Implementation of leak detection and repair (LDAR) program Instrument monitoring: using a handheld analyzer to determine if leaks exist
- Implementation of LDAR Physical inspection: an audio/visual/olfactory (AVO) leak detection program
- Good operating processes
- Certified low-leaking valves

5.16.2 Step 2: Identify Technically Feasible Control Technologies

The use of instrument monitoring LDAR and remote sensing technologies are technically feasible for natural gas and fuel oil components. A LDAR program based on AVO monitoring is determined to be infeasible because the natural gas transmission pipeline that connects directly to the facility will not be odorized with mercaptan, the odorant typically added to distribution lines to allow for olfactory detection of any leaks without instrumentation. Since mercaptan is not present, inspections for gas leakage are accomplished by using leak detector equipment. These leak detection surveys with instrumentation are conducted at intervals as prescribed by applicable state and gas pipeline regulations. AVO inspections for fuel oil are technically feasible. Additionally, good operating practices and certified low-leaking values are also feasible for the natural gas and fuel oil fugitive emissions. Therefore, the instrument monitoring LDAR program, good operating practices, and certified low-leaking valves listed in Step 1 are technically feasible for natural gas. All listed control technologies in Step 1 are technically feasible for fuel oil.

5.16.3 Step 3: Rank the Technically Feasible Control Technologies

LDAR programs are used to inspect fugitive components to identify leaks either by using instruments or by physical inspections. Leaks identified by the inspections are then repaired within a specified time period, thus reducing the emissions.

The top-ranked control strategy is a LDAR program that utilizes instrument leak detection. Based on available data piping components are generally assigned control efficiencies ranging from 30 to 97 percent for valves, relief valves, and sampling connections (TCEQ, 2018).

The second-ranked control option involves implementation of a AVO leak detection program. Per Texas Commission on Environmental Quality (TCEQ) documentation of a control efficiency of 97 percent is generally assigned for a AVO program.

Certified low-leaking valves are a remaining control technology with 80 percent control of VOC and CO₂e.

Good operating processes are considered baseline for the purposes of this BACT analysis. Table 5-50 summarizes the control efficiencies for the various control technology options.

Table 5-50. GHG and VOC Technology Rankings for Natural Gas and Fuel Oil Fugitives

| Rank | Control Technology | Percent Control |
|------|--------------------------------------|---------------------------|
| 1 | LDAR program – instrument monitoring | 97% |
| 2 | LDAR program - AVO leak detection | 97% |
| 3 | Certified low-leaking valves | 80% |
| 4 | Good operating process | Not applicable (baseline) |

Source: TCEQ, 2018

5.16.4 Step 4: Evaluate Most Effective Control Technologies

Since the uncontrolled VOC and CO₂e emissions from the natural gas and fuel oil piping represent less than 0.04 percent of the total site wide VOC emissions and less than 0.04 percent of the total site wide CO₂e emissions, any emission control techniques applied to the piping fugitives will provide minimal additional VOC and CO₂e emission reductions over the baseline.

The economic impacts of installing a LDAR program for instrument monitoring was evaluated. Based on EPA data the estimated cost effectiveness of LDAR programs is shown below in Table 5-51 (EPA, 1992).

Table 5-51: Cost Effectiveness of LDAR Programs

| Control | Annual Cost (\$/year) | Cost Effectiveness – Mass (\$/ton GHG) | Cost Effectiveness – CO₂e (\$/ton CO₂e) |
|--------------------------------------|--------------------------|--|---|
| LDAR program – instrument monitoring | \$76,389 | \$3,258 | \$130 |

The economic impacts of installing low-leaking valves were also evaluated. For the valves that are included in the natural gas and fuel oil piping components emissions unit (F02), the department (WDNR) determined that certified low-leaking valves cost would be \$5,874 per ton of methane (\$234.95 per ton CO₂e) and \$29,826 per ton VOC removed. To provide a basis for determining economic feasibility for CO₂e, the cost of 1 ton of carbon credits in the California cap and trade program is approximately \$19 per ton of CO₂e for the May 2021 auction. Because the control costs are above the levels that the WDNR

considers to be economically feasible as BACT under PSD, certified low-leaking valves have been determined by the department to not be economically feasible

A detailed cost summary analysis is provided in Appendix E.

5.16.5 Step 5: Select BACT

Based on the top-down analysis for natural gas, an instrument monitoring LDAR program is BACT for natural gas components. Instrument monitoring LDAR program was also selected as BACT for fuel oil components.

Any GHG and VOC emissions from the piping components will be fugitive emissions. Fugitive emissions are, by their nature, very difficult to monitor directly, as they are not emitted from a discrete emission point. Therefore, the Owners propose the following compliance demonstrations, recordkeeping and monitoring requirements:

- 1. Conduct instrument monitoring inspections on piping components each calendar quarter to detect leaks of natural gas and fuel oil.
- 2. Keep a log of all the quarterly instrument monitoring inspections from piping components that are part of this Project.
- 3. Develop a Facility Leak Detection Plan

These proposed work practices are consistent with the BACT determinations identified above.

6.0 AIR DISPERSION MODELING

Summary: An updated air quality analysis was performed using WDNR's recently updated meteorological data and background concentrations. Section 6.0 replaces all previously submitted air dispersion modeling analyses. The SO₂ emission rates for modeling provided to WDNR as part of a data request response #7 is provided in Appendix F.

Since the Project is subject to PSD review, an air dispersion modeling analysis is required for each regulated NSR pollutant that exceeds its PSD significance level. According to the emission calculations for this Project, NO_x, CO, PM, PM₁₀, PM_{2.5}, VOC, and CO₂e are subject to PSD review; as a result, an air quality analysis was performed for NO_x, CO, PM₁₀, and PM_{2.5} using the EPA-approved American Meteorological Society (AMS)/EPA Regulatory Model (AERMOD). Consistent with WDNR and EPA guidance, AERMOD modeling of PM, VOC, and CO₂e were not conducted, since there are no modeling thresholds for these pollutants.

A summary of the models, the modeling techniques, and modeling results for the Project are discussed in the following sections.

6.1 Air Dispersion Model

Air dispersion modeling was performed using the latest version of the AERMOD model (Version 21112). The AERMOD model is an EPA-approved, steady-state Gaussian air dispersion model that is designed to estimate downwind ground-level concentrations from single or multiple sources using detailed meteorological data. AERMOD is a model currently approved for industrial sources and PSD permits.

The WDNR requested that the Owners demonstrate regulatory compliance through the use of AERMOD. Major features of the AERMOD model are as follows:

- Plume rise, in stable conditions, is calculated using Briggs equations that consider wind and
 temperature gradients at stack top and half the distance to plume rise; in unstable conditions,
 plume rise is superimposed on the displacements by random convective velocities, accounting for
 updrafts and downdrafts due to momentum and buoyancy as a function of downwind distance for
 stack emissions.
- Plume dispersion receives Gaussian treatment in horizontal and vertical directions for stable conditions and non-Gaussian probability density function in vertical direction for unstable conditions.

- AERMOD creates profiles of wind, temperature, and turbulence, using all available measurement levels and accounts for meteorological data throughout the plume depth.
- Surface characteristics, such as Bowen ratio, albedo, and surface roughness length, may be specified to better simulate the modeling domain.
- Planetary Boundary Layers (PBL) such as friction velocity, Monin-Obukhov length, convective velocity scale, mechanical and convective height, and sensible heat flux may be specified.
- AERMOD uses a convective (based upon hourly accumulation of sensible heat flux) and a
 mechanical mixed layer height.
- AERMOD's terrain pre-processor (AERMAP) provides information for the advanced critical dividing streamline height algorithms and uses National Elevation Dataset (NED) to obtain elevations.
- AERMOD uses vertical and horizontal turbulence-based plume growth (from measurements and/or PBL theory) that varies with height and uses continuous growth functions.
- AERMOD uses convective updrafts and downdrafts in a probability density function to predict
 plume interaction with the mixing lid in convective conditions while using a mechanically mixed
 layer near the ground.
- Plume reflection above the lid is considered.
- AERMOD models impacts that occur within the cavity regions of building downwash via the use
 of the plume rise model enhancements (PRIME) algorithm, and then uses the standard AERMOD
 algorithms for areas without downwash.

Details of the AERMOD modeling options may be found in the User's Guide for AERMOD (EPA, 2021). The regulatory default option was selected for this analysis since it met the EPA guideline requirements and WDNR modeling guidance requirements.

The following default model options were used:

- Elevated Terrain Algorithms
- Stack-tip Downwash
- Gradual Plume Rise
- Buoyancy-induced Dispersion
- Calms and Missing Data Processing Routine
- Calculate Wind Profiles
- Default Vertical Potential Temperature Gradient

• Rural Dispersion

6.2 Model Parameters

Modeling runs were conducted at full load and partial loads of the combustion turbines to confirm that operation of the Project will not result in impacts greater than the NAAQS and PSD Class II Increments. The expected hourly emission rates and modeling parameters for the combustion turbine while combusting natural gas or fuel oil are shown in Table 6-1 and Table 6-2, respectively. These emission rates represent projected worst-case ambient conditions under various operating loads and include start-up and shutdown emissions. The annual emissions are based on worst-case annual emissions. Modeling of VOC and CO₂e will not be carried out because there are no modeling thresholds for these pollutants.

Table 6-1: Combustion Turbine Emissions and Modeling Parameters – Natural Gas Operation

| Pollutant | Unitsª | Duct firing 100% Load | 100% Load | 75% Load | MECL Load | Start-up/ Shutdown | |
|-----------------------------------|--------------------------|--------------------------|--------------|-------------|--------------|-----------------------|--|
| NO | lb/hr | 33.46 | 26.55 | 20.56 | 12.44 | 200.00 ^b | |
| NO_x | tpy | | 255.61 | | | | |
| CO | lb/hr | 15.28 | 12.12 | 9.39 | 5.68 | $7,190.00^{b}$ | |
| DM /DM | lb/hr | 36.31 | 21.80 | 16.81 | 12.94 | 21.80 | |
| $PM_{10}/PM_{2.5}$ | tpy | 162.80 | | | | | |
| Stack Param | neters | | | | | | |
| Stack temper | rature (°F) ^a | 163.55 | 167.12 | 164.93 | 164.93 | 166.94 | |
| Exit velocity (ft/s) ^a | | 64.00 | 63.81 | 48.88 | 36.82 | 61.56 | |
| Stack heig | tht (feet) | 190.0 | | | | | |
| Stack diam | eter (feet) | | | 21.28 | | | |

⁽a) lb/hr = pounds per hour, tpy = tons per year, °F = degrees Fahrenheit, ft/s = feet per second, MECL = minimum emissions compliance load

⁽b) Maximum 1-hour start-up emissions (worst-case combustion turbine emissions during start-up)

| | | | | | | - | |
|--------------------|-------------------------|--------------------------|-----------|----------|--------------|------------------------|--|
| Pollutant | Unitsª | Duct firing 100% Load | 100% Load | 75% Load | MECL Load | Start-up/ Shutdown | |
| NO | lb/hr | 72.68 | 51.55 | 41.04 | 31.10 | 510.00 ^b | |
| NO_x | tpy | 255.61 | | | | | |
| CO | lb/hr | 11.06 | 7.85 | 6.25 | 15.78 | 16,860.00 ^b | |
| D) (/D) (| lb/hr | 54.51 | 39.45 | 37.50 | 35.68 | 39.45 | |
| $PM_{10}/PM_{2.5}$ | tpy | 162.80 | | | | | |
| Stack Paran | neters | | | | | | |
| Stack temper | rature (°F)a | 176.63 | 176.63 | 169.24 | 165.01 | 175.66 | |
| Exit veloc | ity (ft/s) ^a | 71.96 | 71.19 | 57.75 | 43.48 | 68.88 | |
| Stack heig | tht (feet) | 190.0 | | | • | | |
| Stack diam | eter (feet) | | | 21.28 | | | |

Table 6-2: Combustion Turbine Emissions and Modeling Parameters – Fuel Oil Operation

The expected hourly emission rates and modeling parameters for the auxiliary equipment are shown in Table 6-3. Annual emissions for the auxiliary boiler and gas heaters were based on 8,760 hours of operation per year.

| Table 6-3: | Auxiliary Equipment | Emissions and | Modeling Parameter | 'S |
|------------|---------------------|---------------|--------------------|----|
|------------|---------------------|---------------|--------------------|----|

| Pollutant | Unitsª | Auxiliary Boiler | Natural Gas Heater #1 | Natural Gas Heater #2 |
|-----------------------------------|--------------------------|-----------------------------------|--------------------------|--------------------------|
| NO | lb/hr | 1.10 | 0.49 | 0.49 |
| NO_x | tpy | 4.82 | 2.15 | 2.15 |
| CO | lb/hr | 0.37 | 0.82 | 0.82 |
| DM /DM | lb/hr | 0.75 | 0.07 | 0.07 |
| $PM_{10}/PM_{2.5}$ | tpy | 3.26 | 0.33 | 0.33 |
| Stack Param | neters | | | |
| Stack temper | rature (°F) ^a | 290.00 | 750.00 | 750.00 |
| Exit velocity (ft/s) ^a | | elocity (ft/s) ^a 48.00 | | 25.00 |
| Stack height (feet) | | 110.00 | 15.00 | 15.00 |
| Stack diam | eter (feet) | 3.50 | 1.67 | 1.67 |

⁽a) lb/hr = pounds per hour, tpy = tons per year, ${}^oF = degrees$ Fahrenheit, ft/s = feet per second

6.3 Haul Roads

The haul roads included in the model were laid out using the guidance from the March 2, 2012, EPA memo on the *Haul Road Workgroup Final Report* (EPA, 2012). The following parameters were used:

• Vehicle height of 12 feet

⁽a) lb/hr = pounds per hour, tpy = tons per year, °F = degrees Fahrenheit, ft/s = feet per second,

MECL = minimum emissions compliance load

⁽b) Maximum 1-hour start-up emissions (worst-case combustion turbine emissions during start-up)

- Road width of 20 feet
- Top of plume height = 1.7 x vehicle height = 20.40 feet or 6.22 meters
- Volume source release height = 0.5 x top of plume height = 10.20 feet or 3.11 meters
- Width of plume = road width + 6 meters for two lane roadways = 39.69 feet or 12.10 meters
- Initial sigma z = top of plume / 2.15 = 9.49 feet or 2.89 meters
- Initial sigma y = width of plume / 2.15 = 18.46 feet or 5.63 meters
- Adjacent volume source spacing = sigma y x 2.15 = 39.69 feet or 12.10 meters

The calculated road emissions are included in Appendix C.

6.4 Modeling Methodology

The modeling methodology used for this analysis is summarized in the sections below.

6.4.1 Intermittent Emissions

Per WDNR guidance, the Owners propose to only model sources with continuous operation. Emission units that do not have a set operating schedule, operate for short periods of time during the year, and do not contribute to the normal operation of the facility were not included in modeling analysis. Therefore, the emergency diesel fire pump and emergency diesel generator are considered intermittent sources and were not included in the modeling analysis.

6.4.2 Emission Factors

Emissions factor (EMISFACT) modeling options in AERMOD allow a user to model emissions only when certain criteria are met. EMISFACT was not used for any Project sources. EMISFACT was used for the inventory sources where WDNR indicated it was appropriate, specifically for inventory source "UW-16" which operates only from October to April.

6.4.3 Rain Caps and Horizontal Stacks

If horizontal stacks or rain caps are present at the site, the restriction of vertical flow is accounted for through the use of the POINTCAP or POINTHOR keywords within the AERMOD input file. The POINTCAP and POINTHOR keywords were not used for any Project sources. The POINTHOR keyword was used for the Husky Superior inventory sources where WDNR indicated it was appropriate.

6.4.4 Good Engineering Practice Stack Height

Sources are subject to Good Engineering Practice (GEP) stack height requirements outlined in 40 CFR Part 51, Sections 51.100 and 51.118. As defined by the regulations, for stacks in existence on January 12, 1979 and with appropriate permits under 40 CFR Parts 51 and 52, GEP height is calculated as:

$$GEP = 2.5*H$$

Where,

H = the building height

For all other stacks, GEP height is calculated as the greater of 65 meters (measured from the ground level elevation at the base of the stack) or the height resulting from the following formula:

$$GEP = H + 1.5L$$

Where,

H =the building height; and

L = the lesser of the building height or the greatest crosswind distance of the building - also known as maximum projected width.

To meet stack height requirements, the point sources were evaluated in terms of the proximity to nearby structures. The purpose of this evaluation is to determine if the discharge from each stack will become caught in the turbulent wake of a building or other structure, resulting in downwash of the plume.

Downwash of the plume can result in elevated ground-level concentrations. In EPA's 1985 *Guideline for Determination of Good Engineering Practice Stack Height*, EPA provides guidance for determining whether building downwash will occur. The downwash analysis was performed consistent with the methods prescribed in this guidance document.

Calculations for determining the direction-specific downwash parameters were performed using the most current version of the EPA's Building Profile Input Program – Plume Rise Model Enhancements, otherwise referred to as the BPIP-PRIME downwash algorithm (Version 04274). The BPIP-PRIME files are included in the electronic file transfer to the WDNR. After running the BPIP-PRIME model, it was determined that the GEP stack heights do not exceed the greater of 65 meters or the calculated GEP stack height.

The buildings are included in the model per the following WDNR guidance:

• If a building has multiple tiers, the structure was modeled as a single building with multiple tiers (wedding cake methodology).

- Structures that are less than four feet in height were not modeled.
- All structures that present a solid face from the ground to the top of the structure and that have angled corners were included.
- Structures off the ground were not included.
- Average roof heights were used for peaked or sloped tiers.
- Single, individual silos that are taller than they are wide were not included.
- Groupings of silos and large, wide circular grain bins using the eave height were included.

6.4.5 Receptor Grid

The overall purpose of the modeling analysis is to demonstrate that operation of the Project will not result in, or contribute to, concentrations above the NAAQS or PSD Class II Increments. Modeling runs were conducted using the AERMOD model in simple and complex terrain mode within a 20- by 20-kilometer Cartesian grid to determine the significant impact area for each pollutant. Based on guidance from WDNR, the grid incorporated the receptor spacing specified in Table 6-4. Receptors were also placed along the fence line boundary at a spacing of 25 meters.

 Distance from Fence Line (kilometers)
 Receptor Spacing (meters)

 0-0.5 25

 0.5-1 50

 1-2 100

 2-5 250

 5-10 500

Table 6-4: Receptor Spacing from Fence Line Boundary

Source: WDNR, Wisconsin Air Dispersion Modeling Guidelines, 2018

A tight receptor grid provided by WDNR was included to incorporate the high terrain in Duluth as shown in Figure B-3, Appendix B.

Terrain elevations were incorporated into the model. The 1/3 arc second U.S. Geological Survey (USGS) NED data was used to obtain the necessary receptor elevations. North American Datum of 1983 (NAD 83) was used to develop the Universal Transverse Mercator (UTM) coordinates for this Project.

AERMOD has a terrain preprocessor (AERMAP) which uses gridded terrain data for the modeling domain to calculate not only a XYZ coordinate, but also a representative terrain-influence height associated with each receptor location selected. This terrain-influenced height is called the height scale

and is separate for each individual receptor. AERMAP (Version 18081) utilized the electronic NED data to populate the model with receptor elevations.

6.4.6 Meteorological Data

AERMOD requires a preprocessor called AERMET to process meteorological data for 5 years from offsite locations to estimate the boundary layer parameters for the dispersion calculations. AERMET requires the input of surface roughness length, albedo, and Bowen ratio to define land surface characteristics for its calculations. WDNR provides AERMOD-ready processed meteorological data sets; therefore, the site characteristics (Bowen ratio, albedo, surface roughness) were completed by WDNR.

Surface air meteorological data from Sky Harbor Airport, in Duluth, Minnesota (WBAN ID 04919) and upper air data from Minneapolis, Minnesota (WBAN ID 94983) was used in the analysis. The most recent 5-year data set available covers the period of 2015 to 2018 and 2020. A profile base elevation of 186 meters was used in the model. The meteorological data used to develop these data sets has been analyzed by WDNR for data completeness, and these data sets have good data quality.

6.4.7 Land Use Parameters

USGS land cover data was used to determine the rural and urban land use percentages for a 3-kilometer area surrounding the Project site (Figure B-4, Appendix B). Land use categories I1, I2, C1, R2, and R3 were classified as urban land use categories (EPA, 2017). Less than 12 percent of the area surrounding the Nemadji River Site is classified as urban. Since the 3-kilometer area surrounding the Project is more than 50 percent rural, the rural dispersion coefficients option in the AERMOD model were selected.

6.4.8 Modeling Thresholds

The NAAQS, modeling/monitoring significance levels, and PSD Class II Increment thresholds for the modeled pollutants are shown in Table 6-5.

Table 6-5: NAAQS, Monitoring and Monitoring Significance Levels, and PSD Class II Increment

| | Averaging Period | Monitoring Significance Level | Modeling Significance Level | PSD Class II Increment | NAAQS |
|-------------------|---------------------|-------------------------------------|-----------------------------------|---------------------------|--------|
| Pollutant | | microgra | ıms per cubic me | ter (µg/m³) | |
| NO | Annual | 14 | 1 | 25 | 100 |
| NO_x | 1-hour | NA | 7.5 | NA | 188 |
| СО | 8-hour | 575 | 500 | NA | 10,000 |
| | 1-hour | NA | 2,000 | NA | 40,000 |
| DM | Annual | NA | 1 | 17 | NA |
| PM_{10} | 24-hour | 10 | 5 | 30 | 150 |
| D) (| Annual | NA | 0.2 ^b | 4 | 12 |
| PM _{2.5} | 24-hour | 4ª | 1.2 ^b | 9 | 35 |

Source: WDNR Wisconsin Air Dispersion Modeling Guidelines, 2018

The modeled values were modeled using the appropriate form of the standard for each pollutant and averaging period. For significance modeling, all short-term and annual averaging periods were modeled with the impact shown in Table 6-6. For PSD Class II Increment, the short-term averaging periods were compared to the high second highest impacts, and the annual standards were compared to the first highest impacts. The NAAQS thresholds were modeled using the highs shown in Table 6-6 for each averaging period.

Table 6-6: Modeled Highs

| Pollutant | Averaging Period | Significant Impact Level High | NAAQS Modeled High |
|-------------------|------------------|----------------------------------|----------------------------------|
| NO | Annual | 1st highest | 1st highest |
| NO_2 | 1-hour | 5-year average 1st high hour day | 5-year average 8th high hour day |
| 60 | 8-hour | 1st highest | High 2nd highest |
| СО | 1-hour | 1st highest | High 2nd highest |
| D) (| Annual | 1st highest | NA |
| PM_{10} | 24-hour | 1st highest | 6th highest in 5 years |
| DM | Annual | 5-year average year | 5-year average year |
| PM _{2.5} | 24-hour | 5-year average 1st high day | 5-year average 8th high day |

Source: WDNR, Wisconsin Air Dispersion Modeling Guidelines, 2018

⁽a) The PM_{2.5} 24-hour significant monitoring concentration vacated by the United States Court of Appeals for the District of Columbia Circuit on January 22, 2013, is not considered valid in Wisconsin. However, representative local monitoring data is available for use.

⁽b) EPA Memorandum, 2018a, "Guidance on Significant Impact Levels for Ozone and Fine Particles in the Prevention of Significant Deterioration Permitting Program."

6.4.9 PM_{2.5} Significant Impact Level Justification

The United States Court of Appeals for the District of Columbia Circuit on January 22, 2013, vacated and remanded portions of the EPA rule establishing significant impact levels for PM_{2.5}. An analysis was performed to determine whether the vacated PM_{2.5} significant impact levels are justified for this area.

The data that is collected by the monitors is available on the EPA website (http://www.epa.gov/airdata/). The most representative monitor for the 24-hour and annual PM_{2.5} background concentrations is a monitor located at 720 North Central Avenue in Duluth, Minnesota (Air Quality System [AQS] ID: 27-137-7554). This is the closest operating PM_{2.5} monitor and is most representative of the site. This monitor is located approximately 9 kilometers northwest from the Project site. The difference between the representative monitor value and the NAAQS standard (for both the 24-hour and annual standards) is sufficiently greater than the PM_{2.5} significant impact level. Therefore, the use of PM_{2.5} significant impact level is justified for this area, as demonstrated in Table 6-7.

| Dovomatav | PM _{2.5} 24-Hour Average | PM _{2.5} Annual Average | |
|--|------------------------------------|----------------------------------|--|
| Parameter | micrograms per cubic meter (µg/m³) | | |
| 2018-2020 design value ¹ | 16.0 | 5.3 | |
| NAAQS ² | 35.0 | 12.0 | |
| Difference NAAQS minus design value | 19.0 | 6.7 | |
| PSD Class II significant impact level ³ | 1.2 | 0.2 | |

Table 6-7: Duluth PM_{2.5} Monitor (AQS ID: 27-137-7554)

Source:

6.4.10 Ambient Monitoring

The modeling analysis for emission sources for the Project will also address the pre-construction monitoring provision of the PSD regulations (EPA 1987). The regulations specify monitoring *de minimis* levels for each PSD pollutant that, if exceeded, trigger the requirement to perform 1 year of pre-construction ambient air monitoring. If any predicted concentrations reach or exceed the monitoring *de minimis* levels, the Owners will consult with the WDNR to determine if pre-construction ambient air monitoring will be required. If modeled values exceed their respective monitoring *de minimis* values, the Owners will request a waiver to use local ambient monitoring data to fulfill the pre-construction monitoring provisions of the PSD regulations or develop an acceptable monitoring plan at that time. For any impacts predicted to be below the monitoring *de minimis* levels, the Owners will request an

⁽¹⁾ EPA, http://www.epa.gov/airdata/, accessed 2021

⁽²⁾ Title 40 CFR Part 50

⁽³⁾ EPA Memorandum, 2018a, "Guidance on Significant Impact Levels for Ozone and Fine Particles in the Prevention of Significant Deterioration Permitting Program."

exemption from pre-construction ambient air monitoring, given that representative monitors in the area may be used for appropriate background concentrations.

6.4.11 NAAQS and PSD Class II Increment Analysis

When the maximum impacts exceed the significant impact level for any pollutant and averaging time, then a refined modeling analysis is required. The inventories of sources within the radius of impact were developed in accordance with applicable EPA guidance and obtained from the WDNR and Minnesota Pollution Control Agency. For the NAAQS and PSD Class II Increment analysis, all stationary sources identified by WDNR and Minnesota Pollution Control Agency that emit pollutants subject to this analysis and are located within the radius of impact were addressed.

Background air quality concentrations (as described in Section 6.4.12) were added to model-predicted concentrations for comparison to the NAAQS. If the refined analysis does not result in any concentrations above the NAAQS or PSD Class II Increments, no further modeling was conducted.

6.4.12 Background Air Quality

As stated previously, if any pollutant exceeds its respective PSD significance level, a refined analysis (cumulative analysis) was performed for that pollutant and averaging period. The analysis was used to determine compliance with the PSD Class II Increments and the NAAQS. The NAAQS are set up to protect the air quality for all sensitive populations, and attainment is determined by the comparison to the NAAQS thresholds. As such, there are existing concentrations of each criteria pollutant that are present in ambient air that must be included in an analysis to account for items, such as mobile source emissions, that are not already accounted for in the model. Monitored ambient emission levels were added to the modeled ground level impacts to account for these sources.

Regional background values were obtained from the WDNR *Guidance on Background Concentrations* memo (WDNR, 2021) that lists values for both "low" and "high" background categories. The Project is located in an area categorized as a "high" background area; therefore, the "high" background values were used for each pollutant that requires a refined analysis. The values listed in Table 6-8 were used as background levels and were added to the modeled impacts for each pollutant if NAAQS modeling is required.

| Pollutant | Averaging Period | Background Concentration (micrograms per cubic meter) | |
|------------|------------------|---|--|
| NO | Annual | HROFDY & MONTH ^a | |
| NO_2 | 1-hour | HROFDY & MONTH ^a | |
| CO | 8-hour | 916.8 | |
| CO | 1-hour | 1,196.0 | |
| PM_{10} | 24-hour | 33.1 | |
| DM | Annual | 8.0 | |
| $PM_{2.5}$ | 24-hour | 20.8 | |

Table 6-8: Background Concentrations

Source: WDNR, Guidance on Air Quality Background Concentrations, 2021

(a) Hour of day and monthly values are provided in the WDNR background guidance memo

6.4.13 NO₂ Modeling – Multi-Tiered Screening Approach

The AERMOD model gives the emission results for all pollutants, including NO_x. However, impacts of NO₂ must be examined for comparison to the NAAQS, PSD Class II Increments, and significance values. The EPA has a three-tier approach to modeling NO₂ concentrations:

- Tier I total conversion, or all $NO_x = NO_2$
- Tier II use a default NO₂/NO_x ratio
- Tier III case-by-case detailed screening methods, such as the Ozone Limiting Method (OLM) or Plume Volume Molar Ratio Method (PVMRM)

Tier II of the Ambient Ratio Method (ARM2) uses a minimum and maximum ratio that varies based on the modeled level of NO_x . For the 1-hour modeled results, the default minimum and maximum ratios of 0.5 and 0.9, respectively, were applied to determine the predicted ground-level concentration of NO_2 . For the annual modeled results, NO_x was assumed to be equal to NO_2 (Tier I).

6.5 Significance Model Results

Significance modeling was performed for NO₂, CO, PM₁₀, PM_{2.5}, and SO₂ for the appropriate emission sources. The modeled impacts are shown in Table 6-9 below.

| Pollutant ' | Averaging | | | Year | Predicted Concentration | Modeling Significance Level ¹ | Monitoring De Minimis Level ² |
|-------------------|-----------|------------------|----------------------|---------|------------------------------------|--|--|
| | Period | Easting (meters) | Northing (meters) | | micrograms per cubic meter (µg/m³) | | |
| NO | Annual | 572,555.5 | 5,170,865.2 | 2016 | 2.9 | 1 | 14 |
| NO_2 | 1-hour | 568,000.0 | 5,183,000.0 | 5 years | 162.5 ^b | 7.5 | NA |
| СО | 8-hour | 572,900.0 | 5,171,475.0 | 2015 | 2,329.7 | 500 | 575 |
| | 1-hour | 573,025.0 | 5,171,450.0 | 2015 | 5,252.7 | 2,000 | NA |
| DM | Annual | 572,769.1 | 5,171,086.5 | 2018 | 7.0 | 1 | NA |
| PM_{10} | 24-hour | 572,808.9 | 5,171,122.0 | 2020 | 25.8 | 5 | 10 |
| DM | Annual | 572,791.2 | 5,171,106.1 | 2015 | 0.61° | 0.2e | NA |
| PM _{2.5} | 24-hour | 572,300.0 | 5,170,725.0 | 2018 | 6.5 ^d | 1.2e | 4 ^f |

Table 6-9: Maximum Modeled Concentrations for Significance Modeling.

Sources: WDNR, Wisconsin Air Dispersion Modeling Guidelines, 2018

6.5.1 NO₂ Significance Results

After examining the modeling results, it was determined that exceedances of the annual and 1-hour NO₂ modeling significance level occurred, and that refined modeling will be required. The annual predicted impacts were lower than the ambient air monitoring *de minimis* level and therefore no pre-construction ambient monitoring is proposed for NO₂.

6.5.2 CO Significance Results

After examining the modeling results, it was determined that exceedances of the 8-hour or 1-hour CO modeling significance level occurred, and that refined modeling will be required. The 8-hour predicted impacts were greater than the ambient air monitoring *de minimis* level and therefore pre-construction ambient monitoring must be considered for CO. The Owners request that existing monitoring data from the Anoka County Airport monitor located in Blaine, Minnesota (AQS ID: 27-003-1002) be used for existing ambient levels of CO in the area.

⁽a) UTM = Universal Transverse Mercator: NAD83.

⁽b) ARM2 methodology was applied to the model.

⁽c) Impact represents primary and secondary annual PM_{2.5} (0.6 μ g/m³+ 0.01 μ g/m³)

⁽d) Impact represents primary and secondary 24-hour PM_{2.5} (6.3 μ g/m³+ 0.19 μ g/m³)

⁽e) EPA Memorandum, 2018a, "Guidance on Significant Impact Levels for Ozone and Fine Particles in the Prevention of Significant Deterioration Permitting Program."

⁽f) The PM_{2.5} 24-hour significant monitoring concentration vacated by the United States Court of Appeals for the District of Columbia Circuit on January 22, 2013, is not considered valid in Wisconsin. However, representative local monitoring data is available for use.

6.5.3 PM₁₀/PM_{2.5} Significance Results

After examining the modeling results, it was determined that exceedances of the 24-hour and annual PM₁₀ and 24-hour and annual PM_{2.5} modeling significance level occurred, and that refined modeling will be required.

The 24-hour predicted impacts were greater than the PM_{2.5} ambient air monitoring *de minimis* levels and therefore pre-construction ambient monitoring must be considered for PM_{2.5}. The Owners request that existing monitoring data from the 720 North Central Avenue monitor located in Duluth, Minnesota (AQS ID: 27-137-7554) be used for existing ambient levels of PM_{2.5} in the area.

The 24-hour predicted impacts were greater than the PM₁₀ ambient air monitoring *de minimis* levels and therefore pre-construction ambient monitoring must be considered for PM₁₀. The Owners request that existing monitoring data from the 37th Avenue West and Oneota Street monitor located in Duluth, Minnesota (AQS ID: 27-137-0032) be used for existing ambient levels of PM₁₀ in the area.

6.6 PSD Class II Increment Modeling

Refined modeling was performed for NO₂, PM₁₀, and PM_{2.5} to demonstrate compliance with the PSD Class II Increments.

All Project emission sources and all inventory sources (provided by WDNR and Minnesota Pollution Control Agency) were included in the modeling analysis.

There were no modeled PSD Class II Increment exceedances for NO₂, PM₁₀, and PM_{2.5} as shown in Table 6-10. Therefore, the Project will be in compliance with the Class II PSD Increment.

UTM Coordinates^a **PSD Class II Predicted** Averaging Concentration Increment **Pollutant** Year Easting **Northing Period** micrograms per cubic meter (meters) (meters) $(\mu g/m^3)$ 2017 NO_2 Annual 570,600.0 5,170,800.0 25 8.4 2018 17 Annual 572,769.1 5,171,086.5 7.1 PM_{10} 24-hour 30 2020 572,808.9 5,171,122.0 23.9 2015 4 Annual 572,791.2 $0.61^{\rm b}$ 5,171,106.1 $PM_{2.5}$ 24-hour 9 573,300.0 2017 5.3° 5,171,050.0

Table 6-10: Maximum Modeled Concentrations for Increment Modeling

Source: Title 40 CFR 52.21(c).

(a) UTM = Universal Transverse Mercator: NAD83

⁽b) Impact represents primary and secondary annual PM_{2.5} (0.60 $\mu g/m^3 + 0.01 \ \mu g/m^3$)

⁽c) Impact represents primary and secondary 24-hour PM_{2.5} (5.1 μ g/m³+ 0.19 μ g/m³)

6.7 NAAQS Modeling

Refined modeling was performed for NO₂, CO, PM₁₀, and PM_{2.5} for all Project emission sources and all inventory sources (provided by WDNR and Minnesota Pollution Control Agency).

The modeling results showed that the Project will not contribute to any NAAQS exceedance for the pollutants and averaging periods modeled. Therefore, the Project will be in compliance with the NAAQS. The NAAQS analysis modeling results are shown in Table 6-11.

UTM Coordinates^a **Predicted Background** Total **NAAQS** Pollutant and Concentration Concentration Concentration Year **Easting** Northing **Averaging Period** (meters) (meters) micrograms per cubic meter (µg/m³) __b Annual 570,600.0 5,170,800.0 2016 52.5 100 NO_2 1-hour 571,500.0 __b __b 181.9c 5,186,000.0 5 years 188 8-hour 573,300.0 5,171,075.0 2017 1,903.3 916.8 2,820.13 10,000 CO 572,875.0 1-hour 2015 4,954.9 1,196.0 6,150.93 40,000 5,171,525.0 PM_{10} 24-hour 572,808.9 5,171,122.0 2015 19.7 33.1 52.8 150 570,000.0 0.93^{d} 8.0 8.93 Annual 5,175,250.0 5 years 12 $PM_{2.5}$ 24-hour 570,000.0 5.3e 20.8 35 5,175,250.0 5 years 26.1

Table 6-11: Maximum Modeled Concentrations for NAAQS Modeling

Source: Title 40 CFR Part 50

6.8 PSD Class I Increment Screening Analysis

Under the PSD program, Class I areas are protected more stringently than under the NAAQS. Class I areas include national parks, wilderness areas, and other areas of special national and cultural significance.

There are four Class I areas that are within 300 kilometers of the Nemadji River Site

- Rainbow Lake Wilderness, Wisconsin (60 kilometers)
- Boundary Waters Canoe Area Wilderness, Minnesota (126 kilometers)
- Voyageurs National Park, Minnesota (182 kilometers)
- Isle Royale National Park, Michigan (237 kilometers)

⁽a) UTM = Universal Transverse Mercator: NAD83

⁽b) HROFDY & MONTH background data used; therefore, the modeled impact is presented as project impacts and background combined.

⁽c) ARM2 methodology was applied to the model.

⁽d) Impact represents primary and secondary annual PM_{2.5} (0.92 μg/m³+ 0.01 μg/m³)

⁽e) Impact represents primary and secondary 24-hour $PM_{2.5}$ (5.1 $\mu g/m^3 + 0.19 \mu g/m^3$)

There is also one non-Federal Class I area that is within 300 kilometers of the Project, Forest County Potawatomi Community Reservation, Wisconsin (261 kilometers).

Areas that have submitted requests to change the air quality status from Class II to Class I but whose request has yet to be granted were not evaluated for this Project.

The locations of the Project site and the Class I areas are shown in Figure B-5, Appendix B.

An assessment of air quality impacts at Class I areas was performed to demonstrate that the operation of the Project will not result in, or contribute to, concentrations above the PSD Class I Increment threshold. A screening analysis to determine if further analysis is required was performed for the four Class I areas and one non-Federal Class I area. The Class I Increment screening will be analyzed with AERMOD at a 50-kilometer distance from the Project by placing an arc of receptors extending 45 degrees (+/-) from the line connecting the Project and the Class I area. One Class I screening model that combined all Class I receptor arcs into one receptor grid was run for this analysis.

The AERMOD modeled impacts in comparison to the Class I significance thresholds are shown in Table 6-12. Based on the analysis, it was determined that the impacts from the Project will not significantly impact the PSD Class I Increment at the surrounding Class I areas and does not require further analysis.

Table 6-12: Class I Modeled Screening Impacts and Class I Significant Impact Level

| Pollutant | Averaging Time | Maximum Modeled Concentration | Class I Significant Impact Level ¹ | | |
|------------------------------|-------------------|------------------------------------|---|--|--|
| | | micrograms per cubic meter (µg/m³) | | | |
| NO ₂ ^a | Annual | 0.03 | 0.1 | | |
| DM | 24-hour | 0.3 | 0.3 | | |
| PM_{10} | Annual | 0.02 | 0.2 | | |
| PM _{2.5} | 24-hour | 0.27 ^b | 0.27^{2} | | |
| F 1 V1 2.5 | Annual | 0.02° | 0.05^{2} | | |

Sources:

⁽¹⁾ EPA. Prevention of Significant Deterioration (PSD) and Nonattainment New Source Review (NSR) Proposed Rulemaking, July 23, 1996. (61 FR 38249).

⁽²⁾ EPA Memorandum, 2018a, "Guidance on Significant Impact Levels for Ozone and Fine Particles in the Prevention of Significant Deterioration Permitting Program."

⁽a) Modeled as NO_x.

⁽b) Impact represents primary and secondary 24-hour PM_{2.5} (0.265 μ g/m³ + 0.0127 μ g/m³)

⁽c) Impact represents primary and secondary annual $PM_{2.5}$ (0.02 $\mu g/m^3 + 0.0006 \mu g/m^3$)

6.9 Secondary Formation Analysis

An analysis of the impact of secondary formation of ozone (NO_x and VOC) and PM_{2.5} (NO_x and SO₂) was performed. The NAAQS and modeling significance level threshold for ozone and PM_{2.5} are shown in Table 6-13.

| Pollutant | Averaging Period | Modeling Significance Level ^{1,a} | NAAQS ^{2,a} |
|-------------------|---------------------|---|----------------------|
| Ozone | 8-hour | 1.0 ppb | 0.07 ppm (70 ppb) |
| DM | Annual | $0.2 \ \mu g/m^3$ | 12 μg/m ³ |
| PM _{2.5} | 24-hour | $1.2 \ \mu g/m^3$ | $35 \mu g/m^3$ |

Table 6-13: NAAQS and Modeling Significance Levels

Source:

In April 2019, the EPA provided *Guidance on the Development of Modeled Emission Rates for Precursors (MERPS) as a Tier I Demonstration Tool for Ozone and PM_{2.5} under the PSD Permitting Program* (the Guidance) in final form. The MERPS methodology was used to satisfy the compliance demonstration requirements for both ozone and secondary PM_{2.5} for PSD purposes. The Tier 1 assessment in the Guidance uses existing empirical relationships between precursors and secondary impacts based on modeling performed by the EPA. MERPs were used to describe an emission rate of a precursor that is expected to result in a change in ambient ozone or PM_{2.5} that would be less than a specific air quality concentration threshold for ozone or PM_{2.5} to determine whether an impact causes or contributes to a violation of the NAAQS for ozone or PM_{2.5}.

6.9.1 Secondary PM_{2.5} Formation Analysis

The NO_x (269.0 tons per year) emissions from the Project are below the lowest MERP values for the daily and annual PM_{2.5} from the NO_x precursor for the Upper Midwest climate zone shown in Table 4-1 of the Guidance. The SO₂ (29.0 tons per year) emissions from the Project are below the lowest MERP value for the daily and annual PM_{2.5} from the SO₂ precursor for the Upper Midwest climate zone shown in Table 4-1 of the Guidance. Based on these comparisons it was determined that it was appropriate to use the Upper Midwest climate zone data for the PM_{2.5} significant impact level, Class II Increment, and NAAQS analysis.

⁽¹⁾ EPA Memorandum, 2018, "Guidance on Significant Impact Levels for Ozone and Fine Particles in the Prevention of Significant Deterioration Permitting Program."

⁽²⁾ Title 40 CFR Part 50.

⁽a) ppb = parts per billion; ppm = parts per million; micrograms per cubic meter = $\mu g/m^3$.

For the Class I Increment analysis it was determined that it was more appropriate to use a specific hypothetical source in the same region and geographic area for comparison. Therefore, an analysis was performed to determine the most relevant hypothetical source.

Next, the NO_x and SO₂ precursor contributions to the daily and annual average PM_{2.5} were considered together to determine if the Project's air quality impact of PM_{2.5} would exceed the PM_{2.5} significant impact level, Class II Increment, Class I Increment, and NAAQS.

6.9.1.1 Daily PM_{2.5} Source Impact Analysis (µg/m³)

The secondary $PM_{2.5}$ impacts were expressed in $\mu g/m^3$ to add to the primary $PM_{2.5}$ AERMOD results to obtain the overall $PM_{2.5}$ impacts. Using the Project emissions and Upper Midwest air quality impact information the source nitrate and sulfate daily impact is calculated as follows:

Nitrate Impact =
$$\left(1.2 \frac{\mu g}{m3} * \frac{269.0 \text{ tpy}}{2.963 \text{ tpy}}\right) = 0.11 \frac{\mu g}{m3}$$

Sulfate Impact =
$$\left(1.2 \frac{\mu g}{m3} * \frac{29.0 \text{ tpy}}{454 \text{ tpy}}\right) = 0.08 \frac{\mu g}{m3}$$

Therefore, the total daily secondary PM_{2.5} impact is:

Total Daily Secondary PM2.5 Impact =
$$\left(0.11 \frac{\mu g}{m_3} + 0.08 \frac{\mu g}{m_3}\right) = 0.19 \frac{\mu g}{m_3}$$

6.9.1.1.1 Daily PM_{2.5} – Class II Significant Impact Level

When the Project source primary impact (from AERMOD) and daily secondary impacts (from MERP equation) are added together the total impacts are greater than the daily $PM_{2.5}$ Class II significant impact level value of $1.2 \mu g/m^3$ as shown below.

Primary PM2.5 Impact + Secondary PM2.5 Impact =
$$\left(6.3 \frac{\mu g}{m3} + 0.19 \frac{\mu g}{m3}\right) = 6.5 \frac{\mu g}{m3}$$

6.9.1.1.2 Daily PM_{2.5} – Class II Increment

When the Project source primary impact (from AERMOD) and daily secondary impacts (from MERP equation) are added together the total impacts are less than the daily $PM_{2.5}$ Class II Increment value of 9.0 $\mu g/m^3$ as shown below.

Primary PM2.5 Impact + Secondary PM2.5 Impact =
$$\left(5.1 \frac{\mu g}{m3} + 0.19 \frac{\mu g}{m3}\right) = 5.3 \frac{\mu g}{m3}$$

6.9.1.1.3 Daily PM_{2.5} - NAAQS

When the Project source primary impact (from AERMOD), background value, and daily secondary impacts (from MERP equation) are added together the total impacts are less than the daily $PM_{2.5}$ NAAQS value of 35 $\mu g/m^3$ as shown below.

Primary PM2.5 Impact + background + Secondary PM2.5 Impact =
$$\left(5.1 \frac{\mu g}{m3} + 20.8 \frac{\mu g}{m3} + 0.19 \frac{\mu g}{m3}\right) = 26.1 \frac{\mu g}{m3}$$

6.9.1.2 Annual PM_{2.5} Source Impact Analysis (μg/m³) – Class II Significant Impact Level

The secondary $PM_{2.5}$ impacts were expressed in $\mu g/m^3$ to add to the primary $PM_{2.5}$ AERMOD results to obtain the overall $PM_{2.5}$ impacts. Using the Project emissions and Upper Midwest air quality impact information the annual source nitrate and sulfate impact is calculated as follows:

Nitrate Impact =
$$\left(0.2 \frac{\mu g}{m3} * \frac{269.0 \text{ tpy}}{10,011 \text{ tpy}}\right) = 0.01 \frac{\mu g}{m3}$$

Sulfate Impact =
$$\left(0.2 \frac{\mu g}{m3} * \frac{29.0 \text{ tpy}}{2,522 \text{ tpy}}\right) = 0.002 \frac{\mu g}{m3}$$

Therefore, the total annual secondary PM_{2.5} impact is:

Total Annual Secondary PM2.5 Impact =
$$\left(0.01 \frac{\mu g}{m3} + 0.002 \frac{\mu g}{m3}\right) = 0.01 \frac{\mu g}{m3}$$

6.9.1.2.1 Annual PM_{2.5} – Class II Significant Impact Level

When the Project source primary impact (from AERMOD) and secondary impacts (from MERP equation) are added together the total impacts are greater than annual $PM_{2.5}$ Class II significant impact level value of $0.2 \mu g/m^3$ as shown below.

Primary PM2.5 Impact + Secondary PM2.5 Impact =
$$\left(0.60 \frac{\mu g}{m3} + 0.01 \frac{\mu g}{m3}\right) = 0.61 \frac{\mu g}{m3}$$

6.9.1.2.2 Annual PM_{2.5} – Class II Increment

When the Project source primary impact (from AERMOD) and annual secondary impacts (from MERP equation) are added together the total impacts are less than the annual $PM_{2.5}$ Class II Increment value of $4.0 \mu g/m^3$ as shown below.

$$Primary\ PM2.5\ Impact + Secondary\ PM2.5\ Impact = \left(0.60\ \frac{\mu g}{m3} +\ 0.01\ \frac{\mu g}{m3}\right) = 0.61\ \frac{\mu g}{m3}$$

6.9.1.2.3 Annual PM_{2.5} – NAAQS

When the Project source primary impact (from AERMOD), background value, and annual secondary impacts (from MERP equation) are added together the total impacts are less than the annual $PM_{2.5}$ NAAQS value of 12 $\mu g/m^3$ as shown below. Further analysis demonstrated that cumulative impacts from all NSG sources are less than the significant impact level for all modeled NAAQS exceedances.

$$Primary\ PM2.5\ Impact + background + Secondary\ PM2.5\ Impact = \left(0.92\ \frac{\mu g}{m3} + 8.0\ \frac{\mu g}{m3} + \ 0.01\ \frac{\mu g}{m3}\right) = 8.93\ \frac{\mu g}{m3}$$

6.9.1.3 Class I Daily and Annual PM_{2.5}

For the Class I analysis it was determined that it was more appropriate to use a specific hypothetical source in the same region and geographic area for comparison. Therefore, an analysis was performed to determine the most relevant hypothetical source.

6.9.1.3.1 Hypothetical PM_{2.5} Source Impact Analysis

The Project is not located in an area with complex terrain and is not located close to large sources of pollutants that would impact atmospheric chemistry or meteorology (predominately rural area). Nearby hypothetical sources located in Wisconsin and Minnesota were identified and are shown in Table 6-14. According to the distance analysis, the closest hypothetical source is the St. Louis County source (137.8 kilometers away). The St. Louis County source surrounding terrain is representative of the Project site and the source is in a rural area similar to the Project location. A review of the data indicates that the St. Louis County source is representative of this Project.

Distance from Max Nearby Max Nearby **Project Site** County County Terrain (meters) Urban (%) (kilometers) St Louis 431 Minnesota 2.8 137.8 Wisconsin 410 2.3 Rusk 156.5 Dakota Minnesota 292 52.4 233.3 Wadena Minnesota 420 2.2 234.5 Wisconsin 237 32.2 Shawano 365.5

Table 6-14: Hypothetical Source Review

Source: EPA MERPS View Qlik (Accessed October 2021)

Table 6-15 lists the values for the St. Louis County source for the respective emission rates and stack height combination. Project SO_2 and NO_x emissions are each less than 500 tons per year; therefore, the

hypothetical 500 ton per year source was selected. Most of the emissions from project are emitted from a stack height above 50 meters; therefore, the 90-meter stack source was selected. These values were used to calculate the additive secondary impacts for Class I PSD Increment daily and annual PM_{2.5}.

| Metric | Emissions (tons per year) | Stack Height (meters) | Distance (kilometers) ^a | Concentration (µg/m³) ^b |
|--|------------------------------|-----------------------------|---------------------------------------|---------------------------------------|
| Annual PM _{2.5} SO ₂ | 500 | 90 | 60 | 0.003108 |
| Daily PM _{2.5} SO ₂ | 500 | 90 | 60 | 0.0812 |
| Annual PM _{2.5} NO _x | 500 | 90 | 60 | 0.00071 |
| Daily PM _{2.5} NO _x | 500 | 90 | 60 | 0.0149 |

Table 6-15: Hypothetical St. Louis County Source Table Values

Source: EPA MERPS View Qlik (Accessed November 2021)

6.9.1.3.2 Daily Class I PM_{2.5} Source Impact Analysis (µg/m³)

The secondary $PM_{2.5}$ impacts were expressed in $\mu g/m^3$ to add to the primary $PM_{2.5}$ AERMOD results to obtain the overall $PM_{2.5}$ impacts. Using the Project emissions and air quality impact information from St. Louis County Source the source nitrate and sulfate daily impact is calculated as follows:

Nitrate Impact =
$$\left(269.0 \text{ tpy} * \frac{0.0149 \frac{\mu g}{m3}}{500 \text{ tpy}}\right) = 0.0080 \frac{\mu g}{m3}$$

Sulfate Impact =
$$\left(29.0 \text{ tpy} * \frac{0.0812 \frac{\mu g}{m3}}{500 \text{ tpy}}\right) = 0.0047 \frac{\mu g}{m3}$$

Therefore, the total daily secondary PM_{2.5} impact is:

Total Daily Secondary PM2.5 Impact =
$$\left(0.0080 \frac{\mu g}{m3} + 0.0047 \frac{\mu g}{m3}\right) = 0.0127 \frac{\mu g}{m3}$$

6.9.1.3.3 Daily PM_{2.5} – Class I Increment

When the Project source primary impact (from AERMOD) and daily secondary impacts (from MERP equation) are added together the total impacts are less than the daily $PM_{2.5}$ Class I Increment value of 0.27 $\mu g/m^3$ as shown below.

Primary PM2.5 Impact + Secondary PM2.5 Impact =
$$\left(0.265 \frac{\mu g}{m3} + 0.0127 \frac{\mu g}{m3}\right) = 0.278 \frac{\mu g}{m3}$$

⁽a) The analysis was performed using the distance values associated to the nearest Class I area (most conservative), since Rainbow Lake Wilderness is located 60 kilometers from the Project.

⁽b) $\mu g/m^3 = micrograms per cubic meter$

6.9.1.3.4 Annual Class I PM_{2.5} Source Impact Analysis (μg/m³)

Using the Project emissions and air quality impact information from St. Louis County Source the source nitrate and sulfate annual impact is calculated as follows:

Nitrate Impact =
$$\left(269.0 \text{ tpy} * \frac{0.00071 \frac{\mu g}{m3}}{500 \text{ tpy}}\right) = 0.0004 \frac{\mu g}{m3}$$

Sulfate Impact =
$$\left(29.0 \text{ tpy} * \frac{0.003108 \frac{\mu g}{m3}}{500 \text{ tpy}}\right) = 0.0002 \frac{\mu g}{m3}$$

Therefore, the total annual secondary PM_{2.5} impact is:

Total Annual Secondary PM2.5 Impact =
$$\left(0.0004 \frac{\mu g}{m3} + 0.0002 \frac{\mu g}{m3}\right) = 0.0006 \frac{\mu g}{m3}$$

6.9.1.3.5 Annual PM_{2.5} – Class I Increment

When the Project source primary impact (from AERMOD) and annual secondary impacts (from MERP equation) are added together the total impacts are less than the annual $PM_{2.5}$ Class I Increment value of $0.05 \mu g/m^3$ as shown below.

Primary PM2.5 Impact + Secondary PM2.5 Impact =
$$\left(0.02 \frac{\mu g}{m3} + 0.0006 \frac{\mu g}{m3}\right) = 0.02 \frac{\mu g}{m3}$$

6.9.2 Secondary Ozone Formation Analysis

The NO_x (269.0 tons per year) emissions from the Project are greater than the lowest MERP values for 8-hour ozone from NO_x for the Upper Midwest climate zone shown in Table 4-1 of the Guidance. The VOC (250.0 tons per year) emissions from the Project are less than the lowest MERP value for the 8-hour ozone from VOC for the Upper Midwest climate zone shown in Table 4-1 of the Guidance. Therefore, air quality impacts from the Project would be expected to be greater than the critical air quality threshold (CAQT).

The NO_x and VOC precursor contributions to the 8-hour daily maximum ozone need to be considered together to determine if the Project's air quality impact would exceed the CAQT. The additive secondary impacts on 8-hour daily maximum ozone is calculated as follows:

$$\left(\frac{269.0 \ tpy \ NOx}{125 \ tpy \ NOx \ 8hr \ daily \ max}\right) + \left(\frac{250.0 \ tpy \ VOC}{1,560 \ tpy \ VOC \ 8hr \ daily \ max}\right) = 2.15 + 0.16 = 2.31 * 100 = 231\%$$

$$O_3 \ MERP$$

A value greater than 100 percent indicates that the CAQT will be exceeded when considering the combined impacts of these precursors on 8-hour daily maximum ozone; therefore, comparable hypothetical sources were identified to determine the additive secondary impacts on 8-hour daily maximum ozone.

The Project is not located in an area with complex terrain and is not located close to large sources of pollutants that would impact atmospheric chemistry or meteorology (predominately rural area). Nearby hypothetical sources located in the Upper Midwest region were identified. According to the distance analysis, the closest hypothetical source is located in St. Louis County (137.8 kilometers away). The terrain surrounding the St. Louis County source is somewhat representative of the Project site and the source is located in a rural area similar to the Project location. A review of the data indicates that the St. Louis County source is representative of this Project.

Table 6-16 lists the EPA MERPS View Qlik values for the St. Louis County source for the respective emission rates and stack height combination. These values were used to calculate the additive secondary impacts for ozone.

Stack **Emissions** Height **MERP** Metric (tons per year) (meters) (tons per year) 90 Daily ozone NO_x 500 437.0 Daily ozone VOC 500 10^{a} 6.036.0

Table 6-16: Hypothetical Source St. Louis County Values

Source: EPA MERPS View Qlik (Accessed November 2021)

(a) No 90 meter stack data was available; therefore, 10 meter stack data was selected.

The NO_x and VOC precursor contributions to the 8-hour daily maximum ozone were considered together to determine if the Project's air quality impact would exceed the CAQT.

$$NOx\ Impact = \left(1\ ppb * \frac{269.0\ tpy}{437.0\ tpy}\right) = 0.62\ ppb$$

VOC Impact =
$$\left(1 \ ppb * \frac{250.0 \ tpy}{6,036.0 \ tpy}\right) = 0.041 \ ppb$$

The additive secondary impacts on 8-hour daily maximum ozone is calculated as follows:

$$0.61 \ ppb + 0.042 \ ppb = 0.66 \ ppb$$

A value less than the ozone significant impact level value of 1 parts per billion (ppb) indicates that the CAQT will not be exceeded when considering the combined impacts of these precursors on 8-hour daily maximum ozone.

6.10 Dispersion Modeling Conclusion

The modeling results shown in Table 6-9 demonstrate that exceedances of NO_x, CO, PM₁₀, and PM_{2.5}. modeling significance levels occurred and refined modeling is required. A refined modeling analysis was conducted to demonstrate compliance with the PSD Class II Increment and NAAQS for NO_x, CO, PM₁₀, and PM_{2.5}. The Project will not cause or contribute to any modeled Class II PSD Increment or NAAQS exceedances.

Based on the Class I analysis, it was determined that the impacts from the Project will not significantly impact the four Class I area and one non-Federal Class I area that are within 300 kilometers of the Project and does not require further analysis.

The operation of the Project will not cause or contribute to a significant degradation of ambient air quality. After examining the results of the model, it has been determined that the modeling requirements for PM₁₀, PM_{2.5}, CO, and NO₂ have been fulfilled, and no further modeling is required.

7.0 ADDITIONAL IMPACTS ANALYSIS

Section 7 overview: The references to the most current additional impacts sections are presented in Table 7-1. The model values presented in this section have been updated to reflect the latest modeling analysis.

Table 7-1: Additional Impacts Section References

| Report Heading | Previous Application Reference | December 2021 Submittal Location |
|--|---|-------------------------------------|
| Construction Impacts | Section 7.1 January 2021 Submittal | Section 7.1 |
| Vegetation Impacts | Section 7.2 January 2021 Submittal | Section 7.2 |
| Carbon Monoxide | Section 7.2.1 December 2018 Submittal | Section 7.2.1 |
| Carbon Dioxide | Section 7.2.1 January 2021 Submittal | Section 7.2.2 |
| Nitrogen Oxides | Section 7.2.3 December 2018 Submittal | Section 7.2.3 |
| Particulate Matter | Section 7.2.3 January 2021 Submittal | Section 7.2.4 |
| Synergistic Effects of Pollutants | Section 7.2.5 December 2018 Submittal | Section 7.2.5 |
| Sulfuric Acid Mist | Section 7.2.6 December 2018 Submittal | Section 7.2.6 |
| Volatile Organic Compounds | Section 7.2.2 January 2021 Submittal | Section 7.2.7 |
| Soil Impacts | Section 7.3 January 2021 Submittal | Section 7.3 |
| Industrial, Residential, and Commercial Growth Impacts | Section 7.4 January 2021 Submittal | Section 7.4 |
| Visibility and Deposition Analysis | Section 7.5 January 2021 Submittal | Section 7.5 |
| Class I Area Analysis | Section 7.5.1 January 2021 Submittal | Section 7.5.1 |
| Class II Area Analysis | Section 7.5.2 January 2021 Submittal | Section 7.5.2 |
| Conclusion | Section 7.6 January 2021 Submittal | Section 7.6 |

The additional impacts analysis requirement under PSD includes the ambient air quality impact analysis, soils and vegetation impacts, visibility impairment, and growth analysis for the Project.

7.1 Construction Impacts

Construction for the Project has the potential for short-term adverse effects on air quality in the immediate area around the site and will not affect the attainment status for Douglas County. Diesel fumes from

construction vehicles and dust from site preparation and construction vehicle operation can affect local air quality during certain meteorological conditions. However, these instances are limited in time and area of effect.

Low sulfur fuel will be used for construction vehicles that use diesel fuel. Operation of these vehicles is not expected to significantly affect ambient air quality. During prolonged periods without rainfall, fugitive construction-related dust may need to be minimized through the application of water to onsite roads used by construction equipment.

7.2 Vegetation Impacts

The following sections briefly describe the potential effects of CO, CO₂, NO₂, PM/PM₁₀/PM_{2.5}, H₂SO₄ mist, VOC, and synergistic effects of pollutants produced by the installation of the Project on the nearby vegetation. The potential effects of the air emissions on vegetation within the immediate vicinity of the Project were compared to scientific research examining the effects of pollution on vegetation. Damage to vegetation often results from acute exposure to pollution but may also occur after prolonged or chronic exposures. Acute exposures are typically manifested by internal physical damage to leaf tissues, while chronic exposures are associated with the inhibition of physiological processes such as photosynthesis, carbon allocation, and stomatal functioning (Hallgren, 1984; Hill and Littlefield, 1969; Mansfield and Freer-Smith,1984).

7.2.1 Carbon Monoxide

CO is not known to injure plants nor has it been shown to be taken up by plants. Consequently, no adverse impacts to vegetation at or near the Project are expected from CO stack emissions from the Project.

7.2.2 Carbon Dioxide

CO₂ is not known to injure plants. Long-term exposure to elevated CO₂ levels has shown to improve the efficiency of nutrient, water, and photosynthesis in some plants (Drake, et al., 1997; Leakey et al., 2009). However, the improved efficiencies that result from elevated CO₂ levels may not necessarily result in greater yields for crop plants (Morgan et al., 2005). No adverse impacts to vegetation at or near the Project are expected from CO₂ emissions from the Project.

7.2.3 Nitrogen Oxides

During fuel combustion, atmospheric and fuel-bound nitrogen is oxidized to nitrogen oxide and small amounts of NO₂ (Chang, 1981). The NO is photochemically oxidized to NO₂, which is then subsequently

consumed during the production of ozone and peroxyacetyl nitrates. NO₂ has been shown to deleteriously impact vegetation (Taylor et al., 1975; Heath, 1980; Kozlowski and Constantinidou, 1986; Darrall, 1989). Typical leaf injury responses include interveinal necrotic blotches similar to SO₂ injury for angiosperms and red-brown distal necrosis in gymnosperms (Kozlowski and Constantinidou, 1986). Injury threshold concentrations vary by species and dose but are much higher than that of SO₂ as described above. In general, short-term, high concentrations of NO2 are required for deleterious impacts on plants (Prinz and Brandt, 1985). The injury threshold concentration for typical plants that are grown in Wisconsin is 7,380 µg/m³ for tomato (*Lycopersicon esculentum*) and annual sunflower (*Helianthus annuus*). A common, weedy plant found in Wisconsin is lamb's quarters (Chenopodium album); this species was not injured following 2 hours of exposure at concentrations of 1.9 μg/m³ NO₂. Furthermore, short-term fumigations of approximately 1-hour, 20-hours, and 48-hours at NO₂ concentrations of 940 to 38,000 μg/m³, 470 μg/m³, and 3,000 to 5,000 μg/m³, respectively, have been shown to deter photosynthesis in a number of herbaceous [tomato, oats (Avena sativa), alfalfa (Medicago sativa)] and woody plants (Hill and Bennett, 1970; Capron and Mansfield, 1976; Smith, 1981). Moreover, Taylor and McLean (1970), in their review of NO₂ effects on vegetation, noted that long-term exposures of phytotoxic doses of NO₂ ranged from 280 to 560 μ g/m³.

The maximum annual modeled value for the Project is $2.9 \,\mu\text{g/m}^3$ and the maximum 1-hour NO₂ modeled value for the Project is $162.5 \,\mu\text{g/m}^3$. These levels are low, so it is highly unlikely that NO₂ emissions will impact vegetation adjacent to or surrounding the Project.

7.2.4 Particulate Matter

Particulates have been shown to be detrimental to vegetation typically within the immediate vicinity of the source. The most obvious effect of particle deposition on vegetation is a physical smothering of the leaf surface. This will reduce light transmission to the plant and cause a decrease in photosynthesis. The maximum PM_{10} 24-hour modeled value from this Project is 25.8 μ g/m³ and the maximum $PM_{2.5}$ 24-hour modeled value is 6.3 μ g/m³. These levels are low, so it is highly unlikely that PM_{10} and $PM_{2.5}$ emissions will impact vegetation adjacent to the Project.

7.2.5 Synergistic Effects of Pollutants

Air pollutants are known to act in concert to cause injury to or decrease the plant function (Reinert et al., 1975; Omrod, 1982). Synergistic refers to the combined effects of pollutants when they are greater than is expected from the additive effect of the compounds. The inhibitory effects of SO₂ and NO₂, NO₂ and NO, NO₂ and ozone, and ozone and SO₂ have been reported in various short-term studies for crop plants (e.g., soybean, broad bean (*Vicia faba*), annual sunflower, and tomato) and various tree species that grow in

Wisconsin [e.g., eastern cottonwood (*Populus deltoides*), sugar maple (*Acer saccharum*), white ash (*Fraxinus americana*), and black oak (*Quercus velutina*)] (White et al., 1974; Wright et al., 1986; Capron and Mansfield, 1976; Furakawa et al., 1984; Okana et al., 1985; Costonis, 1970, Carlson, 1979; Jensen, 1981; Omrod et al., 1981). Concentrations of pollutants (80 to 981 μg/m³) in these studies are higher than the concentrations predicted to occur near the Project. Consequently, no synergistic effects of the air pollutants are expected to inhibit vegetation at or near the Project.

7.2.6 Sulfuric Acid Mist

H₂SO₄ mist impacts vegetation in much the same way as acid rain, causing foliar damage and necrosis. In a study that examined the effects of acidic mist on crops and trees in London, the H₂SO₄ mist concentrations in polluted regions were insufficient to produce acute injury to vegetation except in close vicinity of intense emission sources. Generally, in experimental studies, the concentrations of acidic aerosol required to produce measurable reductions in growth and noticeable injury to plants vary between 10 to 100 milligrams per cubic meter (mg/m³). Short time exposures of 4-16 hours at rates of 100-200 mg/m³ have been shown to cause injury to plants (Lange, 1979). Kohno and Kobayashi analyzed the effect of simulated acid rain on soybean growth in Japan and found that visible injury to the young, trifoliate leaves occurred only when the pH was below 3.0 (Kohno and Kobayashi, 1989). In the area around the Project, the average sulfate concentration in acid rain is projected to be approximately 1.5 mg/L with a pH ranging from 5.5 to 5.7 (National Atmospheric Deposition Program (NRSP-3), 2018a and 2018b). These concentrations and levels of acidity are not likely to cause foliar damage, as described in the Kohno and Kobayashi study, because the pH is not low enough.

7.2.7 Volatile Organic Compounds

VOCs are formed from the products of incomplete combustion of natural gas. Currently VOCs are not one of the six "criteria" pollutants for which the EPA has set NAAQS (EPA, 2020). Ozone is a gas created by a chemical reaction between NO_x and VOCs in the presence of sunlight. Vegetation that is impacted by ozone is commonly referred to as "ground-level" ozone, where it forms in potential harmful concentrations and becomes a primary constituent of smog. Similar to particulate matter and lead, the primary impact of smog produced by ozone on vegetation is a physical smothering of the leaf surface. Ozone also gets inside the leaf and damages the parts of the leaf that make the sugars. Ozone's effects on plants typically result in mottled markings, yellowing leaves, or a bronzed appearance. As a result, this damage to the leaves interferes with the ability of sensitive plants to produce and store food, making them more susceptible to diseases, insects, other pollutants, and harsh weather. Chronic exposures to ozone concentrations of greater than or equal to $196 \mu g/m^3$ can cause negative impacts to vegetation (Heath, 1975). Reductions in growth and photosynthesis of trees can occur at ozone levels of less than $200 \mu g/m^3$

(Pye, 1988). Trees typically found within the vicinity of the facility that could be impacted by such levels of ozone include sugar, silver, and red maple (*Acer saccharum*, *A. saccharinum* and *A. rubrum*, respectively); white ash, green ash (*Fraxinus pennsylvanica*), and black locust (*Robinia pseudoacacia*). Soybeans, corn, wheat, annual sunflower, and white clover showed decreases in photosynthetic rates with short-term (200 μg/m³ to 1,399 μg/m³ for 1 to 4 hours) and long-term (70 to 270 μg/m³ for 147 to 180 hours in 3 weeks) exposures to ozone (Hill and Littlefield, 1969; Bennett and Hill, 1973, Furukawa et al., 1984; Reich and Amundson, 1985). In a study of three varieties of rice produced commercially in California that were fumigated with ozone at 0.05, 0.10, 0.15, and 0.20 ppm concentrations for 25 hours per week, the effects of the ozone exposure resulted in a reduction of growth and yield and an increase of seed sterility as the ozone concentrations increased (Thompson et al., 1983). However, the ozone exposure concentrations experienced by the three cultivars of rice are higher than would be expected to result from the Project.

It is difficult to determine the contribution the Project would have on local or regional ambient ozone levels. Photoreactive modeling runs would be required to estimate the ozone impacts resulting from the emissions of NO_x and VOC. Due to the transport effects of ozone, it is unlikely that concentrations in the vicinity of the Project would exceed NAAQS.

7.3 Soil Impacts

Eight soil types were mapped at, or in the immediate vicinity of, the Project site and include (Natural Resources Conservation Service, 2018):

- Arnheim mucky silt loam, 0 to 1 percent slopes, frequently flooded (5A)
- Moquah fine sandy loam, 0 to 3 percent slopes, frequently flooded (6A)
- Udorthents, ravines and escarpments, 25 to 60 percent slopes (92F)
- Amnicon-Cuttre complex, 0 to 4 percent slopes (262B)
- Miskoaki clay loam, 6 to 12 percent slopes (274C)
- Miskoaki clay loam, 12 to 25 percent slopes (274D)
- Bergland-Cuttre complex, 0 to 3 percent slopes (347A)
- Lupton, Cathro, and Tawas soils, 0 to 1 percent slopes (405A)

Sulfates and nitrates caused by NO₂ deposition on soil can be both beneficial and detrimental to soils depending on their composition. However, given the low expected deposition from the Project, operation of the Project should not significantly affect the soils onsite or in the immediate vicinity.

7.4 Industrial, Residential, and Commercial Growth Impacts

The Project is expected to increase employment in the area. The building phase will last approximately one year. Construction employment is expected to peak at approximately 150 skilled construction jobs. Projected employment, reflecting full-time jobs directly tied to the operation of the Project, is estimated to be five people at the facility. This will result in moderate amounts of secondary employment being created by the economic activity of the facility. In the immediate vicinity of the Project, increased vehicular traffic is expected; however, these activities are not expected to significantly impact air quality.

An increase in the construction work may temporarily increase the number of people residing in the area for the construction phase. After construction is completed, many of the new employees are expected to already live in the area surrounding the Project. However, some new employees are expected to move into the area, with only a slight increase in the residential growth in the area. This small increase in new residences is not expected to have an impact on the air quality in the area.

Adding additional electricity to the grid in this area may increase industrial growth; however, it is unknown at this time how increasing available electrical power in this area may affect future industrial growth.

7.5 Visibility and Deposition Analysis

The visibility impairment analysis is part of the additional impacts analysis requirement under PSD.

7.5.1 Class I Area Analysis

Under the PSD program, Class I areas are protected more stringently than under the NAAQS. Class I areas include national parks, wilderness areas, and other areas of special national and cultural significance.

There are four Class I areas that are within 300 kilometers of the Nemadji River Site

- Rainbow Lake Wilderness, Wisconsin (60 kilometers)
- Boundary Waters Canoe Area Wilderness, Minnesota (126 kilometers)
- Voyageurs National Park, Minnesota (182 kilometers)
- Isle Royale National Park, Michigan (237 kilometers)

There is also one non-Federal Class I area that is within 300 kilometers of the Project, Forest County Potawatomi Community Reservation, Wisconsin (261 kilometers).

Areas that have submitted requests to change the air quality status from Class II to Class I but whose request has yet to be granted were not evaluated for this Project.

Following the most recent Federal Land Managers' Air Quality Related Values Work Group (FLAG) Workshop procedures (USFS, NPS, and USFWS, 2010), the Screening Procedure (Q/D) was used to determine if the Project could opt (screen) out of an Air Quality Related Value (AQRV) assessment for visibility and deposition. Following the screening procedures in FLAG, to calculate "Q," the emissions of NO_x, SO₂, PM₁₀, and H₂SO₄ were summed based on maximum 24-hour emission rates for the two worst-case emission scenarios and then divided by the distance to the respective Class I area.

Although overall turbine operations are limited to 500 hours per year fuel oil usage, per guidance from the FLMs, the maximum 24-hour emission rate must be used and ratioed for 365-day operation to determine the "Q" value when assessing the need for a full AQRV analysis. Maximum 24-hour emissions include start-up emissions as well as 100 percent load and duct burning for both the natural gas operation and fuel oil operation. Note that the "Q" value also includes the emissions from the auxiliary equipment. Refer to Appendix C for the overall calculation breakdown and maximum emission rates for the units.

The screening analysis is summarized below for each of the areas located within 300 kilometers of the proposed Project in Table 7-2.

Q/D Class I Area **Fuel Oil Natural Gas** (Kilometers) **Duct Firing**^a Duct Firing^b Rainbow Lake Wilderness 60 9.9 7.3 Boundary Waters Canoe Area Wilderness 126 4.7 3.5 182 2.4 Voyageurs National Park 3.3 237 2.5 1.9 Isle Royale National Park Forest County Potawatomi Community 261 2.3 1.7 Reservation

Table 7-2: Class I Screening Analysis

In accordance with the FLAG Guidance, if Q/D is less than 10, then no AQRV analysis is required. Based on the ratio of Q/D, all of the areas listed in the table above do not require further analysis of AQRV. Thus, no visibility or deposition analysis is anticipated for impacts to AQRVs. A notification letter will be submitted to the Federal Land Managers (FLMs) for concurrence with the above assessment.

⁽a) Q duct firing fuel oil =sum $(NO_x+PM_{10}+SO_2+H_2SO_4) = 595.8$ tons per year and includes start-up emissions (b) Q duct firing natural gas =sum $(NO_x+PM_{10}+SO_2+H_2SO_4) = 439.6$ tons per year and includes start-up emissions

7.5.2 Class II Area Analysis

The Project is located in a Class II area. With respect to visibility conditions around the facility, no known Class II screening visibility criteria have been recommended at this time. Per discussions with WDNR, no Class II visibility analysis is required since the application includes a complete, complex dispersion analysis.

7.6 Conclusion

Based upon the results presented in this section of the application and additional supplemental information, it was concluded that the Project will not have a significant adverse impact on the air quality, soils, vegetation, visibility, and growth in the surrounding area.

8.0 REFERENCES

Section 8.0 overview: The report reference sections are listed in Table 8-1. The previous application submittal citations are current except for the updated modeling guidance documents, which have been updated in this section.

Application Report Section

December 2018 Submittal 8.0 References

June 2020 Submittal 3.0 References

8.0 References

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APPENDIX A – FORMS

Facility Details and Permit Actions Air Pollution Control Permit Application Form 4530-100 (R 9/17) Page 1 of 2

Notice: Use of this form is required by the Department for any air pollution control permit application filed pursuant to ss. 285.61, 285.62 or 285.66, Wis. Stats. Completion of this form is mandatory. The Department will not consider or act upon your application unless you complete and submit this application form. You are required to submit two copies in accordance with s. NR 407.05(2), Wis. Adm. Code. Personal information collected will be used for administrative purposes and may be provided to requesters to the extent required by Wisconsin's Open Records Law [ss. 19.31-19.39, Wis. Stats.].

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| 4. S | treet Address (where pollution sources are/will be lo | cated) | 5. City Tow | /n 🔘 ' | ∕illage | 6. Cour | nty |
| | 61 31st Street | | of Superior | | | | Douglas |
| 7. P | rimary Operating Activity (e.g., lead-acid battery manufa | acturer or | su l fite paper mill) | | | | |
| E | Electric generation | | | | | | |
| 8. Is | the facility located in an area designated as "nonatt | ainment" | 9. If yes, indicate the pol | llutant(s) | for the | nonatta | inment designation |
| | (refer to instructions) Yes | No | | | | | |
| | olicant Information | | | | | | |
| | Responsible Official Name (person legally responsible for | the opera | ition of the permitted air pollution | sources [s | ee NR 40 | 00.02(80e |), Wis. Adm. Code]) |
| | Josh Skelton | | 40 F | | | | |
| | Title | | 12. Email | | | | |
| | Vice President - Generation, South Shore Energ | gy,LLC | jskelton@mnpower.c | com | | Ctoto | ZID Codo |
| | Mailing Address | | City | | | State | ZIP Code |
| | 1259 NW 3rd St. | nod by o | Cohasset | | | MN | 55721 |
| | Parent Corporation or Owner Name (if not wholly ow | nied by a | ірріісапі) | | | | |
| | South Shore Energy, LLC Mailing Address | City | | State | ZIP Co | odo. | Country (if not U.S.) |
| | - | Duluth | | MN | | 802 | Country (ii not o.s.) |
| | 30 West Superior Permit Contact Person – to be contacted for additional info | | oncorning air pollution sources | 17. Emai | | 302 | |
| | Melissa Weglarz | Jilliation C | oncerning all pollution sources | | | mnnos | ver.com |
| | Title | | 1 | 19. Phon | | | ver.com |
| | Environmental Audit and Policy Manager | | | 10.111011 | | 218) 35 | 5-3321 |
| | mit Information | | | | (2 | 210) 33 | 5-5521 |
| | Construction Permit Actions: | | | | | | |
| | Instructions: If applying for a construction permit action MUST also apply for an operation permit option. A check forms before the department will begin their review. Applinvoice will be sent when a final permit decision is made | c for the co lication fe | construction permit application ses are listed below in section A | fees MUS A. Additio | ST be su nal fees | bmitted may be | with the application required and a final |
| Α. | Permit Actions: New Construction/Modification | (\$7,500) |) – Anticipated start dates: | | | | |
| | Construction Permit Revision (| | • | Cons | truction | | Operation |
| | List Permit(s) to be revised | | , | | | | |
| | Requesting Expedited Review – If expedited periods, the construction permit review fee—invidepending on the type and how fast the permit | oiced wit | th the final permit—will inclu | ıde a sur | charge | from \$4 | n expected time 000 to \$7500 |
| В. | Construction Permit Exemptions (indicate one): If y | ou are re | equesting a review and resp | onse to | an exen | nption, a | a check must be |
| | Actual Emissions-Based Exemption (for con | | | ice lister | Delow | iii pai ci | illieses. |
| | Research & Testing (\$1,250) | isti uction | r project only) (\$1,230) | | | | |
| | Modification for source with Plant-wide Appl | licability L | Limit (\$1.500 / \$2.400 with n | nodelina |) | | |
| | Significant Net Emissions Increase (\$5,500 | - | | J | | | |
| | General exemption (\$500 - NR 406.04(2)) | | . , | | | | |
| | Specific exemptions (\$500) – Select approOther: | priate co | ode citation(s) from list: _ | | | | |
| | For more information on exemption | citation | s: https://docs.legis.wiscor | nsin.gov/ | code/ac | lmin_co | de/nr/400/406.pdf |
| C. | Operation Permit type for Construction Action (sele | ct one): | | | | | |
| | Original – if you currently do not have a fac | ility-wide | operation permit | | | | |
| | Revision – so that your facility-wide operation | - | | e propos | ed proje | ect | |

Renewal – if you are renewing your facility-wide operation permit in conjunction with the proposed project

Facility Details and Permit Actions Air Pollution Control Permit Application Form 4530-100 (R 9/17) Page 2 of 2

| 21. | Operation Permit Actions: | |
|-----------|--|---|
| A. | Type of Operation Permit Requested (select one): Part 70 Source Synthetic Minor, Non - Part 70 Source Non - Part 70 Source Elective | Facilities that do not have a facility-wide operation permit issued MUST select the appropriate option. All other requests should indicate type of permit, to reflect continued or changing status. |
| B. | Renewal NOTE Operation Permit Renewal | For more information, see website on streamlined renewal application options. |
| C. | Operation Permit Revision: (select one revision type – check of Administrative Revision (NR 407.11) Minor Revision (NR 407.12) Significant Revision (NR 407.13) | ode for criteria) ermit(s) to be revised: |
| D. | Operation Permit Exemption Options: IMPORTANT: (select one type for entire facility) Actual Emissions Based Exemption (NR 407.03(1m)) Natural Minor Source Exemption (NR 407.03(1s)) | The exemption options in Section D. require revocation of existing operation and/or construction permits. Certain construction permit conditions cannot be revoked, and therefore the department would be unable to revoke the permits. Review all existing permits for case-by-case determinations, especially NR 405/NR 408, and discuss with department staff whether conditions are revocable. |
| E. | Other Operation Permit Exemption Options: General exemptions – NR 407.03(2) Specific categories – Must be only air pollution source a Select appropriate code citation(s) from list: | at entire facility |
| - EDEC-12 | For All Permit Actions: | |
| | dditional information attached? Yes No | |
| Sub | mit two paper copies of completed form(s), with ink signature on WISCONSIN DEPARTMENT BUREAU OF AIR P.O. BC MADISON, W | OF NATURAL RESOURCES MANAGEMENT OX 7921 |
| OR | Email an electronic copy to DNRAMAirPermit@wisconsin.g address above. | ov and mail one complete paper copy with ink signature to the |
| 23. | Signature of Responsible Official | Course the second of a second of the second |
| A. | Statement of Completeness: | |
| | I have reviewed this application in its entirety and, based on info I certify that the statements and information contained in this ap | |
| B. | Certification of Facility Compliance Status: (select one box only | This is not a requirement of Non-Part 70 Sources. |
| | I certify that the facility described in this air pollution permit a | pplication is fully in compliance with all applicable requirements. |
| | I certify that the facility described in this air pollution permit a except for the following emissions unit(s) (list all non-comply | pplication is fully in compliance with all applicable requirements, ing units): |
| Sign | 12-2 lature of Responsible Official Date Sig | |

From January 2021 Application

State of Wisconsin
Department of Natural Resources
APPLICATION

FACILITY PLOT PLAN AIR POLLUTION CONTROL PERMIT

Form 4530-101 Rev. 12-99

Use of this form is required by the Department for any air pollution control permit application filed pursuant to ss. 285.61, 285.62 or 285.66, Wis Stats. Completion of this form is mandatory. The Department will not consider or act upon your application unless you complete and submit this form. It is not the Department's intention to use any personally identifiable information from this form for any other purpose.

In order for a comprehensive air quality analysis to be accomplished, a facility plot plan MUST be included with the permit application. If the application is for an initial operation permit, submit the elements under #2 below. If the application is for a renewal, answer #1 below first.

1. Have there been changes to the facility plot plan since the previous operation permit application was

| ubmitted? ☐ No. The plot plan submitted with the original application can be used for the renewal. ☐ Yes. An up-to-date plot plan is attached. | | | | | | |
|--|--|--|--|--|--|--|
| Yes. An up-to-date plot plan is attached. 2. If there have been changes to the facility plot plan since the last operation permit application submittal, RESUBMIT an up-to-date plot plan which must include the following or the permit application will be deemed incomplete: | | | | | | |
| FOR DEPARTMENT USE ONLY | | | | | | |
| COMPLETE INCOMPLETE NOT APPLICABLE | | | | | | |
| | 1. A building layout (blueprint, plan view) including all buildings occupied by or located on the site of the facility. | | | | | |
| | 2. The maximum height of each building (excluding stack height). | | | | | |
| | 3. The location and numerical designation of each stack. Please ensure these designations correspond to the appropriate stacks listed on the other permit forms in this application. | | | | | |
| | 4. The location of fenced property lines (if any). | | | | | |
| | 5. Identify direction "North" on all submittals. | | | | | |
| | 6. All drawings shall be to scale and shall have the scale graphically depicted. | | | | | |
| | 7. An additional regional map depicting the facility location in relation to the surrounding vicinity (roads or other features) shall be included. | | | | | |
| Are there any outdoor storage piles on the facility site? ☐ Yes ☒ No | | | | | | |
| If so, what material does the pile(s) consist of? | | | | | | |
| Are there any dirt roads or unpaved parking lots on the facility site? ☐ Yes ☒ No | | | | | | |

From January 2021 Application

State of Wisconsin Department of Natural Resources

SOURCE AND SITE DESCRIPTIONS AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-102 Rev. 12-99 Information attached? <u>Y (y/n)</u>

Use of this form is required by the Department for any air pollution control permit application filed pursuant to ss. 285.61, 285.62 or 285.66, Wis Stats. Completion of this form is mandatory. The Department will not consider or act upon your application unless you complete and submit this form. It is not the Department's intention to use any personally identifiable information from this form for any other purpose.

1. Briefly describe the proposed project or existing Unit(s) to be permitted. Attached supplemental forms as needed.

The proposed project is a combined-cycle combustion turbine electricity generation facility. Emission units will include one H-class combustion turbine with a heat recovery steam generator (HRSG) and one steam turbine generator. The combustion turbine will primarily combust pipeline-grade natural gas and will combust fuel oil as a back-up fuel. Other emission units for the project include an auxiliary boiler, two natural gas-fired gas heaters, an emergency diesel fire pump, an emergency diesel generator, fuel oil storage tanks, SF_6 circuit breakers, haul road truck traffic, and piping component fugitives.

- 1. Were any new or modified emissions units installed/modified at the facility since the last operation permit issuance date?
 ✓ No. Proceed to form 4530-102A.
 ☐ Yes. Answer the following questions:
- 2. Briefly describe any new/modified emissions units installed at the facility since the last operation permit issuance date and include the following information. Attach supplemental forms as needed.
 - a. List the Department issued construction and/or operation permit number as applicable (identifying which units were covered by which permit if multiple permits issued).
 - i. If operation permit application forms were submitted for the new emission unit(s) covered by the construction permit mentioned above, reference the date of that application.
 - ii. For Part 70 Sources Only: If no operation permit application forms were submitted for the new emissions unit(s) covered by the construction permit mentioned above, complete the appropriate forms 4530-118 through 4530-125.
 - b. Include the Department issued construction permit exemption number, if one was assigned, or reference the date of the letter of the exemption.

2. Site Description

The Project will be located east of the existing Enbridge Energy Superior Terminal Facility on the banks of the Nemadji River in the City of Superior in Douglas County, Wisconsin.

SOURCE DESCRIPTION - SUPPLEMENTAL AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-102A Rev. 12-99 Information attached? N (y/n)

Use of this form is required by the Department for any air pollution control permit application filed pursuant to ss. 285.61, 285.62 or 285.66, Wis Stats. Completion of this form is mandatory. The Department will not consider or act upon your application unless you complete and submit this form. It is not the Department's intention to use any personally identifiable information from this form for any other purpose.

- 1. List all <u>significant</u> existing or proposed air pollution units, operations, and activities at the facility. A short narrative of the inventory of air pollution emissions unit (e.g., boiler, printing line, etc.) followed by equipment specifications will suffice. If the facility consists of several individual emission units, present this information in an outline format. (See instruction booklet for an example Unit description.)
 - A. Combustion Turbine, EU01

Combined cycle with duct burner -S01, P01, C01a (SCR), C01b (oxidation catalyst)

Manufacturer - Siemens SGT6-80000H

Fuel – Natural gas (primary), Fuel oil (back-up)

Maximum continuous heat input – 4,671 MMBtu/hr HHV when combusting natural gas, 4,027 MMBtu/hr, HHV when combusting diesel fuel oil with a natural gas-fired duct burner

Maximum hourly fuel combustion – 4.58 MMscf/hr (natural gas); 22,050 gal/hr (fuel oil)

B. Auxiliary Boiler, EU02, S02, B02, C02 (ultra-low NO_x burners); Flue Gas Recirculation, and Oxidation Catalyst)

Manufacturer – to be determined

Fuel - Natural gas

Maximum continuous heat input – 100 MMBtu/hr

Maximum hourly fuel combustion- 98,040 scf/hr

C. Circuit Breakers, EU 03, F03

Three 345-kV and two 19-kV circuit breakers

Manufacturer – to be determined

D. Natural Gas Heater #1, EU04, S04, P04

Manufacturer – to be determined

Fuel – Natural gas

Maximum continuous heat input - 10 MMBtu/hr

Maximum hourly fuel combustion -9,804 scf/hr

E. Natural Gas Heater #2, EU05, S05, P05

Manufacturer – to be determined

Fuel - Natural gas

Maximum continuous heat input – 10 MMBtu/hr

Maximum hourly fuel combustion – 9,804 scf/hr

F. Emergency Diesel Fire Pump, EU06, S06, P06

Manufacturer – to be determined

Fuel – Fuel oil

Maximum continuous heat input – 282 HP

Maximum hourly fuel combustion – 14.1 gallons per hour

G. Emergency Diesel Generator, EU07, S07, P07

Manufacturer – to be determined

Fuel - Fuel oil

Maximum continuous heat input – 1,490 HP

Maximum hourly fuel combustion – 150 gallons per hour

H. Storage Tank(s)

T01 - One 180,000-gallon fuel oil tank (backup fuel for combustion turbine)

T02 - One 1,700-gallon diesel generator tank

T03- One 350-gallon diesel fire pump tank

- I. Haul road fugitives, F01
- J. Piping component fugitives, F02

For Renewal Applications:

- 1. If there were any new or modified emissions units installed/modified at the facility since the last operation permit issuance date:
 - a. If any of these new/modified units were exempt from construction permit requirements, but are significant emissions units and operation permit application(s) for the new unit(s) were submitted to the Department reference the date of those submittals.
 - b. If any of the new/modified units are insignificant emissions units list them on form 4530-102B.
 - c. If any of the new/modified emissions units do not fit any of the above categories, fill out the appropriate forms for each emissions unit as follows:
 - i. For Part 70 Sources: Fill out the appropriate forms 4530-103 through 4530-133; OR
 - ii. For Synthetic Minor Non Part-70 Sources and Non-Part 70 Sources: Fill out the appropriate forms 4530-103 through 4530-117 and 4530-126 through 4530-129.

State of Wisconsin
Department of Natural Resources
APPLICATION

SOURCE DESCRIPTION - SUPPLEMENTAL AIR POLLUTION CONTROL PERMIT

Form 4530-102B Rev. 12-99

Information attached? N (y/n)

Use of this form is required by the Department for any air pollution control permit application filed pursuant to ss. 285.61, 285.62 or 285.66, Wis Stats. Completion of this form is mandatory. The Department will not consider or act upon your application unless you complete and submit this form. It is not the Department's intention to use any personally identifiable information from this form for any other purpose.

| 1. M | ark all <u>insignificant</u> existing or proposed air pollution units, operations, and activities at the facility listed below. If not listed, provide a short narrative of the inventory of air pollution emissions unit (e.g., boiler, printing line, etc.) followed by equipment specifications. If the facility consists of several individual emission units, present this information in an outline format. For Renewal Applications, identify those that are new since the last update to your application. (See instruction booklet for an example Unit description.) |
|------|---|
| | ☑ Maintenance of Grounds, Equipment, and Buildings (lawn care, painting, etc.) |
| | ☑ Boiler, Turbine, and HVAC System Maintenance |
| | ☑ Pollution Control Equipment Maintenance |
| | ☐ Internal Combustion Engines Used for Warehousing and Material Transport |
| | ☑ Fire Control Equipment |
| | ☑ Janitorial Activities |
| | ☑ Office Activities |
| | ☑ Convenience Water Heating |
| | ☑ Convenience Space Heating (< 5 million BTU/hr Burning Gas, Liquid, or Wood) |
| | ☑ Fuel Oil Storage Tanks (< 10,000 gal.) |
| | ☐ Stockpiled Contaminated Soils |
| | ☑ Demineralization and Oxygen Scavenging of Water for Boilers |
| | ☑ Purging of Natural Gas Lines |
| | ☑ Sanitary Sewer and Plumbing Venting |
| | |
| | |

FACILITY HAZARDOUS AIR POLLUTANT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-127 11-93

Information attached? n (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

2. Facility identification number: To Be Assigned 816127840 1. Facility name: Nemadji Trail Energy Center

3. Complete the following emissions summary for all hazardous air emissions at this facility (as defined in ch. NR 445, Wis Adm. Code, and sec. 112, 1990 Clean Air Act Amendments):

| Code, and sec | c. 112, 1990 Clean Air A | ct Amendments): | • ` | |
|---------------|--------------------------|------------------------|----------------|-----|
| | | | | |
| | | Units | Units | |
| | SEE AI | PPENDIX C FOR HAPS EMI | SSIONS SUMMARY | |
| | | | | TPY |
| | | | | |
| | | | | TPY |

FACILITY EMISSIONS SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-129 11-93 Information attached? <u>Y</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

1. Facility name Nemadji Trail Energy Center:

2. Facility identification number: To Be Assigned 816127840

| Air pollutant | Actual | Maximum theoretical emissions | Potential to emit | Maximum allowable |
|----------------------|---------------------|-------------------------------------|-------------------|----------------------|
| | TPY | TPY | TPY | TPY |
| SI | EE APPENDIX C FOR E | MISSIONS SUMM | ARY | 1 |
| Particulates | | | | |
| Sulfur dioxide | | | | |
| Organic compounds | | | | |
| Carbon monoxide | | | | |
| Lead | | | | |
| Nitrogen oxides | | | | |
| Total reduced sulfur | | | | |
| Mercury | | | | |
| Asbestos | | | | |
| Beryllium | | | | |
| Vinyl chloride | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |

From January 2021 Application CURRENT EMISSIONS REQUIREMENTS AND STATUS OF FACILITY AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-132 11-93 Information attached? $\underline{n}(y/n)$

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | | 2. Facility identification number: 816127840 | | | |
|---|----------------------|--|-----------------------|---------------------------|--|
| | | 5. State Only | | | |
| Ambient Air Quality | NR 404, 40 CFR 50 | | Will comply with rule | Units not constructed yet | |
| State Origin PSD Review | NR 405 | X | Will comply with rule | Units not constructed yet | |
| Construction Permits | NR 406 | X | Will comply with rule | Units not constructed yet | |
| Operation Permits | NR 407, 40 CFR 70 | | Will comply with rule | Units not constructed yet | |
| Air Permit, Emission, and Inspection Fees | NR 410 | X | Will comply with rule | Units not constructed yet | |
| Carbon Monoxide | NR 426 | X | Will comply with rule | Units not constructed yet | |
| Malodorous Emissions and Open Burning | NR 429 | X | Will comply with rule | Units not constructed yet | |
| NO _x and SO ₂ | NR 432 | X | Will comply with rule | Units not constructed yet | |
| Emission Prohibition, Exceptions, Delayed Compliance Orders, and Variance | NR 436 | X | Will comply with rule | Units not constructed yet | |
| Air Contaminant Emission Inventory Reporting Requirements | NR 438 | X | Will comply with rule | Units not constructed yet | |
| Reporting, Recordkeeping, Testing, Inspection, and Determination of Compliance Requirements | NR 439 | X | Will comply with rule | Units not constructed yet | |
| Standards of Performance for New Stationary Sources | NR 440, 40 CFR 60 | | Will comply with rule | Units not constructed yet | |
| Hazardous Pollutants | NR 445 | X | Will comply with rule | Units not constructed yet | |

| 8. Is this facility subject to the provisions governing | g prevention of accidental | l releases of hazardo | us air contaminants contained |
|---|----------------------------|-----------------------|-------------------------------|
| | in section 112(r)(7 |) of the Clean Air A | .ct? □ Yes⊠No |

If you answered yes, please describe how you will achieve compliance with these provisions, including the requirement to formulate a plan for preventing accidental releases (sec. 112(r)(7)(B)(ii)):

| State Only | |
|------------|--|
| | |
| | |
| | |
| | |

From January 2021 Application FACILITY REQUIREMENT COMPLIANCE PLAN COMMITMENTS AND SCHEDULE AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-133 11-93 Information attached? <u>n</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 | | | | | |
|--|--|---|--|--|--|--|
| 3. For facilities that are presently in compliance with all applicable requirements, including any enhanced monitoring a compliance certification requirements under section 114(a)(3) of the Clean Air Act that apply, complete the followable commitments are part of the application for Part 70 permits. | | | | | | |
| ☐ We will continue to operate and maintain this fac | ☐ We will continue to operate and maintain this facility in compliance with all applicable requirements. | | | | | |
| Form 4530-132 includes new requirements that apply or will apply to this facility during the term of the permit. We will meet such requirements on a timely basis. | | | | | | |
| 4. For facilities <u>not</u> presently fully in compliance, complet | te the following. | | | | | |
| ☐ This facility is in compliance with all applicable requaccording to the following schedule: | tirements except for those | indicated below. We will achieve compliance | | | | |
| Applicable Requirement | Corrective Actions | Deadline | | | | |
| 1. | | | | | | |
| | | | | | | |
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| 2. | | | | | | |
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| 3. | | | | | | |
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| | | | | | | |
| Progress reports will be submitted: | Progress reports will be submitted: | | | | | |
| Start date: and every six (6) months thereafter | | | | | | |

exhausting through this stack.

STACK IDENTIFICATION AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-103 11-93

Information attached? \underline{n} (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE 2. Facility identification number: 3. Stack identification number: 1. Facility name: Nemadji Trail S01 To be assigned 816127840 **Energy Center** 4. Exhausting Unit(s), use Unit identification number from appropriate Form(s) 4530-104, 106, 107, 108 and/or 109 4530-104 EU01 4530-107 4530-108 4530-106 4530-109 5. Identify this stack on the plot plan required on Form 4530-101 6. Indicate by checking: This stack has an actual exhaust point. ☐ This stack serves to identify fugitive emissions. If this stack has an actual exhaust point, then provide the following stack parameters 7. Discharge height above ground level: 190 (feet) 8. Inside dimensions at outlet (check one and complete): ✓ Circular 21.28 (feet) ☐ rectangular length (feet) width (feet) 9. Exhaust flow rate: Normal (ACFM) (at 7.9 °F) Maximum (ACFM) (at 7.9 °F) Natural Gas = 1,488,999 (without DB), Natural Gas = 1,496,266 (with DB), Fuel Oil = 1,519,142 (without DB) Fuel Oil = 1,535,605 (with DB) Exhaust gas temperature (normal): Natural Gas = 168, Fuel Oil = 185 Maximum Exhaust gas moisture content: Normal volume percent volume percent Exhaust gas discharge direction: □ Down ☐ Horizontal **✓** Up Is this stack equipped with a rainhat or any obstruction to the free flow of the exhaust ☐ Yes ✓ No gases from the stack? **** Complete the appropriate Air Permit Application Forms(s) 4530-104, 106, 107, 108 or 109 for each Unit *****

BOILER OR FURNACE OPERATION AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-104 11-93 Information attached? __ (y/n)

| 1. Facility name: Nemadji Trail Energy | 2. Facility identification number: To be assigned 816127840 | | | | |
|--|---|--|---------------------|-----------------------|--|
| 3. Stack identification number: S01 | | 4. Boiler/furnace number: EU01 | | | |
| 4a. Unit description: | | | | | |
| Natural gas-fired combustion turbine as oil as a backup fuel. Duct burning capa | | | ined cycle. Capable | of burning No. 2 fuel | |
| 5. Indicate the boiler/furnace control te | chnology status. □ Un | controlled | trolled | | |
| If the boiler/furnace is controlled | , enter the control device nun | nber(s) from the approp | oriate forms: | | |
| 4530-110 4530- 4530-114 4530- | -111 4530-112 -115 4530-116 | 4530-113 <u>C</u> 4530-117 | 01a, C01b | | |
| 6. Furnace type: Combined-Cycle Com | bustion Turbine | 7. Maximum continu 4,671 MMBtu/hi 4,027 MMBtu/hi | r HHV for Natural | Gas; | |
| 8. Manufacturer: Siemens | | 9. Model number: 80 | 000Н | | |
| 10. Date of construction or last modi | fication: 06/01/2021 | | | | |
| | | | | | |
| 11. Fuels and firing conditions: | | | | | |
| | Primary fuel | Backup fuel #1 | Backup fuel #2 | Backup fuel #3 | |
| Fuel name | Natural Gas | Fuel Oil | | | |
| Higher heating value | 1,020 Btu/scf | 137,000 Btu/gal | | | |
| Maximum sulfur content (Wt.%) | 0.5 gr/100 SCF (annual average) | 0.0015% | | | |
| Maximum ash content (Wt.%) | Negligible | Negligible | | | |
| Excess Combustion Air (%O ₂) | N/A | N/A | | | |
| Moisture content (as fired) (%) | Negligible | Negligible | | | |
| Maximum hourly consumption | 3.59 MMscf/hr (CT) 0.99 MMscf/hr (DB) | 22,050 gal/hr (CT) | | | |
| Actual yearly consumption | 40,109 MMscf/yr | 11.0 x 10 ⁶ gal/yr | | | |
| | | | | | |
| ***** For this emissions unit, identi DESCRIPTION OF METHO and its attachment(s) to this for | | ING COMPLIANCE. | Attach Form 4530- | | |

***** Please complete the Air Pollution Control Permit Application Forms 4530-126 and 4530-128 for this Unit. *****

From December 2018 Application

State of Wisconsin Department of Natural Resources

CONTROL EQUIPMENT-CATALYTIC OR THERMAL OXIDATION AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-113 11-93 Information attached? \underline{n} (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| Section A | |
|--|---|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
| 3. Stack identification number: S01 | 4. Unit identification number: EU01 |
| 5. Control device number: C01a | |
| 6. Manufacturer and model number: TBD | |
| 7. Date of installation: 06/01/2021 | |
| 8. Describe in detail the oxidation system. Attach a blueprint or di | agram of the system. Attached? No |

Selective catalytic reduction of NO_x using ammonia injection and a catalyst.

9. List the pollutants to be controlled by this equipment and the expected control efficiency for each pollutant on the table below.

□ Documentation is attached

| Pollutant | Inlet pollutant concentration | | Outlet pollutant concentration | | Efficiency (%) | |
|-------------------|-------------------------------|------|--------------------------------|--------------------------|-----------------|--------------------------|
| | gr/acf | ppmv | gr/acf | ppmv | hood capture | pollutant destruction |
| NOx (Natural gas) | | 35 | | 2.0 @ 15% O ₂ | | 94% |
| NOx (Fuel oil) | | 42 | | 6.0 @ 15% O ₂ | | 85% |
| | | | | | | |

10: Check one: ✓ Catalytic ☐ Thermal oxidizer

11. Discuss how the spent catalyst will be handled for reuse or disposal.

TBD

- 12. Prepare a malfunction prevention and abatement plan (if required under s. NR 439.11) for this pollution control system. Please include the following:
 - a. Identification of the individuals(s), by title, responsible for inspecting, maintaining and repairing this device.
 - b. Operation variables such as temperature that will be monitored in order to detect a malfunction or breakthrough, the correct operating range of these variables, and a detailed description of monitoring or surveillance procedures that will be used to show compliance.
 - c. An inspection schedule and items or conditions that will be inspected. For catalytic oxidizers, discuss the replacement and/or regeneration schedule for the bed and steps you have taken to ensure the bed's proper functioning throughout its expected lifetime.
 - d. A listing of materials and spare parts that will be maintained in inventory.
 - e. Is this plan available for review? No

| Section B | |
|---|--|
| The following questions must be answered by sources installin efficiency of this device by other means. (Catalytic/Thermal de | g new equipment or existing Units which cannot document control ependent on item 10) |
| Catalytic oxidation | Thermal oxidation |
| 13a. Operating temperature (°F): Max <u>TBD</u> Min | b. Operating temperature (°F): Max Min |
| 14a. Catalyst bed volume (ft³): TBD | b. Combustion chamber volume (ft ³): |
| 15a. Gas volumetric flow rate at combustion conditions (ACFM): TBD | b. Maximum gas velocity through the device (ft./min): |
| 16a. Type of fuel used: TBD | b. Type of fuel used: |
| 17a. Maximum fuel use: TBD | b. Maximum fuel used: |
| 18a. Type of catalyst used and volume of catalyst used (ft ³): T | TBD |
| 19a. Residence time (seconds): TBD | b. Residence time (seconds): |

COMPLIANCE CERTIFICATION - MONITORING AND REPORTING DESCRIPTION OF METHODS USED FOR DETERMINING COMPLIANCE

Form 4530-118 11-93

Information attached? n (y/n)

Information attached? (y/n)

Form 4530-113 11-93

CONTROL EQUIPMENT-CATALYTIC OR THERMAL OXIDATION

AIR POLLUTION CONTROL PERMIT APPLICATION

State of Wisconsin Department of Natural Resources

| SFF | INSTRI | ICTIONS | ONREV | VERSE SIDE | 7 |
|------|---------|---------|-------|---------------|----|
| பட்ட | IIIOIIC | CHONS | ONKE | וכווס לוסמודו | `- |

| 2. Facility identification number: To be assigned 816127840 |
|---|
| 4. Unit identification number: EU01 |
| |
| |
| |
| iagram of the system. Attached? <u>Yes</u> |
| |

Oxidation catalyst for the oxidation of CO.

9. List the pollutants to be controlled by this equipment and the expected control efficiency for each pollutant on the table below. ☐ Documentation is attached

| _ Bootmentation is attached | | | | | | |
|-----------------------------|-----------------|---------------|----------------|-------------------------|--------------|-------------|
| Pollutant | Inlet pollutant | concentration | Outlet polluta | ant concentration | Efficie | ncy (%) |
| | gr/acf | ppmv | gr/acf | ppmv | hood capture | pollutant |
| | | | | | | destruction |
| CO (NG or FO with DB) | | | | 1.5 @15% O ₂ | | 50-80% |
| CO (NG pr FO without DB) | | | | 1.5 @15% O ₂ | | 50-80% |
| VOC (NG or FO without) | | | | 0.6 @15% O ₂ | | 35-40% |
| VOC (NG with DB) | | | | 2.7 @15% O ₂ | | 35-40% |
| VOC (FO with DB) | | | | 3.3 @15% O ₂ | | 35-40% |

✓ Catalytic Thermal oxidizer 10: Check one: 11. Discuss how the spent catalyst will be handled for reuse or disposal:

TBD

- Prepare a malfunction prevention and abatement plan (if required under s. NR 439.11) for this pollution control system. Please include the following:
 - a. Identification of the individuals(s), by title, responsible for inspecting, maintaining and repairing this device.
 - b. Operation variables such as temperature that will be monitored in order to detect a malfunction or breakthrough, the correct operating range of these variables, and a detailed description of monitoring or surveillance procedures that will be used to show compliance.
 - c. An inspection schedule and items or conditions that will be inspected. For catalytic oxidizers, discuss the replacement and/or regeneration schedule for the bed and steps you have taken to ensure the bed's proper functioning throughout its expected lifetime.
 - d. A listing of materials and spare parts that will be maintained in inventory.
 - e. Is this plan available for review? No.

| Section | n | | |
|---------|---|--|--|
| | | | |

The following questions must be answered by sources installing new equipment or existing Units which cannot document control efficiency of this device by other means. (Catalytic/Thermal dependent on item 10)

| Catalytic oxidation | Thermal oxidation |
|--|---|
| 13a. Operating temperature (°F): Max <u>TBD</u> Min <u>TBD</u> | b. Operating temperature (°F): Max Min |
| 14a. Catalyst bed volume (ft ³): TBD | b. Combustion chamber volume (ft ³): |
| 15a. Gas volumetric flow rate at combustion conditions (ACFM): TBD | b. Maximum gas velocity through the device (ft./min): |
| 16a. Type of fuel used: N/A | b. Type of fuel used: |
| 17a. Maximum fuel use: TBD | b. Maximum fuel used: |
| 18a. Type of catalyst used and volume of catalyst used (ft ³): TBD | |
| 19a. Residence time (seconds): TBD | b. Residence time (seconds): |

From December 2018 Application

State of Wisconsin Department of Natural Resources

COMPLIANCE CERTIFICATION - MONITORING AND REPORTING DESCRIPTION OF METHODS USED FOR DETERMINING COMPLIANCE Form 4530-118 11-93 Information attached? n (y/n)

All applicants except non-Part 70 sources are required to certify compliance with all applicable air pollution permit requirements by including a statement within the permit application of the methods used for determining compliance (please see sec. NR 407.05(4)(i), Wis. Adm. Code.) This statement must include a description of the monitoring, recordkeeping, and reporting requirements and test methods. In addition, the application must include a schedule for compliance certification submittals during the permit term. These submittals must be no less frequent than annually, and may need to be more frequent if specified by the underlying applicable requirement or by the Department.

| CEE | INCTDI | ICTIONS | ON REVER | CE CIDE |
|-----|--------|---------|----------|---------|

| EE INSTRUCTIONS ON REVERSE SIDE | | |
|---|---|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | |
| 3. Stack identification number: S01 | 4. Unit identification number: EU01 | |
| 5. This Unit will use the following method(s) for determining corand attach the appropriate form(s) to this form). | inpliance with the requirements of the permit (check all that apply | |
| ✓ Continuous Emission Monitoring (CEM) - Form 4530-1 Pollutant(s): NOx | 119 | |
| ☐ Periodic Emission Monitoring Using Portable Monitors Pollutant(s): | - Form 4530-120 | |
| ☐ Monitoring Control System Parameters or Operating Par Pollutant(s): | rameters of a Process - Form 4530-121 | |
| ☐ Monitoring Maintenance Procedures - Form 4530-122 Pollutant(s): | | |
| Stack Testing - Form 4530-123 Pollutant(s): NOx, SO ₂ , CO, VOC, PM ₁₀ , PM _{2.5} , H ₂ SO ₄ , opacity | | |
| ✓ Fuel Sampling and Analysis (FSA) - Form 4530-124 Pollutant(s): SO ₂ | | |
| Recordkeeping - Form 4530-125 Pollutant(s): NO _x , SO ₂ CO, VOC, PM ₁₀ , PM _{2.5} | | |
| ☐ Other (please describe) - Form 4530-135 Pollutant(s): | | |
| 6. Compliance certification reports will be submitted to the De | epartment according to the following schedule: | |
| Start date: 12 months after Title V issuance and every 12 months thereafter. | | |
| Compliance monitoring reports will be submitted to the | Department according to the following schedule: | |
| Start date: 6 months after Title V issuance and every6 months thereafter. | | |

COMPLIANCE DEMONSTRATION BY CONTINUOUS EMISSION MONITORING AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-119 11-93

Information attached? \underline{n} (y/n)

An installation plan for each new (i.e., proposed) Continuous Emission Monitoring (CEM) system shall be submitted with the permit application for Department approval. Installation plans for existing CEMs are not required to be submitted with the permit application. The installation plan shall contain the following information: the name and address of the source; the source facility identification number; a general description of the process and the control equipment; the pollutant or diluent being monitored; the manufacturer, model number, and serial number of each analyzer; the operating principles of each analyzer; a schematic of the CEM system showing the sample acquisition point and the location of the monitors; and an explanation of any deviations from the siting criteria in Performance Specifications 1,2,3,4,5,6 and 7 in 40 CFR part 60, Appendix B, incorporated by reference in ch. NR 484, Wis. Adm. Code.

| SEE INSTRUCTIONS ON REVERSE SIDE | | |
|---|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | |
| 3. Stack identification number: S01 | 4. Unit identification number: EU01 | |
| 5. Pollutant being monitored: (If other than opacity then item 6 or 7 will be required) NOx | | |
| a. Name of manufacturer: TBD | b. Model number: TBD | |
| c. Is this an existing system ☐ Yes ☑ No | d. Installation date: 06/01/2021 | |
| e. Type □ In situ ☑ Extractive □ Dilution □ Other (specify) | | |
| f. Describe how the monitor works: TBD | | |
| g. Backup system: TBD | | |
| h. □ The CEM system certification is attached for Department ap the startup of the CEM system. □ The certification was i. □ A CEM system Quality Assurance/Quality Control Plan is at please submit it within 60 days of the CEM system startum. | tached for Department approval. If the plan is not attached, | |
| 6. Diluent being monitored: TBD | | |
| a. Name of manufacturer: TBD | b. Model number: TBD | |
| c. Is this an existing system ☐ Yes ☑ No d. Installation date: 06/01/2021 | | |
| e. Type □ In situ ☑ Extractive □ O2 □ CO2 □ Other (specify) | | |
| f. Describe how the monitor works: TBD | | |
| g. Backup system: TBD | | |
| h. □ The CEM system certification is attached for Department ap the startup of the CEM system. □ The certification was i. □ A CEM system Quality Assurance/Quality Control Plan is at please submit it within 60 days of the CEM system startum | tached for Department approval. If the plan is not attached, | |
| 7. Flow. No flow meter. Fuel flow meter will be used to calculate s | stack flow. | |
| a. Name of manufacturer: | b. Model number: | |
| c. Is this an existing system ☐ Yes ☐ No d. Installation date: | | |
| e. Type | | |
| f. Describe how the monitor works: | | |
| g. Backup system: | | |
| h. □ The CEM system certification is attached for Department ap the startup of the CEM system. □ The certification was i. □ A CEM system Quality Assurance/Quality Control Plan is at please submit it within 60 days of the CEM system startu | tached for Department approval. If the plan is not attached, | |

COMPLIANCE DEMONSTRATION BY STACK TESTING AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-123 11-93

Information attached? \underline{n} (y/n)

The performance of an EPA stack test method for demonstrating compliance with an emission limitation has always been acceptable. EPA test methods contain quality assurance procedures that shall be strictly adhered to by the source. The applicant shall propose an appropriate program of stack testing for compliance demonstration. The stack testing program shall correlate with the corresponding emission limitation in terms of the frequency and duration of the stack tests. The Department may approve the proposed stack testing program, or other program which the Department determines to be appropriate. The procedures outlined in chapter NR 439 for stack test plans and procedures shall apply to stack test performed for ongoing compliance demonstration.

| SEE INSTRUCTIONS ON REVERSE SIDE | | | |
|---|---|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | | |
| 3. Stack identification number: S01 | 4. Unit identification number: EU01 | | |
| 5. Pollutant being monitored: NO _x , CO, VOC, PM ₁₀ , PM _{2.5} , H ₂ SO | 4, opacity | | |
| 6. Procedure being monitored: N/A | | | |
| 7. Is this an existing method of demonstrating compliance? ☐ Yes ☑ No | 8. Installation date: 06/01/2021 | | |
| 9. EPA or Department approved test method: | | | |
| EPA Test Methods 5, 7, 8, 9, 10, 25, 201A, 202 | | | |
| 10. Backup system N/A | | | |
| 11. Compliance shall be demonstrated: ☐ Daily ☐ Weekly | ☐ Monthly ☑ Upon initial startup | | |
| **** Any measured emission rate that exceeds an emission lin reported as an excess emission. | nitation established by the permit shall be ***** | | |

COMPLIANCE DEMONSTRATION BY FUEL SAMPLING AND ANALYSIS AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-124 11-93

Information attached? \underline{n} (y/n)

An installation plan for each fuel sampling and analysis system (FSA) may be submitted with the permit application for Department approval. The installation plan shall contain the following information: the name and address of the source; the source facility identification number; a general description of the process and the control equipment; the type of fuel being sampled; the manufacturer, model number, and serial number of each sampler; and a schematic of the FSA system showing the sample acquisition point and the location of the machine that produces the daily, weekly, or monthly composite fuel sample. A completed form 4530-124, supplemented to satisfy the requirements of this paragraph, may constitute an installation plan for a FSA system.

| SEE INSTRUCTIONS ON REVERSE SIDE | | | | |
|---|---|--|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | | | |
| 3. Stack identification number: S01 | 4. Unit identification number: EU01 | | | |
| 5. Pollutant being monitored: SO ₂ | 6. Fuel being sampled: Natural gas and fuel oil | | | |
| 7. List the ASTM fuel sample collecting and analyzing methods u | sed: | | | |
| In accordance with 40 CFR Part 75 | | | | |
| 8. Is this an existing FSA system? ☐ Yes ☑ No | 9. Installation date: 06/01/2021 | | | |
| 10. ☐ Automated sampling ☑ Manual sampling | | | | |
| 11. Backup system? No | | | | |
| 12. Compliance shall be demonstrated: ☐ Daily ☐ Weekly | ☐ Monthly ✓ Per shipment of fuel | | | |
| 13. Indicate by checking: | | | | |
| ☐ The FSA system certification is attached for Department approval. ☑ If the certification is not attached, please submit it within 60 days of the FSA system startup. ☐ The certification was submitted to the Department on | | | | |
| ☐ A FSA quality assurance/quality control plan for fuel sampling program is attached for Department approval. ☑ If the plan is not attached, please submit it within 60 days of the CEM startup system. ☐ The plan was submitted to the Department on | | | | |

**** Any composite sample over the emission limit

COMPLIANCE DEMONSTRATION BY RECORDKEEPING AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-125 11-93

Information attached? \underline{n} (y/n)

Recordkeeping may be acceptable as a compliance demonstration method provided that a correlation between the parameter value recorded and the emission rate of a particular pollutant is established in the form of a curve or chart of emission rate versus parameter values. This correlation may constitute the certification of the system. It should be attached for Department approval. If it is not attached, please submit it within 60 days of the startup of the system.

| SEE INSTRUCTIONS ON REVERSE SIDE | | | | |
|--|---|--|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | | | |
| 3. Stack identification number: S01 | 4. Unit identification number: EU01 | | | |
| 5. Pollutant(s) being monitored: PM ₁₀ , PM _{2.5} , VOC | 6. Material or parameter being monitored and recorded: fuel usage | | | |
| 7. Method of monitoring and recording: | | | | |
| Fuel Flow | | | | |
| 8. List any EPA methods used: N/A | | | | |
| 9. Is this an existing method of demonstrating compliance? ☐ Yes ☑ No | 10. Installation date: 06/01/2021 | | | |
| 11. Backup system: | | | | |
| 12. Compliance shall be demonstrated: ☐ Daily ☐ Weekly | ✓ Monthly ☐ Batch (not to exceed monthly) | | | |
| 13. Indicate by checking: | | | | |
| The monitoring system shall be subject to appropriate performance specifications, calibration requirements, and quality assurance procedures. ☐ A quality assurance/quality control plan for the recordkeeping system is attached for Department approval. ☑ If the plan is not attached, please submit it within 60 days of the startup of the recordkeeping program. ☐ The plan was submitted to the Department on | | | | |
| ***** The compliance records shall be available for Department inspection. The format for the compliance ***** certification report and the excess emission report shall be approved by the Department. A proposed format for the compliance certification report and excess emission report shall be submitted at the same time as the application. | | | | |
| ***** The source shall record any malfunction that causes or may cause an emission limit to be exceeded. ***** Malfunctions shall be reported to the Department the next business day. Hazardous air spills shall | | | | |

be reported to the Department immediately.

EMISSION UNIT HAZARDOUS AIR POLLUTANT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-126 11-93 Information attached? <u>y</u> (y/n)

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|---|
| 3. Stack identification number: S01 | 4. Unit identification number: EU01 |

5. Unit material description: Combined Cycle Turbine combusting natural gas and fuel oil

6. Complete the following summary of hazardous air emissions from this unit. Attach sample calculations and emission factor references. Attached? yes see Amendix C

| references. | Attached? yes, see App | endix C | | |
|-------------|------------------------|------------------------|------------|-----|
| | | | | |
| | | Units | Units | |
| | SEE APPEN | DIX C FOR EMISSIONS CA | LCULATIONS | TPV |
| | | | | TPY |
| _ | | | | TPY |
| | | | | TPY |
| _ | | | | TPY |
| _ | | | | TPY |
| | | | | TPY |
| | | | | TPY |

EMISSION UNIT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-128 11-93 Information attached? <u>y</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|---|
| 3. Stack identification number: S01 | 4. Unit identification number: EU01 |

5. Complete the following emissions summary for the following pollutants. Attach sample calculations and emission factor references. Attached? Yes, see Appendix C

| references. Attack | hed? Yes, | see A | ppendix C | | | | | | | |
|----------------------|-----------|-------|-----------|----------|-----|---------|-------|-----|---|-----|
| | | | | | | | | | | |
| | | U | TPY | | U | TPY | | | U | TPY |
| Particulates | SEE AP | PPEN | DIX C FO | R EMISSI | ONS | CALCULA | TIONS | TPY | | |
| Sulfur dioxide | | | | | | | | TPY | | |
| Organic compounds | | | | | | | _ | TPY | | |
| Carbon monoxide | | | | | | | | TPY | | |
| Lead | | | | | | | | TPY | | |
| Nitrogen oxides | | | | | | | | TPY | | |
| Total reduced sulfur | | | | | | | | TPY | | |
| Mercury | | | | | | | | TPY | | |
| Asbestos | | | | | | | | TPY | | |
| Beryllium | | | | | | | | TPY | | |
| Vinyl chloride | | | | | | | | TPY | | |
| | | | | | | | | TPY | | |
| | | | | | | | | TPY | | |
| | | | | | | | | TPY | | |
| | | | | | | | | TPY | | |
| | | | | | | | | TPY | | |

Units (U) should be entered as follows:

- 1 = lb/hr
- 2 = lb/mmBTU
- 3 = grains/dscf
- 4 = lb/gallon
- 5 = ppmdv
- 6 = other (specify)
- 7 = other (specify)
- 8 = other (specify)

CURRENT EMISSIONS REQUIREMENTS AND STATUS OF UNIT AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-130 Rev. 12-99 Information attached? <u>n</u> (y/n)

| Facility name: Nemadji Trail Energy Center Stack identification number: S01 | | 2. Facility identification number: To be assigned 8161278 | | | | | |
|---|---|---|--|---------------------------|--|--|--|
| | | 4. Unit identification number: EU01 | | | | | |
| | | 7. State Only | | | | | |
| Nitrogen Dioxide | 40 CFR 60.4320(a) (Subpart KKKK) | | 15 ppm at 15 percent O ₂ for natural gas; 42 ppm at 15 percent O ₂ for fuel oil. | Units not constructed yet | | | |
| Sulfur Dioxide | 40 CFR 60.4330 (Subpart KKKK) | | 0.90 lb/MW-hr gross output | Units not constructed yet | | | |
| GHG (CO ₂) | 40 CFR Part 60, Subpart TTTT | | 1,000 lb/MW-hr gross output (90% NG) or petition for other standard | Units not constructed yet | | | |
| Opacity | NR 431 | X | 20% opacity | Units not constructed yet | | | |
| Nitrogen Dioxide | NR 432 – Clean Air Interstate Rule NOx Allowances, | | Replaced by Cross-State Air Pollution Rule | Units not constructed yet | | | |
| Ammonia - SCR | NR 445 | X | N/A | Units not constructed yet | | | |
| Carbon Monoxide | NR 426 | X | | Units not constructed yet | | | |
| Volatile Organic Compounds | NR 419 | X | | Units not constructed yet | | | |
| Particulate | NR 415.06(2)(c) | X | 0.10 lb PM/MMBtu | Units not constructed yet | | | |
| Nitrogen Dioxide | 40 CFR 60.4320(a) (Subpart KKKK) | | 96 ppm @ 15% O2 at temperatures below 0 degress Fahrenheit | Units not constructed yet | | | |
| | | | State Only | | | | |
| | | | | | | | |

** PART 70 SOURCES ONLY:

1. Be sure to review the Compliance Assurance Monitoring (CAM) Rule, 40 CFR Part 64, for the Renewal Application. The CAM rule requires owners and operators of Part 70 sources to monitor the operation and maintenance of their control equipment so that they can evaluate the performance of their control devices and report whether or not their facilities meet established emission standards. All facilities that have a Title V, Part 70, Federal Operating Permit are required to meet the CAM rule and submit a CAM plan with this Title V renewal application. The rule requires that a CAM plan be submitted with the Title V renewal application for each pollutant at each emissions unit which has a potential to emit - prior to controls - of that pollutant greater than the major source threshold for the respective pollutant. Please refer to the CAM Technical Guidance web site at http://www.epa.gov/ttn/emc/cam.html for further documentation on the rule and how to prepare a CAM plan for submittal with the renewal application.

2. List all applicable **Maximum Achievable Control Technology** (MACT) rule(s) and the effective date(s) if they were promulgated during the last 3 years of your operation permit term. Identify the emissions units subject to each MACT rule listed.

EMISSION UNIT COMPLIANCE PLAN COMMITMENTS AND SCHEDULE AIR POLLUTION CONTROL PERMIT APPLICATION

| | Form 4530-131 11-93 | Information attached? n_ (y/n) |
|--|--|--------------------------------------|
| SEE INSTRUCTIONS ON REVERSE SID | 3 | |
| Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned | d 816127840 |
| 3. Stack identification number: S01 | 4. Unit identification number: EU01 | |
| | ce with all applicable requirements, including any tion 114(a)(3) of the Clean Air Act that apply, cor tion for Part 70 permits. | |
| ☐ We will continue to operate and | maintain this Unit in compliance with all applicab | ele requirements. |
| Form 4530-130 includes new req | uirements that apply or will apply to this Unit dur ely basis. | ring the term of the permit. We will |

| This Unit is in compliance with all applicable requirements except for those indicated below. | We will achieve compliance |
|---|----------------------------|
| according to the following schedule: | - |

6. For Units not presently fully in compliance, complete the following.

Applicable Requirement Corrective Actions Deadline 1. 2. 3.

STACK IDENTIFICATION AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-103 11-93 Information attached? n (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | | ck identification number: S02 | | | |
|--|--|---------------------------|-------------------------------|--|--|--|
| 4. Exhausting Unit(s), use Unit identification | n number from appropriate Fo | rm(s) 4530-104, 106, | 107, 108 and/or 109 | | | |
| 4530-104 EU02 4530-106 | 4530-107 4530-1 | 108 4530 | -109 | | | |
| 5. Identify this stack on the plot plan require | d on Form 4530-101 | | | | | |
| 6. Indicate by checking: This stack has an actual exhaust po If this stack has an actual exhaust poin | | s to identify fugitive of | emissions. | | | |
| 7. Discharge height above ground level: 1 | | | | | | |
| 8. Inside dimensions at outlet (check one and | l complete): | | | | | |
| ✓ Circular <u>3.50</u> (feet) | ☐ rectangular length | (feet) width (| feet) | | | |
| 9. Exhaust flow rate: | | | | | | |
| Normal <u>27,709</u> (ACFM) | Maximum <u>27,709</u> | (ACFM) | | | | |
| 10. Exhaust gas temperature (normal):2 | <u>.90</u> (°F) | | | | | |
| 11. Exhaust gas moisture content: | Normal volume perce | nt Maxi | mum volume percent | | | |
| 12. Exhaust gas discharge direction: | ✓ Up □ Dov | wn □ He | orizontal | | | |
| 13. Is this stack equipped with a rainhat or any obstruction to the free flow of the exhaust gases from the stack? ✓ No | | | | | | |
| ***** Complete the appropriate Air Permit Application Forms(s) 4530-104, 106, 107, 108 or 109 for each Unit ***** exhausting through this stack. | | | | | | |

BOILER OR FURNACE OPERATION AIR POLLUTION CONTROL PERMIT APPLICATION Form 4520 104 11 02

Form 4530-104 11-93 Information attached? <u>n</u> (y/n)

| SEE INSTRUCTIONS ON REVERSE SI | DE | | | | | |
|--|---|----------------------------------|----------------------|----------------|--|--|
| 1. Facility name: Nemadji Trail Energy | 2. Facility identific | ation number: To be a | ssigned 816127840 | | | |
| 3. Stack identification number: S02 | 4. Boiler/furnace number: EU02 | | | | | |
| 4a. Unit description: 100-MMBtu/hr Auxiliary boiler respons | ible for delivering suppl | emental steam to the o | combined-cycle combu | stion turbine. | | |
| 5. Indicate the boiler/furnace control tech | hnology status. | Uncontrolled 🗹 (| Controlled | | | |
| If the boiler/furnace is controlled, | enter the control device r | number(s) from the ap | ppropriate forms: | | | |
| 4530-110 <u>C02</u> 4530-114 <u>4530-114</u> 4530-1 | 30-111 4530-1 15 4530-116 | 12 4530-1 4530-117 | 13 | | | |
| 6. Furnace type: Unknown | | 7. Maximum conti | nuous rating: 100 MM | MBtu/hr | | |
| 8. Manufacturer: TBD | | 9. Model number: | TBD | | | |
| 10. Date of construction or last modifi | cation: 06/01/2021 | | | | | |
| | | | | | | |
| 11. Fuels and firing conditions: | | | | <u> </u> | | |
| | Primary fuel | Backup fuel #1 | Backup fuel #2 | Backup fuel #3 | | |
| Fuel name | Natural Gas | | | | | |
| Higher heating value | 1,020 Btu/scf | | | | | |
| Maximum sulfur content (Wt.%) | Pipeline-grade | | | | | |
| Maximum ash content (Wt.%) | N/A | | | | | |
| Excess Combustion Air (%O ₂) | N/A | | | | | |
| Moisture content (as fired) (%) | N/A | | | | | |
| Maximum hourly consumption | 98,039 scf/hr | | | | | |
| Actual yearly consumption | Actual yearly consumption 859 x 10 ⁶ scf | | | | | |
| ***** For this emissions unit, identify the method of compliance demonstration by completing Form 4530-118, ***** DESCRIPTION OF METHODS USED FOR DETERMINING COMPLIANCE. Attach Form 4530-118 and its attachment(s) to this form. This is not a requirement of non-Part 70 sources. | | | | | | |

***** Please complete the Air Pollution Control Permit Application Forms 4530-126 and 4530-128 for this Unit. *****

CONTROL EQUIPMENT MISCELLANEOUS AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-110 11-93 Information attached? n_ (y/n)

| SEE IN | ISTRUC | TIONS | ON REV | ERSE | SIDE |
|--------|--------|-------|--------|------|------|
| | | | | | |

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|---|
| 3. Stack identification number: S02 | 4. Unit identification number: EU02 |
| 5. Control device number: C02 | |
| 6. Manufacturer and model number: TBD | |

7. Date of installation: 06/01/2021

8. Describe in detail the device in use. Ultra-low NO_x burners and flue gas recirculation (FGR) and Oxidation Catalyst (OxCat)

Attach a diagram of the system. Attached? No

9. List the pollutants to be controlled by this equipment and the expected control efficiency for each pollutant on the table below. □ Documentation is attached?

| Pollutant | Inlet pollutant concentration | | Hood capture efficiency (%) | | pollutant ntration | Efficiency (%) |
|-----------------|-------------------------------|------|-----------------------------|-------------|-----------------------|-----------------|
| | gr/acf | ppmv | | gr/acf ppmv | | |
| NO _x | | | 50% | | 9 ppm | 0.011 lb/MMBtu |
| VOC | | | 50% | | | 0.0027 lb/MMBtu |
| CO | | | 90% | | | 0.0037 lb/MMBtu |

- 10. Discuss how the collected material will be handled for reuse or disposal. Ultra-low NO_x burners control the formation of NO_x using a two-stage combustion process. Oxidation catalyst system is an add-on control that converts CO and VOC to CO2 by use of a catalyst.
- 11. Prepare a malfunction prevention and abatement plan (if required under s. NR 439.11) for this pollution control system. Please include the following:
 - a. Identification of the individuals(s), by title, responsible for inspecting, maintaining and repairing this device.
 - b. Operation variables such as temperature that will be monitored in order to detect a malfunction or breakthrough, the correct operating range of these variables, and a detailed description of monitoring or surveillance procedures that will be used to show compliance.
 - c. What type of monitoring equipment will be provided (temperature sensors, pressure sensors, CEMs).
 - d. An inspection schedule and items or conditions that will be inspected.
 - e. A listing of materials and spare parts that will be maintained in inventory.
 - f. Is this plan available for review? No

COMPLIANCE CERTIFICATION - MONITORING AND REPORTING DESCRIPTION OF METHODS USED FOR DETERMINING COMPLIANCE Form 4530-118 11-93 Information attached? \underline{n} (y/n)

All applicants except non-Part 70 sources are required to certify compliance with all applicable air pollution permit requirements by including a statement within the permit application of the methods used for determining compliance (please see sec. NR 407.05(4)(i), Wis. Adm. Code.) This statement must include a description of the monitoring, recordkeeping, and reporting requirements and test methods. In addition, the application must include a schedule for compliance certification submittals during the permit term. These submittals must be no less frequent than annually, and may need to be more frequent if specified by the underlying applicable requirement or by the Department.

| CEE | INICTDI | ICTIONS | ON DEVERSE | CIDE |
|-----|---------|---------|------------|------|

| INSTRUCTIONS ON REVERSE SIDE | | | | | |
|---|--|--|--|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | | | | |
| 3. Stack identification number: S02 | 4. Unit identification number: EU02 | | | | |
| 5. This Unit will use the following method(s) for determining con and attach the appropriate form(s) to this form). | apliance with the requirements of the permit (check all that apply | | | | |
| ☐ Continuous Emission Monitoring (CEM) - Form 4530-1 Pollutant(s): | 19 | | | | |
| ☐ Periodic Emission Monitoring Using Portable Monitors - Pollutant(s): | Form 4530-120 | | | | |
| ☐ Monitoring Control System Parameters or Operating Para Pollutant(s): | ameters of a Process - Form 4530-121 | | | | |
| ☐ Monitoring Maintenance Procedures - Form 4530-122 Pollutant(s): | | | | | |
| ☐ Stack Testing - Form 4530-123 Pollutant(s): | | | | | |
| ☐ Fuel Sampling and Analysis (FSA) - Form 4530-124 Pollutant(s): 2 | | | | | |
| Recordkeeping - Form 4530-125 Pollutant(s): All | | | | | |
| ☐ Other (please describe) - Form 4530-135 Pollutant(s): | | | | | |
| 6. Compliance certification reports will be submitted to the De | epartment according to the following schedule: | | | | |
| Start date: At date of permit issuance and every 12 months thereafter. | | | | | |
| Compliance monitoring reports will be submitted to the | Department according to the following schedule: | | | | |
| Start date: At date of permit issuance and every 6 months thereafter. | | | | | |

COMPLIANCE DEMONSTRATION BY RECORDKEEPING AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-125 11-93

Information attached? \underline{n} (y/n)

Recordkeeping may be acceptable as a compliance demonstration method provided that a correlation between the parameter value recorded and the emission rate of a particular pollutant is established in the form of a curve or chart of emission rate versus parameter values. This correlation may constitute the certification of the system. It should be attached for Department approval. If it is not attached, please submit it within 60 days of the startup of the system.

| SEE INSTRUCTIONS ON REVERSE SIDE | |
|---|---|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
| 3. Stack identification number: S02 | 4. Unit identification number: EU02 |
| 5. Pollutant(s) being monitored: SO ₂ | 6. Material or parameter being monitored and recorded: Sulfur content of natural gas. |
| 7. Method of monitoring and recording: Owners will keep records of the sulfur content of the natural daily usage of natural gas. | l gas as certified by the supplier or test data and record the |
| 8. List any EPA methods used: N/A | |
| 9. Is this an existing method of demonstrating compliance? ☐ Yes ☑ No | 10. Installation date: 06/01/2021 |
| 11. Backup system: N/A | |
| 12. Compliance shall be demonstrated: ☑ Daily ☐ Weekly | ☐ Monthly ☐ Batch (not to exceed monthly) |
| 13. Indicate by checking: | |
| assurance procedures. A quality assurance/quality co | ase submit it within 60 days of the startup of the recordkeeping |
| ***** The compliance records shall be available for Department certification report and the excess emission report shal format for the compliance certification report and excessame time as the application. | l be approved by the Department. A proposed |
| ***** The source shall record any malfunction that causes or ma Malfunctions shall be reported to the Department the n be reported to the Department immediately. | |

COMPLIANCE DEMONSTRATION BY RECORDKEEPING AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-125 11-93 Information attached? <u>n</u> (y/n)

Recordkeeping may be acceptable as a compliance demonstration method provided that a correlation between the parameter value recorded and the emission rate of a particular pollutant is established in the form of a curve or chart of emission rate versus parameter values. This correlation may constitute the certification of the system. It should be attached for Department approval. If it is not attached, please submit it within 60 days of the startup of the system.

| SEE INSTRUCTIONS ON REVERSE SIDE | |
|---|---|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
| 3. Stack identification number: S02 | 4. Unit identification number: EU02 |
| 5. Pollutant(s) being monitored: All | 6. Material or parameter being monitored and recorded: Hours of operation of the natural gas heater will be recorded so that emissions may be calculated. |
| 7. Method of monitoring and recording: Hours of operation | |
| 8. List any EPA methods used: Not applicable | |
| 9. Is this an existing method of demonstrating compliance? ☐ Yes ☑ No | 10. Installation date: 06/01/2021 |
| 11. Backup system: N/A | |
| 12. Compliance shall be demonstrated: ☐ Daily ☐ Weekly | ✓ Monthly ☐ Batch (not to exceed monthly) |
| assurance procedures. A quality assurance/quality co | ase submit it within 60 days of the startup of the recordkeeping |
| ***** The compliance records shall be available for Department certification report and the excess emission report shal format for the compliance certification report and excessame time as the application. | l be approved by the Department. A proposed |
| ***** The source shall record any malfunction that causes or ma Malfunctions shall be reported to the Department the n | |

be reported to the Department immediately.

EMISSION UNIT HAZARDOUS AIR POLLUTANT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-126 11-93

Information attached? y (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|---|
| 3. Stack identification number: S02 | 4. Unit identification number: EU02 |

5. Unit material description: Natural gas combustion

6. Complete the following summary of hazardous air emissions from this unit. Attach sample calculations and emission factor references. Attached? See Appendix C

| references. Attached? | See Appendix C | | | | |
|-----------------------|----------------|--|------------------|-----------|-------------------|
| Pollutant CAS | Actual emiss | tual emissions Maximum theoretical emissions | | | Potential to emit |
| | | Units | | Units | |
| | SEE APPENDIX | C FOR HA | PS EMISSIONS CAL | CULATIONS | |
| | | | | | TPY |

EMISSION UNIT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-128 11-93 Information

Information attached? <u>y</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|--|
| 3. Stack identification number: S02 | 4. Unit identification number: EU02 |

5. Complete the following emissions summary for the following pollutants. Attach sample calculations and emission factor references. Attached? See Appendix C

| Air pollutant | Actua | al | Maximum theoretical emissions | | | Potential to emit | Maxin | Maximum allowable | | |
|---------------|-------|-----|-------------------------------|---|-----|-------------------|-------|-------------------|-----|--|
| | U | TPY | | U | TPY | | | U | TPY | |

SEE APPENDIX C FOR EMISSIONS CALCULATIONS

| Sulfur dioxide | | | | TPY | | |
|----------------------|--|--|--|-----|--|--|
| Organic compounds | | | | TPY | | |
| Carbon monoxide | | | | TPY | | |
| Lead | | | | TPY | | |
| Nitrogen oxides | | | | TPY | | |
| Total reduced sulfur | | | | TPY | | |
| Mercury | | | | TPY | | |
| Asbestos | | | | TPY | | |
| Beryllium | | | | TPY | | |
| Vinyl chloride | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |

Units (U) should be entered as follows:

- 1 = lb/hr
- 2 = lb/mmBTU
- $3 = \frac{\text{grains/dscf}}{\text{grains/dscf}}$
- 4 = lb/gallon
- 5 = ppmdv
- 6 = other (specify)
- 7 = other (specify)
- 8 = other (specify)

CURRENT EMISSIONS REQUIREMENTS AND STATUS OF UNIT AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-130 Rev. 12-99 Information attached? <u>n</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| EE INSTRUCTIONS ON REVE | RSE SIDE | 1 | | | | | | |
|---|---|--|---|---------------------------|--|-------------------------------------|--|--|
| 1. Facility name: Nemadji Tra | ail Energy Center | 2. Facility identification number: To be assigned 816127840 | | | | | | |
| 3. Stack identification numbe | r: S02 | 4. Unit identification number: EU02 | | | | | | |
| 5. Pollutant | 6. Wis. Adm. Code Wis. Stats., 40 CFR | 7. State Only | 8. Limitation | | 9. Compliance Status (in or out) | | | |
| Particulate | NR415 | X | 0.15 lb PM/MMbtu | | Units not | constructed yet | | |
| Sulfur Dioxide | NR 417, NSPS 40 CFR 60, Subpart Dc | | Keep records of the sulfur content of the natural gas, a certified by the supplier or data and record of the daily usage of natural gas | Units not constructed yet | | | | |
| Nitrogen Dioxide | NR 428 | X | | | Units not constructed yet | | | |
| Carbon Monoxide | NR 426 | X | | Un | | | | |
| Lead | NR 427 | X | | | Units not constructed yet | | | |
| Volatile Organic Compounds | NR 419 | X | | | Units not | constructed yet | | |
| Opacity | NR 431 | X | 20% opacity | | Units not constructed yet | | | |
| 10. Other requirements (e.g., material existing permit, etc.) | alfunction reporting, sp | ecial operati | ng conditions from an | Star | te Only | Compliance Status (in or out) | | |
| | | | | | | | | |

** PART 70 SOURCES ONLY:

- 1. Be sure to review the Compliance Assurance Monitoring (CAM) Rule, 40 CFR Part 64, for the Renewal Application. The CAM rule requires owners and operators of Part 70 sources to monitor the operation and maintenance of their control equipment so that they can evaluate the performance of their control devices and report whether or not their facilities meet established emission standards. All facilities that have a Title V, Part 70, Federal Operating Permit are required to meet the CAM rule and submit a CAM plan with this Title V renewal application. The rule requires that a CAM plan be submitted with the Title V renewal application for each pollutant at each emissions unit which has a potential to emit prior to controls of that pollutant greater than the major source threshold for the respective pollutant. Please refer to the CAM Technical Guidance web site at http://www.epa.gov/ttn/emc/cam.html for further documentation on the rule and how to prepare a CAM plan for submittal with the renewal application.
- 2. List all applicable **Maximum Achievable Control Technology** (MACT) rule(s) and the effective date(s) if they were promulgated during the last 3 years of your operation permit term. Identify the emissions units subject to each MACT rule listed.

Start date:

State of Wisconsin Department of Natural Resources

EMISSION UNIT COMPLIANCE PLAN COMMITMENTS AND SCHEDULE AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-131 11-93 Information attached? \underline{n} (y/n)

1. Facility name: Nemadji Trail Energy
Center

2. Facility identification number: To be assigned 816127840

3. Stack identification number: S02

4. Unit identification number: EU02

5. For Units that are presently in compliance with all applicable requirements, including any enhanced monitoring and compliance certification requirements under section 114(a)(3) of the Clean Air Act that apply, complete the following. These commitments are part of the application for Part 70 permits.

□ We will continue to operate and maintain this Unit in compliance with all applicable requirements.

□ Form 4530-130 includes new requirements that apply or will apply to this Unit during the term of the permit. We will meet such requirements on a timely basis.

6. For Units not presently fully in compliance, complete the following.

This Unit is in compliance with all applicable requirements except for those indicated below. We will achieve compliance

| | according to the | e following schedule | : : | |
|----|------------------|----------------------|--------------------|----------|
| | Applicable | Requirement | Corrective Actions | Deadline |
| 1. | | | | |
| 1. | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| 2. | | | | |
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| | | | | |
| 3. | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | Progress reports | s will be submitted: | | |

and every six (6) months thereafter

F03 June 2020

State of Wisconsin

STACK IDENTIFICATION

Department of Natural Resources

AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-103 11-93 Information attached? <u>n</u> (y/n)

| SEE INSTRUCTIONS ON REVERSE SIDE | 1 01111 1000 100 11 70 | <u> </u> | | | | | | | |
|---|--|------------------------------------|--|--|--|--|--|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 | 3. Stack identification number: NA | | | | | | | |
| 4. Exhausting Unit(s), use Unit identification | n number from appropriate Form(s) 4530-10 | 4, 106, 107, 108 and/or 109 | | | | | | | |
| 4530-104 4530-106 | 4530-107 4530-108 | 4530-109 <u>F01</u> F03 | | | | | | | |
| 5. Identify this stack on the plot plan require | d on Form 4530-101 | | | | | | | | |
| 6. Indicate by checking: ☐ This stack has an actual exhaust po If this stack has an actual exhaust poin | int. This stack serves to identify fu | | | | | | | | |
| 7. Discharge height above ground level: (feet) | | | | | | | | | |
| 8. Inside dimensions at outlet (check one and | l complete): | | | | | | | | |
| ☐ Circular (feet) | ☐ rectangular length (feet) | width (feet) | | | | | | | |
| 9. Exhaust flow rate: | | | | | | | | | |
| Normal(ACFM) | Maximum(ACFM | I) | | | | | | | |
| 10. Exhaust gas temperature (normal): | _(°F) | | | | | | | | |
| 11. Exhaust gas moisture content: | Normal volume percent | Maximum volume percent | | | | | | | |
| 12. Exhaust gas discharge direction: | □ Up □ Down | ☐ Horizontal | | | | | | | |
| 13. Is this stack equipped with a rainhat or exhaust gases from the stack? | any obstruction to the free flow of the | □ Yes □ No | | | | | | | |
| ***** Complete the appropriate Air Perm exhausting through this stack. | it Application Forms(s) 4530-104, 106, 107, | 108 or 109 for each Unit ***** | | | | | | | |

MISCELLANEOUS PROCESSES AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-109 11-93 Information attached? <u>n</u> (y/n)

| SEE INSTRUCTIONS | ON REVERSE SIDE | | | | / |
|-------------------------|---|-----------------------------------|---------------|---|------------|
| 1. Facility name: Nem | adji Trail Energy Center | 2. Facility identification | number: 816 | 5127840 | |
| 3. Stack identification | number: NA | 4. Process number: F01 | F03 | | |
| 4a. Unit description: | circuit breakers | | | | |
| 5. Indicate the control | technology status. | olled Controlled | | | |
| If the process is | controlled, enter the control device | ee number(s) from the app | ropriate form | n(s): | |
| 4530-110 4530-114 | | 530-112 4530- 530-116 4530- | | | |
| 6. Source Classificatio | n Code (SCC): 31300500 | | | | |
| 7. Date of construction | or last modification: TBD | | | | |
| 8. Normal operating so | chedule: <u>24</u> hrs./day <u>7</u> d | ays/wk. <u>365</u> days/yı | :. | | |
| | ss (please attach a flow diagram o will interrupt current flow after a | | | Attached? See next pag Figures are at end of | |
| 10. List the types an | d amounts of raw materials used i | in this process: | | rigules are at end of | Appendix A |
| Material | Storage/material handling process | Average usage | Units | Maximum usage | Units |
| SF ₆ | Circuit breaker (19 kV) | 0.23 | lbs/yr | 0.23 | lbs/yr |
| SF ₆ | Circuit breaker (345 kV) | 10.31 | lbs/yr | 10.31 | lbs/yr |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| 11. List the types an | d amounts of finished products: | | | | |
| Material | Storage/material handling process | Average amount produced | Units | Maximum amount produced | Units |
| N/A | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| 12. Process fuel usage | | | | | |
| Type of fuel | Maximum heat input to process million BTU/hr. | Average usage | Units | Maximum usage | Units |
| N/A | | | | | |
| | | | | | |
| | | | | | |
| | gitive emissions associated with thoads, open conveyors, etc.: N/A | nis process, such as outdoo | or storage | Attached? No | /A |
| DESCRIPTION | sions unit, identify the method(s) ON OF METHODS USED FOR I ment(s) to this form. This is not | DETERMINING COMPL | LIANCE. At | eleting Form 4530-118, ** tach Form 4530-118 | **** |
| | te the Air Pollution Control Permi | | | 30-128 for this Unit. *** | ** |

F03

State of Wisconsin Department of Natural Resources COMPLIANCE CERTIFICATION - MONITORING AND REPORTING DESCRIPTION OF METHODS USED FOR DETERMINING COMPLIANCE Form 4530-118 11-93 Information attached? <u>n</u> (y/n)

All applicants except non-Part 70 sources are required to certify compliance with all applicable air pollution permit requirements by including a statement within the permit application of the methods used for determining compliance (please see sec. NR 407.05(4)(i), Wis. Adm. Code.) This statement must include a description of the monitoring, recordkeeping, and reporting requirements and test methods. In addition, the application must include a schedule for compliance certification submittals during the permit term. These submittals must be no less frequent than annually, and may need to be more frequent if specified by the underlying applicable requirement or by the Department.

| SEE | INCTRI | ICTIONS | ON REVERSE | SIDE |
|------|---------|---------|-------------|------|
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| EE INSTRUCTIONS ON REVERSE SIDE | |
|---|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 |
| 3. Stack identification number: NA | 4. Unit identification number: F01 F03 |
| | mpliance with the requirements of the permit (check all that apply |
| ☐ Continuous Emission Monitoring (CEM) - Form 4530-1 Pollutant(s): | 19 |
| ☐ Periodic Emission Monitoring Using Portable Monitors Pollutant(s): | - Form 4530-120 |
| ☐ Monitoring Control System Parameters or Operating Par Pollutant(s): | rameters of a Process - Form 4530-121 |
| ☐ Monitoring Maintenance Procedures - Form 4530-122 Pollutant(s): | |
| ☐ Stack Testing - Form 4530-123 Pollutant(s): | |
| ☐ Fuel Sampling and Analysis (FSA) - Form 4530-124 Pollutant(s): | |
| Recordkeeping - Form 4530-125 Pollutant(s): Geenhouse gases – sulfur hexafluoride (SF | · · · · · · · · · · · · · · · · · · · |
| ☐ Other (please describe) - Form 4530-135 Pollutant(s): | |
| 6. Compliance certification reports will be submitted to the D | epartment according to the following schedule: |
| • | eparament according to the following senedate. |
| Start date: At date of permit issuance and every 12 months thereafter. | |
| Compliance monitoring reports will be submitted to the | Department according to the following schedule: |
| Start date: At date of permit issuance and every 6 months thereafter. | |

F03

State of Wisconsin Department of Natural Resources

COMPLIANCE DEMONSTRATION BY RECORDKEEPING AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-125 11-93 Information attached? <u>n</u> (y/n)

Recordkeeping may be acceptable as a compliance demonstration method provided that a correlation between the parameter value recorded and the emission rate of a particular pollutant is established in the form of a curve or chart of emission rate versus parameter values. This correlation may constitute the certification of the system. It should be attached for Department approval. If it is not attached, please submit it within 60 days of the startup of the system.

| SEE INSTRUCTIONS ON REVERSE SIDE | |
|---|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 |
| 3. Stack identification number: NA | 4. Unit identification number: F01 F03 |
| 5. Pollutant(s) being monitored: Greenhouse gases – sulfur hexafluoride (SF ₆) | 6. Material or parameter being monitored and recorded: SF ₆ |
| 7. Method of monitoring and recording: recordkeeping | |
| 8. List any EPA methods used: N/A | |
| 9. Is this an existing method of demonstrating compliance? ☐ Yes ✓ No | 10. Installation date: TBD |
| 11. Backup system: N/A | |
| 12. Compliance shall be demonstrated: ☐ Daily ☐ Weekly | ■ Monthly □ Batch (not to exceed monthly) |
| assurance procedures. A quality assurance/quality co | ase submit it within 60 days of the startup of the recordkeeping |
| ***** The compliance records shall be available for Department certification report and the excess emission report shal format for the compliance certification report and excessame time as the application. | l be approved by the Department. A proposed |
| ***** The source shall record any malfunction that causes or ma Malfunctions shall be reported to the Department the r | |

be reported to the Department immediately.

EMISSION UNIT HAZARDOUS AIR POLLUTANT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-126 11-93

Information attached? n (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| DEE II (DIRECTION DIVIE CENDE DIDE | |
|---|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 |
| 3. Stack identification number: NA | 4. Unit identification number: F01 F03 |

5. Unit material description: Greenhouse gases – SF₆

6. Complete the following summary of hazardous air emissions from this unit. Attach sample calculations and emission factor

| references. A | ttached?no | ruous un cimission | S Hom tins time. Attac | ii sampre carcaration | is and emission factor |
|---------------|------------|--------------------|------------------------|-----------------------|------------------------|
| | | | | | |
| | | Units | | Units | |
| | NO HAP | S EMISSIONS FI | ROM THE CIRCUIT E | BREAKERS | |
| | | | | | TPY |
| | | | | | ТРҮ |
| | | | | | TPY |
| | | | | | |
| | | | | | TPY |
| | | | | | TPY |
| | | | | | TPY |
| | | | | + + | TPY |
| | | | | | TPY |
| | | | | | TPY |

EMISSION UNIT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-128 11-93 Information a

Information attached? <u>y</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 |
|---|--|
| 3. Stack identification number: NA | 4. Unit identification number: F01 F03 |

5. Complete the following emissions summary for the following pollutants. Attach sample calculations and emission factor references. Attached? _See Appendix B Appendix C

| | U | TPY | U | TPY | | | | U | TPY |
|--|---|-----|---|-----|--|--|--|---|-----|

Appendix C SEE APPENDIX B-FOR EMISSION CALCULATIONS

| Sulfur dioxide | | | | TPY | | |
|----------------------|--|--|---|-----|--|--|
| | | | | | | |
| Organic compounds | | | - | TPY | | |
| Carbon monoxide | | | | TPY | | |
| Lead | | | | TPY | | |
| Nitrogen oxides | | | | TPY | | |
| Total reduced sulfur | | | | TPY | | |
| Mercury | | | | TPY | | |
| Asbestos | | | | TPY | | |
| Beryllium | | | | TPY | | |
| Vinyl chloride | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |

Units (U) should be entered as follows:

^{1 =} lb/hr

^{2 =} lb/mmBTU

^{3 =} grains/dscf

^{4 =} lb/gallon

^{5 =} ppmdv

^{6 =} other (specify)

^{7 =} other (specify)

^{8 =} other (specify)

CURRENT EMISSIONS REQUIREMENTS AND STATUS OF UNIT AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-130 Rev. 12-99 Information attached? __(y/n)

| EE INSTRUCTIONS ON REVE | RSE SIDE | - | | | |
|---|----------|--|--|------------|--|
| 1. Facility name: Nemadji Trail Energy Center | | 2. Facility identification number: 816127840 | | | |
| 3. Stack identification number | : NA | 4. Unit identification number: F01 F03 | | | |
| | | 7. State Only | | | |
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| | _ | | | State Only | |
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** PART 70 SOURCES ONLY:

1. Be sure to review the Compliance Assurance Monitoring (CAM) Rule, 40 CFR Part 64, for the Renewal Application. The CAM rule requires owners and operators of Part 70 sources to monitor the operation and maintenance of their control equipment so that they can evaluate the performance of their control devices and report whether or not their facilities meet established emission standards. All facilities that have a Title V, Part 70, Federal Operating Permit are required to meet the CAM rule and submit a CAM plan with this Title V renewal application. The rule requires that a CAM plan be submitted with the Title V renewal application for each pollutant at each emissions unit which has a potential to emit - prior to controls - of that pollutant greater than the major source threshold for the respective pollutant. Please refer to the CAM Technical Guidance web site at http://www.epa.gov/ttn/emc/cam.html for further documentation on the rule and how to prepare a CAM plan for submittal with the renewal application.

2. List all applicable Maximum Achievable Control Technology (MACT) rule(s) and the effective date(s) if they were promulgated during the last 3 years of your operation permit term. Identify the emissions units subject to each MACT rule listed.

EMISSION UNIT COMPLIANCE PLAN COMMITMENTS AND SCHEDULE AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-131 11-93 Information attached? <u>n</u> (y/n)

| SEE INSTRUCTIONS ON REVERSE SID | <u>E</u> | | | | |
|--|--|---|--|--|--|
| Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 | | | | |
| 3. Stack identification number: NA | 4. Unit identification number: F01 F03 | i e | | | |
| 5. For Units that are presently in complian certification requirements under secton commitments are part of the applica. ☐ We will continue to operate and ☐ Form 4530-130 includes new recommet such requirements on a time. | tice with all applicable requirements, includition 114(a)(3) of the Clean Air Act that application for Part 70 permits. maintain this Unit in compliance with all a quirements that apply or will apply to this lely basis. | ding any enhanced monitoring and compliance oply, complete the following. These | | | |
| 6. For Units <u>not</u> presently fully in complia ☐ This Unit is in compliance with all a according to the following schedule: Applicable Requirement | applicable requirements except for those in | ndicated below. We will achieve compliance Deadline | | | |
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| Progress reports will be submitted: | ix (6) months thereafter | | | | |

From June 2020 Application FACILITY REQUIREMENT COMPLIANCE PLAN COMMITMENTS AND SCHEDULE AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-133 11-93

Information attached? \underline{n} (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification | number: 816127840 | | | | | |
|--|----------------------------|---|--|--|--|--|--|
| 3. For facilities that are presently in compliance with all applicable requirements, including any enhanced monitoring and compliance certification requirements under section 114(a)(3) of the Clean Air Act that apply, complete the following. These commitments are part of the application for Part 70 permits. | | | | | | | |
| ☐ We will continue to operate and maintain this facility in compliance with all applicable requirements. | | | | | | | |
| Form 4530-132 includes new requirements that apply or will apply to this facility during the term of the permit. We will meet such requirements on a timely basis. | | | | | | | |
| 4. For facilities <u>not</u> presently fully in compliance, complet | e the following. | | | | | | |
| ☐ This facility is in compliance with all applicable requaccording to the following schedule: | irements except for those | indicated below. We will achieve compliance | | | | | |
| Applicable Requirement | Corrective Actions | Deadline | | | | | |
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| Progress reports will be submitted: | | | | | | | |
| Start date: and every six (6) months the | reafter | | | | | | |

STACK IDENTIFICATION AIR POLLUTION CONTROL PERMIT APPLICATION Form 4520 103 11 03

Form 4530-103 11-93 Information attached? <u>n</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE 1. Facility name: Nemadji Trail Energy 2. Facility identification number: To be 3. Stack identification number: S04 Center assigned 816127840 4. Exhausting Unit(s), use Unit identification number from appropriate Form(s) 4530-104, 106, 107, 108 and/or 109 4530-107 4530-108 4530-104 EU04 4530-106 4530-109 5. Identify this stack on the plot plan required on Form 4530-101 6. Indicate by checking: ✓ This stack has an actual exhaust point. ☐ This stack serves to identify fugitive emissions. If this stack has an actual exhaust point, then provide the following stack parameters 7. Discharge height above ground level: 15 (feet) 8. Inside dimensions at outlet (check one and complete): 1.67__(feet) ✓ Circular □ rectangular length (feet) width (feet) 9. Exhaust flow rate: Maximum 3,272 (ACFM) Normal 3,272 (ACFM) Exhaust gas temperature (normal): <u>750</u> (°F) 11. Exhaust gas moisture content: Normal volume percent Maximum volume percent Exhaust gas discharge direction: **☑** Up □ Down ☐ Horizontal Is this stack equipped with a rainhat or any obstruction to the free flow of the ☐ Yes ✓ No exhaust gases from the stack? Complete the appropriate Air Permit Application Forms(s) 4530-104, 106, 107, 108 or 109 for each Unit ***** exhausting through this stack.

BOILER OR FURNACE OPERATION AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-104 11-93

Information attached? \underline{n} (y/n)

| SEE INSTRUCTIONS ON REVERSE SIDE | <u> </u> | | | | |
|--|----------------------------|--------------------------------|----------------------------------|----------------------|--|
| 1. Facility name: Nemadji Trail Energy Cer | nter | 2. Facility identificat | ion number: To be ass | igned 816127840 | |
| 3. Stack identification number: S04 | | 4. Boiler/furnace number: EU04 | | | |
| 4a. Unit description: | | | | | |
| Natural gas-fired heater for maintaining the combustion turbine. | e pipeline-grade natura | l gas at or above the m | ixture's dew point bef | ore injection in the | |
| 5. Indicate the boiler/furnace control technology | ology status. | Jncontrolled 🗹 Co | ontrolled | | |
| If the boiler/furnace is controlled, ent | er the control device n | umber(s) from the app | ropriate forms: | | |
| 4530-110 4530-111 4530-114 4530-115 | 4530-112 _ 4530-116 _ | 4530-113 4530-117 | _ | | |
| 6. Furnace type: | | 7. Maximum continu | ous rating: 10 MMBt | u/hr | |
| 8. Manufacturer: TBD | | 9. Model number: TI | BD . | | |
| 10. Date of construction or last modificat | ion: 06/01/2021 | | | | |
| | | | | | |
| 11. Fuels and firing conditions: | | | | | |
| | Primary fuel | Backup fuel #1 | Backup fuel #2 | Backup fuel #3 | |
| Fuel name | Natural Gas | | | | |
| Higher heating value | 1,020 Btu/scf | | | | |
| Maximum sulfur content (Wt.%) | Pipeline-grade | | | | |
| Maximum ash content (Wt.%) | N/A | | | | |
| Excess Combustion Air (%O ₂) | N/A | | | | |
| Moisture content (as fired) (%) | N/A | | | | |
| Maximum hourly consumption | 9,804 scf/hr | | | | |
| Actual yearly consumption | 85.9 x 10 ⁶ scf | | | | |

CONTROL EQUIPMENT MISCELLANEOUS AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-110 11-93 Information attached? \underline{N} (y/n)

| SEE | INS | TRU | CTIC | NS | ON RE | EVERSE | SIDE |
|-----|-----|-----|------|----|-------|--------|------|
| | | | | | | | |

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|--|
| 3. Stack identification number: S04 | 4. Unit identification number: EU04 |
| 5. Control device number: C04 | |
| | |

6. Manufacturer and model number: TBD

7. Date of installation: 06/01/2021

8. Describe in detail the device in use. Attach a diagram of the system. Attached? No Low NO_x burner – Low NO_x burners control flame temperatures by using a two-stage combustion process which limits thermal NO_x formation.

9. List the pollutants to be controlled by this equipment and the expected control efficiency for each pollutant on the table below.

□ Documentation is attached?

| Pollutant | Inlet po concen | | Hood capture efficiency (%) | poll | itlet utant ntration | Efficiency |
|-----------------|--------------------|------|-----------------------------|------------|----------------------------|---|
| | gr/acf | ppmv | | gr/ac f | ppmv | |
| NO _x | | | 100% | | | Controls emissions of NO _x to 0.049 lb/MMBtu of heat input |
| | | | | | | |
| | | | | | | |

10. Discuss how the collected material will be handled for reuse or disposal.

N/A.

- 11. Prepare a malfunction prevention and abatement plan (if required under s. NR 439.11) for this pollution control system. Please include the following:
 - a. Identification of the individuals(s), by title, responsible for inspecting, maintaining and repairing this device.
 - b. Operation variables such as temperature that will be monitored in order to detect a malfunction or breakthrough, the correct operating range of these variables, and a detailed description of monitoring or surveillance procedures that will be used to show compliance.
 - c. What type of monitoring equipment will be provided (temperature sensors, pressure sensors, CEMs).
 - d. An inspection schedule and items or conditions that will be inspected.
 - e. A listing of materials and spare parts that will be maintained in inventory.
 - f. Is this plan available for review?

COMPLIANCE CERTIFICATION - MONITORING AND REPORTING DESCRIPTION OF METHODS USED FOR DETERMINING COMPLIANCE Form 4530-118 11-93 Information attached? n (y/n)

All applicants except non-Part 70 sources are required to certify compliance with all applicable air pollution permit requirements by including a statement within the permit application of the methods used for determining compliance (please see sec. NR 407.05(4)(i), Wis. Adm. Code.) This statement must include a description of the monitoring, recordkeeping, and reporting requirements and test methods. In addition, the application must include a schedule for compliance certification submittals during the permit term. These submittals must be no less frequent than annually, and may need to be more frequent if specified by the underlying applicable requirement or by the Department.

| SEE | INCTR | RUCTIO | VIS O | NREV | JERSE | SIDE |
|-----|---------|----------|-------|-------|-------|------|
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| EE INSTRUCTIONS ON REVERSE SIDE | | | | | | |
|---|--|--|--|--|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | | | | | |
| 3. Stack identification number: S04 | 4. Unit identification number: EU04 | | | | | |
| 5. This Unit will use the following method(s) for determining con and attach the appropriate form(s) to this form). | appliance with the requirements of the permit (check all that apply | | | | | |
| ☐ Continuous Emission Monitoring (CEM) - Form 4530-1 Pollutant(s): | 19 | | | | | |
| ☐ Periodic Emission Monitoring Using Portable Monitors - Pollutant(s): | - Form 4530-120 | | | | | |
| ☐ Monitoring Control System Parameters or Operating Par Pollutant(s): | ameters of a Process - Form 4530-121 | | | | | |
| ☐ Monitoring Maintenance Procedures - Form 4530-122 Pollutant(s): | | | | | | |
| ☐ Stack Testing - Form 4530-123 Pollutant(s): | | | | | | |
| ☐ Fuel Sampling and Analysis (FSA) - Form 4530-124 Pollutant(s): | | | | | | |
| Recordkeeping - Form 4530-125 Pollutant(s): all pollutants | | | | | | |
| ☐ Other (please describe) - Form 4530-135 Pollutant(s): | | | | | | |
| 6. Compliance certification reports will be submitted to the De | epartment according to the following schedule: | | | | | |
| Start date: At date of permit issuance and every 12 months thereafter. | | | | | | |
| Compliance monitoring reports will be submitted to the | Department according to the following schedule: | | | | | |
| Start date: At date of permit issuance and every6 months thereafter. | | | | | | |

COMPLIANCE DEMONSTRATION BY RECORDKEEPING AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-125 11-93

Information attached? \underline{n} (y/n)

Recordkeeping may be acceptable as a compliance demonstration method provided that a correlation between the parameter value recorded and the emission rate of a particular pollutant is established in the form of a curve or chart of emission rate versus parameter values. This correlation may constitute the certification of the system. It should be attached for Department approval. If it is not attached, please submit it within 60 days of the startup of the system.

| SEE INSTRUCTIONS ON REVERSE SIDE | |
|---|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
| 3. Stack identification number: S04 | 4. Unit identification number: EU04 |
| 5. Pollutant(s) being monitored: SO ₂ | Material or parameter being monitored and recorded: Sulfur content of natural gas. |
| 7. Method of monitoring and recording: Owners will keep records of the sulfur content of the natural daily usage of natural gas. | gas as certified by the supplier or test data and record the |
| 8. List any EPA methods used: N/A | |
| 9. Is this an existing method of demonstrating compliance? ☐ Yes ☑ No | 10. Installation date: 06/01/2021 |
| 11. Backup system: N/A | |
| 12. Compliance shall be demonstrated: ☑ Daily ☐ Weekly | ☐ Monthly ☐ Batch (not to exceed monthly) |
| 13. Indicate by checking: | |
| assurance procedures. A quality assurance/quality co | ase submit it within 60 days of the startup of the recordkeeping |
| ***** The compliance records shall be available for Department certification report and the excess emission report shal format for the compliance certification report and excessame time as the application. | l be approved by the Department. A proposed |
| ***** The source shall record any malfunction that causes or ma Malfunctions shall be reported to the Department the n be reported to the Department immediately. | |

COMPLIANCE DEMONSTRATION BY RECORDKEEPING AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-125 11-93 Information attached? <u>n</u> (y/n)

Recordkeeping may be acceptable as a compliance demonstration method provided that a correlation between the parameter value recorded and the emission rate of a particular pollutant is established in the form of a curve or chart of emission rate versus parameter values. This correlation may constitute the certification of the system. It should be attached for Department approval. If it is not attached, please submit it within 60 days of the startup of the system.

| SEE INSTRUCTIONS ON REVERSE SIDE | | | |
|---|---|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | | |
| 3. Stack identification number: S04 | 4. Unit identification number: EU04 | | |
| 5. Pollutant(s) being monitored: All | 6. Material or parameter being monitored and recorded: Hours of operation of the natural gas heater will be recorded so that emissions may be calculated. | | |
| 7. Method of monitoring and recording: Hours of operation | | | |
| 8. List any EPA methods used: Not applicable | | | |
| 9. Is this an existing method of demonstrating compliance? ☐ Yes ☑ No | 10. Installation date: 06/01/2021 | | |
| 11. Backup system: N/A | | | |
| 12. Compliance shall be demonstrated: ☐ Daily ☐ Weekly | ✓ Monthly ☐ Batch (not to exceed monthly) | | |
| assurance procedures. A quality assurance/quality co | ase submit it within 60 days of the startup of the recordkeeping | | |
| ***** The compliance records shall be available for Department certification report and the excess emission report shal format for the compliance certification report and excessame time as the application. | l be approved by the Department. A proposed | | |
| **** The source shall record any malfunction that causes or may cause an emission limit to be exceeded. ***** Malfunctions shall be reported to the Department the next business day. Hazardous air spills shall | | | |

be reported to the Department immediately.

EMISSION UNIT HAZARDOUS AIR POLLUTANT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-126 11-93 Information attached? <u>v</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|--|
| 3. Stack identification number: S04 | 4. Unit identification number: EU04 |

5. Unit material description: Natural Gas Combustion

6. Complete the following summary of hazardous air emissions from this unit. Attach sample calculations and emission factor references. Attached? See Appendix C

| references. Attached? | See Appendix C | | 1 | | |
|-----------------------|----------------|----------|--------------------|--------------|-------------------|
| Pollutant CAS | Actual emiss | ions | Maximum theoretica | al emissions | Potential to emit |
| | | Units | | Units | |
| | SEE APPENDIX | C FOR HA | PS EMISSIONS CAL | CULATIONS | |
| | | | | | TPY |

EMISSION UNIT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-128 11-93

Information attached? y_ (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|--|
| 3. Stack identification number: S04 | 4. Unit identification number: EU04 |

5. Complete the following emissions summary for the following pollutants. Attach sample calculations and emission factor references. Attached? See Appendix C

| Air pollutant | Actua | al | Maximum theoretical emissions | | | | Maxin | num a | llowable |
|---------------|-------|-----|-------------------------------|---|-----|--|-------|-------|----------|
| | U | TPY | | U | TPY | | | U | TPY |

SEE APPENDIX C FOR EMISSIONS CALCULATIONS

| | | · · | | |
|----------------------|------------------|-----|---|---|
| Sulfur dioxide | | TPY | 7 | |
| Organic compounds | | TPY | 7 | _ |
| Carbon monoxide | | TPY | 7 | |
| Lead | | TPY | 7 | |
| Nitrogen oxides | | TPY | 7 | |
| Total reduced sulfur | | TPY | 7 | |
| Mercury | | TPY | 7 | |
| Asbestos | | TPY | 7 | |
| Beryllium | | TPY | 7 | |
| Vinyl chloride | | TPY | 7 | |
| | | TPY | | |

Units (U) should be entered as follows:

- 1 = lb/hr
- 2 = lb/mmBTU
- $3 = \frac{\text{grains}}{\text{dscf}}$
- 4 = lb/gallon
- 5 = ppmdv
- 6 = other (specify)
- 7 = other (specify)
- 8 = other (specify)

CURRENT EMISSIONS REQUIREMENTS AND STATUS OF UNIT AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-130 Rev. 12-99 Information attached? \underline{n} (y/n)

| EE INSTRUCTIONS ON REVE | RSE SIDE | | | | | | |
|---|---|---|--|---|--|--|--|
| 1. Facility name: Nemadji Tra | ail Energy Center | 2. Facility identification number: To be assigned 816127840 | | | | | |
| 3. Stack identification number: S04 | | | 4. Unit identification number: EU04 | | | | |
| 5. Pollutant | 6. Wis. Adm. Code Wis. Stats., 40 CFR | 7. State Only | State State | | | | |
| Particulate | NR 415 | X | 0.15 lb/MMBtu | Units not constructed yet | | | |
| Sulfur Dioxide | NR 417, NSPS 40 CFR 60, Subpart Dc | | Keep records of the sulfur content of the natural gas as certified by the supplier or test data and record the daily usage | Units not constructed yet | | | |
| Nitrogen Dioxide | NR 428 | X | | Units not constructed yet | | | |
| Carbon Monoxide | NR 426 | X | | Units not constructed yet | | | |
| Lead | NR 427 | X | | Units not constructed yet | | | |
| Volatile Organic Compounds Opacity | NR 419 NR 431 | X X | 20% opacity | Units not constructed yet Units not constructed yet | | | |
| 10. Other requirements (e.g., materisting permit, etc.) | alfunction reporting, spe | cial operati | ng conditions from an Sta | compliance Status (in or out) | | | |
| | | | | | | | |

** PART 70 SOURCES ONLY:

1. Be sure to review the Compliance Assurance Monitoring (CAM) Rule, 40 CFR Part 64, for the Renewal Application. The CAM rule requires owners and operators of Part 70 sources to monitor the operation and maintenance of their control equipment so that they can evaluate the performance of their control devices and report whether or not their facilities meet established emission standards. All facilities that have a Title V, Part 70, Federal Operating Permit are required to meet the CAM rule and submit a CAM plan with this Title V renewal application. The rule requires that a CAM plan be submitted with the Title V renewal application for each pollutant at each emissions unit which has a potential to emit - prior to controls - of that pollutant greater than the major source threshold for the respective pollutant. Please refer to the CAM Technical Guidance web site at http://www.epa.gov/ttn/emc/cam.html for further documentation on the rule and how to prepare a CAM plan for submittal with the renewal application.

2. List all applicable Maximum Achievable Control Technology (MACT) rule(s) and the effective date(s) if they were promulgated during the last 3 years of your operation permit term. Identify the emissions units subject to each MACT rule listed.

EMISSION UNIT COMPLIANCE PLAN COMMITMENTS AND SCHEDULE AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-131 11-93 Information attached? \underline{n} (y/n)

| SEE INSTRUCTIONS ON REVERSE SII | DE | |
|---|--|---|
| Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To b | e assigned 816127840 |
| 3. Stack identification number: S04 | 4. Unit identification number: EU04 | |
| 5. For Units that are presently in complia | ection 114(a)(3) of the Clean Air Act that | uding any enhanced monitoring and compliance apply, complete the following. These |
| ☐ We will continue to operate and | d maintain this Unit in compliance with al | l applicable requirements. |
| Form 4530-130 includes new remeet such requirements on a til | | s Unit during the term of the permit. We will |
| 6. For Units <u>not</u> presently fully in comp ☐ This Unit is in compliance with all according to the following schedul | applicable requirements except for those | indicated below. We will achieve compliance |
| Applicable Requirement | Corrective Actions | Deadline |
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| Progress reports will be submitted: | | |
| | six (6) months thereafter | |

STACK IDENTIFICATION AIR POLLUTION CONTROL PERMIT APPLICATION Form 4520 103 11 03

Form 4530-103 11-93 Information attached? <u>n</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE 2. Facility identification number: To be 1. Facility name: Nemadji Trail Energy 3. Stack identification number: S05 Center assigned 816127840 4. Exhausting Unit(s), use Unit identification number from appropriate Form(s) 4530-104, 106, 107, 108 and/or 109 4530-107 4530-108 4530-104 EU05 4530-106 4530-109 5. Identify this stack on the plot plan required on Form 4530-101 6. Indicate by checking: ✓ This stack has an actual exhaust point. ☐ This stack serves to identify fugitive emissions. If this stack has an actual exhaust point, then provide the following stack parameters 7. Discharge height above ground level: 15 (feet) 8. Inside dimensions at outlet (check one and complete): 1.67__(feet) ✓ Circular □ rectangular length (feet) width (feet) 9. Exhaust flow rate: Maximum 3,272 (ACFM) Normal 3,272 (ACFM) Exhaust gas temperature (normal): <u>750</u> (°F) 11. Exhaust gas moisture content: Normal volume percent Maximum volume percent Exhaust gas discharge direction: **☑** Up □ Down ☐ Horizontal Is this stack equipped with a rainhat or any obstruction to the free flow of the ☐ Yes ✓ No exhaust gases from the stack? Complete the appropriate Air Permit Application Forms(s) 4530-104, 106, 107, 108 or 109 for each Unit ***** exhausting through this stack.

Maximum hourly consumption

Actual yearly consumption

BOILER OR FURNACE OPERATION AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-104 11-93

Information attached? n (v/n)

| SEE INSTRUCTIONS ON REVERSE SID | | | miorinat | ion attached? <u>II</u> (y/II | | | |
|---|------------------------------|---|--------------------------|-------------------------------|--|--|--|
| 1. Facility name: Nemadji Trail Energy Ce | enter | 2. Facility identification number: To be assigned 816127840 | | | | | |
| 3. Stack identification number: S05 | | 4. Boiler/furnace nu | mber: EU05 | | | | |
| 4a. Unit description: | | | | | | | |
| Natural gas-fired heater for maintaining th combustion turbine. | e pipeline-grade natura | l gas at or above the m | iixture's dew point befo | ore injection in the | | | |
| 5. Indicate the boiler/furnace control techn | ology status. | Incontrolled | ontrolled | | | | |
| If the boiler/furnace is controlled, en | ter the control device n | umber(s) from the app | ropriate forms: | | | | |
| 4530-110 4530-11 4530-114 4530-11: | 1 4530-112 _ 5 4530-116 _ | 4530-113 4530-117 | <u>-</u> | | | | |
| 6. Furnace type: 7. Maximum continuous rating: 10 MMBtu/hr | | | | | | | |
| 8. Manufacturer: TBD | | 9. Model number: TBD | | | | | |
| 10. Date of construction or last modification: 06/01/2021 | | | | | | | |
| | | | | | | | |
| 11. Fuels and firing conditions: | | | _ | | | | |
| | Primary fuel | Backup fuel #1 | Backup fuel #2 | Backup fuel #3 | | | |
| Fuel name | Natural Gas | | | | | | |
| Higher heating value | 1,020 Btu/scf | | | | | | |
| Maximum sulfur content (Wt.%) | Pipeline-grade | | | | | | |
| Maximum ash content (Wt.%) | N/A | | | | | | |
| Excess Combustion Air (%O ₂) | N/A | | | | | | |
| Moisture content (as fired) (%) | N/A | | | | | | |
| Maximum hourly consumntion | 9,804 scf/hr | | | | | | |

 $85.9 \times 10^6 \text{ scf}$

CONTROL EQUIPMENT MISCELLANEOUS AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-110 11-93 Information attached? \underline{N} (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|---|
| 3. Stack identification number: S05 | 4. Unit identification number: EU05 |
| 5. Control device number: C05 | |
| | |

6. Manufacturer and model number: TBD

7. Date of installation: 06/01/2021

8. Describe in detail the device in use. Attach a diagram of the system. Attached? No Low NO_x burner – Low NO_x burners control flame temperatures by using a two-stage combustion process which limits thermal NO_x formation.

9. List the pollutants to be controlled by this equipment and the expected control efficiency for each pollutant on the table below.

| _ | T | • | | . 1 10 |
|-----|--------------|---------|-----|-----------|
| - 1 | Llacuman | tation | 10 | attached? |
| _ | 170000111011 | tationi | 1.5 | anaciicu: |

| Pollutant | Inlet pollutant concentration | | | | itlet utant ntration | Efficiency |
|-----------|-------------------------------|------|------|------------|----------------------------|---|
| | gr/acf | ppmv | | gr/ac f | ppmv | |
| NO_x | | | 100% | | | Controls emissions of NO _x to 0.049 lb/MMBtu of heat input |
| | | | | | | |
| | | | | | | |

10. Discuss how the collected material will be handled for reuse or disposal.

N/A.

- 11. Prepare a malfunction prevention and abatement plan (if required under s. NR 439.11) for this pollution control system. Please include the following:
 - a. Identification of the individuals(s), by title, responsible for inspecting, maintaining and repairing this device.
 - b. Operation variables such as temperature that will be monitored in order to detect a malfunction or breakthrough, the correct operating range of these variables, and a detailed description of monitoring or surveillance procedures that will be used to show compliance.
 - c. What type of monitoring equipment will be provided (temperature sensors, pressure sensors, CEMs).
 - d. An inspection schedule and items or conditions that will be inspected.
 - e. A listing of materials and spare parts that will be maintained in inventory.
 - f. Is this plan available for review?

COMPLIANCE CERTIFICATION - MONITORING AND REPORTING DESCRIPTION OF METHODS USED FOR DETERMINING COMPLIANCE Form 4530-118 11-93 Information attached? <u>n</u> (y/n)

All applicants except non-Part 70 sources are required to certify compliance with all applicable air pollution permit requirements by including a statement within the permit application of the methods used for determining compliance (please see sec. NR 407.05(4)(i), Wis. Adm. Code.) This statement must include a description of the monitoring, recordkeeping, and reporting requirements and test methods. In addition, the application must include a schedule for compliance certification submittals during the permit term. These submittals must be no less frequent than annually, and may need to be more frequent if specified by the underlying applicable requirement or by the Department.

SEE INSTRUCTIONS ON REVERSE SIDE

| EE INSTRUCTIONS ON REVERSE SIDE | | | | | |
|--|--|--|--|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | | | | |
| 3. Stack identification number: S05 | 4. Unit identification number: EU05 | | | | |
| 5. This Unit will use the following method(s) for determining compliance with the requirements of the permit (check all that apply and attach the appropriate form(s) to this form). □ Continuous Emission Monitoring (CEM) - Form 4530-119 | | | | | |
| Pollutant(s): | | | | | |
| ☐ Periodic Emission Monitoring Using Portable Monitors Pollutant(s): | - Form 4530-120 | | | | |
| ☐ Monitoring Control System Parameters or Operating Parameters of a Process - Form 4530-121 Pollutant(s): | | | | | |
| ☐ Monitoring Maintenance Procedures - Form 4530-122 Pollutant(s): | | | | | |
| ☐ Stack Testing - Form 4530-123 Pollutant(s): | | | | | |
| ☐ Fuel Sampling and Analysis (FSA) - Form 4530-124 Pollutant(s): | | | | | |
| Recordkeeping - Form 4530-125 Pollutant(s): all pollutants | | | | | |
| ☐ Other (please describe) - Form 4530-135 Pollutant(s): | | | | | |
| | | | | | |
| 6. Compliance certification reports will be submitted to the D | epartment according to the following schedule: | | | | |
| Start date: At date of permit issuance and every 12 months thereafter. | | | | | |
| Compliance monitoring reports will be submitted to the Department according to the following schedule: | | | | | |
| Start date: At date of permit issuance and every6 months thereafter. | | | | | |

COMPLIANCE DEMONSTRATION BY RECORDKEEPING AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-125 11-93

Information attached? \underline{n} (y/n)

Recordkeeping may be acceptable as a compliance demonstration method provided that a correlation between the parameter value recorded and the emission rate of a particular pollutant is established in the form of a curve or chart of emission rate versus parameter values. This correlation may constitute the certification of the system. It should be attached for Department approval. If it is not attached, please submit it within 60 days of the startup of the system.

| SEE INSTRUCTIONS ON REVERSE SIDE | | | | | |
|--|---|--|--|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | | | | |
| 3. Stack identification number: S05 | 4. Unit identification number: EU05 | | | | |
| 5. Pollutant(s) being monitored: SO ₂ | 6. Material or parameter being monitored and recorded: Sulfur content of natural gas. | | | | |
| 7. Method of monitoring and recording: Owners will keep records of the sulfur content of the natural daily usage of natural gas. | gas as certified by the supplier or test data and record the | | | | |
| 8. List any EPA methods used: N/A | | | | | |
| 9. Is this an existing method of demonstrating compliance? ☐ Yes ☑ No | 10. Installation date: 06/01/2021 | | | | |
| 11. Backup system: N/A | | | | | |
| 12. Compliance shall be demonstrated: ☑ Daily ☐ Weekly | ☐ Monthly ☐ Batch (not to exceed monthly) | | | | |
| 13. Indicate by checking: | | | | | |
| The monitoring system shall be subject to appropriate performance specifications, calibration requirements, and quality assurance procedures. □ A quality assurance/quality control plan for the recordkeeping system is attached for Department approval. ☑ If the plan is not attached, please submit it within 60 days of the startup of the recordkeeping program. □ The plan was submitted to the Department on | | | | | |
| ***** The compliance records shall be available for Department inspection. The format for the compliance ***** certification report and the excess emission report shall be approved by the Department. A proposed format for the compliance certification report and excess emission report shall be submitted at the same time as the application. | | | | | |
| ***** The source shall record any malfunction that causes or may cause an emission limit to be exceeded. ***** Malfunctions shall be reported to the Department the next business day. Hazardous air spills shall | | | | | |

be reported to the Department immediately.

COMPLIANCE DEMONSTRATION BY RECORDKEEPING AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-125 11-93

Information attached? n (y/n)

Recordkeeping may be acceptable as a compliance demonstration method provided that a correlation between the parameter value recorded and the emission rate of a particular pollutant is established in the form of a curve or chart of emission rate versus parameter values. This correlation may constitute the certification of the system. It should be attached for Department approval. If it is not attached, please submit it within 60 days of the startup of the system.

| SEE INSTRUCTIONS ON REVERSE SIDE | | | | |
|--|---|--|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | | | |
| 3. Stack identification number: S05 | 4. Unit identification number: EU05 | | | |
| 5. Pollutant(s) being monitored: All | 6. Material or parameter being monitored and recorded: Hours of operation of the natural gas heater will be recorded so that emissions may be calculated. | | | |
| 7. Method of monitoring and recording: Hours of operation | | | | |
| 8. List any EPA methods used: Not applicable | | | | |
| 9. Is this an existing method of demonstrating compliance? ☐ Yes ☑ No | 10. Installation date: 06/01/2021 | | | |
| 11. Backup system: N/A | | | | |
| 12. Compliance shall be demonstrated: ☐ Daily ☐ Weekly | ✓ Monthly ☐ Batch (not to exceed monthly) | | | |
| assurance procedures. A quality assurance/quality co | ase submit it within 60 days of the startup of the recordkeeping | | | |
| **** The compliance records shall be available for Department certification report and the excess emission report shal format for the compliance certification report and excessame time as the application. | l be approved by the Department. A proposed | | | |
| ***** The source shall record any malfunction that causes or may cause an emission limit to be exceeded. ***** Malfunctions shall be reported to the Department the next business day. Hazardous air spills shall | | | | |

be reported to the Department immediately.

EMISSION UNIT HAZARDOUS AIR POLLUTANT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-126 11-93 Information attached? <u>y</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|---|
| 3. Stack identification number: S05 | 4. Unit identification number: EU05 |

5. Unit material description: Natural Gas Combustion

6. Complete the following summary of hazardous air emissions from this unit. Attach sample calculations and emission factor references. Attached? See Appendix C

| references. Attached? | ? See Appendix C | | | | | |
|-----------------------|------------------|-----------|--------------------|--------------|-------------------|--|
| Pollutant CAS | Actual emiss | ions | Maximum theoretica | al emissions | Potential to emit | |
| | | Units | | Units | | |
| | SEE APPENDIX | C FOR HAI | PS EMISSIONS CALO | CULATIONS | | |
| | | | | | TPY | |
| | | | | | TPY | |
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EMISSION UNIT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-128 11-93 Information

Information attached? <u>y</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|--|
| 3. Stack identification number: S05 | 4. Unit identification number: EU05 |

5. Complete the following emissions summary for the following pollutants. Attach sample calculations and emission factor references. Attached? See Appendix C

| Air pollutant | Actua | al | Maximum theoretical emissions | | | Potential to emit | Maxin | Maximum allowable | |
|---------------|-------|-----|-------------------------------|---|-----|-------------------|-------|-------------------|-----|
| | U | TPY | | U | TPY | | | U | TPY |

SEE APPENDIX C FOR EMISSIONS CALCULATIONS

| Sulfur dioxide | | | | TPY | | |
|----------------------|--|--|---|-----|--|--|
| Organic compounds | | | : | TPY | | |
| Carbon monoxide | | | | TPY | | |
| Lead | | | | TPY | | |
| Nitrogen oxides | | | | TPY | | |
| Total reduced sulfur | | | | TPY | | |
| Mercury | | | | TPY | | |
| Asbestos | | | | TPY | | |
| Beryllium | | | | TPY | | |
| Vinyl chloride | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |

Units (U) should be entered as follows:

- 1 = lb/hr
- 2 = lb/mmBTU
- $3 = \frac{\text{grains}}{\text{dscf}}$
- 4 = lb/gallon
- 5 = ppmdv
- 6 = other (specify)
- 7 = other (specify)
- 8 = other (specify)

CURRENT EMISSIONS REQUIREMENTS AND STATUS OF UNIT AIR POLLUTION CONTROL PERMIT APPLICATION
Form 4530-130 Rev. 12-99 Information attached? <u>n</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | | 2. Facili | 2. Facility identification number: To be assigned 816127840 | | | | | |
|---|--|---------------------|--|----------------------------------|--|--|--|--|
| 3. Stack identification numbe | er: S05 | 4. Unit i | 4. Unit identification number: EU05 | | | | | |
| 5. Pollutant | 6. Wis. Adm. Code Wis. Stats., 40 CFR | 7. State Only | 8. Limitation | 9. Compliance Status (in or out) | | | | |
| Particulate | NR 415 | X | 0.15 lb/MMBtu | Units not constructed yet | | | | |
| Sulfur Dioxide | NR 417, NSPS 40 CFR 60, Subpart Dc | | Keep records of the sulfur content of the natural gas as certified by the supplier or test data and record the daily usage | Units not constructed yet | | | | |
| Nitrogen Dioxide | NR 428 | X | | Units not constructed yet | | | | |
| Carbon Monoxide | NR 426 | X | | Units not constructed yet | | | | |
| Lead | NR 427 | X | | Units not constructed yet | | | | |
| Volatile Organic Compounds | NR 419 | X | | Units not constructed yet | | | | |
| Opacity | NR 431 | X | 20% opacity | Units not constructed yet | | | | |
| | | | | | | | | |
| | alfunction reporting | , special ope | rating conditions from an | State Only Compliance Status | | | | |

** PART 70 SOURCES ONLY:

1. Be sure to review the Compliance Assurance Monitoring (CAM) Rule, 40 CFR Part 64, for the Renewal Application. The CAM rule requires owners and operators of Part 70 sources to monitor the operation and maintenance of their control equipment so that they can evaluate the performance of their control devices and report whether or not their facilities meet established emission standards. All facilities that have a Title V, Part 70, Federal Operating Permit are required to meet the CAM rule and submit a CAM plan with this Title V renewal application. The rule requires that a CAM plan be submitted with the Title V renewal application for each pollutant at each emissions unit which has a potential to emit - prior to controls - of that pollutant greater than the major source threshold for the respective pollutant. Please refer to the CAM Technical Guidance web site at http://www.epa.gov/ttn/emc/cam.html for further documentation on the rule and how to prepare a CAM plan for submittal with the renewal application.

2. List all applicable **Maximum Achievable Control Technology** (MACT) rule(s) and the effective date(s) if they were promulgated during the last 3 years of your operation permit term. Identify the emissions units subject to each MACT rule listed.

EMISSION UNIT COMPLIANCE PLAN COMMITMENTS AND SCHEDULE AIR POLLUTION CONTROL PERMIT A

AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-131 11-93 Information attached? <u>n</u> (y/n)

| SEE INSTRUCTIONS O | ON REVERSE SID | Е | | | | | |
|---|---|--|--|--|--|--|--|
| 1. Facility name: Nema Center | adji Trail Energy | 2. Facility identification number: To be | 2. Facility identification number: To be assigned 816127840 | | | | |
| 3. Stack identification 1 | number: S05 | 4. Unit identification number: EU05 | | | | | |
| 5. For Units that are procertification requirements are ☐ We will conti | Stack identification number: S05 4. Unit identification number: EU05 For Units that are presently in compliance with all applicable requirements, including any enhanced monitoring and comp certification requirements under section 114(a)(3) of the Clean Air Act that apply, complete the following. These commitments are part of the application for Part 70 permits. ☐ We will continue to operate and maintain this Unit in compliance with all applicable requirements. ☑ Form 4530-130 includes new requirements that apply or will apply to this Unit during the term of the permit. We will need such requirements on a timely basis. | | | | | | |
| ☐ This Unit is in co | ntly fully in complia ompliance with all a following schedule | : | ndicated below. We will achieve compliance | | | | |
| Applicable | Requirement | Corrective Actions | Deadline | | | | |
| 1. | | | | | | | |
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| | | | | | | | |
| | will be submitted:and every si | ix (6) months thereafter | | | | | |

STACK IDENTIFICATION AIR POLLUTION CONTROL PERMIT APPLICATION From 4520 102 11 02

Form 4530-103 11-93 Information attached? <u>n</u> (y/n)

| SEE INSTRUCTIONS ON REVERSE SIDE | | |
|--|---|------------------------------------|
| 1. Facility name: | 2. Facility identification number: | 3. Stack identification number: |
| Nemadji Trail | To be assigned 816127840 | S06 |
| Energy Center | | |
| 4. Exhausting Unit(s), use Unit identification | n number from appropriate Form(s) 4530- | -104, 106, 107, 108 and/or 109 |
| 4530-104 EU06 4530-106 | 4530-107 4530-108 | 4530-109 |
| 5. Identify this stack on the plot plan require | d on Form 4530-101 | |
| 6. Indicate by checking: This stack has an actual exhaust po | int. ☐ This stack serves to identify | fugitive emissions. |
| If this stack has an actual exhaust poin | t, then provide the following stack param | eters |
| <u> </u> | | |
| 7. Discharge height above ground level: 1 | | |
| 8. Inside dimensions at outlet (check one and | l complete): | |
| ✓ Circular <u>0.5</u> (feet) | ☐ rectangular length (feet) | width (feet) |
| 9. Exhaust flow rate: | | |
| Normal <u>1,813</u> (ACFM) | Maximum <u>1,813</u> (ACFM | |
| 10. Exhaust gas temperature (normal):1 | <u>,030</u> (°F) | |
| 11. Exhaust gas moisture content: | Normalvolume percent | Maximum volume percent |
| 12. Exhaust gas discharge direction: | ☑ Up ☐ Down | ☐ Horizontal |
| 13. Is this stack equipped with a rainhat or exhaust gases from the stack? | any obstruction to the free flow of the | ☐ Yes ✓ No |
| ***** Complete the appropriate Air Perm exhausting through this stack. | it Application Forms(s) 4530-104, 106, 1 | 07, 108 or 109 for each Unit ***** |

BOILER OR FURNACE OPERATION AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-104 11-93 Information attached? \underline{n} (y/n)

| SEE INSTRUCTIONS ON REVERSE SID | E | | | | |
|--|--|------------------------|----------------------|----------------|--|
| 1. Facility name: Nemadji Trail Energy Ce | 2. Facility identification number: To be assigned 816127840 | | | | |
| 3. Stack identification number: S06 | 4. Boiler/furnace number: EU06 | | | | |
| 4a. Unit description: | | | | | |
| 282-hp emergency diesel fire pump. | | | | | |
| 5. Indicate the boiler/furnace control techn | ology status. | Jncontrolled □ Co | ontrolled | | |
| If the boiler/furnace is controlled, en | ter the control device n | number(s) from the app | propriate forms: | | |
| 4530-110 4530-111 4530-112 4530-113 4530-114 4530-115 4530-116 4530-117 | | | | | |
| 6. Furnace type: | | 7. Maximum continu | uous rating: 1.95 MM | Btu/hr | |
| 8. Manufacturer: TBD | | 9. Model number: T | BD | | |
| 10. Date of construction or last modifica | tion: 06/01/2021 | | | | |
| | | | | | |
| 11. Fuels and firing conditions: | | _ | | | |
| | Primary fuel | Backup fuel #1 | Backup fuel #2 | Backup fuel #3 | |
| Fuel name | Fuel oil | | | | |
| Higher heating value | 137,000 Btu/gal | | | | |
| Maximum sulfur content (Wt.%) | ULSD | | | | |
| Maximum ash content (Wt.%) | N/A | | | | |
| Excess Combustion Air (%O ₂) | N/A | | | | |
| Moisture content (as fired) (%) | N/A | | | | |
| Maximum hourly consumption | 14.1 gal/hr | | | | |
| Actual yearly consumption | 7,050 gal/yr | | | | |
| | | | | | |
| ***** For this emissions unit, identify the method of compliance demonstration by completing Form 4530-118, ***** DESCRIPTION OF METHODS USED FOR DETERMINING COMPLIANCE. Attach Form 4530-118 and its attachment(s) to this form. This is not a requirement of non-Part 70 sources. | | | | | |

***** Please complete the Air Pollution Control Permit Application Forms 4530-126 and 4530-128 for this Unit. *****

COMPLIANCE CERTIFICATION - MONITORING AND REPORTING DESCRIPTION OF METHODS USED FOR DETERMINING COMPLIANCE Form 4530-118 11-93 Information attached? n (y/n)

All applicants except non-Part 70 sources are required to certify compliance with all applicable air pollution permit requirements by including a statement within the permit application of the methods used for determining compliance (please see sec. NR 407.05(4)(i), Wis. Adm. Code.) This statement must include a description of the monitoring, recordkeeping, and reporting requirements and test methods. In addition, the application must include a schedule for compliance certification submittals during the permit term. These submittals must be no less frequent than annually, and may need to be more frequent if specified by the underlying applicable requirement or by the Department.

| CEE | INICTDI | ICTIONS | ON REVERSE | CIDE |
|-------|---------|-------------|------------|-------|
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| EE INSTRUCTIONS ON REVERSE SIDE | | | | | |
|--|---|--|--|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | | | | |
| 3. Stack identification number: S06 | 4. Unit identification number: EU06 | | | | |
| 5. This Unit will use the following method(s) for determining compliance with the requirements of the permit (check all that apply and attach the appropriate form(s) to this form). Continuous Emission Monitoring (CEM) - Form 4530-119 Pollutant(s): Periodic Emission Monitoring Using Portable Monitors - Form 4530-120 Pollutant(s): | | | | | |
| ☐ Monitoring Control System Parameters or Operating Parameters of a Process - Form 4530-121 Pollutant(s): | | | | | |
| ☐ Monitoring Maintenance Procedures - Form 4530-122 Pollutant(s): | | | | | |
| ☐ Stack Testing - Form 4530-123 Pollutant(s): | | | | | |
| ✓ Fuel Sampling and Analysis (FSA) - Form 4530-124 Pollutant(s): SO₂ ✓ Recordkeeping - Form 4530-125 Pollutant(s): <u>All</u> | | | | | |
| ☐ Other (please describe) - Form 4530-135 Pollutant(s): | | | | | |
| 6. Compliance certification reports will be submitted to the De Start date: At date of permit issuance and every 12 months thereafter. Compliance monitoring reports will be submitted to the Start date: At date of permit issuance | | | | | |
| and every <u>6</u> months thereafter. | | | | | |

COMPLIANCE DEMONSTRATION BY FUEL SAMPLING AND ANALYSIS AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-124 11-93 Information attached? <u>n</u> (y/n)

An installation plan for each fuel sampling and analysis system (FSA) may be submitted with the permit application for Department approval. The installation plan shall contain the following information: the name and address of the source; the source facility identification number; a general description of the process and the control equipment; the type of fuel being sampled; the manufacturer, model number, and serial number of each sampler; and a schematic of the FSA system showing the sample acquisition point and the location of the machine that produces the daily, weekly, or monthly composite fuel sample. A completed form 4530-124, supplemented to satisfy the requirements of this paragraph, may constitute an installation plan for a FSA system.

| SEE INSTRUCTIONS ON REVERSE SIDE | |
|---|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
| 3. Stack identification number: S06 | 4. Unit identification number: EU06 |
| 5. Pollutant being monitored: SO ₂ | 6. Fuel being sampled: Diesel fuel oil |
| 7. List the ASTM fuel sample collecting and analyzing methods used: <u>In accordance with 40 CFR Part 75</u> | |
| 8. Is this an existing FSA system? ☐ Yes ✓ No | 9. Installation date: 06/01/2021 |
| 10. ☐ Automated sampling ✓ Manual sampling | |
| 11. Backup system? Not applicable | |
| 12. Compliance shall be demonstrated: ☐ Daily ☐ Weekly ☐ Monthly ✓ Per shipment of diesel fuel | |
| 13. Indicate by checking: | |
| ☐ The FSA system certification is attached for Department approval. ☑ If the certification is not attached, please submit it within 60 days of the FSA system startup. ☐ The certification was submitted to the Department on | |
| ☐ A FSA quality assurance/quality control plan for fuel sampling program is attached for Department approval. ✓ If the plan is not attached, please submit it within 60 days of the CEM startup system. ☐ The plan was submitted to the Department on | |

**** Any composite sample over the emission limit shall be reported as an excess emission. *****

COMPLIANCE DEMONSTRATION BY RECORDKEEPING AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-125 11-93

Information attached? \underline{n} (y/n)

Recordkeeping may be acceptable as a compliance demonstration method provided that a correlation between the parameter value recorded and the emission rate of a particular pollutant is established in the form of a curve or chart of emission rate versus parameter values. This correlation may constitute the certification of the system. It should be attached for Department approval. If it is not attached, please submit it within 60 days of the startup of the system.

| SEE INSTRUCTIONS ON REVERSE SIDE | |
|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
| 3. Stack identification number: S06 | 4. Unit identification number: EU06 |
| 5. Pollutant(s) being monitored: All | 6. Material or parameter being monitored and recorded: The hours of operation of the emergency fire pump will be recorded so that emissions may be calculated. |
| 7. Method of monitoring and recording: Hours of operation | |
| 8. List any EPA methods used: | |
| 9. Is this an existing method of demonstrating compliance? ☐ Yes ✓ No | 10. Installation date: 06/01/2021 |
| 11. Backup system: | |
| 12. Compliance shall be demonstrated: ☐ Daily ☐ Weekly ☑ Monthly ☐ Batch (not to exceed monthly) | |
| 13. Indicate by checking: | |
| The monitoring system shall be subject to appropriate performance specifications, calibration requirements, and quality assurance procedures. ☐ A quality assurance/quality control plan for the recordkeeping system is attached for Department approval. ☑ If the plan is not attached, please submit it within 60 days of the startup of the recordkeeping program. ☐ The plan was submitted to the Department on | |
| **** The compliance records shall be available for Department inspection. The format for the compliance ***** certification report and the excess emission report shall be approved by the Department. A proposed format for the compliance certification report and excess emission report shall be submitted at the same time as the application. | |
| **** The source shall record any malfunction that causes or may cause an emission limit to be exceeded. **** Malfunctions shall be reported to the Department the next business day. Hazardous air spills shall | |

be reported to the Department immediately.

EMISSION UNIT HAZARDOUS AIR POLLUTANT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-126 11-93

Information attached? y (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|---|
| 3. Stack identification number: S06 | 4. Unit identification number: EU06 |

5. Unit material description: Fuel oil combustion

6. Complete the following summary of hazardous air emissions from this unit. Attach sample calculations and emission factor references. Attached? See Appendix C

| references. Attached? | See Appendix C | | | | |
|-----------------------|----------------|----------|--------------------|--------------|-------------------|
| Pollutant CAS | Actual emiss | ions | Maximum theoretica | al emissions | Potential to emit |
| | | Units | | Units | |
| | SEE APPENDIX | C FOR HA | PS EMISSIONS CAL | CULATIONS | |
| | | | | | TPY |

EMISSION UNIT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-128 11-93 Information attached? <u>y</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|--|
| 3. Stack identification number: S06 | 4. Unit identification number: EU06 |

5. Complete the following emissions summary for the following pollutants. Attach sample calculations and emission factor references. Attached? See Appendix C

| Air pollutant | Actua | al | Maximum theoretical emissions | | | Potential to emit | Maxin | Maximum allowable | |
|---------------|-------|-----|-------------------------------|---|-----|-------------------|-------|-------------------|-----|
| | U | TPY | | U | TPY | | | U | TPY |

SEE APPENDIX C FOR EMISSIONS CALCULATIONS

| Sulfur dioxide | | | | TPY | | |
|----------------------|--|--|---|-----|--|--|
| Organic compounds | | | : | TPY | | |
| Carbon monoxide | | | | TPY | | |
| Lead | | | | TPY | | |
| Nitrogen oxides | | | | TPY | | |
| Total reduced sulfur | | | | TPY | | |
| Mercury | | | | TPY | | |
| Asbestos | | | | TPY | | |
| Beryllium | | | | TPY | | |
| Vinyl chloride | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |

Units (U) should be entered as follows:

- 1 = lb/hr
- 2 = lb/mmBTU
- 3 = grains/dscf
- 4 = lb/gallon
- 5 = ppmdv
- 6 = other (specify)
- 7 = other (specify)
- 8 = other (specify)

CURRENT EMISSIONS REQUIREMENTS AND STATUS OF UNIT AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-130 Rev. 12-99 Information attached? <u>n</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | | | 2. Facility identification number: To be assigned 816127840 | | | |
|---|---|-------------------------------------|--|----------------------------------|--|--|
| 3. Stack identification number | r: S06 | 4. Unit identification number: EU06 | | | | |
| 5. Pollutant | 6. Wis. Adm. Code Wis. Stats., 40 CFR | 7. State Only | 8. Limitation | 9. Compliance Status (in or out) | | |
| Particulate | NR415, 40 CFR Part 60, Subpart IIII, 40 CFR Part 63 ZZZZ | | 0.15 lb/MMBtu and 0.15 g/hp-hr | Units not constructed yet | | |
| Sulfur Dioxide | NR 417 | X | | Units not constructed yet | | |
| Nitrogen Dioxide | NR 428, 40 CFR Part 60, Subpart IIII, 40 CFR Part 63 ZZZZ | | NMHC + $NO_x = 3.0$ g/hp-hr | Units not constructed yet | | |
| Carbon Monoxide | NR 426, 40 CFR Part 60, Subpart IIII, 40 CFR Part 63 ZZZZ | | 2.6 g/hp-hr | Units not constructed yet | | |
| Lead | NR 427 | X | | Units not constructed yet | | |
| Volatile Organic Compounds | NR 419 | X | | Units not constructed yet | | |
| Opacity | NR 431 | X | 20% opacity | Units not constructed yet | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| 10. Other requirements (e.g., ma existing permit, etc.) | alfunction reporting, special opera | ting conditi | ions from an State Only | Compliance Status (in or out) | | |
| | | | | | | |
| _ | | | | | | |

3.

State of Wisconsin Department of Natural Resources

EMISSION UNIT COMPLIANCE PLAN COMMITMENTS AND SCHEDULE AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-131 11-93

Information attached? \underline{n} (y/n) SEE INSTRUCTIONS ON REVERSE SIDE 1. Facility name: Nemadji Trail Energy 2. Facility identification number: To be assigned 816127840 Center 3. Stack identification number: S06 4. Unit identification number: EU06 5. For Units that are presently in compliance with all applicable requirements, including any enhanced monitoring and compliance certification requirements under section 114(a)(3) of the Clean Air Act that apply, complete the following. These commitments are part of the application for Part 70 permits. ☐ We will continue to operate and maintain this Unit in compliance with all applicable requirements.

| | Form 4530-130 includes new requirements that apply or will apply to this Unit during the term of the permit. We will meet such requirements on a timely basis. | | | | |
|------|---|-----------------------|-------------------------------|----------|--|
| 6. F | For Units <u>not</u> prese | ently fully in compli | ance, complete the following. | | |
| | ☐ This Unit is in compliance with all applicable requirements except for those indicated below. We will achieve compliance according to the following schedule: | | | | |
| | Applicable | Requirement | | | |
| | | | Corrective Actions | Deadline | |
| 1. | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| 2. | | | | | |
| | | | | | |
| | | | | | |

Progress reports will be submitted: Start date: _____ and every six (6) months thereafter

STACK IDENTIFICATION AIR POLLUTION CONTROL PERMIT APPLICATION From 4520 102 11 02

Form 4530-103 11-93 Information attached? <u>n</u> (y/n)

| SEE INSTRUCTIONS ON REVERSE SIDE | | | | | |
|---|--|------------------------------------|-------|--|--|
| 1. Facility name: Nemadji Trail | 2. Facility identification number: To be assigned 816127840 | 3. Stack identification number S07 | er: | | |
| Energy Center | | | | | |
| 4. Exhausting Unit(s), use Unit identification | n number from appropriate Form(s) 4530-1 | 04, 106, 107, 108 and/or 109 | | | |
| 4530-104 EU07 4530-106 | 4530-107 4530-108 | 4530-109 | | | |
| 5. Identify this stack on the plot plan required | d on Form 4530-101 | | | | |
| 6. Indicate by checking: ☐ This stack has an actual exhaust point. ☐ This stack serves to identify fugitive emissions. If this stack has an actual exhaust point, then provide the following stack parameters | | | | | |
| 7. Discharge height above ground level: 15 (feet) | | | | | |
| 8. Inside dimensions at outlet (check one and | 8. Inside dimensions at outlet (check one and complete): | | | | |
| ✓ Circular <u>0.67</u> (feet) | □ rectangular length (feet) | _ width (feet) | | | |
| 9. Exhaust flow rate: | | | | | |
| Normal <u>7,540</u> (ACFM) | Maximum <u>7,540</u> (ACFM) | | | | |
| 10. Exhaust gas temperature (normal):8 | 10. Exhaust gas temperature (normal): 890 (°F) | | | | |
| 11. Exhaust gas moisture content: | Normal volume percent | Maximum volume pe | rcent | | |
| 12. Exhaust gas discharge direction: | ✓ Up □ Down | ☐ Horizontal | | | |
| 13. Is this stack equipped with a rainhat or any obstruction to the free flow of the exhaust gases from the stack? ✓ No | | | | | |
| ***** Complete the appropriate Air Permit Application Forms(s) 4530-104, 106, 107, 108 or 109 for each Unit ***** exhausting through this stack. | | | | | |

BOILER OR FURNACE OPERATION AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-104 11-93 Information attached? <u>n</u> (y/n)

| SEE INSTRUCTIONS ON REVERSE SI | DE | _ | | | | |
|--|---|--------------------------------|-----------------------------------|------------------|--|--|
| 1. Facility name: Nemadji Trail Energy | Center | 2. Facility identification | ation number: To be as | signed 816127840 | | |
| 3. Stack identification number: S07 | | 4. Boiler/furnace number: EU07 | | | | |
| 4a. Unit description: | | | | | | |
| 1,490-hp emergency diesel generator. | | | | | | |
| 5. Indicate the boiler/furnace control tech | nnology status. | Uncontrolled □ C | ontrolled | | | |
| If the boiler/furnace is controlled, | enter the control device | number(s) from the ap | propriate forms: | | | |
| 4530-110 4530-1 4530-114 4530-1 | 4530-110 4530-111 4530-112 4530-113 4530-114 4530-115 4530-116 4530-117 | | | | | |
| 6. Furnace type: | | 7. Maximum contir | nuous rating: 21.0 MM | IBtu/hr | | |
| 8. Manufacturer: Cummins | | 9. Model number: I | OQFAD | | | |
| 10. Date of construction or last modifi | cation: 06/01/2021 | | | | | |
| | | | | | | |
| 11. Fuels and firing conditions: | | | | | | |
| | Primary fuel | Backup fuel #1 | Backup fuel #2 | Backup fuel #3 | | |
| Fuel name | Fuel Oil | | | | | |
| Higher heating value | 137,000 Btu/gal | | | | | |
| Maximum sulfur content (Wt.%) | ULSD | | | | | |
| Maximum ash content (Wt.%) | N/A | | | | | |
| Excess Combustion Air (%O ₂) | N/A | | | | | |
| Moisture content (as fired) (%) | N/A | | | | | |
| Maximum hourly consumption | 150 gal/hr | | | | | |
| Actual yearly consumption | 75,000 gal/yr | | | | | |
| ***** For this emissions unit, identify the method of compliance demonstration by completing Form 4530-118, ***** DESCRIPTION OF METHODS USED FOR DETERMINING COMPLIANCE. Attach Form 4530-118 and its attachment(s) to this form. This is not a requirement of non-Part 70 sources. | | | | | | |

***** Please complete the Air Pollution Control Permit Application Forms 4530-126 and 4530-128 for this Unit. *****

COMPLIANCE CERTIFICATION - MONITORING AND REPORTING DESCRIPTION OF METHODS USED FOR DETERMINING COMPLIANCE Form 4530-118 11-93 Information attached? \underline{n} (y/n)

All applicants except non-Part 70 sources are required to certify compliance with all applicable air pollution permit requirements by including a statement within the permit application of the methods used for determining compliance (please see sec. NR 407.05(4)(i), Wis. Adm. Code.) This statement must include a description of the monitoring, recordkeeping, and reporting requirements and test methods. In addition, the application must include a schedule for compliance certification submittals during the permit term. These submittals must be no less frequent than annually, and may need to be more frequent if specified by the underlying applicable requirement or by the Department.

| app | DICTED | LICTIONIC | ONIDENTEDGE | OIDE |
|-----|--------|-----------|-------------|------|
| SEE | INSTR | UCTIONS | ON REVERSE | SIDE |

| EE INSTRUCTIONS ON REVERSE SIDE | | | | |
|--|---|--|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | | | |
| 3. Stack identification number: S07 | 4. Unit identification number: EU07 | | | |
| 3. Stack identification number: S07 4. Unit identification number: EU07 5. This Unit will use the following method(s) for determining compliance with the requirements of the permit (check all that apply and attach the appropriate form(s) to this form). Continuous Emission Monitoring (CEM) - Form 4530-119 Pollutant(s): Periodic Emission Monitoring Using Portable Monitors - Form 4530-120 Pollutant(s): Monitoring Control System Parameters or Operating Parameters of a Process - Form 4530-121 Pollutant(s): Monitoring Maintenance Procedures - Form 4530-122 Pollutant(s): | | | | |
| Pollutant(s): ✓ Fuel Sampling and Analysis (FSA) - Form 4530-124 Pollutant(s): SO ₂ ✓ Recordkeeping - Form 4530-125 Pollutant(s): All Other (please describe) - Form 4530-135 Pollutant(s): | | | | |
| 6. Compliance certification reports will be submitted to the De Start date: At date of permit issuance and every 12 months thereafter. Compliance monitoring reports will be submitted to the Start date: At date of permit issuance and every 6 months thereafter. | | | | |

COMPLIANCE DEMONSTRATION BY FUEL SAMPLING AND ANALYSIS AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-124 11-93 Information attached? <u>n</u> (y/n)

An installation plan for each fuel sampling and analysis system (FSA) may be submitted with the permit application for Department approval. The installation plan shall contain the following information: the name and address of the source; the source facility identification number; a general description of the process and the control equipment; the type of fuel being sampled; the manufacturer, model number, and serial number of each sampler; and a schematic of the FSA system showing the sample acquisition point and the location of the machine that produces the daily, weekly, or monthly composite fuel sample. A completed form 4530-124, supplemented to satisfy the requirements of this paragraph, may constitute an installation plan for a FSA system.

| SEE INSTRUCTIONS ON REVERSE SIDE | | | | |
|---|---|--|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | | | |
| 3. Stack identification number: S07 | 4. Unit identification number: EU07 | | | |
| 5. Pollutant being monitored: SO ₂ | 6. Fuel being sampled: Diesel fuel oil | | | |
| 7. List the ASTM fuel sample collecting and analyzing methods used: In accordance with 40 CFR Part 75 | | | | |
| 8. Is this an existing FSA system? ☐ Yes ✓ No | 9. Installation date: 06/01/2021 | | | |
| 10. □ Automated sampling ✓ Manual sampling | | | | |
| 11. Backup system? Not applicable | | | | |
| 12. Compliance shall be demonstrated: ☐ Daily ☐ Weekly ☐ Monthly ✓ Per shipment of diesel fuel | | | | |
| 13. Indicate by checking: | | | | |
| ☐ The FSA system certification is attached for Department approval. ☑ If the certification is not attached, please submit it within 60 days of the FSA system startup. ☐ The certification was submitted to the Department on | | | | |
| ☐ A FSA quality assurance/quality control plan for fuel sampling program is attached for Department approval. ✓ If the plan is not attached, please submit it within 60 days of the CEM startup system. ☐ The plan was submitted to the Department on | | | | |
| | | | | |

**** Any composite sample over the emission limit shall be reported as an excess emission. *****

COMPLIANCE DEMONSTRATION BY RECORDKEEPING AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-125 11-93

Information attached? \underline{n} (y/n)

Recordkeeping may be acceptable as a compliance demonstration method provided that a correlation between the parameter value recorded and the emission rate of a particular pollutant is established in the form of a curve or chart of emission rate versus parameter values. This correlation may constitute the certification of the system. It should be attached for Department approval. If it is not attached, please submit it within 60 days of the startup of the system.

| SEE INSTRUCTIONS ON REVERSE SIDE | |
|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
| 3. Stack identification number: S07 | 4. Unit identification number: EU07 |
| 5. Pollutant(s) being monitored: All | 6. Material or parameter being monitored and recorded: The hours of operation of the emergency generator will be recorded so that emissions may be calculated. |
| 7. Method of monitoring and recording: Hours of operation | |
| 8. List any EPA methods used: N/A | |
| 9. Is this an existing method of demonstrating compliance? ☐ Yes ✓ No | 10. Installation date: 06/01/2021 |
| 11. Backup system: N/A | |
| 12. Compliance shall be demonstrated: ☐ Daily ☐ Weekly | ✓ Monthly ☐ Batch (not to exceed monthly) |
| 13. Indicate by checking: | |
| assurance procedures. A quality assurance/quality co | ase submit it within 60 days of the startup of the recordkeeping |
| **** The compliance records shall be available for Department certification report and the excess emission report shal format for the compliance certification report and excessame time as the application. | inspection. The format for the compliance **** I be approved by the Department. A proposed |
| ***** The source shall record any malfunction that causes or ma | · |

be reported to the Department immediately.

EMISSION UNIT HAZARDOUS AIR POLLUTANT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-126 11-93

Information attached? <u>y</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|---|
| 3. Stack identification number: S07 | 4. Unit identification number: EU07 |

5. Unit material description: Fuel Oil Combustion

6. Complete the following summary of hazardous air emissions from this unit. Attach sample calculations and emission factor references. Attached? See Appendix C

| Pollutant CAS | Actual emiss | ions | Maximum theoretica | al emissions | Potential to emit |
|---------------|--------------|----------|--------------------|--------------|-------------------|
| | | Units | | Units | |
| | SEE APPENDIX | C FOR HA | PS EMISSIONS CAL | CULATIONS | |
| | | | | | TPY |

EMISSION UNIT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-128 11-93 Information attached? <u>y</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |
|---|--|
| 3. Stack identification number: S07 | 4. Unit identification number: EU07 |

5. Complete the following emissions summary for the following pollutants. Attach sample calculations and emission factor references. Attached? <u>See Appendix C</u>

| Air pollutant | Actua | al | Maximum theoretical emissions | | | Potential to emit | Maxin | num a | llowable |
|---------------|-------|-----|-------------------------------|---|-----|-------------------|-------|-------|----------|
| | U | TPY | | U | TPY | | | U | TPY |

SEE APPENDIX C FOR EMISSION CALCULATIONS

| Sulfur dioxide | | | | TPY | | |
|----------------------|--|--|--|-----|--|--|
| Organic compounds | | | | TPY | | |
| Carbon monoxide | | | | TPY | | |
| Lead | | | | TPY | | |
| Nitrogen oxides | | | | TPY | | |
| Total reduced sulfur | | | | TPY | | |
| Mercury | | | | TPY | | |
| Asbestos | | | | TPY | | |
| Beryllium | | | | TPY | | |
| Vinyl chloride | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |

Units (U) should be entered as follows:

^{1 = 1}b/hr

^{2 =} lb/mmBTU

^{3 =} grains/dscf

^{4 =} lb/gallon

^{5 =} ppmdv

^{6 =} other (specify)

^{7 =} other (specify)

^{8 =} other (specify)

CURRENT EMISSIONS REQUIREMENTS AND STATUS OF UNIT AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-130 Rev. 12-99 Information attached? <u>n</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| Facility name: Nemadji Trail Energy Center | | | 2. Facility identification number: To be assigned 81612784 | | | | |
|---|---|-------------------------------------|---|----------------------------------|--|--|--|
| 3. Stack identification numbe | r: S07 | 4. Unit identification number: EU07 | | | | | |
| 5. Pollutant | 6. Wis. Adm. Code Wis. Stats., 40 CFR | 7. State Only | | 9. Compliance Status (in or out) | | | |
| Particulate | NR415, 40 CFR Part 60, Subpart IIII, 40 CFR Part 63 ZZZZ | | 0.15 lb/MMBtu and 0.15 g/hp-hr | Units not constructed yet | | | |
| Sulfur Dioxide | NR 417 | X | | Units not constructed yet | | | |
| Nitrogen Dioxide | NR 428, 40 CFR Part 60, Subpart IIII, 40 CFR Part 63 ZZZZ | | Units not constructed yet | | | | |
| Carbon Monoxide | NR 426, 40 CFR Part 60, Subpart IIII, 40 CFR Part 63 ZZZZ | Х | CO = 2.6 g/hp-hr | Units not constructed yet | | | |
| Lead | NR 427 | X | | Units not constructed yet | | | |
| Volatile Organic Compounds | NR 419 | X | | Units not constructed yet | | | |
| Opacity | NR 431 | X | 20% opacity | Units not constructed yet | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| 10. Other requirements (e.g., material existing permit, etc.) | alfunction reporting, special opera | nting condit | ions from an State Or | Compliance Status (in or out) | | | |
| | | | | | | | |
| | | | | | | | |

meet such requirements on a timely basis.

6. For Units <u>not</u> presently fully in compliance, complete the following.

EMISSION UNIT COMPLIANCE PLAN COMMITMENTS AND SCHEDULE

AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-131 11-93 Information attached? \underline{n} (y/n) SEE INSTRUCTIONS ON REVERSE SIDE 1. Facility name: Nemadji Trail Energy 2. Facility identification number: To be assigned 816127840 Center 3. Stack identification number: S07 4. Unit identification number: EU07 5. For Units that are presently in compliance with all applicable requirements, including any enhanced monitoring and compliance certification requirements under section 114(a)(3) of the Clean Air Act that apply, complete the following. These commitments are part of the application for Part 70 permits. ☐ We will continue to operate and maintain this Unit in compliance with all applicable requirements. Form 4530-130 includes new requirements that apply or will apply to this Unit during the term of the permit. We will

This Unit is in compliance with all applicable requirements except for those indicated below. We will achieve compliance

according to the following schedule:

Applicable Requirement **Corrective Actions** Deadline 1. 2. 3. Progress reports will be submitted: Start date: _____ and every six (6) months thereafter

STACK IDENTIFICATION AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-103 11-93 Information attached? <u>n</u> (y/n)

| SEE INSTRUCTIONS ON REVERSE SIDE | | |
|---|--|-------------------------------------|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | 3. Stack identification number: S08 |
| 4. Exhausting Unit(s), use Unit identification | n number from appropriate Form(s) 4530-1 | 04, 106, 107, 108 and/or 109 |
| 4530-104 4530-106 | 4530-107 4530-108 | 4530-109 |
| 5. Identify this stack on the plot plan required | d on Form 4530-101 | |
| 6. Indicate by checking: ☐ This stack has an actual exhaust point If this stack has an actual exhaust point | nt. This stack serves to identify fug | |
| • | 0 (feet) | |
| 8. Inside dimensions at outlet (check one and | | |
| ☐ Circular (feet) | rectangular length (feet) | _width (feet) |
| 9. Exhaust flow rate: | | |
| Normal (ACFM) | Maximum (ACFM) | |
| 10. Exhaust gas temperature (normal): | _(°F) | |
| 11. Exhaust gas moisture content: | Normal volume percent | Maximum volume percent |
| 12. Exhaust gas discharge direction: | □ Up □ Down | ☐ Horizontal |
| 13. Is this stack equipped with a rainhat or exhaust gases from the stack? | any obstruction to the free flow of the | □ Yes ⊠ No |
| ***** Complete the appropriate Air Perm exhausting through this stack. | it Application Forms(s) 4530-104, 106, 10 | 7, 108 or 109 for each Unit ***** |

T01

State of Wisconsin Department of Natural Resources

From December 2018 Application STORAGE TANKS
AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-105 11-93 Information attached? __ (y/n) Information attached? $\underline{\hspace{1cm}}$ (y/n)

SEE ATTACHED SHEET FOR INSTRUCTIONS

| 1.Facility Name: Nemadji River Energy Center | 2.Facility Identification Number 816127840 3.Storage Tank Number: EU08 |
|---|---|
| 4.Control Device Number (use number from appropriate Form(s) 45 111, 112, 113, 114, 115, 116, or 117) | 30-110, 5.Storage Tank Capacity 180,000 gallons gallons 6.Date of Installation or Last Modification 06/01/2021 |
| 7.Tank Height: 30 ft 8.Tank Diameter: 33 ft | 9.Color of Tank (check one) White Other Underground |
| 10.Is this tank equipped with a submerged fill pipe? | 11.Is this tank equipped with a pressure/vacuum conservation vent?Yes |
| _ <u>√</u> YesNo | If yes; at what pressure is it set?(psia) at what vacuum is it set?(psia) |
| 12.Type of Storage Tank (check one) Open Top Tank Pressurized Tank External Floating Ro | Fixed Roof w/Internal Floating Roof Other (specify) of Variable Vapor Space |
| 13. For all Fixed Roof Tanks: | |
| a.Tank Configuration (check one): | ylinder) Horizontal |
| b.Tank Roof Type (check one): (required if vertical was selected) Cone Roof - I | Indicate tank roof height 5 (feet) ndicate tank roof height (feet) - Indicate tank shell radius (feet) |
| 14.For all Floating Roof Tanks (both internal and external) - Shell C | ondition (check one):Light RustDense RustGunite Lined |
| | Riveted Tank |
| b.Average Wind Speed at Tank Site: | (mph) |
| Shoe Primary, Rim Secondary Var | Vapor Mounted Primary |
| d.Roof Type (check one): Pontoon Roof | Double Deck Roof |
| e.Roof Fitting Types (indicate the number of each type): | |
| | Unslotted guide-pole well 8" diameter unslotted pole, 21" diameter well) Ungasketed sliding cover Gasketed sliding cover Bolted cover, gasketed Bolted cover, gasketed |
| Gauge-Hatch/sample well (8" diameter) Weighted mechanical actuation, gasketed | /acuum Breaker (10" diameter well) Weighted mechanical actuation, gasketed Roof Drain (3-inch diameter) Open90% closed |
| Weighted mechanical actuation, ungasketed | Weighted mechanical actuation, ungasketed |
| Slotted guide-pole/sample well (8" diameter diameter slotted pole, 21" diameter well) | eg (3" diameter) Roof leg(2-1/2" diameter) Adjustable, pontoon area Roof leg(2-1/2" diameter) Adjustable, pontoon area |
| Ungasketed sliding cover, without float | Adjustable, center area Adjustable, center area |
| Ungasketed sliding cover, with float Gasketed sliding cover, without float | Adjustable, double-deck roofs Fixed Adjustable, double deck roofs Fixed Fixed |
| Gasketed sliding cover, with float | |

From December 2018 Application

STORAGE TANKS AIR POLLUTION CONTROL PERMIT

| State of Wisconsin | |
|---------------------------------|--|
| Department of Natural Resources | |
| APPLICATION | |

| y/n) | | | | | Form 4530-105 | 11-93 Information | attached? |
|---|---|---|---|---|--|--|---------------------------------------|
| 6.For Internal Floatin | g Roof Tanks: | | | | page 2 | | |
| | m Description (check one |): Vapor Mo Liqu | ounted Primary aid Mounted Primary | Vapor Mount Liquid M | ed Primary plus Secon ounted Primary plus S | ndary Seal econdary Seal | |
| b.Number of Col | umns: | | | | | | |
| c.Effective Colur | nn Diameter: | (1 | Ceet) | | | | |
| d.Deck Type (che | eck one): | Welded | Bolted | | | | |
| e.Total Deck Sea | m Length: | (feet) | | | | | |
| f.Deck Area: | | | (square feet) | | | | |
| g.Deck Fitting Ty | ypes (indicate the number | of each type): | | | | | |
| Column Wo | ch (24" diameter) Bolted cover, gasketed Unbolted cover, gasketed Unbolted cover, ungaskete ell (24" diameter) | ed Sample | atic gauge float well Bolted cover, y Unbolted cove Unbolted cover, ung | r, gasketed gasketed eter) | Roof leg or hange | (36" diameter) Sliding cover, gas Sliding cover, ung | keted ;asketed |
| | Builtup column-sliding co Builtup column-sliding co Pipe column-flexible fabr Pipe column-sliding cover Pipe column-sliding cover | over, ungasketed ic sleeve seal r, gasketed | | iding cover, gasketed iding cover, ungaske ric seal 10% open ard diameter) | | Adjustable ixed | |
| | eaker (10" diameter) Weighted mechanical actu Weighted mechanical actu | | | | | | |
| 7.For Variable Vapor 8.Complete the follow | Space Tanks: Vol | | ecity | (gallons) | | | |
| Material Stored | Annual Throughput (gal/yr) | Daily Average Amount Stored (gallons) | Material Molecular Weight (lb/lb-mole) | Material Vapor Pressure (psia) | Storage Pressure (psia) | Average Storage Temperature (°F) | Material Liqui Density (lb/gal) |
| No. 2 Fuel Oil | 10,791,748 | 180,000 | | | | Ambient | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| 9.Maximum Liquid L | oading Rate of Tank: | | (gallons) | | | • | |
| | ided at the same time other | | Yes | _ ∠ _ No | | | |
| If yes, indicate w | hich other tanks can be lo | aded at the same time | e: | | | | |

21. Describe the operations this tank will serve: 180,000 tank stores No. 2 fuel oil as a backup fuel for the combustion turbine at the facility.

EMISSION UNIT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-128 11-93

Information attached? <u>y</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | | | | |
|---|---|--|--|--|--|
| 3. Stack identification number: S08 | 4. Unit identification number: EU08 | | | | |
| 5. Complete the following emissions summary for the following pollutants. Attach sample calculations and emission factor references. Attached? See Appendix C | | | | | |

| Tereferees. Tittaer. | | | | | | | | | |
|----------------------|--|---|-----|--|---|-----|--|---|-----|
| | | | | | | | | | |
| | | U | TPY | | U | TPY | | U | TPY |

SEE APPENDIX C FOR EMISSIONS CALCULATIONS

| Sulfur dioxide | | | | TPY | | |
|----------------------|--|--|--|-----|--|--|
| Organic compounds | | | | TPY | | |
| Carbon monoxide | | | | TPY | | |
| Lead | | | | TPY | | |
| Nitrogen oxides | | | | TPY | | |
| Total reduced sulfur | | | | TPY | | |
| Mercury | | | | TPY | | |
| Asbestos | | | | TPY | | |
| Beryllium | | | | TPY | | |
| Vinyl chloride | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |

Units (U) should be entered as follows:

^{1 =} lb/hr

^{2 =} lb/mmBTU

^{3 =} grains/dscf 4 = lb/ gallon

^{5 =} ppmdv

^{6 =} other (specify)

^{7 =} other (specify)

^{8 =} other (specify)

STACK IDENTIFICATION AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-103 11-93 Information attached? <u>n</u> (y/n)

| SEE INSTRUCTIONS ON REVERSE SIDE | | | | | | | | |
|---|--|---------------------------------|-----------------|--|--|--|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification numb To be assigned 816127840 | | ication number: | | | | | |
| 4. Exhausting Unit(s), use Unit identification | number from appropriate Form | n(s) 4530-104, 106, 107, 108 | and/or 109 | | | | | |
| 4530-104 4530-106 | 4530-107 4530-10 | 8 4530-109 | | | | | | |
| 5. Identify this stack on the plot plan require | d on Form 4530-101 | | | | | | | |
| 6. Indicate by checking: ☐ This stack has an actual exhaust point. ☐ This stack serves to identify fugitive emissions. If this stack has an actual exhaust point, then provide the following stack parameters | | | | | | | | |
| 7. Discharge height above ground level: (feet) | | | | | | | | |
| 8. Inside dimensions at outlet (check one and complete): | | | | | | | | |
| ☐ Circular (feet) | ☐ rectangular length (f | eet) width (feet) | | | | | | |
| 9. Exhaust flow rate: | | | | | | | | |
| Normal (ACFM) | Maximum (A | ACFM) | | | | | | |
| 10. Exhaust gas temperature (normal): | _(°F) | | | | | | | |
| 11. Exhaust gas moisture content: | Normal volume percent | Maximum | volume percent | | | | | |
| 12. Exhaust gas discharge direction: | □ Up □ Down | n 🔲 Horizontal | | | | | | |
| 13. Is this stack equipped with a rainhat or any obstruction to the free flow of the exhaust gases from the stack? ✓ Yes ✓ Yes | | | | | | | | |
| ***** Complete the appropriate Air Perm exhausting through this stack. | it Application Forms(s) 4530-10 | 04, 106, 107, 108 or 109 for ea | ach Unit ***** | | | | | |

From December 2018 Application

T02 State of Wisconsin Department of Natural Resources

STORAGE TANKS
AIR POLLUTION CONTROL PERMIT APPLICATION
Form 4530-105 11-93 Information attached? n_ Information attached? $n_{\underline{\hspace{1cm}}}(y/n)$

SEE ATTACHED SHEET FOR INSTRUCTIONS

| 1.Facility Name: | Nemadji River Energy Center | • | 2.Facility Id | lentification | n Number 8161 | 27840 3.St | torage Tank Number | : EU09 |
|--|---|--|---|---------------------------|-------------------------------------|---------------|---|----------------------------|
| 4.Control Device Number 111, 112, 113, 114, 115, | (use number from appropriate Fo | rm(s) 4530-110, 5 | S.Storage Tank C | | 1,700 gallons gallons | 6.Date of | Installation or Last 1 06/01/2021 | Modification |
| 7.Tank Height: | 8. Tank Diameter: | 9.Colo | or of Tank (check | | | | ** 1 | |
| 14 ft x 6.5 ft x 1.2 ft | t Belly Tank (approximate speci | fications) | \ | VhiteOtl | ner | | Underground | |
| 10.Is this tank equipped w | vith a submerged fill pipe? | | 11.Is this ta | nk equippe | d with a pressi | ıre/vacuum | conservation vent? | / N |
| | _ <u>√_</u> Yes | No | | | | | | es <u>√</u> No |
| | | | If yes; | at what pr at what va | essure is it set acuum is it set | ? | (psia (psia |)) |
| 12.Type of Storage Tank Open Top Tank Pressurized Tank | Fixed Roof | oating Roof | Fixed Ro Variable | oof w/Interr Vapor Spa | nal Floating Roce | oof | <u>√</u> Other (s Generator Belly Ta | |
| 13.For all Fixed Roof Tar | | | | | | | | |
| a.Tank Configuratio | on (check one): Vertical (up | oright cylinder) | _ √ _ I | Iorizontal | | | | |
| b.Tank Roof Type (required if vertical | check one): Cone was selected) Dome | Roof - Indicate tank Roof - Indicate tanl | roof height k roof height | | (feet) (feet) - Ind | icate tank sł | hell radius | (feet) |
| 14.For all Floating Roof | Tanks (both internal and external) | - Shell Condition (cl | heck one): | Light I | Rust | Dense Rust | Gunite Lir | ned |
| 15.For External Floating l a.Tank Construction | | ed Tank Riv | reted Tank | _ 0 | _ | | _ | |
| b.Average Wind Spe | eed at Tank Site: | | (mph) | | | | | |
| Shoe Moun Shoe Prima | Description (check one): tted Primary try, Rim Secondary try, Shoe Secondary | Vapor Primary | ounted Primary , Rim Secondary imary w/Weathe | r Shield | _ | Liquid Prim | Liquid Mounted Prin nary, Rim Secondary Liquid Primary w/Wo | • |
| d.Roof Type (check | one):Ponto | on Roof | _ Double Deck | Roof | | | | |
| e.Roof Fitting Types | s (indicate the number of each type | e): | | | | | | |
| Boi | (24" diameter well) lted cover, gasketed bolted cover, ungasketed bolted cover, gasketed | (8" diameter Ungas | uide-pole well runslotted pole, keted sliding cov Gasketed sliding | er | er well) | Gau | uge-float well (20" di Unbolted cov Unbolted cover, ga Bolted cover | ver, ungasketed asketed |
| We | sample well (8" diameter) eighted mechanical actuation, usketed | Weigh | eaker (10" diame ted mechanical a gasketed | | | Roo Ope | of Drain (3-inch diamen 90% closed | neter) |
| | eighted mechanical actuation, | | ted mechanical a | actuation, | | | | |
| | pole/sample well (8" diameter ed pole, 21" diameter well) | Roof leg (3" diam | neter) Adjustable, ponto | oon area | | Roof leg(| (2-1/2" diameter) Adjustable, p | oontoon area |
| Un | gasketed sliding cover, without flo | oatA | Adjustable, cente | r area | | | Adjustable, c | enter area |
| | gasketed sliding cover, with float sketed sliding cover, without float | | Adjustable, doub Fixed | le-deck roo | fs | | Adjustable, c | louble deck roofs |
| Gas | sketed sliding cover, with float | | | | | | | |
| | | | | | | | | |

From December 2018 Application

State Depa

ΠT

| e of Wisconsin | STORAGE TANKS |
|-------------------------------|--|
| partment of Natural Resources | AIR POLLUTION CONTROL PERMIT |
| PLICATION | |
| | Form 4530-105 11-93 Information attached |

| (y/n) | | | | 2 | | | | |
|---|--|---|---|----------------------------------|--|--------------------------------------|--|--|
| 16.For Internal Floating Roof Tanks: | | | | page 2 | | | | |
| a.Rim Seal System Description (check one): | Vapor Mo Liqu | ounted Primary aid Mounted Primary | nted Primary Vapor Mounted Primary plus Secondary Seal d Mounted Primary Liquid Mounted Primary plus Secondary Seal | | | | | |
| b.Number of Columns: | | | | | | | | |
| c.Effective Column Diameter: | (1 | feet) | | | | | | |
| d.Deck Type (check one): | elded | Bolted | | | | | | |
| e.Total Deck Seam Length: | (feet) | | | | | | | |
| f.Deck Area: | | (square feet) | | | | | | |
| g.Deck Fitting Types (indicate the number of | each type): | | | | | | | |
| Access Hatch (24" diameter) Bolted cover, gasketed Unbolted cover, gasketed Unbolted cover, ungasketed Unbolted cover, ungasketed Unbolted cover, ungasketed Column Well (24" diameter) Builtup column-sliding cove Pipe column-flexible fabric s Pipe column-sliding cover, g Pipe column-sliding cover, g Pipe column-sliding cover, ungasketed Vacuum breaker (10" diameter) Weighted mechanical actuat Weighted mechanical actuat Volum 17.For Variable Vapor Space Tanks: Volum | Sample r, gasketed r, ungasketed sleeve seal gasketed ingasketed ion, gasketed ion, ungasketed | Slotted pipe-sl Sample well-slit fab Stub drain (1" | r, gasketed gasketed eter) iding cover, gasketed iding cover, ungaske ric seal 10% open and diameter) | Roof leg or hanger I ted F | (36" diameter) Sliding cover, gasl Sliding cover, ung well Adjustable ixed | ceted asketed | | |
| Annual Throughput Material Stored (gal/yr) | Daily Average Amount Stored (gallons) | Material Molecular Weight (lb/lb-mole) | Material Vapor Pressure (psia) | Storage Pressure (psia) | Average Storage Temperature | Material Liqu Density (lb/gal) | | |
| | 1,700 | (22.22.22.2) | ([) | (2.11) | Ambient | (g) | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| 19. Maximum Liquid Loading Rate of Tank: 20. Can this tank be loaded at the same time other tanks to the same time other tanks. | | (gallons) Yes | _ √ No | 1 | | | | |
| 21.Describe the operations this tank will serve: 1,70 | | | | | | | | |

EMISSION UNIT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-128 11-93 Information attached? <u>y</u> (y/n)

| SEE INSTRUCTIONS ON REVERSE SIDE | | \ |
|---|---|---------------|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 | |
| 3. Stack identification number: S09 | 4. Unit identification number: EU09 | |

5. Complete the following emissions summary for the following pollutants. Attach sample calculations and emission factor references. Attached? See Appendix C

| | U | TPY | U | TPY | | U | TPY |
|--|---|-----|---|-----|--|---|-----|

SEE APPENDIX C FOR EMISSIONS CALCULATIONS

| Sulfur dioxide | | | | TPY | | |
|----------------------|--|--|------|-----|--|--|
| Organic compounds | | | | TPY | | |
| Carbon monoxide | | | | TPY | | |
| Lead | | | - | TPY | | |
| Nitrogen oxides | | | | TPY | | |
| Total reduced sulfur | | | | TPY | | |
| Mercury | | | | TPY | | |
| Asbestos | | | | TPY | | |
| Beryllium | | | | TPY | | |
| Vinyl chloride | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |

Units (U) should be entered as follows:

^{1 =} lb/hr

^{2 =} lb/mmBTU

^{3 =} grains/dscf

^{4 =} lb/gallon

^{5 =} ppmdv

^{6 =} other (specify)

^{7 =} other (specify)

^{8 =} other (specify)

exhausting through this stack.

STACK IDENTIFICATION AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-103 11-93 Information attached? <u>n</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE 1. Facility name: 2. Facility identification number: 3. Stack identification number: Nemadji Trail Energy Center To be assigned 816127840 S10 4. Exhausting Unit(s), use Unit identification number from appropriate Form(s) 4530-104, 106, 107, 108 and/or 109 4530-107 4530-104 4530-106 4530-108 4530-109 5. Identify this stack on the plot plan required on Form 4530-101 6. Indicate by checking: ☐ This stack has an actual exhaust point. This stack serves to identify fugitive emissions. If this stack has an actual exhaust point, then provide the following stack parameters 7. Discharge height above ground level: (feet) 8. Inside dimensions at outlet (check one and complete): ☐ rectangular width (feet) ☐ Circular (feet) length (feet) 9. Exhaust flow rate: Normal (ACFM) Maximum (ACFM) (°F) 10. Exhaust gas temperature (normal): 11. Exhaust gas moisture content: Normal volume percent Maximum volume percent Exhaust gas discharge direction: ☐ Horizontal 12. □ Up □ Down 13. Is this stack equipped with a rainhat or any obstruction to the free flow of the **⋈** No \square Yes exhaust gases from the stack? Complete the appropriate Air Permit Application Forms(s) 4530-104, 106, 107, 108 or 109 for each Unit *****

T03 State of Wisconsin

Department of Natural Resources

From December 2018 Application

STORAGE TANKS

AIR POLLUTION CONTROL PERMIT APPLICATION
Form 4530-105 11-93 Information attached? __n (y/n)

SEE ATTACHED SHEET FOR INSTRUCTIONS

1. Facility Name: Nemadji River Energy Center 2. Facility Identification Number 816127840 3. Storage Tank Number: EU10 4.Control Device Number (use number from appropriate Form(s) 4530-110, 5.Storage Tank Capacity 180,000 gallons 6.Date of Installation or Last Modification 111, 112, 113, 114, 115, 116, or 117) 06/01/2021 gallons 7. Tank Height: 8. Tank Diameter: 9. Color of Tank (check one) _____ Underground ✓ White Other 3.5 ft x 3.5 ft x 5 ft Belly Tank (approximate specifications) 10.Is this tank equipped with a submerged fill pipe? 11.Is this tank equipped with a pressure/vacuum conservation vent? __ Yes _<u>√</u>_ No <u>√</u> Yes _ No If yes; at what pressure is it set? at what vacuum is it set? 12. Type of Storage Tank (check one) __ Fixed Roof Open Top Tank Fixed Roof w/Internal Floating Roof ✓ Other (specify) __ External Floating Roof __ Variable Vapor Space Pressurized Tank Generator belly tank 13. For all Fixed Roof Tanks: __ Vertical (upright cylinder) ✓ Horizontal a. Tank Configuration (check one): b.Tank Roof Type (check one): __ Cone Roof - Indicate tank roof height _____(feet) (required if vertical was selected) Dome Roof - Indicate tank roof height (feet) - Indicate tank shell radius (feet) 14. For all Floating Roof Tanks (both internal and external) - Shell Condition (check one): Light Rust Dense Rust Gunite Lined 15.For External Floating Roof Tanks: __ Riveted Tank a.Tank Construction (check one): Welded Tank b. Average Wind Speed at Tank Site: (mph) c.Rim Seal System Description (check one): Liquid Mounted Primary Shoe Mounted Primary Vapor Mounted Primary __ Vapor Primary, Rim Secondary Shoe Primary, Rim Secondary Liquid Primary, Rim Secondary __ Vapor Primary w/Weather Shield Shoe Primary, Shoe Secondary Liquid Primary w/Weather Shield __ Double Deck Roof d.Roof Type (check one): Pontoon Roof e.Roof Fitting Types (indicate the number of each type): Access Hatch (24" diameter well) Unslotted guide-pole well Gauge-float well (20" diameter) Bolted cover, gasketed (8" diameter unslotted pole, 21" diameter well) Unbolted cover, ungasketed Unbolted cover, gasketed Unbolted cover, ungasketed __ Ungasketed sliding cover ____ Gasketed sliding cover ____ Bolted cover, gasketed Unbolted cover, gasketed Roof Drain (3-inch diameter) Gauge-Hatch/sample well (8" diameter) Vacuum Breaker (10" diameter well) ____ Weighted mechanical actuation, Weighted mechanical actuation, Open 90% closed gasketed gasketed _ Weighted mechanical actuation, Weighted mechanical actuation, ungasketed ungasketed Roof leg (3" diameter) Slotted guide-pole/sample well (8" diameter Roof leg(2-1/2" diameter) diameter slotted pole, 21" diameter well) ____ Adjustable, pontoon area ____ Adjustable, pontoon area Ungasketed sliding cover, without float Adjustable, center area Adjustable, center area Ungasketed sliding cover, with float Adjustable, double-deck roofs Adjustable, double deck roofs Gasketed sliding cover, without float Fixed Gasketed sliding cover, with float

(y/n)

From December 2018 Application

Information attached?

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STORAGE TANKS CONTROL PERMIT

| ate of Wisconsin | STURAGE TANKS |
|--------------------------------|----------------------|
| epartment of Natural Resources | AIR POLLUTION CONTRO |
| PPLICATION | |
| | Form 4530-105 11-93 |

| CE I . 1EL .: | D CT 1 | | | | page 2 | | |
|--|--|--|--|---|----------------------------|---|---------------------------------------|
| 6.For Internal Floating | g Roof Tanks: m Description (check one |): Vapor Mo | ounted Primary | Vapor Mount | ed Primary plus Secon | ndary Seal | |
| antani sea syste | D toonputen (through the | | aid Mounted Primary | Liquid M | ounted Primary plus S | econdary Seal | |
| b.Number of Col | umns: | | | | | | |
| c.Effective Colum | nn Diameter: | (1 | feet) | | | | |
| d.Deck Type (che | eck one): | Welded | _ Bolted | | | | |
| e.Total Deck Sea | m Length: | (feet) | | | | | |
| f.Deck Area: | | | (square feet) | | | | |
| g.Deck Fitting Ty | ypes (indicate the number | of each type): | | | | | |
| 1 | ch (24" diameter) Bolted cover, gasketed Unbolted cover, gasketed Unbolted cover, ungaskete | | atic gauge float well Bolted cover, a Unbolted cover Unbolted cover, ung | r, gasketed | Ladder Well – – | (36" diameter) Sliding cover, gasl Sliding cover, ung | |
| 1 1 1 | ell (24" diameter) Builtup column-sliding co Builtup column-sliding co Pipe column-flexible fabri Pipe column-sliding cover Pipe column-sliding cover | ver, gasketed ver, ungasketed c sleeve seal , gasketed | | iding cover, gasketed iding cover, ungaske ric seal 10% open ar | ted F | r well Adjustable ïixed | |
| | eaker (10" diameter) Weighted mechanical actu Weighted mechanical actu | | | | | | |
| 7.For Variable Vapor 8.Complete the follow | Space Tanks: Vol ving table for materials to | | acity | (gallons) | | | |
| Material Stored No. 2 Fuel Oil | Annual Throughput (gal/yr) 7,292 | Daily Average Amount Stored (gallons) 350 | Material Molecular Weight (lb/lb-mole) | Material Vapor Pressure (psia) | Storage Pressure (psia) | Average Storage Temperature (°F) Ambient | Material Liqui Density (lb/gal) |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| 9.Maximum Liquid L | oading Rate of Tank: | | (gallons) | | | | |
| 0.Can this tank be loa | ded at the same time other | r tanks are loaded? | Yes | _ ⊈ _ No | | | |
| If yes, indicate w | hich other tanks can be lo | aded at the same time | e: | | | | |
| 1 Describe the energy | ions this tople will some 2 | 50 gallon tank stone | as No. 2 fuel oil for ama | uaanay fina nuumn a | naina tanlı | | |

3. Stack identification number: S10

EMISSION UNIT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-128 11-93 Information attached? <u>n</u> (y/n)

| SEE INSTRUCTIONS ON REVERSE SIDE | |
|--|---|
| Facility name: Nemadji Trail Energy Center | 2. Facility identification number: To be assigned 816127840 |

5. Complete the following emissions summary for the following pollutants. Attach sample calculations and emission factor

| _ | references. Attacl | ned? <u>See <i>A</i></u> | ppendix C | | 1 | 1 | | |
|---|--------------------|--------------------------|-----------|---|----------|---|-------|-----|
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | 1 | |
| | | U | TPY | U | TPY | | U | TPY |
| • | | <u> </u> | | | <u>'</u> | | | |

4. Unit identification number: EU10

SEE APPENDIX C FOR EMISSIONS CALCULATIONS

| Sulfur dioxide | | | | TPY | | |
|----------------------|--|--|--|-----|--|--|
| Organic compounds | | | | TPY | | |
| Carbon monoxide | | | | TPY | | |
| Lead | | | | TPY | | |
| Nitrogen oxides | | | | TPY | | |
| Total reduced sulfur | | | | TPY | | |
| Mercury | | | | TPY | | |
| Asbestos | | | | TPY | | |
| Beryllium | | | | TPY | | |
| Vinyl chloride | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |

Units (U) should be entered as follows:

- 1 = lb/hr
- 2 = lb/mmBTU
- $3 = \frac{\text{grains}}{\text{dscf}}$
- 4 = lb/gallon
- 5 = ppmdv
- 6 = other (specify)
- 7 = other (specify)
- 8 = other (specify)

State of Wisconsin STACK IDENTIFICATION

Department of Natural Resources

AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-103 11-93 Information attached? <u>n</u> (y/n)

| SEE INSTRUCTIONS ON REVERSE SIDE | | | | | | | | | |
|---|--|---|--|--|--|--|--|--|--|
| Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 | 3. Stack identification number: NA | | | | | | | |
| 4. Exhausting Unit(s), use Unit identification | | | | | | | | | |
| 4530-104 4530-106 | 4530-107 4530-108 | 4530-109 <u>F01</u> | | | | | | | |
| 5. Identify this stack on the plot plan require | d on Form 4530-101 | | | | | | | | |
| 6. Indicate by checking: ☐ This stack has an actual exhaust point. ☐ This stack serves to identify fugitive emissions. | | | | | | | | | |
| If this stack has an actual exhaust point, then provide the following stack parameters | | | | | | | | | |
| 7. Discharge height above ground level: (feet) | | | | | | | | | |
| 8. Inside dimensions at outlet (check one and complete): | | | | | | | | | |
| ☐ Circular(feet) | ☐ rectangularlength (feet) | width (feet) | | | | | | | |
| 9. Exhaust flow rate: | | | | | | | | | |
| Normal(ACFM) | Maximum | (ACFM) | | | | | | | |
| 10. Exhaust gas temperature (normal): | _(°F) | | | | | | | | |
| 11. Exhaust gas moisture content: | Normal volume percent | Maximum volume percent | | | | | | | |
| 12. Exhaust gas discharge direction: | □ Up □ Down | ☐ Horizontal | | | | | | | |
| 13. Is this stack equipped with a rainhat or exhaust gases from the stack? | any obstruction to the free flow of the | ne □ Yes □ No | | | | | | | |
| ***** Complete the appropriate Air Perm exhausting through this stack. | ait Application Forms(s) 4530-104, 1 | 06, 107, 108 or 109 for each Unit ***** | | | | | | | |

MISCELLANEOUS PROCESSES AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-109 11-93 Information attached? \underline{n} (y/n)

| SEE INSTRUCTIONS | ON REVERSE SIDE | | | | |
|-------------------------|--|----------------------------------|---------------|---------------------------|-------|
| 1. Facility name: Nem | adji Trail Energy Center | 2. Facility identification | number: 816 | 127840 | |
| 3. Stack identification | number: NA | 4. Process number: F01 | | | |
| 4a. Unit description: | : haul road fugitives | | | | |
| 5. Indicate the control | technology status. | olled Controlled | | | |
| If the process is | controlled, enter the control device | e number(s) from the appr | ropriate form | (s): | |
| 4530-110 4530-114 | 4530-111 4 4530-115 4 | 530-112 4530-1 530-116 4530-1 | 113 <u> </u> | | |
| 6. Source Classificatio | n Code (SCC): 30502011 | | | | |
| 7. Date of construction | or last modification: TBD | | | | |
| 8. Normal operating so | chedule: 24 hrs./day 7 day | ays/wk. <u>365</u> days/yr | | | |
| | ss (please attach a flow diagram of om haul road truck traffic. | f the process). | | Attached? See next pag | e. |
| 10. List the types and | d amounts of raw materials used i | n this process: | | | |
| Material | Storage/material handling process | Average usage | Units | Maximum usage | Units |
| N/A | • | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | d amounts of finished products: | | 77.1 | 26.1 | |
| Material | Storage/material handling process | Average amount produced | Units | Maximum amount produced | Units |
| N/A | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| 12. Process fuel usage | : | | | | |
| Type of fuel | Maximum heat input to process million BTU/hr. | Average usage | Units | Maximum usage | Units |
| N/A | | | | | |
| | | | | | |
| | | | | | |
| | gitive emissions associated with thoads, open conveyors, etc.: N/A | nis process, such as outdoo | or storage | Attached? No | /A |
| DESCRIPTION | sions unit, identify the method(s) ON OF METHODS USED FOR I ument(s) to this form. This is not a | DETERMINING COMPL | IANCE. Atta | | *** |
| ***** Please complet | te the Air Pollution Control Permi | it Application Forms 4530 | -126 and 453 | 0-128 for this Unit. *** | ** |

COMPLIANCE CERTIFICATION - MONITORING AND REPORTING DESCRIPTION OF METHODS USED FOR DETERMINING COMPLIANCE Form 4530-118 11-93 Information attached? n (y/n)

All applicants except non-Part 70 sources are required to certify compliance with all applicable air pollution permit requirements by including a statement within the permit application of the methods used for determining compliance (please see sec. NR 407.05(4)(i), Wis. Adm. Code.) This statement must include a description of the monitoring, recordkeeping, and reporting requirements and test methods. In addition, the application must include a schedule for compliance certification submittals during the permit term. These submittals must be no less frequent than annually, and may need to be more frequent if specified by the underlying applicable requirement or by the Department.

| CEE | INCTRI | ICTIONS | ON REVER | CE CIDE |
|-----|--------|---------|----------|---------|

| EE INSTRUCTIONS ON REVERSE SIDE | |
|---|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 |
| 3. Stack identification number: NA | 4. Unit identification number: F01 |
| 5. This Unit will use the following method(s) for determining con and attach the appropriate form(s) to this form). Continuous Emission Monitoring (CEM) - Form 4530-1 Pollutant(s): | mpliance with the requirements of the permit (check all that apply |
| ☐ Periodic Emission Monitoring Using Portable Monitors Pollutant(s): | - Form 4530-120 |
| ☐ Monitoring Control System Parameters or Operating Par Pollutant(s): | rameters of a Process - Form 4530-121 |
| ☐ Monitoring Maintenance Procedures - Form 4530-122 Pollutant(s): | |
| ☐ Stack Testing - Form 4530-123 Pollutant(s): | |
| ☐ Fuel Sampling and Analysis (FSA) - Form 4530-124 Pollutant(s): | |
| Recordkeeping - Form 4530-125 Pollutant(s): PM/PM ₁₀ /PM _{2.5} | |
| ☐ Other (please describe) - Form 4530-135 Pollutant(s): | |
| 6. Compliance certification reports will be submitted to the D Start date: At date of permit issuance and every 12 months thereafter. Compliance monitoring reports will be submitted to the Start date: At date of permit issuance | |
| and every <u>6</u> months thereafter. | |

COMPLIANCE DEMONSTRATION BY RECORDKEEPING AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-125 11-93

Information attached? \underline{n} (y/n)

Recordkeeping may be acceptable as a compliance demonstration method provided that a correlation between the parameter value recorded and the emission rate of a particular pollutant is established in the form of a curve or chart of emission rate versus parameter values. This correlation may constitute the certification of the system. It should be attached for Department approval. If it is not attached, please submit it within 60 days of the startup of the system.

| SEE INSTRUCTIONS ON REVERSE SIDE | |
|---|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 |
| 3. Stack identification number: NA | 4. Unit identification number: F01 |
| 5. Pollutant(s) being monitored: PM/PM ₁₀ /PM _{2.5} | 6. Material or parameter being monitored and recorded: Fugitive dust |
| 7. Method of monitoring and recording: <u>Comply with fugitive dust control plan</u> | |
| 8. List any EPA methods used: N/A | |
| 9. Is this an existing method of demonstrating compliance? ☐ Yes ☑ No | 10. Installation date: TBD |
| 11. Backup system: N/A | |
| 12. Compliance shall be demonstrated: ☐ Daily ☐ Weekly | ☑ Monthly ☐ Batch (not to exceed monthly) |
| 13. Indicate by checking: | |
| assurance procedures. A quality assurance/quality co | ase submit it within 60 days of the startup of the recordkeeping |
| ***** The compliance records shall be available for Department certification report and the excess emission report shal format for the compliance certification report and excessame time as the application. | l be approved by the Department. A proposed |
| ***** The source shall record any malfunction that causes or ma Malfunctions shall be reported to the Department the n | |

be reported to the Department immediately.

EMISSION UNIT HAZARDOUS AIR POLLUTANT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-126 11-93 Information attached? n (y/n)

| SEE INSTRUCTIONS ON REVERSE SIDE | | |
|---|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 | |
| 3. Stack identification number: NA | 4. Unit identification number: F01 | |

5. Unit material description: PM, PM₁₀, PM_{2.5} fugitives

6 Complete the following summary of hazardous air emissions from this unit. Attach sample calculations and emission factor

| references. Attached?no | | | | |
|-------------------------|----------------|---------------|-------|-------|
| | 11.4 | | T1 '4 | |
| | Units NO HA | APS EMISSIONS | Units | |
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EMISSION UNIT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION Form 4530-128 11-93

Information attached? y (y/n)

| SEE INSTRUCTIONS ON REVERS | CH CIDE | |
|----------------------------|---------|--|

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 |
|---|--|
| 3. Stack identification number: NA | 4. Unit identification number: F01 |

5. Complete the following emissions summary for the following pollutants. Attach sample calculations and emission factor references. Attached? See Appendix C

| J | I TPV | | | TPY | | U | TPY |
|---|-------|--|--|-----|--|---|-----|

SEE APPENDIX C FOR EMISSION CALCULATIONS

| | T 1 | | · · | | l | | |
|----------------------|-----|---|-----|-----|---|---|---|
| Sulfur dioxide | | | | TPY | | | |
| Organic compounds | | | | TPY | | | |
| Carbon monoxide | | | | TPY | | | |
| Lead | | | | TPY | | | |
| Nitrogen oxides | | | | TPY | | | |
| Total reduced sulfur | | | | TPY | | | |
| Mercury | | | | TPY | | | |
| Asbestos | | | | TPY | | | |
| Beryllium | | | | TPY | | | |
| Vinyl chloride | | | | TPY | | | |
| | | | | TPY | | | |
| | | | | TPY | | | |
| | | | | TPY | | | |
| | | | | TPY | | | |
| | | _ | | TPY | | _ | _ |

Units (U) should be entered as follows:

^{1 =} lb/hr

^{2 =} lb/mmBTU

^{3 =} grains/dscf

^{4 =} lb/gallon

^{5 =} ppmdv

^{6 =} other (specify)

^{7 =} other (specify)

^{8 =} other (specify)

CURRENT EMISSIONS REQUIREMENTS AND STATUS OF UNIT AIR POLLUTION CONTROL PERMIT APPLICATION
Form 4530-130 Rev. 12-99 Information attached? <u>n</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | | 2. Facility identification number: 816127840 | | | |
|---|--|--|--|------------|--|
| 3. Stack identification number: NA | | 4. Unit identification number: F01 | | | |
| | | 7. State Only | | | |
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** PART 70 SOURCES ONLY:

1. Be sure to review the Compliance Assurance Monitoring (CAM) Rule, 40 CFR Part 64, for the Renewal Application. The CAM rule requires owners and operators of Part 70 sources to monitor the operation and maintenance of their control equipment so that they can evaluate the performance of their control devices and report whether or not their facilities meet established emission standards. All facilities that have a Title V, Part 70, Federal Operating Permit are required to meet the CAM rule and submit a CAM plan with this Title V renewal application. The rule requires that a CAM plan be submitted with the Title V renewal application for each pollutant at each emissions unit which has a potential to emit - prior to controls - of that pollutant greater than the major source threshold for the respective pollutant. Please refer to the CAM Technical Guidance web site at http://www.epa.gov/ttn/emc/cam.html for further documentation on the rule and how to prepare a CAM plan for submittal with the renewal application.

2. List all applicable **Maximum Achievable Control Technology** (MACT) rule(s) and the effective date(s) if they were promulgated during the last 3 years of your operation permit term. Identify the emissions units subject to each MACT rule listed.

EMISSION UNIT COMPLIANCE PLAN COMMITMENTS AND SCHEDULE AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-131 11-93 Information attached? \underline{n} (y/n) SEE INSTRUCTIONS ON REVERSE SIDE 1. Facility name: Nemadji Trail Energy 2. Facility identification number: 816127840 Center 3. Stack identification number: NA 4. Unit identification number: F01 5. For Units that are presently in compliance with all applicable requirements, including any enhanced monitoring and compliance certification requirements under section 114(a)(3) of the Clean Air Act that apply, complete the following. These commitments are part of the application for Part 70 permits. ☐ We will continue to operate and maintain this Unit in compliance with all applicable requirements. Form 4530-130 includes new requirements that apply or will apply to this Unit during the term of the permit. We will meet such requirements on a timely basis. 6. For Units <u>not</u> presently fully in compliance, complete the following. This Unit is in compliance with all applicable requirements except for those indicated below. We will achieve compliance according to the following schedule: Applicable Requirement Corrective Actions Deadline 1. 2. 3.

| Progress reports will be submitted: | | | |
|-------------------------------------|-------------------------------------|--|--|
| Start date: | and every six (6) months thereafter | | |

State of Wisconsin STACK IDENTIFICATION

Department of Natural Resources

AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-103 11-93 Information attached? <u>n</u> (y/n)

| SEE INSTRUCTIONS ON REVERSE SIDE | | | | |
|--|--|------------------------------------|--|--|
| Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 | 3. Stack identification number: NA | | |
| 4. Exhausting Unit(s), use Unit identification | n number from appropriate Form(s) 4530 | 0-104, 106, 107, 108 and/or 109 | | |
| 4530-104 4530-106 | 4530-107 4530-108 | 4530-109 <u>F02</u> | | |
| 5. Identify this stack on the plot plan require | d on Form 4530-101 | | | |
| 6. Indicate by checking: ☐ This stack has an actual exhaust po | int. | y fugitive emissions. | | |
| If this stack has an actual exhaust poin | t, then provide the following stack paran | neters | | |
| 7. Discharge height above ground level: | _(feet) | | | |
| 8. Inside dimensions at outlet (check one and complete): | | | | |
| Circular (feet) | ☐ rectangularlength (feet) | width (feet) | | |
| 9. Exhaust flow rate: | | | | |
| Normal (ACFM) Maximum (ACFM) | | | | |
| 10. Exhaust gas temperature (normal): | _(°F) | | | |
| 11. Exhaust gas moisture content: | Normal volume percent | Maximum volume percent | | |
| 12. Exhaust gas discharge direction: | □ Up □ Down | ☐ Horizontal | | |
| 13. Is this stack equipped with a rainhat or any obstruction to the free flow of the exhaust gases from the stack? ☐ Yes ☐ No | | | | |
| ***** Complete the appropriate Air Permit Application Forms(s) 4530-104, 106, 107, 108 or 109 for each Unit ***** exhausting through this stack. | | | | |

MISCELLANEOUS PROCESSES AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-109 11-93 Information attached? n (y/n)

| SEE INSTRUCTIONS | ON REVERSE SIDE | | | | | | |
|---|---|----------------------------|--|-------------------------|-------------------------------|--|--|
| 1. Facility name: Nem | . Facility name: Nemadji Trail Energy Center 2 | | 2. Facility identification number: 816127840 | | | | |
| 3. Stack identification number: NA | | 4. Process number: F02 | | | | | |
| 4a. Unit description: | piping fugitives | | | | | | |
| 5. Indicate the control | technology status. | olled Controlled | | | | | |
| If the process is | controlled, enter the control devic | e number(s) from the appr | ropriate form(| (s): | | | |
| 4530-110 4530-114 | 4530-110 4530-111 4530-112 4530-113 4530-114 4530-115 4530-116 4530-117 | | | | | | |
| 6. Source Classificatio | n Code (SCC): 30180001 | | | | | | |
| 7. Date of construction | or last modification: TBD | | | | | | |
| 8. Normal operating so | chedule: <u>24</u> hrs./day <u>7</u> da | ays/wk. <u>365</u> days/yr | • | | | | |
| 9. Describe this process (please attach a flow diagram of the process). Fugitive emissions from piping components (valves, flanges, compressors, sampling connections and relief valves). Attached? See next page. Figures are at the end of Appendix | | | | | e. f Appendix A | | |
| 10. List the types and | d amounts of raw materials used i | n this process: | | | | | |
| Material | Storage/material handling process | Average usage | Units | Maximum usage | Units | | |
| N/A | | | | | | | |
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| 11 71 1 | 1 | | | | | | |
| | d amounts of finished products: | A4 | II:4- | M | I I:4- | | |
| Material | Storage/material handling process | Average amount produced | Units | Maximum amount produced | Units | | |
| N/A | • | · | | • | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| 12. Process fuel usage: | | | | | | | |
| Type of fuel | Maximum heat input to process million BTU/hr. | Average usage | Units | Maximum usage | Units | | |
| N/A | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| 13. Describe any fugitive emissions associated with this process, such as outdoor storage piles, unpaved roads, open conveyors, etc.: N/A | | | | | | | |
| ***** For this emissions unit, identify the method(s) of compliance demonstration by completing Form 4530-118, ***** DESCRIPTION OF METHODS USED FOR DETERMINING COMPLIANCE. Attach Form 4530-118 and its attachment(s) to this form. This is not a requirement of non-Part 70 sources. | | | | | | | |
| ***** Please complete the Air Pollution Control Permit Application Forms 4530-126 and 4530-128 for this Unit. ***** | | | | | | | |

COMPLIANCE CERTIFICATION - MONITORING AND REPORTING DESCRIPTION OF METHODS USED FOR DETERMINING COMPLIANCE Form 4530-118 11-93

Information attached? n (y/n)

All applicants except non-Part 70 sources are required to certify compliance with all applicable air pollution permit requirements by including a statement within the permit application of the methods used for determining compliance (please see sec. NR 407.05(4)(i), Wis. Adm. Code.) This statement must include a description of the monitoring, recordkeeping, and reporting requirements and test methods. In addition, the application must include a schedule for compliance certification submittals during the permit term. These submittals must be no less frequent than annually, and may need to be more frequent if specified by the underlying applicable requirement or by the Department.

| SEE INSTRUCTIONS ON REVERSE SIDE | |
|---|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 |
| | |

| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 | | | |
|--|--|--|--|--|
| 3. Stack identification number: NA | 4. Unit identification number: F02 | | | |
| 5. This Unit will use the following method(s) for determining compliance with the requirements of the permit (check all that apply and attach the appropriate form(s) to this form). | | | | |
| ☐ Continuous Emission Monitoring (CEM) - Form 4530-119 Pollutant(s): | | | | |
| ☐ Periodic Emission Monitoring Using Portable Monitors - Form 4530-120 Pollutant(s): | | | | |
| ☐ Monitoring Control System Parameters or Operating Parameters of a Process - Form 4530-121 Pollutant(s): | | | | |
| ✓ Monitoring Maintenance Procedures - Form 4530-122 Pollutant(s): GHG and VOC | | | | |
| ☐ Stack Testing - Form 4530-123 Pollutant(s): | | | | |
| ☐ Fuel Sampling and Analysis (FSA) - Form 4530-124 Pollutant(s): | | | | |
| Recordkeeping - Form 4530-125 Pollutant(s): GHG and VOC | | | | |
| ☐ Other (please describe) - Form 4530-135 Pollutant(s): | | | | |
| | | | | |
| 6. Compliance certification reports will be submitted | ed to the Department according to the following schedule: | | | |
| Start date: At date of permit issuance and every 12 months thereafter. | | | | |
| Compliance monitoring reports will be subm | itted to the Department according to the following schedule: | | | |
| Start date: At date of permit issuance and every 6 months thereafter. | | | | |

From January 2021 Application

State of Wisconsin Department of Natural Resources COMPLIANCE DEMONSTRATION BY MONITORING MAINTENANCE PROCEDURES AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-122 11-93

Information attached? ___ (y/n)

The monitoring of a maintenance procedure may be acceptable as a compliance demonstration method provided that a correlation between the procedure and the emission rate of a particular pollutant is established in the form of a curve of emission rate versus the frequency the procedure is performed. VOC leak detection programs or fugitive dust control programs are examples of procedures that could be monitored. The correlation shall be established using stack test data. This correlation shall constitute the certification of the monitoring system. It should be attached for Department approval. If it is not attached, please submit it within 60 days of the startup of the monitoring program.

| SEE INSTRUCTIONS ON REVERSE SIDE | | | | | | |
|--|--|--|--|--|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 | | | | | |
| 3. Stack identification number: NA | 4. Unit identification number: F02 | | | | | |
| 5. Pollutant(s) being monitored: GHG and VOC | | | | | | |
| 6. Procedure being monitored: GHG and VOC fugitives from pipi | ng components | | | | | |
| 7. Is this an existing maintenance procedure? □ Yes □ No 8. Installation date: TBD | | | | | | |
| 9. Method of monitoring: Quarterly and/or semi-annual inspection smell. | of equipment using instrumental methods, sight, sound, and | | | | | |
| 10. Compliance shall be demonstrated: ☐ Daily ☐ Weekly | ☐ Monthly - Quarterly and/or semi-annual inspection | | | | | |
| 11. Indicate by checking: | | | | | | |
| The monitoring program shall be subject to appropriate performance specifications, calibration requirements, and quality assurance procedures. ☐ A quality assurance/quality control plan for the monitoring program is attached for Department approval. ☑ If the plan is not attached, please submit it within 60 days of the startup of the monitoring program. ☐ The plan was submitted to the Department on | | | | | | |

**** Any failure to fulfill a maintenance requirement shall be reported as an excess emission. *****

COMPLIANCE DEMONSTRATION BY RECORDKEEPING AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-125 11-93

Information attached? \underline{n} (y/n)

Recordkeeping may be acceptable as a compliance demonstration method provided that a correlation between the parameter value recorded and the emission rate of a particular pollutant is established in the form of a curve or chart of emission rate versus parameter values. This correlation may constitute the certification of the system. It should be attached for Department approval. If it is not attached, please submit it within 60 days of the startup of the system.

| SEE INSTRUCTIONS ON REVERSE SIDE | | | | | | |
|--|---|--|--|--|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 | | | | | |
| 3. Stack identification number: NA | 4. Unit identification number: F02 | | | | | |
| 5. Pollutant(s) being monitored: GHG and VOC | 6. Material or parameter being monitored and recorded: GHG and VOC fugitives from piping components | | | | | |
| 7. Method of monitoring and recording: Per plan, comply with inspection of equipment using instrur | nental methods, sight, sound, and smell. | | | | | |
| 8. List any EPA methods used: N/A | | | | | | |
| 9. Is this an existing method of demonstrating compliance? ☐ Yes ✓ No | 10. Installation date: TBD | | | | | |
| 11. Backup system: N/A | | | | | | |
| 12. Compliance shall be demonstrated: ☐ Daily ☐ Weekly Applicant proposes quarterly and/or semi-annual compliance dem | | | | | | |
| 13. Indicate by checking: | | | | | | |
| The monitoring system shall be subject to appropriate performance specifications, calibration requirements, and quality assurance procedures. A quality assurance/quality control plan for the recordkeeping system is attached for Department approval. If the plan is not attached, please submit it within 60 days of the startup of the recordkeeping program. The plan was submitted to the Department on | | | | | | |
| ***** The compliance records shall be available for Department inspection. The format for the compliance ***** certification report and the excess emission report shall be approved by the Department. A proposed format for the compliance certification report and excess emission report shall be submitted at the same time as the application. | | | | | | |
| **** The source shall record any malfunction that causes or may cause an emission limit to be exceeded. **** Malfunctions shall be reported to the Department the next business day. Hazardous air spills shall | | | | | | |

be reported to the Department immediately.

EMISSION UNIT HAZARDOUS AIR POLLUTANT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-126 11-93 Information attached? \underline{n} (y/n)

| SEE INSTRUCTIONS ON REVERSE SIDE | |
|--|--|
| 1. Facility name: Nemadji Trail Energy Center | 2. Facility identification number: 816127840 |
| 3. Stack identification number: NA | 4. Unit identification number: F02 |
| 5. Unit material description: Piping fugitives (GHG and VOC) | |

6. Complete the following summary of hazardous air emissions from this unit. Attach sample calculations and emission factor references. Attached? no

| references. Att | ached?no | dous un Chinssion | The state of the s | ii sumpre carearan | ons and emission factor |
|-----------------|----------|-------------------|--|--------------------|-------------------------|
| | | | | | |
| | | Units | | Units | |
| | | | PS EMISSIONS | | |
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EMISSION UNIT SUMMARY AIR POLLUTION CONTROL PERMIT APPLICATION

| Form 4530-128 11-93 In: SEE INSTRUCTIONS ON REVERSE SIDE | | | | | | | nformation | attach | ned? <u>y</u> (y/n) | | |
|---|---------------------------------|-------|--------|------------|--------|---------------|------------|---------|---------------------|---|-----|
| | EE INSTRUCTIONS ON REVERSE SIDE | | | | | | | | | | |
| 1. Facility name: Nemad | lji Trail E | nergy | Center | 2. Facilit | y ider | ntification n | umber: 816 | 5127840 | | | |
| 3. Stack identification no | umber: N | 4 | | 4. Unit id | lentif | ication num | ber: F02 | | | | |
| 5. Complete the following emissions summary for the following pollutants. Attach sample calculations and emission factor references. Attached? See Appendix C | | | | | | | | | | | |
| | | | | | | | | | | | |
| | | U | TPY | | U | TPY | | | | U | TPY |
| SEE APPENDIX C FOR EMISSION CALCULATIONS | | | | | | | | | | | |
| _ | | | | | | | | | | | |

| Sulfur dioxide | | | | TPY | | |
|----------------------|--|--|---|-----|--|--|
| Organic compounds | | | | TPY | | |
| Carbon monoxide | | | | TPY | | |
| Lead | | | | TPY | | |
| Nitrogen oxides | | | | TPY | | |
| Total reduced sulfur | | | | TPY | | |
| Mercury | | | · | TPY | | |
| Asbestos | | | | TPY | | |
| Beryllium | | | · | TPY | | |
| Vinyl chloride | | | | TPY | | |
| | | | | TPY | | |
| | | | | TPY | | |
| | | | - | TPY | | |
| | | | - | TPY | | |
| | | | | TPY | | |

Units (U) should be entered as follows:

 $[\]begin{array}{l} 1 = lb/hr \\ 2 = lb/mmBTU \end{array}$

^{3 =} grains/dscf 4 = lb/ gallon

^{5 =} ppmdv 6 = other (specify) 7 = other (specify) 8 = other (specify)

CURRENT EMISSIONS REQUIREMENTS AND STATUS OF UNIT AIR POLLUTION CONTROL PERMIT APPLICATION
Form 4530-130 Rev. 12-99 Information attached? <u>n</u> (y/n)

SEE INSTRUCTIONS ON REVERSE SIDE

| 1. Facility name: Nemadji Trail Energy Center | | | 2. Facility identification number: 816127840 | | | |
|---|-------|------------------------------------|--|------------|--|--|
| 3. Stack identification number | r: NA | 4. Unit identification number: F02 | | | | |
| | | 7. State Only | | | | |
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** PART 70 SOURCES ONLY:

1. Be sure to review the Compliance Assurance Monitoring (CAM) Rule, 40 CFR Part 64, for the Renewal Application. The CAM rule requires owners and operators of Part 70 sources to monitor the operation and maintenance of their control equipment so that they can evaluate the performance of their control devices and report whether or not their facilities meet established emission standards. All facilities that have a Title V, Part 70, Federal Operating Permit are required to meet the CAM rule and submit a CAM plan with this Title V renewal application. The rule requires that a CAM plan be submitted with the Title V renewal application for each pollutant at each emissions unit which has a potential to emit - prior to controls - of that pollutant greater than the major source threshold for the respective pollutant. Please refer to the CAM Technical Guidance web site at http://www.epa.gov/ttn/emc/cam.html for further documentation on the rule and how to prepare a CAM plan for submittal with the renewal application.

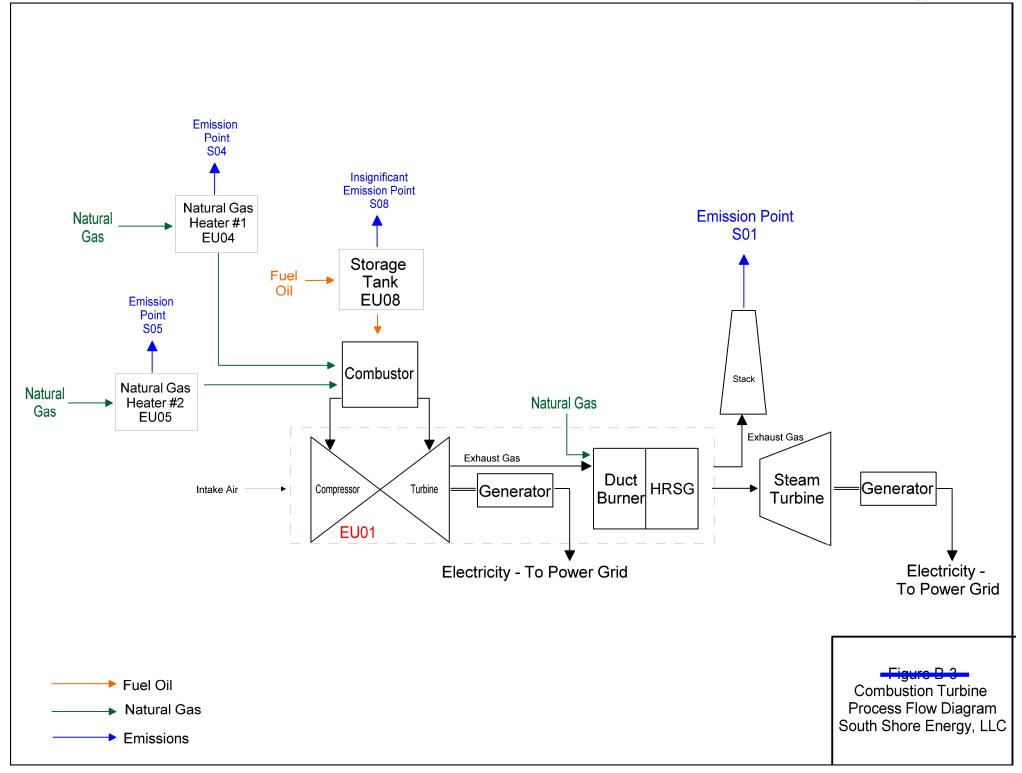
2. List all applicable **Maximum Achievable Control Technology** (MACT) rule(s) and the effective date(s) if they were promulgated during the last 3 years of your operation permit term. Identify the emissions units subject to each MACT rule listed.

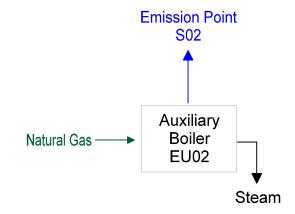
Progress reports will be submitted:

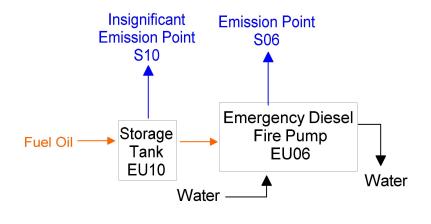
Start date: _____ and every six (6) months thereafter

EMISSION UNIT COMPLIANCE PLAN COMMITMENTS AND SCHEDULE AIR POLLUTION CONTROL PERMIT APPLICATION

Form 4530-131 11-93 Information attached? \underline{n} (y/n) SEE INSTRUCTIONS ON REVERSE SIDE 1. Facility name: Nemadji Trail Energy 2. Facility identification number: 816127840 Center 3. Stack identification number: NA 4. Unit identification number: F02 5. For Units that are presently in compliance with all applicable requirements, including any enhanced monitoring and compliance certification requirements under section 114(a)(3) of the Clean Air Act that apply, complete the following. These commitments are part of the application for Part 70 permits. ☐ We will continue to operate and maintain this Unit in compliance with all applicable requirements. Form 4530-130 includes new requirements that apply or will apply to this Unit during the term of the permit. We will meet such requirements on a timely basis. 6. For Units <u>not</u> presently fully in compliance, complete the following. This Unit is in compliance with all applicable requirements except for those indicated below. We will achieve compliance according to the following schedule: Applicable Requirement Corrective Actions Deadline 1. 2. 3.







Fuel Oil

Natural Gas

Emissions

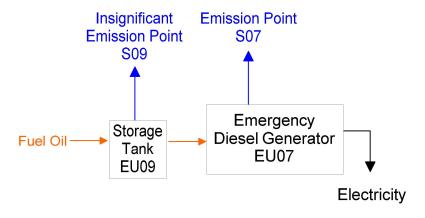
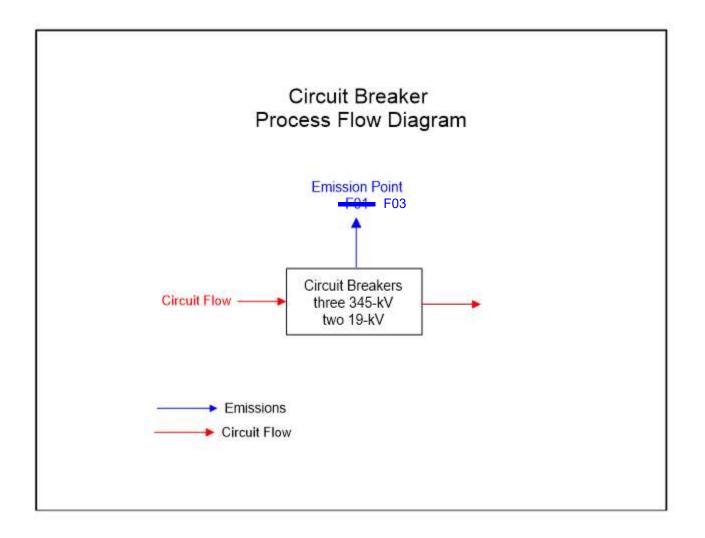
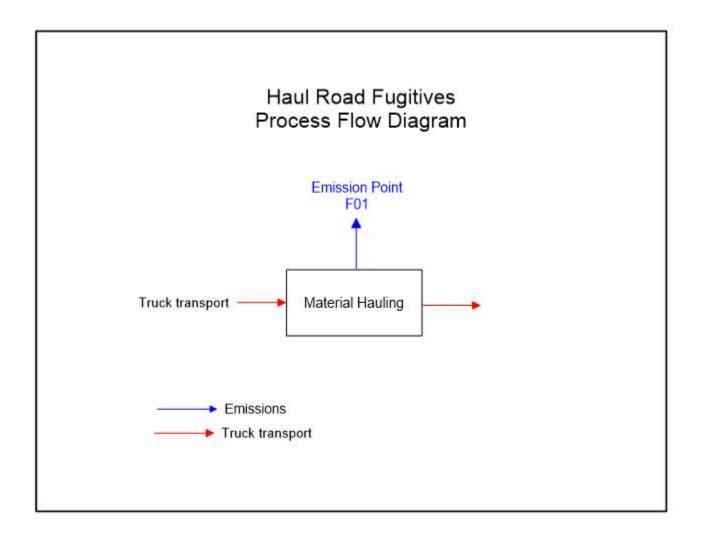
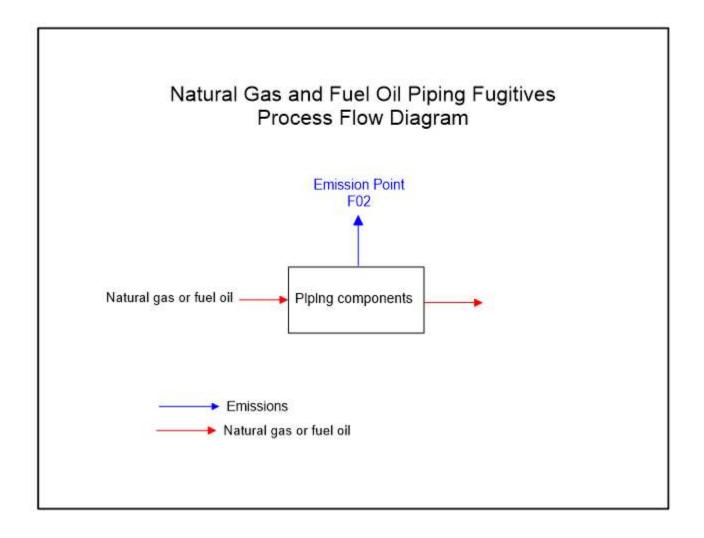


Figure B 1

Auxiliary Equipment
Process Flow Diagram
South Shore Energy, LLC







APPENDIX B - FIGURES

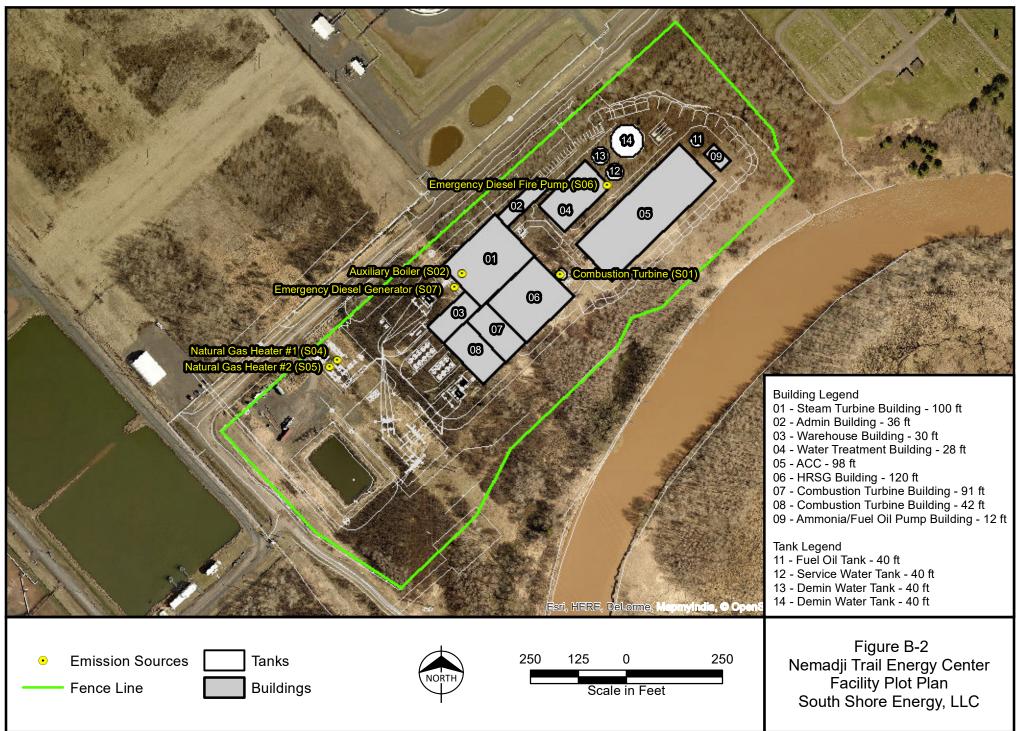
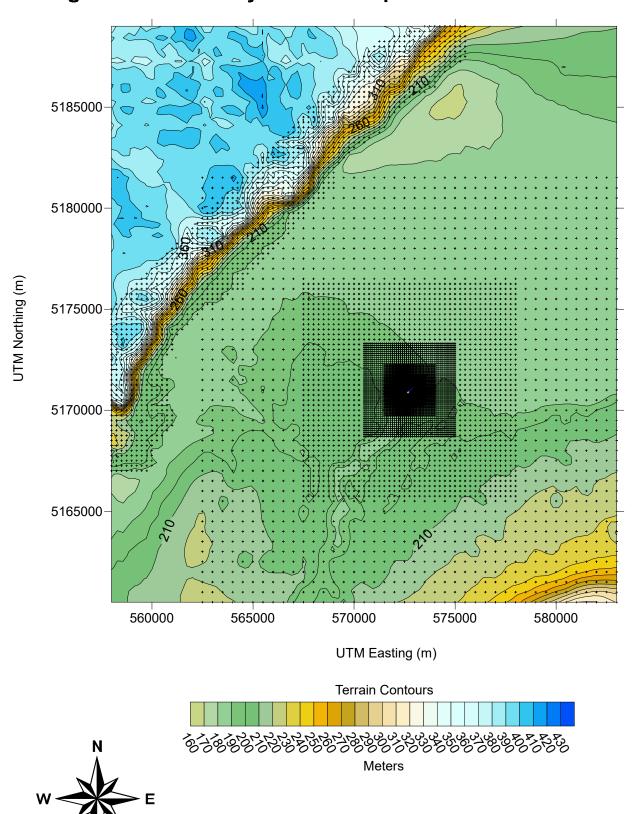


Figure B-3: 20 km by 20 km Receptor Grid and Elevation Map



County

Kilometers

Developed, High Intensity

Grassland/Herbaceous



South Shore Energy, LLC - Nemadji Trail Energy Center **Project Emissions**

Maximum Facility Emissions

| Pollutant | Permitted Potential Emissions ^a (tpy) | Project Potential Emissions ^b (tpy) | Total Facility Potential Emissions (tpy) |
|-------------------|--|--|---|
| NO _x | 269.1 | - | 269 |
| CO | 2,002.52 | - | 2,003 |
| PM | 166.9 | 0.10 | 167 |
| PM ₁₀ | 166.9 | 0.02 | 167 |
| PM _{2.5} | 166.9 | 0.005 | 167 |
| SO ₂ | 28.7 | | 29 |
| VOC | 239 | 10.4 | 250 |
| H₂SO₄ | 43.2 | | 43 |
| Lead | 0.0 | | 0.01 |
| CO₂e | 2,738,317.8 | 976.6 | 2,739,294 |

(a) Construction Permit Number: 18-MMC-168 (b) Construction Permit Number: 21-MMC-011

Maximum Annual Emission Rates

| Waxiiiaiii Aiiiia | illual Elilission Rates | | | | | | | | | | | |
|--------------------------------|---|--|--|--|---|---|---|-------------------------------------|--|----------------------------------|-----------------------------|---|
| | | Construction Permit Number: 18-MMC-168 | | | | | | | | Permit Number: IMC-011 | | |
| Pollutant | P01 Combined-Cycle Combustion Turbine ^a (tpy) | B02 Auxiliary Boiler (tpy) | P04 Natural Gas Heater #1 (tpy) | P05 Natural Gas Heater #2 (tpy) | P06 Emergency Diesel Fire Pump (tpy) | P07 Emergency Diesel Generator (tpy) | T01, T02, T03 Storage Tanks (tpy) | F03 Circuit Breakers (tpy) | F01 Haul Road Fugitives (tpy) | F02 Piping Fugitives (tpy) | Total ^b (tpy) | PSD Significant Emission Rates (tpy) |
| NO _x | 255,6 | 4.8 | 2.1 | 2.1 | 0.5 | 3.9 | - | _ | - | | 269 | 40 |
| CO | 1,991.1 | 1.6 | 3.6 | 3.6 | 0.4 | 2.1 | | | | | 2,003 | 100 |
| PM | 162.8 | 3.3 | 0.3 | 0.3 | 0.02 | 0.1 | | | 0.10 | | 167 | 25 |
| PM ₁₀ | 162.8 | 3.3 | 0.3 | 0.3 | 0.02 | 0.1 | - | - | 0.02 | | 167 | 15 |
| PM _{2.5} | 162.8 | 3.3 | 0.3 | 0.3 | 0.02 | 0.1 | - | - | 0.005 | | 167 | 10 |
| SO ₂ | 28.2 | 0.3 | 0.03 | 0.03 | 0.1 | 4.5.E-03 | - | - | _ | | 29 | 40 |
| VOC | 237.3 | 1.2 | 0.2 | 0.2 | 0.2 | 0.3 | 0.04 | | - | 10.4 | 250 | 40 |
| H ₂ SO ₄ | 43.2 | 0.04 | 3.9.E-03 | 3.9.E-03 | 0.02 | 6.9.E-04 | | | | | 43 | 7 |
| Lead | 0.01 | 2.1.E-04 | 4.3.E-05 | 4.3.E-05 | | | | - | - | | 0.01 | 0.6 |
| CO₂e | 2,675,731 | 51,289 | 5,129 | 5,129 | 80 | 841 | | 120 | | 977 | 2,739,294 | 75,000 |

(a) Represents worse-case emissions scenario (b) Numbers in bold indicate the PSD significance level is exceeded

| | Assumptions | | | | | | |
|----------------------------|------------------|--|--|--|--|--|--|
| Unit | Limitation | Units | | | | | |
| | 8,760 | Natural gas hours per year | | | | | |
| | 50 | Number of natural gas cold starts per year | | | | | |
| | 150 | Number of natural gas warm starts per year | | | | | |
| | 900 | Number of natural gas hot/fast starts per year | | | | | |
| | 1,100 | Total number of combined natural gas start-ups per year (cold/warm/hot/fast) | | | | | |
| Turbine | 1,100 | Total number of natural gas shutdowns per year | | | | | |
| | 1,525.0 | Hours of natural gas Startup/Shutdown per year | | | | | |
| | 500 | Fuel oil hours per year with or without duct burning | | | | | |
| | 11,025,196 | gallons/year fuel oil | | | | | |
| | 42 | Number of fuel oil startup/shutdowns per year | | | | | |
| | 105.0 | Hours of fuel oil Startup/Shutdown | | | | | |
| Natural Gas Duct Firing | 8,760 | Hours per year | | | | | |
| Auxiliary Boiler | 8,760 | Hours per year | | | | | |
| Cooling Tower | 8,760 | Hours per year | | | | | |
| Natural Gas Heater #1 | 8,760 | Hours per year | | | | | |
| Natural Gas Heater #2 | 8,760 | Hours per year | | | | | |
| Emergency Diesel Fire Pump | 500 | Hours per year | | | | | |
| Emergency Diesel Generator | 500 | Hours per year | | | | | |
| Fuel oil heating value | 137,000 | Btu/gal | | | | | |

South Shore Energy, LLC - Nemadji Trail Energy Center Combustion Turbine

| | Natural Gas | | | | | | |
|--|--------------|---------|-------|--|--|--|--|
| | Duct Burning | 100 | 75 | Minimum Emissions Compliance Load | | | |
| Pollutants | lb/hr | lb/hr | lb/hr | lb/hr | | | |
| NO _X | 33.5 | 26.5 | 20.6 | 12.4 | | | |
| CO | 15.3 | 12.1 | 9.4 | 5.7 | | | |
| PM/PM ₁₀ /PM _{2.5} | 36.3 | 21.8 | 16.8 | 12.9 | | | |
| SO ₂ | 6.4 | 5.1 | 4.0 | 2.4 | | | |
| VOC | 15.5 | 2.8 | | | | | |
| H ₂ SO ₄ | 9.9 | 7.8 | | | | | |
| Lead | 0.0 | 0.0 | | | | | |
| CO ₂ | 495,325 | 392,985 | | | | | |
| N ₂ O | 303.5 | 240.8 | | | | | |
| CH₄ | 254.6 | 202.0 | | | | | |
| CO ₂ e (sum) | 592,127 | 469,787 | | | | | |

167.12

63.81

| Natural Gas | Startup/Shutdown | Emissions |
|-------------|------------------|-----------|

163.55

64.00

Temperature

Velocity

| Pollutant | Start-up Emissions (lb/cold start) ^{b,d} | Start-up Emissions (lb/warm start) ^{b, d} | Start-up Emissions (lb/hot-fast start) ^{b, d} | Shutdown Emissions (lb/shutdown) ^c | Start-up/ Shutdown Emissions (tpy) |
|--|---|--|---|---|---|
| NOx ^a | 335.0 | 233.0 | 111.0 | 59.0 | 108.3 |
| CO ^a | 11,066 | 6,495 | 779.0 | 463.0 | 1,369 |
| PM/PM ₁₀ /PM _{2.5} | 43.6 | 29.1 | 16.3 | 10.9 | 16.6 |
| SO ₂ | 10.2 | 6.8 | 3.8 | 2.6 | 3.9 |
| VOCª | 950.0 | 558.0 | 67.0 | 40.0 | 117.8 |
| H ₂ SO ₄ | 15.6 | 10.4 | 5.9 | 3.9 | 6.0 |
| Lead | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| CO ₂ | 785,971 | 523,981 | 294,739 | 196,493 | 299,651 |
| N ₂ O | 482 | 321 | 181 | 120 | 184 |
| CH₄ | 404 | 269 | 151 | 101 | 154 |
| CO ₂ e | 939,573 | 626,382 | 352,340 | 234,893 | 358,212 |

164.93

48.88

164.93

36.82

- (a) Start-up emissions based on vendor load and startup profiles
- (b) Cold start-up period is 2 hours, warm start-up period is 80 minutes, hot/fast start-up period is 45 minutes
- (c) Shutdown emissions from "startup summary" (assumes half hour)
- (d) Emissions are based on 1525 hours spent in start-up/shutdown operation

| | Fuel Oil | | | | | | |
|--|--------------|---------|--------|-----------------------------------|--|--|--|
| | Duct Burning | 100 | 75 | Minimum Emissions Compliance Load | | | |
| Pollutants | lb/hr | lb/hr | lb/hr | lb/hr | | | |
| NO _X | 72.7 | 51.6 | 41.0 | 31.1 | | | |
| CO | 11.1 | 7.8 | 6.2 | 15.8 | | | |
| PM/PM ₁₀ /PM _{2.5} | 54.5 | 39.4 | 37.5 | 35.7 | | | |
| SO ₂ | 6.1 | 4.6 | 3.6 | 2.8 | | | |
| VOC | 14.1 | 1.8 | | | | | |
| H ₂ SO ₄ | 9.3 | 7.0 | | | | | |
| Lead | 0.04 | 0.04 | | | | | |
| CO ₂ | 559,613 | 452,619 | | | | | |
| N ₂ O | 1,256.3 | 1,190.8 | | | | | |
| CH ₄ | 554.4 | 499.5 | | | | | |
| CO ₂ e (sum) | 947,846 | 819,965 | | | | | |
| | | | | | | | |
| Temperature | 176.63 | 176.63 | 169.24 | 165.01 | | | |
| Velocity | 71.96 | 71.19 | 57.75 | 43.48 | | | |

Fuel Oil Startup/Shutdown Emissions

| Pollutant | Start-up Emissions (lb/cold start) ^b | Shutdown Emissions (lb/shutdown) ^c | Number of Starts Per Turbine | Start-up/ Shutdown Emissions (tpy) |
|--|---|---|------------------------------------|---|
| NOx ^a | 860.0 | 108.0 | 42 | 20.3 |
| CO ^a | 25,846 | 1,227 | 42 | 568.5 |
| PM/PM ₁₀ /PM _{2.5} | 78.9 | 19.7 | 42 | 2.1 |
| SO ₂ | 9.2 | 2.3 | 42 | 0.2 |
| VOCª | 2,951 | 122.0 | 42 | 64.5 |
| H ₂ SO ₄ | 14.0 | 3.5 | 42 | 0.4 |
| Lead | 0.08 | 0.02 | 42 | 0.002 |
| CO ₂ | 905,239 | 226,310 | 42 | 23,763 |
| N ₂ O | 2,382 | 595 | 42 | 63 |
| CH ₄ | 999 | 250 | 42 | 26 |
| CO ₂ e | 1,639,929 | 409,982 | 42 | 43,048 |

- (a) Start-up emissions based on vendor load and startup profiles
- (b) Start-up emissions are 2 hours.
- (c) Shutdown emissions from "startup summary" (assumes half hour)

South Shore Energy, LLC - Nemadji Trail Energy Center Combustion Turbine Emissions

DB= Duct Burning NG= Natural Gas SUSD= Startup Shutdown FO=Fuel Oil

| | DB NG | NG 100 | DB FO | FO 100 |
|--|---------|---------|---------|---------|
| Pollutant | lb/hr | lb/hr | lb/hr | lb/hr |
| NO_X | 33.5 | 26.5 | 72.7 | 51.6 |
| CO | 15.3 | 12.1 | 11.1 | 7.8 |
| PM/PM ₁₀ /PM _{2.5} | 36.3 | 21.8 | 54.5 | 39.4 |
| SO ₂ | 6.4 | 5.1 | 6.1 | 4.6 |
| VOC | 15.5 | 2.8 | 14.1 | 1.8 |
| H ₂ SO ₄ | 9.9 | 7.8 | 9.3 | 7.0 |
| Lead | 0.0 | 0.0 | 0.042 | 0.042 |
| CO ₂ | 495,325 | 392,985 | 559,613 | 452,619 |
| N ₂ O | 303.5 | 240.8 | 1,256.3 | 1,190.8 |
| CH ₄ | 254.6 | 202.0 | 554.4 | 499.5 |
| CO ₂ e (sum) | 592,127 | 469,787 | 947,846 | 819,965 |

| NG Start- up/Shutdown Emissions | FO Start- up/Shutdown Emissions |
|---------------------------------------|---------------------------------------|
| tpy | tpy |
| 108.3 | 20.3 |
| 1,369.0 | 568.5 |
| 16.6 | 2.1 |
| 3.9 | 0.2 |
| 117.8 | 64.5 |
| 6.0 | 0.4 |
| 0.0 | 0.002 |
| 299,651 | 23,763 |
| 184 | 63 |
| 154 | 26 |
| 358,212 | 43,048 |

| Scenario 1 | Hours |
|-------------|-------|
| DB NG | 8,760 |
| NG | 0 |
| NG SSSD | 0 |
| DB FO | 0 |
| FO | 0 |
| FO SUSD | 0 |
| Total Hours | 8,760 |

| Pollutant | DB NG | NG | NG SSSD | DB FO | FO | FO SUSD | SUM |
|--|-----------|-----|---------|-------|-----|---------|-----------|
| | tpy | tpy | tpy | tpy | tpy | tpy | tpy |
| NO _X | 146.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 146.5 |
| CO | 66.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 66.9 |
| PM/PM ₁₀ /PM _{2.5} | 159.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 159.0 |
| SO ₂ | 28.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 28.2 |
| VOC | 68.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 68.0 |
| H ₂ SO ₄ | 43.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 43.2 |
| Lead | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.00 |
| CO ₂ | 2,169,524 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2,169,524 |
| N ₂ O | 1,329 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1,329 |
| CH ₄ | 1,115 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1,115 |
| CO ₂ e (sum) | 2,593,514 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2,593,514 |

| | Hours | | | | | | |
|-------------|------------|------------|------------|------------|------------|------------|------------|
| | Scenario 1 | Scenario 2 | Scenario 3 | Scenario 4 | Scenario 5 | Scenario 6 | Scenario 7 |
| DB NG | 8,760 | 7,235 | 6,735 | 0 | 0 | 8,260 | 6,735 |
| NG | 0 | 0 | 0 | 7,235 | 6,735 | 0 | 0 |
| NG SUSD | 0 | 1,525 | 1,525 | 1,525 | 1,525 | 0 | 1,525 |
| DB FO | 0 | 0 | 0 | 0 | 0 | 395 | 395 |
| FO | 0 | 0 | 395 | 0 | 395 | 0 | 0 |
| FO SUSD | 0 | 0 | 105 | 0 | 105 | 105 | 105 |
| Total Hours | 8,760 | 8,760 | 8,760 | 8,760 | 8,760 | 8,760 | 8,760 |

| | Scenario 1 | Scenario 2 | Scenario 3 | Scenario 4 | Scenario 5 | Scenario 6 | Scenario 7 | Maximum |
|--|------------|------------|------------|------------|------------|------------|------------|-----------|
| Pollutant | | | | tons p | er year | | | |
| NO _X | 146.5 | 229.3 | 251.4 | 204.3 | 228.2 | 172.9 | 255.6 | 255.6 |
| CO | 66.9 | 1,424.2 | 1,990.5 | 1,412.8 | 1,979.9 | 633.8 | 1,991.1 | 1,991.1 |
| PM/PM ₁₀ /PM _{2.5} | 159.0 | 148.0 | 148.8 | 95.5 | 99.9 | 162.8 | 151.7 | 162.8 |
| SO ₂ | 28.2 | 27.2 | 26.7 | 22.4 | 22.2 | 28.0 | 27.0 | 28.2 |
| VOC | 68.0 | 173.9 | 234.9 | 127.8 | 192.0 | 131.4 | 237.3 | 237.3 |
| H ₂ SO ₄ | 43.2 | 41.6 | 40.9 | 34.3 | 34.1 | 42.9 | 41.4 | 43.2 |
| Lead | 0.00 | 0.00 | 0.01 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 |
| CO ₂ | 2,169,524 | 2,091,490 | 2,080,813 | 1,721,276 | 1,736,185 | 2,179,979 | 2,101,945 | 2,179,979 |
| N ₂ O | 1,329 | 1,281 | 1,503 | 1,055 | 1,292 | 1,564 | 1,516 | 1,564 |
| CH₄ | 1,115 | 1,075 | 1,136 | 885 | 959 | 1,187 | 1,147 | 1,187 |
| CO ₂ e (sum) | 2,593,514 | 2,500,230 | 2,557,190 | 2,057,666 | 2,145,210 | 2,675,731 | 2,582,446 | 2,675,731 |

| Scenario 2 | Hours |
|-------------|-------|
| DB NG | 7,235 |
| NG | 0 |
| NG SSSD | 1525 |
| DB FO | 0 |
| FO | 0 |
| FO SUSD | 0 |
| Total Hours | 8,760 |

| Pollutant | DB NG | NG | NG SSSD | DB FO | FO | FO SUSD | SUM |
|--|-----------|-----|---------|-------|-----|---------|-----------|
| | tpy | tpy | tpy | tpy | tpy | tpy | tpy |
| NO _X | 121.0 | 0.0 | 108.3 | 0.0 | 0.0 | 0.0 | 229.3 |
| CO | 55.3 | 0.0 | 1,369.0 | 0.0 | 0.0 | 0.0 | 1,424.2 |
| PM/PM ₁₀ /PM _{2.5} | 131.4 | 0.0 | 16.6 | 0.0 | 0.0 | 0.0 | 148.0 |
| SO ₂ | 23.3 | 0.0 | 3.9 | 0.0 | 0.0 | 0.0 | 27.2 |
| VOC | 56.1 | 0.0 | 117.8 | 0.0 | 0.0 | 0.0 | 173.9 |
| H ₂ SO ₄ | 35.7 | 0.0 | 6.0 | 0.0 | 0.0 | 0.0 | 41.6 |
| Lead | 0.00 | 0.0 | 0.00 | 0.0 | 0.0 | 0.0 | 0.00 |
| CO ₂ | 1,791,838 | 0.0 | 299,651 | 0.0 | 0.0 | 0.0 | 2,091,490 |
| N ₂ O | 1,098 | 0.0 | 184 | 0.0 | 0.0 | 0.0 | 1,281 |
| CH ₄ | 921 | 0.0 | 154 | 0.0 | 0.0 | 0.0 | 1,075 |
| CO ₂ e (sum) | 2,142,018 | 0.0 | 358,212 | 0.0 | 0.0 | 0.0 | 2,500,230 |

| Scenario 3 | Hours |
|-------------|-------|
| DB NG | 6,735 |
| NG | 0 |
| NG SSSD | 1525 |
| DB FO | 0 |
| FO | 395 |
| FO SUSD | 105 |
| Total Hours | 8,760 |

| Pollutant | DB NG | NG | NG SSSD | DB FO | FO | FO SUSD | SUM |
|--|-----------|-----|---------|-------|---------|---------|-----------|
| | tpy | tpy | tpy | tpy | tpy | tpy | tpy |
| NO_X | 112.7 | 0.0 | 108.3 | 0.0 | 10.2 | 20.3 | 251.4 |
| CO | 51.4 | 0.0 | 1,369.0 | 0.0 | 1.5 | 568.5 | 1,990.5 |
| PM/PM ₁₀ /PM _{2.5} | 122.3 | 0.0 | 16.6 | 0.0 | 7.8 | 2.1 | 148.8 |
| SO ₂ | 21.7 | 0.0 | 3.9 | 0.0 | 0.9 | 0.2 | 26.7 |
| VOC | 52.3 | 0.0 | 117.8 | 0.0 | 0.4 | 64.5 | 234.9 |
| H ₂ SO ₄ | 33.2 | 0.0 | 6.0 | 0.0 | 1.4 | 0.4 | 40.9 |
| Lead | 0.00 | 0.0 | 0.00 | 0.0 | 0.01 | 0.00 | 0.01 |
| CO ₂ | 1,668,007 | 0.0 | 299,651 | 0.0 | 89,392 | 23,763 | 2,080,813 |
| N ₂ O | 1,022 | 0.0 | 184 | 0.0 | 235 | 63 | 1,503 |
| CH ₄ | 857 | 0.0 | 154 | 0.0 | 99 | 26 | 1,136 |
| CO ₂ e (sum) | 1,993,986 | 0.0 | 358,212 | 0.0 | 161,943 | 43,048 | 2,557,190 |

| Scenario 4 | Hours |
|-------------|-------|
| DB NG | 0 |
| NG | 7,235 |
| NG SSSD | 1,525 |
| DB FO | 0 |
| FO | 0 |
| FO SUSD | 0 |
| Total Hours | 8,760 |

| Pollutant | DB NG | NG | NG SSSD | DB FO | FO | FO SUSD | SUM |
|--|-------|-----------|---------|-------|-----|---------|-----------|
| | tpy | tpy | tpy | tpy | tpy | tpy | tpy |
| NO _X | 0.0 | 96.0 | 108.3 | 0.0 | 0.0 | 0.0 | 204.3 |
| CO | 0.0 | 43.9 | 1,369.0 | 0.0 | 0.0 | 0.0 | 1,412.8 |
| PM/PM ₁₀ /PM _{2.5} | 0.0 | 78.9 | 16.6 | 0.0 | 0.0 | 0.0 | 95.5 |
| SO ₂ | 0.0 | 18.5 | 3.9 | 0.0 | 0.0 | 0.0 | 22.4 |
| VOC | 0.0 | 10.0 | 117.8 | 0.0 | 0.0 | 0.0 | 127.8 |
| H ₂ SO ₄ | 0.0 | 28.3 | 6.0 | 0.0 | 0.0 | 0.0 | 34.3 |
| Lead | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.00 |
| CO ₂ | 0.0 | 1,421,625 | 299,651 | 0.0 | 0.0 | 0.0 | 1,721,276 |
| N ₂ O | 0.0 | 871.0 | 183.6 | 0.0 | 0.0 | 0.0 | 1,055 |
| CH ₄ | 0.0 | 730.7 | 154.0 | 0.0 | 0.0 | 0.0 | 885 |
| CO ₂ e (sum) | 0.0 | 1,699,454 | 358,212 | 0.0 | 0.0 | 0.0 | 2,057,666 |

| Scenario 5 | Hours |
|-------------|-------|
| DB NG | 0 |
| NG | 6,735 |
| NG SSSD | 1,525 |
| DB FO | 0 |
| FO | 395 |
| FO SUSD | 105 |
| Total Hours | 8,760 |

| Pollutant | DB NG | NG | NG SSSD | DB FO | FO | FO SUSD | SUM |
|--|-------|-----------|---------|-------|---------|---------|-----------|
| | tpy | tpy | tpy | tpy | tpy | tpy | tpy |
| NO _X | 0.0 | 89.4 | 108.3 | 0.0 | 10.2 | 20.3 | 228.2 |
| CO | 0.0 | 40.8 | 1,369.0 | 0.0 | 1.5 | 568.5 | 1,979.9 |
| PM/PM ₁₀ /PM _{2.5} | 0.0 | 73.4 | 16.6 | 0.0 | 7.8 | 2.1 | 99.9 |
| SO ₂ | 0.0 | 17.2 | 3.9 | 0.0 | 0.9 | 0.2 | 22.2 |
| VOC | 0.0 | 9.4 | 117.8 | 0.0 | 0.4 | 64.5 | 192.0 |
| H ₂ SO ₄ | 0.0 | 26.3 | 6.0 | 0.0 | 1.4 | 0.4 | 34.1 |
| Lead | 0.0 | 0.00 | 0.00 | 0.0 | 0.01 | 0.00 | 0.01 |
| CO ₂ | 0.0 | 1,323,379 | 299,651 | 0.0 | 89,392 | 23,763 | 1,736,185 |
| N ₂ O | 0.0 | 811 | 184 | 0.0 | 235 | 63 | 1,292 |
| CH ₄ | 0.0 | 680 | 154 | 0.0 | 99 | 26 | 959 |
| CO ₂ e (sum) | 0.0 | 1,582,007 | 358,212 | 0.0 | 161,943 | 43,048 | 2,145,210 |

| Hours |
|-------|
| 8,260 |
| 0 |
| 0 |
| 395 |
| 0 |
| 105 |
| 8,760 |
| |

| Pollutant | DB NG | NG | NG SSSD | DB FO | FO | FO SUSD | SUM |
|--|-----------|-----|---------|---------|-----|---------|-----------|
| | tpy | tpy | tpy | tpy | tpy | tpy | tpy |
| NO_X | 138.2 | 0.0 | 0.0 | 14.4 | 0.0 | 20.3 | 172.9 |
| CO | 63.1 | 0.0 | 0.0 | 2.2 | 0.0 | 568.5 | 633.8 |
| PM/PM ₁₀ /PM _{2.5} | 150.0 | 0.0 | 0.0 | 10.8 | 0.0 | 2.1 | 162.8 |
| SO ₂ | 26.6 | 0.0 | 0.0 | 1.2 | 0.0 | 0.2 | 28.0 |
| VOC | 64.1 | 0.0 | 0.0 | 2.8 | 0.0 | 64.5 | 131.4 |
| H ₂ SO ₄ | 40.7 | 0.0 | 0.0 | 1.8 | 0.0 | 0.4 | 42.9 |
| Lead | 0.00 | 0.0 | 0.0 | 0.01 | 0.0 | 0.00 | 0.01 |
| CO ₂ | 2,045,693 | 0.0 | 0.0 | 110,524 | 0.0 | 23762.5 | 2,179,979 |
| N ₂ O | 1253.4 | 0.0 | 0.0 | 248.1 | 0.0 | 62.5 | 1,564 |
| CH ₄ | 1051.5 | 0.0 | 0.0 | 109.5 | 0.0 | 26.2 | 1,187 |
| CO ₂ e (sum) | 2,445,483 | 0.0 | 0.0 | 187,200 | 0.0 | 43048.1 | 2,675,731 |

| Scenario 7 | Hours |
|-------------|-------|
| DB NG | 6,735 |
| NG | 0 |
| NG SSSD | 1,525 |
| DB FO | 395 |
| FO | 0 |
| FO SUSD | 105 |
| Total Hours | 8,760 |

| Pollutant | DB NG | NG | NG SSSD | DB FO | FO | FO SUSD | SUM |
|--|-----------|-----|---------|---------|-----|---------|-----------|
| | tpy | tpy | tpy | tpy | tpy | tpy | tpy |
| NO _X | 112.7 | 0.0 | 108.3 | 14.4 | 0.0 | 20.3 | 255.6 |
| CO | 51.4 | 0.0 | 1,369.0 | 2.2 | 0.0 | 568.5 | 1,991.1 |
| PM/PM ₁₀ /PM _{2.5} | 122.3 | 0.0 | 16.6 | 10.8 | 0.0 | 2.1 | 151.7 |
| SO ₂ | 21.7 | 0.0 | 3.9 | 1.2 | 0.0 | 0.2 | 27.0 |
| VOC | 52.3 | 0.0 | 117.8 | 2.8 | 0.0 | 64.5 | 237.3 |
| H ₂ SO ₄ | 33.2 | 0.0 | 6.0 | 1.8 | 0.0 | 0.4 | 41.4 |
| Lead | 0.00 | 0.0 | 0.00 | 0.01 | 0.0 | 0.00 | 0.01 |
| CO ₂ | 1,668,007 | 0.0 | 299,651 | 110,524 | 0.0 | 23,763 | 2,101,945 |
| N ₂ O | 1,022 | 0.0 | 184 | 248 | 0.0 | 63 | 1,516 |
| CH₄ | 857 | 0.0 | 154 | 110 | 0.0 | 26 | 1,147 |
| CO ₂ e (sum) | 1,993,986 | 0.0 | 358,212 | 187,200 | 0.0 | 43,048 | 2,582,446 |



Cold Start

Warm Start

Hot Start

Shutdown

Startup Emissions per Gas Turbine

CO

lb/Start

11,066

6,495

779

463

Client NTEC

NOx

lb/Start

335

233

111 59

Project 1x1 Combined Cycle

40

Combined Cycle Startup Emissions Estimate (Natural Gas) 1x1 8000H Configuration

| VOC | |
|----------|--|
| lb/Start | |
| 950 | |
| 558 | |
| 67 | |

| Max Hourly Startup Emissions per Turbine | | | | | |
|--|-------|-------|-------|--|--|
| | | | | | |
| | CO | NOx | VOC | | |
| | lb/hr | lb/hr | lb/hr | | |
| Cold Start | 7,190 | 200 | 620 | | |
| Warm Start | 6,480 | 210 | 560 | | |
| Hot Start | 1,200 | 170 | 100 | | |
| Shutdown | 3,920 | 210 | 340 | | |

| Startup Times (No Margin) | | | | |
|---------------------------|------------------------------------|-------------------|--|--|
| | Time to Emissions Compliance | Time to Full Load | | |
| | Minutes | | | |
| Cold Start | 105 | 170 | | |
| Warm Start | 70 | 113 | | |
| Hot Start | 29 | 72 | | |
| Shutdown | 25 | 31 | | |

| Startup Times (With Margin) | | | | | | | | | | |
|-----------------------------|------------------------------------|-------------------|--|--|--|--|--|--|--|--|
| | Time to Emissions Compliance | Time to Full Load | | | | | | | | |
| | Minutes | | | | | | | | | |
| Cold Start | 120 | 210 | | | | | | | | |
| Warm Start | 80 | 130 | | | | | | | | |
| Hot Start | 45 | 90 | | | | | | | | |
| Shutdown | 30 | 35 | | | | | | | | |

1) Startup period is defined as the operation period beginning when continuous fuel flow to the gas turbine is initiated and ending when stack emissions compliance is achieved.

Rev: 0 Date: 4/18/2018

- Maximum lb/hr values are based on the maximum lbs of emission over a rolling hour through out the start up period.
- 3) Startup emissions estimates assume there is no removal from the catalysts
- Start Times to emissions compliance start at gas turbine ignition and end when stack emissions compliance is achieved.
- 5) Start Times to full load start at gas turbine start command and end when gas turbine is at full load, steam turbine is valves wide open, and Bypass valves are closed.
- Shutdown Times are from gas turbine minimum emissions compliance load (MECL) or gas turbine Full load to flameout.



Client NTEC

Project 1x1 Combined Cycle

Combined Cycle Startup Emissions Estimate (Fuel Oil)
1x1 8000H Configuration

Rev: 0

Date: 4/18/2018

| Startup Emissions per Gas Turbine | | | | | | | | | |
|-----------------------------------|----------|----------|----------|--|--|--|--|--|--|
| | | | | | | | | | |
| | CO | NOx | VOC | | | | | | |
| | lb/Start | lb/Start | lb/Start | | | | | | |
| Cold Start | 25,846 | 860 | 2,951 | | | | | | |
| Warm Start | 12,364 | 618 | 1,405 | | | | | | |
| Hot Start | 1,854 | 326 | 192 | | | | | | |
| Shutdown | 1,227 | 108 | 122 | | | | | | |

| Max Hourly | Max Hourly Startup Emissions per Turbine | | | | | | | | |
|------------|--|-------|-------|--|--|--|--|--|--|
| | | | | | | | | | |
| | CO | NOx | VOC | | | | | | |
| | lb/hr | lb/hr | lb/hr | | | | | | |
| Cold Start | 16,860 | 510 | 1,930 | | | | | | |
| Warm Start | 12,140 | 530 | 1,390 | | | | | | |
| Hot Start | 2,850 | 500 | 300 | | | | | | |
| Shutdown | 10,440 | 580 | 1,040 | | | | | | |

| Startup Times (No Margin) | | | | | | | | | | |
|---------------------------|------------------------------------|----------------------|--|--|--|--|--|--|--|--|
| | Time to Emissions Compliance | Time to Full Load | | | | | | | | |
| | Minu | tes | | | | | | | | |
| Cold Start | 105 | 170 | | | | | | | | |
| Warm Start | 70 | 113 | | | | | | | | |
| Hot Start | 29 | 72 | | | | | | | | |
| Shutdown | 25 | 31 | | | | | | | | |

| Startup Times (With Margin) | | | | | | | | | |
|-----------------------------|------------------------------------|-------------------|--|--|--|--|--|--|--|
| | Time to Emissions Compliance | Time to Full Load | | | | | | | |
| | Minu | tes | | | | | | | |
| Cold Start | 120 | 210 | | | | | | | |
| Warm Start | 80 | 130 | | | | | | | |
| Hot Start | 45 | 90 | | | | | | | |
| Shutdown | 30 | 35 | | | | | | | |

Notes

- Startup period is defined as the operation period beginning when continuous fuel flow to the gas turbine is initiated and ending when stack emissions compliance is achieved.
- Maximum lb/hr values are based on the maximum lbs of emission over a rolling hour through out the start up period.
- 3) Startup emissions estimates assume there is no removal from the catalysts 4) Start Times to emissions compliance start at gas turbine ignition and end when stack emissions compliance is achieved. 5) Start Times to full load start at gas turbine start command and end when gas turbine is at full load, steam turbine is valves wide open, and Bypass valves are closed.
- closed 6) Shutdown Times are from gas turbine minimum emissions compliance load (MECL) or gas turbine Full load to flameout.

| South Shore Energy, LLC - Nemadji Trail Energ | y Center | | | | | | | | | | | | | | | | | | | | | |
|--|-------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|-----------------------------|----------------------------|----------------------------|----------------------------|---------------------------|--------------------------------|----------------------------|-----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------|
| Combustion Turbine Case # | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 |
| оизо # | | · | | Ů | 7 | · | Ů | | Ů | Ť | | | | | | 10 | | | 10 | | 20 | |
| | | Fired Evap OFF Minimum | Fired Evap OFF Winter Peak | Fired Evap OFF | Fired Evap OFF Annual Average | Fired Evap ON Summer | Fired Evap ON Summer Peak | Fired Evap ON Maximum | Unfired Evap OFF Minimum | Unfired Evap OFF Winter | Unfired Evap OFF Winter | Unfired Evap OFF Annual | Unfired Evap ON Summer | Unfired Evap ON Summer Peak | Unfired Evap ON Maximum | Unfired Evap OFF Minimum | Unfired Evap OFF Winter | Unfired Evap OFF Winter | Unfired Evap OFF Annual | Unfired Evap OFF Summer | Unfired Evap OFF Summer | Unfired Evap |
| | | Ambient 1x100% | Ambient 1x100% | Ambient 1x100% | 6 Ambient 1x100% | Average Ambient | Ambient 1x100% | Ambient 1x100% | Ambient 1x100% | Peak Ambient | Average Ambient | Average Ambient | Average Ambient | Ambient 1x100% | Ambient 1x100% | Ambient 1x75% | Peak Ambient | Average Ambient | Average Ambient | Average Ambient | Peak Ambient | Max Ambient |
| Case Description | | GTG | GTG | GTG | GTG | 1x100% GTG | GTG | GTG | GTG | 1x100% GTG | 1x100% GTG | 1x100% GTG | 1x100% GTG | GTG | GTG | GTG | 1x75% GTG | 1x75% GTG | 1x75% GTG | 1x75% GTG | 1x75% GTG | 1x75% GTG |
| Ambient Temperature | | -34.3 F | 7.9 F | 15.4 F | 39.1 F | 61 F | 76.8 F | 95.5 F | -34.3 F | 7.9 F | 15.4 F | 39.1 F | 61 F | 76.8 F | 95.5 F | -34.3 F | 7.9 F | 15.4 F | 39.1 F | 61 F | 76.8 F | 95.5 F |
| Gas Turbine Load | | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 75% | 75% | 75% | 75% | 75% | 75% | 75% |
| Evaporative Cooling Water Injection | | OFF OFF | OFF OFF | OFF OFF | OFF OFF | COOLING ON OFF | COOLING ON OFF | COOLING ON OFF | OFF OFF | OFF OFF | OFF OFF | OFF OFF | COOLING ON OFF | COOLING ON OFF | COOLING ON OFF | OFF OFF | OFF OFF | OFF OFF | OFF OFF | OFF OFF | OFF OFF | OFF OFF |
| Duct Firing | | FIRING ON | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF |
| Inlet Chiller | | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF |
| No. of Gas Turbines In Operation | | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 1 | 1 | 1 | 1 | 1 | 1 |
| Gas Turbine Fuel Duct Burner Fuel | | Natural Gas 1 Natural Gas 1 | Natural Gas 1 N/A | Natural Gas 1 N/A | Natural Gas 1 N/A | Natural Gas 1 N/A | Natural Gas 1 N/A | Natural Gas 1 N/A | Natural Gas 1 N/A | Natural Gas 1 N/A | Natural Gas 1 N/A | Natural Gas 1 N/A | Natural Gas 1 N/A | Natural Gas 1 N/A | Natural Gas 1 N/A | Natural Gas 1 N/A |
| Duct Bullet 1 del | | radarar Gao r | reduita Guo i | riatara oao i | reacardi Gao i | Hatarar Gao 1 | Hatara Gao I | Tractarar Gab 1 | 1071 | 1071 | 1071 | 7071 | 1471 | 1471 | 7477 | 1471 | | 1071 | 7471 | 7477 | 10/1 | 1071 |
| Ambient Conditions | | | | | | | | | | | | | | | | | | | | | | |
| Temperature | degree F | -34.3 | 7.9 | 15.4 | 39.1 | 61 | 76.8 | 95.5 | -34.3 | 7.9 | 15.4 | 39.1 | 61 | 76.8 | 95.5 | -34.3 | 7.9 | 15.4 | 39.1 | 61 | 76.8 | 95.5 |
| Relative Humidity | % dograd E | 70% | 69% 6.5 | 70% 13.5 | 70% 35.4 | 76% 56.4 | 62% 67.3 | 36% 73.6 | 70% -34.5 | 69% 6.5 | 70% | 70% | 76% 56.4 | 62% 67.3 | 36% 73.6 | 70% -34.5 | 69% 6.5 | 70% | 70% 35.4 | 76% 56.4 | 62% 67.3 | 36% |
| Wet Bulb Temperature Pressure | degree F | -34.5 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 13.5 14.34 | 35.4 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 13.5 14.34 | 14.34 | 14.34 | 14.34 | 73.6 14.34 |
| Gas Turbine Generator Performance | P | | | | | | | | | | | | | | | | | | | | | |
| Electrical Output | kW | 305,185 | 321,687 | 318,848 | 308,281 | 299,825 | 290,408 | 284,119 | 305,185 | 321,687 | 318,848 | 308,281 | 299,825 | 290,408 | 284,119 | 228,890 | 241,193 | 239,136 | 231,211 | 222,417 | 211,956 | 196,065 |
| Heat Rate - LHV | Btu/kWh | 10,583 | 10,270 | 10,241 | 10,220 | 10,216 | 10,285 | 10,307 | 10,583 | 10,270 | 10,241 | 10,220 | 10,216 | 10,285 | 10,307 | 11,029 | 10,606 | 10,607 | 10,633 | 10,694 | 10,802 | 11,051 |
| Heat Rate - HHV GTG Heat Input- LHV | Btu/kWh MMBtu/hr | 11,740 3,230 | 11,393 3,304 | 11,361 3,265 | 11,338 3,151 | 11,333 3,063 | 11,410 2,987 | 11,434 2,928 | 11,740 3,230 | 11,393 3,304 | 11,361 3,265 | 11,338 3,151 | 11,333 3,063 | 11,410 2,987 | 11,434 2,928 | 12,235 2,524 | 11,766 2,558 | 11,767 2,536 | 11,796 2,459 | 11,864 2,379 | 11,984 2,290 | 12,259 2,167 |
| GTG Heat Input- LHV | MMBtu/hr | 3,583 | 3,665 | 3,622 | 3,495 | 3,398 | 3,314 | 3,249 | 3,583 | 3,665 | 3,622 | 3,495 | 3,398 | 3,314 | 3,249 | 2,801 | 2,838 | 2,814 | 2,727 | 2,639 | 2,540 | 2,404 |
| Water / Sprint Injection Rate (per HRSG) | lb/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exhaust Flow (per HRSG) | lb/hr | 6,341,490 | 6,495,270 | 6,440,176 | 6,268,714 | 6,106,456 | 5,964,540 | 5,857,095 | 6,341,490 | 6,495,270 | 6,440,176 | 6,268,714 | 6,106,456 | 5,964,540 | 5,857,096 | 5,046,885 | 5,102,834 | 5,086,122 | 5,000,930 | 4,898,065 | 4,772,174 | 4,543,438 |
| Exhaust Temperature Steam Turbine Generator Performance | degree F | 1,184 | 1,195 | 1,195 | 1,202 | 1,208 | 1,217 | 1,220 | 1,184 | 1,195 | 1,195 | 1,202 | 1,208 | 1,217 | 1,220 | 1,192 | 1,202 | 1,202 | 1,205 | 1,210 | 1,214 | 1,225 |
| Steam Turbine Generator Performance Electrical Output | kW | 254,623 | 255,309 | 255,183 | 255,424 | 254,270 | 252,656 | 247,917 | 158,036 | 164,309 | 162,993 | 160,825 | 157,486 | 154,524 | 151,354 | 127,005 | 130,306 | 129,736 | 128,215 | 125,965 | 121,942 | 115,982 |
| Duct Burner Fuel Consumption | IVAA | 204,020 | 200,000 | 200,100 | 200,424 | 204,210 | 202,000 | 241,511 | 155,050 | 104,005 | 102,000 | 100,020 | 107,400 | 104,024 | 101,004 | 121,003 | 100,000 | 123,730 | 120,210 | 120,500 | 121,042 | 113,302 |
| Heat Input, LHV (per HRSG) | MMBtu/hr | 907.1 | 860.3 | 870.1 | 887.9 | 896.3 | 898.5 | 882.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Heat Input, HHV (per HRSG) | MMBtu/hr | 1006.3 | 954.4 | 965.2 | 985.0 | 994.3 | 996.8 | 978.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Stack Volumetric Analysis, Wet | 0/ | 0.000/ | 0.000/ | 0.000/ | 0.000/ | 0.070/ | 0.000/ | 0.000/ | 0.000/ | 0.000/ | 0.000/ | 0.000/ | 0.000/ | 0.070/ | 0.070/ | 0.000/ | 0.000/ | 0.000/ | 0.000/ | 0.000/ | 0.000/ | 0.070/ |
| Ar CO2 | % % | 0.88% 5.42% | 0.88% 5.33% | 0.88% 5.34% | 0.88% 5.35% | 0.87% 5.36% | 0.86% 5.37% | 0.86% 5.35% | 0.89% 4.29% | 0.89% 4.28% | 0.89% 4.27% | 0.89% 4.23% | 0.88% 4.20% | 0.87% 4.19% | 0.87% 4.17% | 0.89% 4.22% | 0.89% 4.22% | 0.89% 4.20% | 0.89% 4.14% | 0.88% 4.07% | 0.88% 4.02% | 0.87% 3.99% |
| H2O | % | 10.51% | 10.45% | 10.52% | 10.90% | 11.85% | 12.54% | 12.97% | 8.31% | 8.41% | 8.44% | 8.72% | 9.61% | 10.26% | 10.71% | 8.16% | 8.29% | 8.31% | 8.55% | 9.23% | 9.66% | 9.72% |
| CO2 H2O N2 | % | 73.93% | 73.91% | 73.86% | 73.57% | 72.84% | 72.30% | 71.95% | 74.80% | 74.71% | 74.68% | 74.43% | 73.71% | 73.19% | 72.84% | 74.86% | 74.76% | 74.73% | 74.49% | 73.91% | 73.54% | 73.47% |
| 02 | % | 9.22% | 9.39% | 9.36% | 9.27% | 9.05% | 8.88% | 8.82% | 11.68% | 11.67% | 11.69% | 11.70% | 11.56% | 11.45% | 11.39% | 11.84% | 11.80% | 11.84% | 11.90% | 11.87% | 11.87% | 11.91% |
| Stack Emissions at Exit | | | - | - | | - | | | | - | - | | | | | | | | | | | - |
| NOx Emissions | nnmud | 22.4 | 22.5 | 22.4 | 22.4 | 22.2 | 22.2 | 22.2 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 3E 0 | 25.0 | 25.0 |
| NOx,@15% O2 Into SCR NOx, as NO2 Into SCR (per HRSG) | ppmvd lb/hr | 33.4 554.9 | 33.5 560.1 | 33.4 555.8 | 33.4 541.6 | 33.3 530.2 | 33.3 519.8 | 33.3 509.7 | 35.0 454.2 | 35.0 464.6 | 35.0 459.2 | 35.0 443.1 | 35.0 430.8 | 35.0 420.1 | 35.0 411.9 | 35.0 355.0 | 359.8 | 356.7 | 345.8 | 35.0 334.5 | 35.0 322.0 | 35.0 304.7 |
| NOx,@15% O2 Out of SCR | ppmvd | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| NOx, as NO2 Out of SCR (per HRSG) | lb/hr | 33.2 | 33.5 | 33.2 | 32.5 | 31.8 | 31.2 | 30.6 | 26.0 | 26.5 | 26.2 | 25.3 | 24.6 | 24.0 | 23.5 | 20.3 | 20.6 | 20.4 | 19.8 | 19.1 | 18.4 | 17.4 |
| SCR NOx Removal Efficiency | % | 94.0% | 94.0% | 94.0% | 94.0% | 94.0% | 94.0% | 94.0% | 94.3% | 94.3% | 94.3% | 94.3% | 94.3% | 94.3% | 94.3% | 94.3% | 94.3% | 94.3% | 94.3% | 94.3% | 94.3% | 94.3% |
| NH3 Emissions | lb/hr | 251.0 | 252.4 | 251.5 | 245.0 | 220.0 | 225.4 | 220.6 | 206.1 | 210.0 | 2004 | 201.1 | 40E E | 100.6 | 100.0 | 161.1 | 162.2 | 161.0 | 156.0 | 1E1 0 | 146.1 | 120.2 |
| NH3 Reacted with NOx (per HRSG) NH3 slip @ 15% O2 | ppmvd | 251.0 10 | 253.4 10 | 251.5 10 | 10 | 239.8 10 | 235.1 10 | 230.6 10 | 206.1 10 | 210.8 10 | 208.4 10 | 201.1 10 | 195.5 10 | 190.6 10 | 186.9 10 | 161.1 10 | 163.2 10 | 101.9 | 156.9 10 | 151.8 10 | 140.1 | 138.3 10 |
| NH3 slip (per HRSG) | lb/hr | 61.5 | 61.9 | 61.5 | 60.1 | 58.9 | 57.8 | 56.7 | 48.0 | 49.1 | 48.6 | 46.9 | 45.6 | 44.4 | 43.6 | 37.6 | 38.1 | 37.7 | 36.6 | 35.4 | 34.1 | 32.2 |
| CO Emissions | | | | | | | | | | | | | | | | | | | | | | |
| CO into catalyst | ppmvd | 19.8 | 18.8 | 19.0 | 19.7 | 20.3 | 20.8 | 20.9 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 13.5 | 13.6 | 13.5 | 13.3 | 13.2 | 13.1 | 13.0 |
| CO into catalyst, @ 15% O2 CO into catalyst (per HRSG) | ppmvd lb/hr | 11.1 112.1 | 10.7 108.7 | 10.8 109.2 | 11.1 109.6 | 11.3 109.5 | 11.5 109.0 | 11.5 107.0 | 4.0 31.6 | 4.0 32.3 | 4.0 32.0 | 4.0 30.8 | 4.0 30.0 | 4.0 29.2 | 4.0 28.7 | 10.0 61.8 | 10.0 62.6 | 10.0 62.1 | 10.0 60.2 | 10.0 58.2 | 10.0 56.0 | 10.0 53.0 |
| CO out of catalyst | ppmvd | 2.69 | 2.64 | 2.64 | 2.66 | 2.69 | 2.72 | 2.73 | 2.07 | 2.07 | 2.06 | 2.05 | 2.06 | 2.06 | 2.07 | 2.03 | 2.04 | 2.03 | 2.00 | 1.99 | 1.97 | 1.96 |
| CO out of catalyst, @ 15% O2 | ppmvd | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 |
| CO out of catalyst (per HRSG) | lb/hr | 15.2 | 15.3 | 15.2 | 14.8 | 14.5 | 14.3 | 14.0 | 11.9 | 12.1 | 12.0 | 11.6 | 11.2 | 11.0 | 10.7 | 9.3 | 9.4 | 9.3 | 9.0 | 8.7 | 8.4 | 8.0 |
| CO Catalyst Removal Efficiency SO2 Emissions | % | 86.5% | 85.9% | 86.1% | 86.5% | 86.7% | 86.9% | 86.9% | 62.5% | 62.5% | 62.5% | 62.5% | 62.5% | 62.5% | 62.5% | 85.0% | 85.0% | 85.0% | 85.0% | 85.0% | 85.0% | 85.0% |
| SO2 Emissions SO2 in Exh. Gas @ 15% O2 (assuming no conversion) | ppmvw | 0.247 | 0.248 | 0.247 | 0.246 | 0.244 | 0.242 | 0.241 | 0.253 | 0.253 | 0.253 | 0.252 | 0.250 | 0.248 | 0.247 | 0.254 | 0.253 | 0.253 | 0.253 | 0.251 | 0.250 | 0.249 |
| SO2 in Exh. Gas @ 15% O2 (assuming no conversion) | ppmvd | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 |
| SO2 in Exhaust Gas (assuming no conversion) (per HRSG) | lb/hr | 6.4 | 6.4 | 6.4 | 6.2 | 6.1 | 6.0 | 5.9 | 5.0 | 5.1 | 5.0 | 4.9 | 4.7 | 4.6 | 4.5 | 3.9 | 4.0 | 3.9 | 3.8 | 3.7 | 3.5 | 3.4 |
| SO2 in Exhaust Gas (assuming no conversion) (per HRSG) | lb/MMBtu | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 | 0.00139 |
| Volatile Organic Compounds | nnessed | 2.7 | 2.7 | 2.7 | 9.7 | 2.7 | 27 | 2.7 | 0.6 | 0.6 | 0.0 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| VOC @ 15% O2 VOC as CH4 (per HRSG) | ppmvd lb/hr | 2.7 15.4 | 2.7 15.5 | 2.7 15.4 | 15.0 | 2.7 14.8 | 2.7 14.5 | 2.7 14.2 | 0.6 2.7 | 2.8 | 2.7 | 2.6 | 0.6 2.6 | 2.5 | 0.6 2.5 | 0.6 2.1 | 2.2 | 0.6 2.1 | 2.1 | 2.0 | 1.9 | 0.6 1.8 |
| VOC % Removal in Catalyst | % | 37% | 35% | 35% | 38% | 39% | 40% | 40% | 40% | 40% | 40% | 40% | 40% | 40% | 40% | 40% | 40% | 40% | 40% | 40% | 40% | 40% |
| Particulates | | | | | | | | | | | | | | | | | | | | | | |
| PM10, front including (NH4)2SO4 (per HRSG) | lb/hr | 28.8 | 28.5 | 28.4 | 28.2 | 27.8 | 27.5 | 26.9 | 15.8 | 16.2 | 16.0 | 15.5 | 15.0 | 14.6 | 14.3 | 12.4 | 12.5 | 12.4 | 12.2 | 11.9 | 11.6 | 11.2 |
| PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) | lb/hr lb/MMBtu | 36.3 0.00791 | 36.0 0.00780 | 36.0 0.00784 | 35.6 0.00794 | 35.1 0.00799 | 34.6 0.00803 | 33.9 0.00803 | 21.3 0.00595 | 21.8 0.00595 | 21.6 0.00596 | 20.9 0.00598 | 20.3 0.00597 | 19.7 0.00596 | 19.3 0.00595 | 16.7 0.00596 | 16.8 0.00592 | 16.7 0.00595 | 16.5 0.00605 | 16.2 0.00615 | 16.0 0.00628 | 15.6 0.00647 |
| PM10, front & back including (NH4)2SO4 (per HRSG) H2SO4 Emissions | iD/iviMBtu | 0.00791 | 0.00780 | 0.00784 | 0.00794 | 0.00799 | 0.00803 | 0.00803 | 0.00595 | 0.00595 | 0.00596 | 0.00598 | 0.00597 | 0.00596 | 0.00595 | 0.00596 | 0.00592 | 0.00595 | 0.00605 | 0.00615 | 0.00628 | 0.00647 |
| H2SO4 EMISSIONS H2SO4 in Exhaust Gas (per HRSG) | lb/hr | 9.79 | 9.86 | 9.79 | 9.56 | 9.37 | 9.20 | 9.02 | 7.65 | 7.82 | 7.73 | 7.46 | 7.25 | 7.07 | 6.93 | 5.98 | 6.06 | 6.01 | 5.82 | 5.63 | 5.42 | 5.13 |
| H2SO4 in Exhaust Gas | lb/MMBtu | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 | 0.00213 |
| GHG Emissions | | | | | | | | | | | | | | | | | | | | | | |
| CO2 in Exhaust Gas (per HRSG) | lb/MMBtu | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 | 116.98 |
| CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) | lb/hr lb/MWh (gross) | 492,096 879.0 | 495,325 858.5 | 491,927 857.0 | 480,427 852.3 | 470,968 850.0 | 462,194 851.1 | 453,310 852.0 | 384,196 829.4 | 392,985 808.6 | 388,425 806.1 | 374,804 799.0 | 364,352 796.7 | 355,313 798.6 | 348,348 799.9 | 300,304 843.8 | 304,291 819.1 | 301,730 818.0 | 292,457 813.7 | 282,953 812.2 | 272,368 815.7 | 257,741 826.0 |
| CO2 in Exhaust Gas (per HRSG) CH4 in Exhaust Gas (per HRSG) | lb/MMBtu | 5.5116E-02 | 5.5116E-02 | 5.5116E-02 | 5.5116E-02 | 799.0 5.5116E-02 | 5.5116E-02 | 5.5116E-02 | 5.5116E-02 | 5.5116E-02 | 5.5116E-02 | 5.5116E-02 | 5.5116E-02 | 5.5116E-02 | 5.5116E-02 | 5.5116E-02 |
| CH4 in Exhaust Gas (per HRSG) | lb/hr | 252.9 | 254.6 | 252.8 | 246.9 | 242.1 | 237.6 | 233.0 | 197.5 | 202.0 | 199.6 | 192.6 | 187.3 | 182.6 | 179.1 | 154.4 | 156.4 | 155.1 | 150.3 | 145.4 | 140.0 | 132.5 |
| N2O in Exhaust Gas (per HRSG) | lb/MMBtu | 6.5698E-02 | 6.5698E-02 | 6.5698E-02 | 6.5698E-02 | 6.5698E-02 | 6.5698E-02 | 6.5698E-02 | 6.5698E-02 | 6.5698E-02 | 6.5698E-02 | 6.5698E-02 | 6.5698E-02 | 6.5698E-02 | 6.5698E-02 | 6.5698E-02 |
| N2O in Exhaust Gas (per HRSG) | lb/hr | 301.5 | 303.5 | 301.4 | 294.4 | 288.6 | 283.2 | 277.7 | 235.4 | 240.8 | 238.0 | 229.6 | 223.2 | 217.7 | 213.4 | 184.0 | 186.4 | 184.9 | 179.2 | 173.4 | 166.9 | 157.9 |
| GHG in Exhaust Gas (per HRSG) Stack Exit | lb/hr | 492,650.7 | 495,883.1 | 492,480.8 | 480,967.9 | 471,498.8 | 462,715.1 | 453,820.2 | 384,629.3 | 393,428.3 | 388,862.6 | 375,226.2 | 364,762.5 | 355,713.3 | 348,740.7 | 300,642.0 | 304,634.1 | 302,070.4 | 292,786.6 | 283,271.5 | 272,674.5 | 258,031.2 |
| AND THE PARTY OF T | | 164 | 164 | 164 | 165 | 165 | 165 | 165 | 167 | 168 | 167 | 167 | 169 | 170 | 171 | 165 | 165 | 165 | 165 | 165 | 165 | 165 |
| Temperature | degree F | | | | | 6.149.863 | 6.008.056 | 5.899.829 | 6.341.490 | 6,495,270 | 6.440.176 | 6,268,714 | 6.106.456 | 5.964.540 | 5.857.096 | 5,046,885 | 5,102,834 | 5,086,122 | 5,000,930 | 4.898.065 | 4,772,174 | 4,543,438 |
| Flow Rate (per HRSG) | degree F lb/hr | 6,385,420 | 6,536,937 | 6,482,315 | 6,311,717 | | | | | | | | | | | | | | | | | |
| Flow Rate (per HRSG) Flow Rate (per HRSG) | lb/hr scfm | 1,187,865 | 1,216,129 | 1,206,283 | 1,176,216 | 1,150,232 | 1,126,707 | 1,108,344 | 1,174,082 | 1,203,057 | 1,193,062 | 1,162,725 | 1,136,614 | 1,113,056 | 1,094,939 | 934,102 | 944,911 | 941,950 | 927,225 | 910,735 | 888,969 | 846,630 |
| Temperature Flow Rate (per HRSG) Flow Rate (per HRSG) Flow Rate (per HRSG) | lb/hr scfm acfm | 1,187,865 1,460,169 | 1,216,129 1,496,266 | 1,206,283 1,484,101 | 1,176,216 1,449,619 | 1,150,232 1,416,832 | 1,126,707 1,388,416 | 1,108,344 1,365,742 | 1,174,082 1,451,496 | 1,203,057 1,488,999 | 1,193,062 1,475,747 | 1,162,725 1,437,799 | 1,136,614 1,409,239 | 1,113,056 1,382,539 | 1,094,939 1,361,747 | 934,102 1,151,028 | 944,911 1,164,375 | 941,950 1,160,709 | 927,225 1,142,353 | 910,735 1,122,002 | 888,969 1,095,221 | 846,630 1,043,011 |
| Flow Rate (per HRSG) Flow Rate (per HRSG) | lb/hr scfm | 1,187,865 | 1,216,129 | 1,206,283 | 1,176,216 | 1,150,232 | 1,126,707 | 1,108,344 | 1,174,082 | 1,203,057 | 1,193,062 | 1,162,725 | 1,136,614 | 1,113,056 | 1,094,939 | 934,102 | 944,911 | 941,950 | 927,225 | 910,735 | 888,969 | 846,630 |

Notes:

1. Particulate values exclude catalyst and other entrained particles.

2. Emission values do not include heavy metals (lead, mercury, etc.).

3. Differing fuel composition may change the calculated emissions.

4. CTG performance based on performance runs provided by SEI.

5. Fuel based on natural gas analysis provided by NTEC.

6. 35 pm N0x control on 8000H gas turbine.

8. Stack SO2 content reported with no conversion to SO3.

9. Particulate emissions assume 100% conversion of SO2-SO3, and 100% coversion of SO3 to (NH4)2SO4.

10. H2SO4 assumes 100% conversion of SO2-SO3, and 100% conversion of SO3 to H2SO4.

11. Greenhouse Gas (GHG) emissions are based on EPA 40 CFR Part 98 emissions factors for natural gas.

12. 20% margin in Fuel flow and 20% margin in exhaust flow are included.

13. Emissions reported on the basis of pounds per hour are for one combustion turbine and one HRSG.

14. Emissions estimates are for information only and are NOT guaranteed.

| South Shore Energy, LLC - Nemadji Trail Energy C Combustion Turbine | Center | | | | | | | | | | | | | | | | | | | | | |
|--|---|---|---|--|--|--|---|--|--|---|--|--|---|---|---|---|---|--|---|---|---|---|
| Case # | _ | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 |
| | | Hefinad 5 | 11-6 15 | 11-6 | Unford 5 | Hefer 15 | Hefer d F | Hafar 15 | Fired NG CTG Fuel Oil Evap | Fired NG CTG | Fired NG CTG | Fired NG CTG | Fired NG CTG | Find NO OTO | Fired NG CTG | Unford F. 10" | Unford F. 100 | U-6 4 F 1 A- | Hafard 5 16" | Unfired Fuel Oil | Unfined 5 10" | Unfired Fuel O |
| | | Unfired Evap OFF Minimum | Unfired Evap OFF Winter | Unfired Evap OFF Winter | Unfired Evap OFF Annual | Unfired Evap OFF Summer | Unfired Evap OFF Summer | Unfired Evap OFF Maximum | OFF Min | Fuel Oil Evap OFF Winter | Fuel Oil Evap OFF Winter | Fuel Oil Evap OFF Annual | Fuel Oil Evap ON Summer | Fired NG CTG Fuel Oil Evap ON | Fuel Oil Evap ON Maximum | Unfired Fuel Oil Evap OFF Min | Unfired Fuel Oil Evap OFF | Unfired Fuel Oil Evap OFF | Unfired Fuel Oil Evap OFF | Evap ON Summer | Unfired Fuel Oil Evap ON | Evap ON Maximum |
| | | Ambient | Peak Ambient | Average Ambient | Average Ambient | Average Ambient | Peak Ambient | Ambient | Ambient 1x100% | Peak 1x100% | Average 1x100% | Average 1x100% | Average 1x100% | Summer Peak | | Ambient 1x100% | Winter Peak | Winter Average | Annual Average | Average 1x100% | Summer Peak | Ambient 1x100 |
| Case Description | | 1xMECL GTG | 1xMECL GTG | 1xMECL GTG | 1xMECL GTG | 1xMECL GTG | 1xMECL GTG | 1xMECL GTG | CTG | CTG | CTG | CTG | CTG | 1x100% CTG | CTG | CTG | 1x100% CTG | 1x100% CTG | 1x100% CTG | CTG | 1x100% CTG | CTG |
| Ambient Temperature | | -34.3 F | 7.9 F | 15.4 F | 39.1 F | 61 F | 76.8 F | 95.5 F | -34.3 F | 7.9 F | 15.4 F | 39.1 F | 61 F | 76.8 F | 95.5 F | -34.3 F | 7.9 F | 15.4 F | 39.1 F | 61 F | 76.8 F | 95.5 F |
| Gas Turbine Load | | 34% OFF | 33% OFF | 33% OFF | 34% OFF | 35% OFF | 36% OFF | 37% OFF | 100% OFF | 100% OFF | 100% OFF | 100% OFF | 100% COOLING ON | 100% COOLING ON | 100% COOLING ON | 100% OFF | 100% OFF | 100% OFF | 100% OFF | 100% COOLING ON | 100% COOLING ON | 100% COOLING ON |
| Evaporative Cooling Water Injection | | OFF | OFF | OFF | OFF | OFF | OFF | OFF | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION O |
| Duct Firing | | OFF | OFF | OFF | OFF | OFF | OFF | OFF | FIRING ON | FIRING ON | FIRING ON | FIRING ON | FIRING ON | FIRING ON | FIRING ON | OFF | OFF | OFF | OFF | OFF | OFF | OFF |
| Inlet Chiller | | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF |
| No. of Gas Turbines In Operation Gas Turbine Fuel | | 1 Natural Gas 1 | 1 Natural Gas 1 | 1 Natural Gas 1 | 1 Natural Gas 1 | 1 Natural Gas 1 | 1 Natural Gas 1 | 1 Natural Gas 1 | 1 Fuel Oil | 1 Fuel Oil | 1 Fuel Oil | 1 Fuel Oil | 1 Fuel Oil | 1 Fuel Oil | 1 Fuel Oil | 1 Fuel Oil | 1 Fuel Oil | 1 Fuel Oil | 1 Fuel Oil | 1 Fuel Oil | 1 Fuel Oil | 1 Fuel Oil |
| Duct Burner Fuel | | N/A | N/A | N/A | N/A | N/A | N/A | N/A | | Natural Gas 1 | | | | Natural Gas 1 | Natural Gas 1 | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| | | | | | | | | | | | | | • | • | | | <u> </u> | <u> </u> | | | | |
| Ambient Conditions | | | | | | | | | | | | | | | | | | | | | | |
| Temperature | degree F | -34.3 | 7.9 | 15.4 | 39.1 | 61 | 76.8 | 95.5 | -34.3 | 7.9 | 15.4 | 39.1 | 61 | 76.8 | 95.5 | -34.3 | 7.9 | 15.4 | 39.1 | 61 | 76.8 | 95.5 |
| Relative Humidity Wet Bulb Temperature | degree F | 70% -34.5 | 69% 6.5 | 70% 13.5 | 70% 35.4 | 76% 56.4 | 62% 67.3 | 36% 73.6 | 70% -34.5 | 69% 6.5 | 70% 13.5 | 70% 35.4 | 76% 56.4 | 62% 67.3 | 36% 73.6 | 70% -34.5 | 69% 6.5 | 70% 13.5 | 70% 35.4 | 76% 56.4 | 62% 67.3 | 36% 73.6 |
| Pressure | psia | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 |
| Gas Turbine Generator Performance | | | | | | | | | | | | • | • | • | | • | • | • | | | | |
| Electrical Output | kW | 104,700 | 104,700 | 104,732 | 104,700 | 104,700 | 104,700 | 104,700 | 238,275 | 258,677 | 258,311 | 258,880 | 260,519 | 261,332 | 255,498 | 238,275 | 258,677 | 258,311 | 258,880 | 260,519 | 261,332 | 255,498 |
| Heat Rate - LHV | Btu/kWh | 14,789 | 14,356 15,926 | 14,302 | 14,148 | 14,030 15,565 | 13,946 15,472 | 13,898 15,418 | 11,341 | 10,807 11,606 | 10,776 | 10,733 11,526 | 10,732 11,525 | 10,764 11,560 | 10,826 11,627 | 11,341 | 10,807 | 10,776 11,573 | 10,733 11,526 | 10,732 | 10,764 | 10,826 11,627 |
| Heat Rate - HHV GTG Heat Input- LHV | Btu/kWh MMBtu/hr | 16,406 1,548 | 15,926 1,503 | 15,866 1,498 | 15,695 1,481 | 15,565 1,469 | 15,472 1,460 | 15,418 1,455 | 12,180 2,702 | 11,606 2,796 | 11,573 2,784 | 11,526 2,779 | 11,525 2,796 | 11,560 2,813 | 11,627 2,766 | 12,180 2,702 | 11,606 2,796 | 11,573 2,784 | 11,526 2,779 | 11,525 2,796 | 11,560 2,813 | 11,627 2,766 |
| GTG Heat Input- LHV | MMBtu/hr | 1,718 | 1,667 | 1,662 | 1,643 | 1,630 | 1,620 | 1,614 | 2,902 | 3,002 | 2,764 | 2,779 | 3,002 | 3,021 | 2,700 | 2,702 | 3,002 | 2,784 | 2,779 | 3,002 | 3,021 | 2,700 |
| Water / Sprint Injection Rate (per HRSG) | lb/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 46,871 | 54,548 | 55,823 | 69,275 | 78,798 | 85,376 | 86,959 | 46,871 | 54,548 | 55,823 | 69,275 | 78,798 | 85,376 | 86,959 |
| Exhaust Flow (per HRSG) | lb/hr | 3,526,941 | 3,452,470 | 3,452,088 | 3,454,351 | 3,454,625 | 3,456,818 | 3,444,104 | 6,374,610 | 6,542,912 | 6,490,652 | 6,339,790 | 6,194,311 | 6,064,364 | 5,960,302 | 6,374,610 | 6,542,912 | 6,490,652 | 6,339,790 | 6,194,311 | 6,064,364 | 5,960,302 |
| Exhaust Temperature Steam Turbine Generator Performance | degree F | 1,202 | 1,210 | 1,210 | 1,210 | 1,210 | 1,210 | 1,210 | 1,001 | 1,012 | 1,020 | 1,046 | 1,076 | 1,104 | 1,109 | 1,001 | 1,012 | 1,020 | 1,046 | 1,076 | 1,104 | 1,109 |
| Electrical Output | kW | 86,643 | 84,982 | 85,488 | 85,946 | 86,527 | 85,303 | 83,931 | 211,873 | 212,141 | 214,219 | 219,919 | 227,467 | 230,308 | 225,980 | 115,287 | 121,141 | 122,029 | 125,319 | 130,683 | 132,177 | 129,417 |
| Duct Burner Fuel Consumption | LAA | 00,043 | 04,302 | 05,400 | 05,340 | 00,321 | 05,303 | 05,831 | 211,013 | 212,141 | 214,218 | 215,818 | 221,401 | 230,300 | 223,900 | 115,201 | 121,141 | 122,029 | 120,019 | 130,003 | 102,177 | 129,417 |
| Heat Input, LHV (per HRSG) | MMBtu/hr | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 907.2 | 860.3 | 870.1 | 887.9 | 896.3 | 898.5 | 882.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Heat Input, HHV (per HRSG) | MMBtu/hr | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1006.4 | 954.4 | 965.2 | 985.0 | 994.3 | 996.8 | 978.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Stack Volumetric Analysis, Wet | 0/ | 0.000/ | 0.000/ | 0.000/ | 0.000/ | 0.000/ | 0.000/ | 0.000/ | 0.070/ | 0.070/ | 0.000/ | 0.000/ | 0.050/ | 0.0404 | 0.000/ | 0.000/ | 0.000/ | 0.070/ | 0.070/ | 0.000/ | 0.050/ | 0.040/ |
| Ar CO3 | % | 0.90% | 0.89% | 0.89% 3.67% | 0.89% | 0.88% | 0.88% | 0.88% | 0.87% | 0.87% | 0.86% | 0.86% | 0.85% | 0.84% | 0.83% | 0.88% | 0.88% | 0.87% | 0.87% | 0.86% | 0.85% | 0.84% |
| CO2 H2O | % | 3.71% 7.18% | 3.68% 7.24% | 3.67% 7.27% | 3.62% 7.55% | 3.58% 8.27% | 3.55% 8.76% | 3.55% 8.87% | 5.77% 8.00% | 5.72% 8.13% | 5.75% 8.28% | 5.88% 9.16% | 6.03% 10.49% | 6.17% 11.50% | 6.15% 12.01% | 4.66% 5.79% | 4.69% 6.09% | 4.71% 6.21% | 4.79% 7.01% | 4.91% 8.30% | 5.03% 9.28% | 5.02% 9.80% |
| N2 | % | 75.25% | 7.24% | 7.27% 75.14% | 7.55% 74.89% | 74.29% | 73.89% | 73.81% | 72.90% | 72.74% | 72.63% | 71.98% | 70.97% | 70.20% | 69.80% | 73.75% | 73.52% | 73.43% | 72.80% | 71.80% | 71.04% | 70.63% |
| 02 | % | 12.94% | 12.98% | 13.00% | 13.02% | 12.94% | 12.89% | 12.87% | 12.42% | 12.51% | 12.43% | 12.08% | 11.62% | 11.25% | 11.16% | 14.89% | 14.79% | 14.75% | 14.49% | 14.10% | 13.77% | 13.67% |
| Stack Emissions at Exit | | | | | | | | | | | | | | | | | | | | | | |
| NOx Emissions | | 05.5 | 05.5 | | 05.5 | 05.5 | | 05.5 | | | 00. | | | | 00 - | | | | 40.5 | 40.5 | 40.5 | , |
| NOx,@15% O2 Into SCR | ppmvd | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 | 35.0 | 37.9 | 38.1 | 38.1 | 38.0 | 38.0 | 38.0 | 38.0 | 42.0 | 42.0 | 42.0 | 42.0 | 42.0 | 42.0 | 42.0 |
| NOx, as NO2 Into SCR (per HRSG) NOx,@15% O2 Out of SCR | lb/hr ppmvd | 217.8 2.0 | 211.4 2.0 | 210.7 2.0 | 208.3 2.0 | 206.6 2.0 | 205.4 2.0 | 204.7 2.0 | 448.1 6.0 | 454.8 6.0 | 454.3 6.0 | 455.4 6.0 | 458.3 6.0 | 460.6 6.0 | 452.7 6.0 | 347.4 6.0 | 359.3 6.0 | 357.8 6.0 | 356.9 6.0 | 358.9 6.0 | 360.9 6.0 | 354.9 6.0 |
| NOx, as NO2 Out of SCR (per HRSG) | lb/hr | 12.4 | 12.1 | 12.0 | 11.9 | 11.8 | 11.7 | 11.7 | 71.0 | 71.6 | 71.6 | 71.9 | 72.4 | 72.7 | 71.4 | 49.6 | 51.3 | 51.1 | 51.0 | 51.3 | 51.6 | 50.7 |
| SCR NOx Removal Efficiency | % | 94.3% | 94.3% | 94.3% | 94.3% | 94.3% | 94.3% | 94.3% | 84.2% | 84.3% | 84.2% | 84.2% | 84.2% | 84.2% | 84.2% | 85.7% | 85.7% | 85.7% | 85.7% | 85.7% | 85.7% | 85.7% |
| NH3 Emissions | | | | | | | | | | | | | | | | | | | | | | |
| NH3 Reacted with NOx (per HRSG) | lb/hr | 98.8 | 95.9 | 95.6 | 94.5 | 93.7 | 93.2 | 92.9 | 181.5 | 184.4 | 184.2 | 184.6 | 185.7 | 186.7 | 183.5 | 143.3 | 148.2 | 147.6 | 147.2 | 148.0 | 148.9 | 146.4 |
| NH3 slip @ 15% O2 NH3 slip (per HRSG) | ppmvd lb/br | 10 23.0 | 10 22.4 | 10 22.3 | 10 22.0 | 10 21.9 | 10 21.7 | 10 21.6 | 10 43.8 | 10 44.2 | 10 44.2 | 10 44.4 | 10 44.6 | 10 44.8 | 10 44 1 | 10 30.6 | 10 31 7 | 10 31.5 | 10 31.5 | 10 31.6 | 10 31.8 | 10 31.3 |
| CO Emissions | 10/11/ | 20.0 | 22.4 | 22.0 | 22.0 | 21.5 | 21.1 | 21.0 | 40.0 | 71.4 | 77.2 | 77.77 | 77.0 | 77.0 | 77.1 | 50.0 | 51.7 | 01.0 | 01.0 | 01.0 | 01.0 | 01.0 |
| CO into catalyst | ppmvd | 11.8 | 11.7 | 11.7 | 11.5 | 11.5 | 11.5 | 11.5 | 22.7 | 21.8 | 22.1 | 23.0 | 24.0 | 24.8 | 24.9 | 8.6 | 8.7 | 8.8 | 9.0 | 9.4 | 9.7 | 9.7 |
| CO into catalyst, @ 15% O2 | ppmvd | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 18.2 | 17.7 | 17.8 | 17.9 | 17.9 | 17.9 | 17.9 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| CO into catalyst (per HRSG) | lb/hr | 37.9 | 36.8 | 36.6 | 36.2 | 35.9 | 35.7 | 35.6 | 130.9 | 128.4 | 129.1 | 130.5 | 131.6 | 132.1 | 129.8 | 50.4 | 52.1 | 51.9 | 51.7 | 52.0 | 52.3 | 51.4 |
| CO out of catalyst CO out of catalyst, @ 15% O2 | ppmvd ppmvd | 1.77 1.50 | 1.75 1.50 | 1.75 1.50 | 1.73 1.50 | 1.72 1.50 | 1.72 1.50 | 1.72 1.50 | 1.88 1.50 | 1.85 1.50 | 1.87 1.50 | 1.93 1.50 | 2.01 1.50 | 2.08 1.50 | 2.08 1.50 | 1.30 1.50 | 1.31 1.50 | 1.32 1.50 | 1.35 1.50 | 1.41 1.50 | 1.45 1.50 | 1.46 1.50 |
| CO out of catalyst (per HRSG) | lb/hr | 5.7 | 5.5 | 5.5 | 5.4 | 5.4 | 5.4 | 5.3 | 10.8 | 10.9 | 10.9 | 10.9 | 11.0 | 11.1 | 10.9 | 7.6 | 7.8 | 7.8 | 7.8 | 7.8 | 7.8 | 7.7 |
| CO Catalyst Removal Efficiency | % | 85.0% | 85.0% | 85.0% | 85.0% | 85.0% | 85.0% | 85.0% | 91.7% | 91.5% | 91.6% | 91.6% | 91.6% | 91.6% | 91.6% | 85.0% | 85.0% | 85.0% | 85.0% | 85.0% | 85.0% | 85.0% |
| SO2 Emissions | | | | | | | | | | | | | | | | | | | | | | |
| SO2 in Exh. Gas @ 15% O2 (assuming no conversion) | ppmvw | 0.257 | 0.256 | 0.256 | 0.255 | 0.253 | 0.252 | 0.252 | 0.329 | 0.330 | 0.329 | 0.326 | 0.322 | 0.318 | 0.316 | 0.360 | 0.359 | 0.358 | 0.356 | 0.351 | 0.347 | 0.345 |
| SO2 in Exh. Gas @ 15% O2 (assuming no conversion) | ppmvd | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.276 | 0.358 | 0.360 | 0.359 | 0.359 | 0.359 | 0.360 | 0.360 | 0.382 | 0.382 | 0.382 | 0.382 | 0.383 | 0.383 | 0.383 |
| SO2 in Exhaust Gas (assuming no conversion) (per HRSG) SO2 in Exhaust Gas (assuming no conversion) (per HRSG) | lb/hr lb/MMBtu | 2.4 0.00139 | 2.3 0.00139 | 2.3 0.00139 | 2.3 0.00139 | 2.3 0.00139 | 2.3 0.00139 | 2.3 0.00139 | 5.9 0.00151 | 6.0 0.00151 | 6.0 0.00151 | 6.0 0.00151 | 6.0 0.00151 | 6.1 0.00151 | 6.0 0.00151 | 4.4 0.00152 | 4.6 0.00152 | 4.5 0.00152 | 4.5 0.00152 | 4.6 0.00152 | 4.6 0.00152 | 4.5 0.00152 |
| Volatile Organic Compounds | .D/WWW.DIU | 0.00103 | 0.00100 | 0.00103 | 0.00105 | 0.00105 | 0.00105 | 0.00100 | 0.00101 | 0.00101 | 0.00101 | 0.00101 | 0.00101 | 0.00101 | 0.00101 | 0.00102 | 0.00102 | 0.00102 | 0.00102 | 0.00102 | 0.00102 | 0.00102 |
| VOC @ 15% O2 | ppmvd | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| | | 1.3 | 1.3 | 1.3 | 1.2 | 1.2 | 1.2 | 1.2 | 13.8 | 13.9 | 13.9 | 13.9 | 14.0 | 14.1 | 13.9 | 1.7 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 | 1.8 |
| VOC as CH4 (per HRSG) | lb/hr | | 40% | 40% | 40% | 40% | 40% | 40% | 40% | 37% | 38% | 38% | 39% | 39% | 38% | 40% | 40% | 40% | 40% | 40% | 40% | 40% |
| VOC % Removal in Catalyst | lb/hr % | 40% | | | | 0.7 | 0.7 | 0.0 | 37.0 | 36.0 | 27.0 | 27.2 | 27.4 | 27.5 | 27.4 | 24.4 | 24.4 | 24.4 | 24.3 | 24.4 | 24.4 | 24.0 |
| VOC % Removal in Catalyst Particulates | % | 40% | | 0.0 | 0.7 | | | 8.6 | 37.2 | 36.9 | 37.0 | 37.2 | 37.4 | 37.5 | 37.1 | 24.1 | 24.4 | 24.4 | | 24.4 | 24.4 | |
| VOC % Removal in Catalyst Particulates PM10, front including (NH4)2SO4 (per HRSG) | % lb/hr | 8.9 | 8.8 | 8.8 12.8 | 8.7 12.7 | 8.7 12.7 | 12.7 | 12.6 | 5/1.2 | 53.0 | 53.0 | 54.2 | 54.4 | 54.5 | 54.1 | 30.1 | 00.4 | 30.4 | 00.0 | 30.4 | | 24.3 |
| VOC % Removal in Catalyst | % | 40% | | 8.8 12.8 0.00769 | 8.7 12.7 0.00774 | 8.7 12.7 0.00778 | 12.7 0.00781 | 12.6 0.00783 | 54.3 0.01389 | 53.8 0.01360 | 53.9 0.01364 | 54.2 0.01366 | 54.4 0.01362 | 54.5 0.01357 | 54.1 0.01369 | 39.1 0.01347 | 39.4 0.01312 | 39.4 0.01316 | 39.3 0.01318 | 39.4 0.01312 | 39.4 0.01306 | 39.3 |
| VOC % Removal in Catalyst Particulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) | % lb/hr lb/hr | 8.9 12.9 | 8.8 12.8 | 12.8 | | 12.7 | | | | | | | | | | | 39.4 | | 39.3 | | 39.4 | 00.0 |
| VOC % Removal in Catalyst Particulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) HZSO4 Emissions HZSO4 in Exhaust Gas (per HRSG) | lb/hr lb/hr lb/MMBtu | 8.9 12.9 0.00753 | 8.8 12.8 0.00767 | 12.8 0.00769 | 0.00774 3.51 | 12.7 0.00778 | 0.00781 3.46 | 0.00783 | 0.01389 9.03 | 0.01360 9.14 | 0.01364 9.14 | 0.01366 9.17 | 0.01362 9.24 | 0.01357 9.28 | 0.01369 9.13 | 0.01347 6.74 | 39.4 0.01312 6.97 | 0.01316 6.94 | 39.3 0.01318 6.93 | 0.01312 6.97 | 39.4 0.01306 7.01 | 39.3 0.01323 6.90 |
| VOC % Removal in Catalyst Particulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) HM10, front & back including (NH4)2SO4 (per HRSG) H2SO4 Emissions H2SO4 in Exhaust Gas (per HRSG) H2SO4 in Exhaust Gas | % Ib/hr Ib/hr Ib/MMBtu | 8.9 12.9 0.00753 | 8.8 12.8 0.00767 | 12.8 0.00769 | 0.00774 | 12.7 0.00778 | 0.00781 | 0.00783 | 0.01389 | 0.01360 | 0.01364 | 0.01366 | 0.01362 | 0.01357 | 0.01369 | 0.01347 | 39.4 0.01312 | 0.01316 | 39.3 0.01318 | 0.01312 | 39.4 0.01306 | 39.3 0.01323 |
| VOC % Removal in Catalyst Particulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) H2SO4 Emissions H2SO4 in Exhaust Gas (per HRSG) H2SO4 in Exhaust Gas GH6 Emissions | % Ib/hr Ib/hr Ib/MMBtu Ib/hr Ib/MMBtu | 8.9 12.9 0.00753 3.67 0.00213 | 8.8 12.8 0.00767 3.56 0.00213 | 12.8 0.00769 3.55 0.00213 | 0.00774 3.51 0.00213 | 12.7 0.00778 3.48 0.00213 | 0.00781 3.46 0.00213 | 0.00783 3.45 0.00213 | 9.03 0.00231 | 9.14 0.00231 | 0.01364 9.14 0.00231 | 9.17 0.00231 | 9.24 0.00231 | 9.28 0.00231 | 9.13 0.00231 | 0.01347 6.74 0.00232 | 39.4 0.01312 6.97 0.00232 | 0.01316 6.94 0.00232 | 39.3 0.01318 6.93 0.00232 | 0.01312 6.97 0.00232 | 39.4 0.01306 7.01 0.00232 | 39.3 0.01323 6.90 0.00232 |
| VOC % Removal in Catalyst Particulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM26A Emissions H2SO4 in Exhaust Gas (per HRSG) H2SO4 in Exhaust Gas GH6 Emissions CO2 in Exhaust Gas | % Ib/hr Ib/hr Ib/MMBtu Ib/hr Ib/MMBtu Ib/MMBtu | 8.9 12.9 0.00753 3.67 0.00213 | 8.8 12.8 0.00767 3.56 0.00213 | 12.8 0.00769 3.55 0.00213 | 0.00774 3.51 0.00213 116.98 | 12.7 0.00778 3.48 0.00213 | 3.46 0.00213 116.98 | 0.00783 3.45 0.00213 116.98 | 9.03 0.00231 163.45 | 9.14 0.00231 163.45 | 9.14 0.00231 163.45 | 9.17 0.00231 163.45 | 9.24 0.00231 163.45 | 9.28 0.00231 163.45 | 9.13 0.00231 163.45 | 0.01347 6.74 0.00232 163.45 | 39.4 0.01312 6.97 0.00232 163.45 | 0.01316 6.94 0.00232 163.45 | 39.3 0.01318 6.93 0.00232 | 0.01312 6.97 0.00232 163.45 | 39.4 0.01306 7.01 0.00232 | 39.3 0.01323 6.90 0.00232 |
| VOC % Removal in Catalyst Particulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) H2SO4 Emissions H2SO4 in Exhaust Gas (per HRSG) H2SO4 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) | % Ib/hr Ib/hr Ib/hr Ib/hr Ib/MMBtu Ib/MMBtu Ib/MMBtu Ib/MMBtu | 8.9 12.9 0.00753 3.67 0.00213 116.98 184,191 | 8.8 12.8 0.00767 3.56 0.00213 116.98 178,796 | 12.8 0.00769 3.55 0.00213 116.98 178,178 | 3.51 0.00213 116.98 176,210 | 12.7 0.00778 3.48 0.00213 116.98 174,746 | 3.46 0.00213 116.98 173,699 | 0.00783 3.45 0.00213 116.98 173,102 | 9.03 0.00231 163.45 542,846 | 0.01360 9.14 0.00231 163.45 552,266 | 9.14 0.00231 163.45 551,496 | 9.17 0.00231 163.45 552,807 | 9.24 0.00231 163.45 556,581 | 9.28 0.00231 163.45 559,613 | 9.13 0.00231 163.45 550,152 | 0.01347 6.74 0.00232 163.45 434,815 | 39.4 0.01312 6.97 0.00232 163.45 449,819 | 0.01316 6.94 0.00232 163.45 447,886 | 39.3 0.01318 6.93 0.00232 163.45 447,073 | 0.01312 6.97 0.00232 163.45 449,853 | 39.4 0.01306 7.01 0.00232 163.45 452,619 | 39.3 0.01323 6.90 0.00232 163.45 445,081 |
| VOC % Removal in Catalyst PArticulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) HZSO4 Emissions HZSO4 in Exhaust Gas (per HRSG) HZSO4 in Exhaust Gas (per HRSG) GHG Emissions CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) | % Ib/hr Ib/hr Ib/MMBtu Ib/hr Ib/MMBtu Ib/MMBtu | 8.9 12.9 0.00753 3.67 0.00213 116.98 184,191 962.6 | 8.8 12.8 0.00767 3.56 0.00213 116.98 178,796 942.6 | 12.8 0.00769 3.55 0.00213 116.98 178,178 936.7 | 0.00774 3.51 0.00213 116.98 | 12.7 0.00778 3.48 0.00213 116.98 174,746 913.8 | 3.46 0.00213 116.98 | 0.00783 3.45 0.00213 116.98 173,102 917.7 | 9.03 0.00231 163.45 | 9.14 0.00231 163.45 | 9.14 0.00231 163.45 | 9.17 0.00231 163.45 | 9.24 0.00231 163.45 | 9.28 0.00231 163.45 | 9.13 0.00231 163.45 | 0.01347 6.74 0.00232 163.45 | 39.4 0.01312 6.97 0.00232 163.45 | 0.01316 6.94 0.00232 163.45 | 39.3 0.01318 6.93 0.00232 | 0.01312 6.97 0.00232 163.45 | 39.4 0.01306 7.01 0.00232 | 39.3 0.01323 6.90 0.00232 163.45 445,081 1,156.3 |
| VOC % Removal in Catalyst Particulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) H2SO4 Emissions H2SO4 in Exhaust Gas (per HRSG) H2SO4 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) Ib. CH4 in Exhaust Gas (per HRSG) | % Ib/hr Ib/hr Ib/hr Ib/hr Ib/MMBtu Ib/MMBtu Ib/MMBtu Ib/hr Ib/MMBtu Ib/hr | 8.9 12.9 0.00753 3.67 0.00213 116.98 184,191 | 8.8 12.8 0.00767 3.56 0.00213 116.98 178,796 | 12.8 0.00769 3.55 0.00213 116.98 178,178 | 0.00774 3.51 0.00213 116.98 176,210 924.3 | 12.7 0.00778 3.48 0.00213 116.98 174,746 | 0.00781 3.46 0.00213 116.98 173,699 914.2 | 0.00783 3.45 0.00213 116.98 173,102 | 0.01389 9.03 0.00231 163.45 542,846 1,205.9 | 0.01360 9.14 0.00231 163.45 552,266 1,173.0 | 9.14 0.00231 163.45 551,496 1,167.1 | 9.17 0.00231 163.45 552,807 1,154.6 | 9.24 0.00231 163.45 556,581 1,140.6 | 9.28 0.00231 163.45 559,613 1,138.3 | 9.13 0.00231 163.45 550,152 1,142.6 | 0.01347 6.74 0.00232 163.45 434,815 1,229.8 | 39.4 0.01312 6.97 0.00232 163.45 449,819 1,184.3 | 0.01316 6.94 0.00232 163.45 447,886 1,177.6 | 39.3 0.01318 6.93 0.00232 163.45 447,073 1,163.6 | 0.01312 6.97 0.00232 163.45 449,853 1,149.9 | 39.4 0.01306 7.01 0.00232 163.45 452,619 1,150.2 | 39.3 0.01323 6.90 0.00232 163.45 445,081 1,156.3 |
| VOC % Removal in Catalyst Particulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) H2SO4 Emissions H2SO4 in Exhaust Gas (per HRSG) H2SO4 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CH4 in Exhaust Gas (per HRSG) CH4 in Exhaust Gas (per HRSG) CH4 in Exhaust Gas (per HRSG) N2O in Exhaust Gas (per HRSG) | % Ib/hr Ib/hr Ib/hr Ib/hr Ib/hr Ib/hr Ib/MBtu Ib/MBtu Ib/hr Ib/MMBtu Ib/hr Ib/MVh (gross) Ib/MMBtu Ib/hr Ib/MMBtu | 40% 8.9 12.9 0.00753 3.67 0.00213 116.98 184,191 962.6 5.5116E-02 94.7 6.5698E-02 | 8.8 12.8 0.00767 3.56 0.00213 116.98 178,796 942.6 5.5116E-02 91.9 6.5698E-02 | 12.8 0.00769 3.55 0.00213 116.98 178,178 936.7 5.5116E-02 91.6 6.5698E-02 | 3.51 0.00213 116.98 176.210 924.3 5.5116E-02 90.6 6.5698E-02 | 12.7 0.00778 3.48 0.00213 116.98 174,746 913.8 5.5116E-02 89.8 6.5698E-02 | 3.46 0.00213 116.98 173,699 914.2 5.5116E-02 89.3 6.5698E-02 | 3.45 0.00213 116.98 173,102 917.7 5.5116E-02 89.0 6.5698E-02 | 9.03 0.00231 163.45 542,846 1,205.9 1.6535E-01 535.3 3.9419E-01 | 9.14 0.00231 163.45 552,266 1,173.0 1.6535E-01 549.0 3.9419E-01 | 9.14 0.00231 163.45 551,496 1,167.1 1.6535E-01 547.5 3.9419E-01 | 9.17 0.00231 163.45 552,807 1,154.6 1.6535E-01 547.7 3.9419E-01 | 9.24 0.00231 163.45 556,581 1,140.6 1.6535E-01 551.2 3.9419E-01 | 9.28 0.00231 163.45 559,613 1,138.3 1.6535E-01 554.4 3.9419E-01 | 9.13 0.00231 163.45 550,152 1,142.6 1.6535E-01 545.1 3.9419E-01 | 0.01347 6.74 0.00232 163.45 434.815 1,229.8 1.6535E-01 479.8 3.9419E-01 | 39.4 0.01312 6.97 0.00232 163.45 449.819 1,184.3 1.6535E-01 496.4 3.9419E-01 | 0.01316 6.94 0.00232 163.45 447.886 1,177.6 1.6535E-01 494.3 3.9419E-01 | 39.3 0.01318 6.93 0.00232 163.45 447,073 1,163.6 1.6533E-01 493.4 3.9419E-01 | 6.97 0.00232 163.45 449.853 1,149.9 1.65535E-01 496.4 3.9419E-01 | 39.4 0.01306 7.01 0.00232 163.45 452,619 1,150.2 1.6535E-01 499.5 3.9419E-01 | 39.3 0.01323 6.90 0.00232 163.45 445,081 1,156.3 1.6535E-01 491.2 3.9419E-01 |
| VOC % Removal in Catalyst Particulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) H2SO4 in Exhaust Gas (per HRSG) H2SO4 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO4 in Exhaust Gas (per HRSG) CO4 in Exhaust Gas (per HRSG) CO5 in Exhaust Gas (per HRSG) CO6 in Exhaust Gas (per HRSG) CO7 in Exhaust Gas (per HRSG) CH4 in Exhaust Gas (per HRSG) CH5 in Exhaust Gas (per HRSG) CH6 in Exhaust Gas (per HRSG) CN20 in Exhaust Gas (per HRSG) CN20 in Exhaust Gas (per HRSG) CN20 in Exhaust Gas (per HRSG) | % Ib/hr Ib/hr Ib/hr Ib/hMBtu Ib/hr Ib/MMBtu Ib/hr Ib/MMBtu Ib/hr Ib/MMBtu Ib/hr Ib/MMBtu Ib/hr Ib/MMBtu Ib/hr | 40% 8.9 12.9 0.00753 3.67 0.00213 116.98 184,191 962.6 5.5116E-02 94.7 6.5696E-02 112.9 | 8.8 12.8 0.00767 3.56 0.00213 116.98 178,796 942.6 5.5116E-02 91.9 6.5698E-02 | 12.8 0.00769 3.55 0.00213 116.98 178.178 936.7 5.5116E-02 91.6 6.5698E-02 109.2 | 3.51 0.00213 116.98 176,210 924.3 5.5116E-02 90.6 6.5698E-02 108.0 | 12.7 0.00778 3.48 0.00213 116.98 174,746 913.8 5.5116E-02 89.8 6.5698E-02 107.1 | 3.46 0.00213 116.98 173,699 914.2 5.5116E-02 89.3 6.5698E-02 106.4 | 0.00783 3.45 0.00213 116.98 173,102 917.7 5.5116E-02 89.0 6.5698E-02 106.1 | 0.01389 9.03 0.00231 163.45 542,846 1,205.9 1.6535E-01 535.3 3.9419E-01 1,210.1 | 9.14 0.00231 163.45 552,266 1,173.0 1.6535E-01 549.0 3.9419E-01 1,246.1 | 9.14 0.00231 163.45 551,496 1,167.1 1.6535E-01 547.5 3.9419E-01 1,241.8 | 9.17 0.00231 163.45 552,807 1,154.6 1.6535E-01 547.7 3.9419E-01 1,240.9 | 9.24 0.00231 163.45 556,581 1,140.6 1.8535E-01 551.2 3.9419E-01 1,248.8 | 9.28 0.00231 163.45 559,613 1,138.3 1.6535E-01 554.4 3.9419E-01 1,256.3 | 9.13 0.00231 163.45 550,152 1,142.6 1.8535E-01 545.1 3.9419E-01 1,235.3 | 0.01347 6.74 0.00232 163.45 434,815 1,229.8 1.6535E-01 479.8 3.9419E-01 1,144.0 | 39.4 0.01312 6.97 0.00232 163.45 449.819 1,184.3 1.6535E-01 496.4 3.9419E-01 1,183.4 | 0.01316 6.94 0.00232 163.45 447,886 1,177.6 1.6535E-01 494.3 3.9419E-01 1,178.3 | 39.3 0.01318 6.93 0.00232 163.45 447,073 1,163.6 1.6535E-01 493.4 3.9419E-01 1,176.2 | 0.01312 6.97 0.00232 163.45 449,853 1,149.9 1.6535E-01 496.4 3.9419E-01 1,183.5 | 39.4 0.01306 7.01 0.00232 163.45 452,619 1,150.2 1.6535E-01 499.5 3.9419E-01 1,190.8 | 39.3 0.01323 6.90 0.00232 163.45 445,081 1,156.3 1.6535E-01 491.2 3.9419E-01 1,171.0 |
| VOC % Removal in Catalyst Particulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) H2SO4 Emissions H2SO4 in Exhaust Gas (per HRSG) H2SO4 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CH4 in Exhaust Gas (per HRSG) LH4 in Exhaust Gas (per HRSG) NZO in Exhaust Gas (per HRSG) NZO in Exhaust Gas (per HRSG) H2SO4 in Exhaust Gas (per HRSG) NZO in Exhaust Gas (per HRSG) NZO in Exhaust Gas (per HRSG) | % Ib/hr Ib/hr Ib/hr Ib/hr Ib/hr Ib/hr Ib/MBtu Ib/MBtu Ib/hr Ib/MMBtu Ib/hr Ib/MVh (gross) Ib/MMBtu Ib/hr Ib/MMBtu | 40% 8.9 12.9 0.00753 3.67 0.00213 116.98 184,191 962.6 5.5116E-02 94.7 6.5698E-02 | 8.8 12.8 0.00767 3.56 0.00213 116.98 178,796 942.6 5.5116E-02 91.9 6.5698E-02 | 12.8 0.00769 3.55 0.00213 116.98 178,178 936.7 5.5116E-02 91.6 6.5698E-02 | 3.51 0.00213 116.98 176.210 924.3 5.5116E-02 90.6 6.5698E-02 | 12.7 0.00778 3.48 0.00213 116.98 174,746 913.8 5.5116E-02 89.8 6.5698E-02 | 3.46 0.00213 116.98 173,699 914.2 5.5116E-02 89.3 6.5698E-02 | 3.45 0.00213 116.98 173,102 917.7 5.5116E-02 89.0 6.5698E-02 | 9.03 0.00231 163.45 542,846 1,205.9 1.6535E-01 535.3 3.9419E-01 | 9.14 0.00231 163.45 552,266 1,173.0 1.6535E-01 549.0 3.9419E-01 | 9.14 0.00231 163.45 551,496 1,167.1 1.6535E-01 547.5 3.9419E-01 | 9.17 0.00231 163.45 552,807 1,154.6 1.6535E-01 547.7 3.9419E-01 | 9.24 0.00231 163.45 556,581 1,140.6 1.6535E-01 551.2 3.9419E-01 | 9.28 0.00231 163.45 559,613 1,138.3 1.6535E-01 554.4 3.9419E-01 | 9.13 0.00231 163.45 550,152 1,142.6 1.6535E-01 545.1 3.9419E-01 | 0.01347 6.74 0.00232 163.45 434.815 1,229.8 1.6535E-01 479.8 3.9419E-01 | 39.4 0.01312 6.97 0.00232 163.45 449.819 1,184.3 1.6535E-01 496.4 3.9419E-01 | 0.01316 6.94 0.00232 163.45 447.886 1,177.6 1.6535E-01 494.3 3.9419E-01 | 39.3 0.01318 6.93 0.00232 163.45 447,073 1,163.6 1.6533E-01 493.4 3.9419E-01 | 6.97 0.00232 163.45 449.853 1,149.9 1.65535E-01 496.4 3.9419E-01 | 39.4 0.01306 7.01 0.00232 163.45 452,619 1,150.2 1.6535E-01 499.5 3.9419E-01 | 39.3 0.01323 6.90 0.00232 163.45 445,081 1,156.3 1.6535E-01 491.2 3.9419E-01 1,171.0 |
| VOC & Removal in Catalyst Particulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) H2SO4 in Exhaust Gas (per HRSG) H2SO4 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO4 in Exhaust Gas (per HRSG) CO4 in Exhaust Gas (per HRSG) CH4 in Exhaust Gas (per HRSG) NC4 in Exhaust Gas (per HRSG) NC4 in Exhaust Gas (per HRSG) NC6 in Exhaust Gas (per HRSG) NC7 in Exhaust Gas (per HRSG) NC8 in Exhaust Gas (per HRSG) NC9 in Exhaust Gas (per HRSG) NC9 in Exhaust Gas (per HRSG) SGG in Exhaust Gas (per HRSG) | 96 Ib/hr | 8.9 12.9 0.00753 3.67 0.00213 116.98 184,191 94.7 6.5698E-02 112.9 184,398.8 | 8.8 12.8 0.00767 3.56 0.00213 116.98 178.796 942.6 5.5116E-02 91.9 6.5698E-02 109.5 178.997.4 | 12.8 0.00769 3.55 0.00213 116.98 178,178 936.7 5.5116E-02 91.6 6.5698E-02 109.2 178,378.5 | 3.51 0.00213 116.98 176,210 924.3 5.5116E-02 90.6 6.5698E-02 108.0 176,408.8 | 12.7 0.00778 3.48 0.00213 116.98 174,746 913.8 5.5116E-02 107.1 174,942.5 | 3.46 0.00213 116.98 173,699 914.2 5.5116E-02 89.3 6.5698E-02 106.4 173,895.1 | 3.45 0.00213 116.98 173,102 917.7 5.5116E-02 89.0 6.5698E-02 106.1 173,296.6 | 0.01389 9.03 0.00231 163.45 542,846 1,205.9 1.6535E-01 535.3 3.9419E-01 1,210.1 | 0.01360 9.14 0.00231 163.45 552,266 1,173.0 1.6535E-01 549.0 3.9419E-01 1,246.1 554,061.4 | 9.14 0.00231 163.45 551.496 1.167.1 1.6535E-01 547.5 3.9419E-01 1.241.8 553,285.6 | 0.01366 9.17 0.00231 163.45 552,807 1,154.6 1.8535E-01 547.7 3.9419E-01 1,240.9 554,595.3 | 9.24 0.00231 163.45 556,581 1,140.6 1.8535E-01 551.2 3.9419E-01 1,248.8 558,381.6 | 9.28 0.00231 163.45 559,613 1,138.3 1.6535E-01 554.4 3.9419E-01 1,256.3 561,423.9 | 9.13 0.00231 163.45 550,152 1,142.6 1.8535E-01 545.1 3.9419E-01 1,235.3 551,932.5 | 0.01347 6.74 0.00232 163.45 434,815 1,229.8 1.6535E-01 479.8 3.9419E-01 1,144.0 436,438.8 | 39.4 0.01312 6.97 0.00232 163.45 449.819 1,184.3 1,6535E-01 496.4 3,9419E-01 1,183.4 451,499.0 | 0.01316 6.94 0.00232 163.45 447.886 1.177.6 1.6535E-01 494.3 3.9419E-01 1.178.3 449.558.6 | 39.3 0.01318 6.93 0.00232 163.45 447,073 1,163.6 1.6535E-01 493.4 3.9419E-01 1,176.2 448,742.6 | 0.01312 6.97 0.00232 163.45 449.853 1,149.9 1.6535E-01 496.4 3,9419E-01 1,183.5 451,533.3 | 39.4 0.01306 7.01 0.00232 163.45 452,619 1,150.2 1.6535E-01 499.5 3.9419E-01 1,190.8 454,309.8 | 39.3 0.01323 6.90 0.00232 163.45 445,081 1,156.3 1.6535E-01 491.2 3.9419E-01 1,171.0 446,742.6 |
| VOC % Removal in Catalyst PArticulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) HZSO4 in Exhaust Gas (per HRSG) HZSO4 in Exhaust Gas (per HRSG) HZSO4 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) CO4 in Exhaust Gas (per HRSG) CH4 in Exhaust Gas (per HRSG) NZO in Exhaust Gas (per HRSG) SZO IN Exhaust Gas (per HRSG) | % Ib/hr Ib/hMBtu Ib/MMBtu Ib/MMBtu Ib/MMBtu Ib/MMBtu Ib/MMBtu Ib/MMBtu Ib/hr Ib/MMBtu Ib/hr Ib/hr Ib/hr Ib/hr Ib/hr Ib/hr Ib/hr Ib/hr Ib/hr | 8.9 12.9 0.00753 3.67 0.00213 116.98 184,191 962.6 5.5116E-02 94.7 6.5698E-02 112.9 184,398.8 | 8.8 12.8 0.00767 3.56 0.00213 116.98 178.796 942.6 5.5116E-02 91.9 6.5698E-02 109.5 178.997.4 | 12.8 0.00769 3.55 0.00213 116.98 178.178 936.7 5.5116E-02 91.6 6.5698E-02 109.2 178.378.5 | 0.00774 3.51 0.00213 116.98 176.210 924.3 5.5116E-02 90.6 6.5698E-02 108.0 176.408.8 | 12.7 0.00778 3.48 0.00213 116.98 174,746 913.8 5.5116E-02 98.8 6.5998E-02 107.1 174,942.5 | 0.00781 3.46 0.00213 116.98 173,699 914.2 5.5116E-02 89.3 6.5698E-02 106.4 173,895.1 | 0.00783 3.45 0.00213 116.98 173,102 917.7 5.5116E-02 89.0 6.5698E-02 106.1 173,296.6 | 0.01389 9.03 0.00231 163.45 542,846 1,205.9 1.6535E-01 535.3 3.9419E-01 1,210.1 544,591.4 | 0.01360 9.14 0.00231 163.45 552,266 1,173.0 1.6535E-01 549.0 3.9419E-01 1,246.1 554,061.4 | 0.01364 9.14 0.00231 163.45 551,496 1,167.1 1.6535E-01 547.5 3.9419E-01 1,241.8 553,285.6 | 0.01366 9.17 0.00231 163.45 552,807 1,154.6 1,6535E-01 547.7 3,9419E-01 1,240.9 554,595.3 | 9.24 0.00231 163.45 556,581 1,140.6 1,6535E-01 551.2 3,9419E-01 1,248.8 558,381.6 | 9.28 0.00231 163.45 559,613 1,138.3 1,138.3 1,1533E-01 554.4 3,9419E-01 1,256.3 561,423.9 | 9.13 0.00231 163.45 550,152 1,142.6 1,6535E-01 545.1 3,9419E-01 1,235.3 551,932.5 | 0.01347 6.74 0.00232 163.45 434,815 1,229.8 1,6535E-01 479.8 3,9419E-01 1,144.0 436,438.8 | 39.4 0.01312 6.97 0.00232 163.45 449.819 1.184.3 1.6535E-01 496.4 3.9419E-01 1.183.4 451,499.0 | 0.01316 6.94 0.00232 163.45 447,886 1,177.6 1.5535E-01 494.3 3.9419E-01 1,178.3 449,558.6 | 39.3 0.01318 6.93 0.00232 163.45 447.073 1,163.6 1.6535E-01 493.4 3.9419E-01 1,176.2 448.742.6 | 0.01312 6.97 0.00232 163.45 449.853 1,149.9 1.6535E-01 496.4 3.9419E-01 1,183.5 451.533.3 | 39.4 0.01306 7.01 0.00232 163.45 452,619 1,150.2 1.6535E-01 499.5 3.9419E-01 1,190.8 454,309.8 | 39.3 0.01323 6.90 0.00232 163.45 445,081 1,156.3 1.6535E-01 491.2 3.9419E-01 1,171.0 446,742.6 |
| VOC % Removal in Catalyst Particulates Ph/10, front including (NH4)2SO4 (per HRSG) Ph/10, front & back including (NH4)2SO4 (per HRSG) Ph/10, front & back including (NH4)2SO4 (per HRSG) Ph/10, front & back including (NH4)2SO4 (per HRSG) HZSO4 emissions HZSO4 in Exhaust Gas (per HRSG) HZSO4 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) NCO1 in Exhaust Gas (per HRSG) NCH in Exhaust Gas (per HRSG) NZO in Exhaust Gas (per HRSG) NZO in Exhaust Gas (per HRSG) NZO in Exhaust Gas (per HRSG) SIACH Exit | 96 Ib/hr | 8.9 12.9 0.00753 3.67 0.00213 116.98 184,191 94.7 6.5698E-02 112.9 184,398.8 | 8.8 12.8 0.00767 3.56 0.00213 116.98 178.796 942.6 5.5116E-02 91.9 6.5698E-02 109.5 178.997.4 | 12.8 0.00769 3.55 0.00213 116.98 178,178 936.7 5.5116E-02 91.6 6.5698E-02 109.2 178,378.5 | 3.51 0.00213 116.98 176,210 924.3 5.5116E-02 90.6 6.5698E-02 108.0 176,408.8 | 12.7 0.00778 3.48 0.00213 116.98 174,746 913.8 5.5118E-02 98.8 6.5698E-02 107.1 174,942.5 | 3.46 0.00213 116.98 173,699 914.2 5.5116E-02 89.3 6.5698E-02 106.4 173,895.1 | 0.00783 3.45 0.00213 116.98 173,102 917.7 5.5116E-02 89.0 6.5698E-02 106.1 173,296.6 165 3.444,104 | 0.01389 9.03 0.00231 163.45 542,846 1,205.9 1.6535E-01 535.3 3.9419E-01 1,210.1 | 0.01360 9.14 0.00231 163.45 552,266 1.173.0 1.6535E-01 549.0 3.9419E-01 1,246.1 554,061.4 | 9.14 0.00231 163.45 551.496 1.167.1 1.6535E-01 547.5 3.9419E-01 1.241.8 553,285.6 | 0.01366 9.17 0.00231 163.45 552,807 1,154.6 1.8535E-01 547.7 3.9419E-01 1,240.9 554,595.3 | 9.24 0.00231 163.45 556,581 1,140.6 1.8535E-01 551.2 3.9419E-01 1,248.8 558,381.6 | 9.28 0.00231 163.45 559,613 1,138.3 1.6535E-01 554.4 3.9419E-01 1,256.3 561,423.9 | 9.13 0.00231 163.45 550,152 1,142.6 1.6535E-01 545.1 3.9419E-01 1,235.3 551,932.5 | 0.01347 6.74 0.00232 163.45 434,815 1,229.8 1.6535E-01 479.8 3.9419E-01 1,144.0 436,438.8 | 39.4 0.01312 6.97 0.00232 163.45 449.819 1,184.3 1,6535E-01 496.4 3,9419E-01 1,183.4 451,499.0 | 0.01316 6.94 0.00232 163.45 447.886 1.177.6 1.6535E-01 494.3 3.9419E-01 1.178.3 449.558.6 | 39.3 0.01318 6.93 0.00232 163.45 447,073 1,163.6 1.6535E-01 493.4 3.9419E-01 1,176.2 448,742.6 | 0.01312 6.97 0.00232 163.45 449.853 1,149.9 1.6535E-01 496.4 3,9419E-01 1,183.5 451,533.3 | 39.4 0.01306 7.01 0.00232 163.45 452,619 1,150.2 1.6535E-01 499.5 3.9419E-01 1,190.8 454,309.8 | 39.3 0.01323 6.90 0.00232 163.45 445,081 1,156.3 1.6535E-01 491.2 3.9419E-01 1,171.0 446,742.6 |
| VOC % Removal in Catalyst Particulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) H2SO4 in Exhaust Gas (per HRSG) H2SO4 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) NO2 in Exhaust Gas (per HRSG) SIGHE in Exhaust Gas (per HRSG) SIGHE in Exhaust Gas (per HRSG) SIGHE in Exhaust Gas (per HRSG) FIGURE SIGHE SI | 96 Ib/hr | 8.9 12.9 0.00753 3.67 0.00213 116.98 184,191 962.6 5.5116E-02 94.7 6.5698E-02 112.9 184,398.8 | 8.8 12.8 0.00767 3.56 0.00213 116.98 178.796 942.6 5.5116E-02 91.9 6.5698E-02 109.5 178.997.4 | 12.8 0.00769 3.55 0.00213 116.98 178,178 936.7 5.5118E-02 91.6 6.5698E-02 109.2 178,378.5 | 0.00774 3.51 0.00213 116.98 176.210 924.3 5.5116E-02 906.0 90.6098E-02 108.0 176.408.8 165 3.454,351 | 12.7 0.00778 3.48 0.00213 116.98 174,746 913.8 5.5116E-02 98.8 6.5998E-02 107.1 174,942.5 | 0.00781 3.46 0.00213 116.98 173,699 914.2 5.5116E-02 89.3 6.5698E-02 106.4 173,895.1 165 3,456,818 | 0.00783 3.45 0.00213 116.98 173,102 917.7 5.5116E-02 89.0 6.5698E-02 106.1 173,296.6 | 0.01389 9.03 0.00231 163.45 542,846 1.205.9 1.6535E-01 5353 3.9419E-01 1,210.1 544,591.4 186 6,418,548 | 0.01360 9.14 0.00231 163.45 552,266 1,173.0 1.6535E-01 549.0 3.9419E-01 1,246.1 554,061.4 | 0.01364 9.14 0.00231 163.45 551,496 1,167.1 1.6535E-01 547.5 3.9419E-01 1,241.8 553,285.6 | 0.01366 9.17 0.00231 163.45 552,807 1,154.6 1.6535E-01 547.7 3.9419E-01 1,240.9 554,595.3 6,382,793 | 9.24 0.00231 163.45 556,581 1,140.6 1.6535E-01 53.9419E-01 1,248.8 558,381.6 | 9.28 0.00231 163.45 559.613 1,138.3 1,6535E-01 554.4 3,9419E-01 1,256.3 561,423.9 | 9.13 0.00231 163.45 550,152 1,142.6 1,6535E-01 545.1 3,9419E-01 1,235.3 551,932.5 | 0.01347 6.74 0.00232 163.45 434.815 1,229.8 1.6535E-01 479.8 3.9419E-01 1,144.0 436.438.8 | 39.4 0.01312 6.97 0.00232 163.45 449,819 1.184.3 1.6535E-01 496.4 3.9419E-01 1.183.4 451,499.0 | 0.01316 6.94 0.00232 163.45 447.886 1,177.6 1.6535E-01 494.3 3.9419E-01 1,178.3 449.558.6 | 99.3 0.01318 6.93 0.00232 163.45 447,073 1.163.6 1.6535E-01 493.4 3.9419E-01 1.176.2 448,742.6 | 0.01312 6.97 0.00232 163.45 449,853 1,149,9 1,6535E-01 1,183.5 451,533.3 | 39.4 0.01306 7.01 0.00232 163.45 452,619 1,150.2 1,6538E-01 499.5 3,9419E-01 1,190.8 454,309.8 | 39.3 0.01323 6.90 0.00232 163.45 445,081 1,156.3 1,6533E-01 491.2 3.9419E-01 1,171.0 446,742.6 |
| VOC % Removal in Catalyst Particulates PM10, front including (NH4)2SO4 (per HRSG) PM10, front including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) PM10, front & back including (NH4)2SO4 (per HRSG) HZSO4 Emissions HZSO4 in Exhaust Gas (per HRSG) HZSO4 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) NO2 in Exhaust Gas (per HRSG) SO3 in Exhaust Gas (per HRSG) NO3 in Exhaust Gas (per HRSG) NO4 in Exhaust Gas (per HRSG) SO3 in Exhaust Gas (per HRSG) SO3 in Exhaust Gas (per HRSG) SO4 in Exhaust Gas (per HRSG) SO5 in Exhaust Gas (per HRSG) | % Ib/hr Ib/hr Ib/hr Ib/hMBtu Ib/hr Ib/hMBtu Ib/hr Ib/h/h (gross) Ib/hMBtu Ib/hr | 40% 8.9 12.9 0.00753 3.67 0.00213 116.98 184,191 962.6 5.5116E-02 94.7 6.5698E-02 112.9 184,398.8 165 3,526,941 651,405 | 8.8 12.8 0.00767 3.56 0.00213 116.98 178.796 942.6 5.5116E-02 91.9 6.5698E-02 109.5 178.997.4 | 12.8 0.00769 3.55 0.00213 116.98 178,178 936.7 5.5116E-02 91.6 6.5698E-02 109.2 178,378.5 | 0.00774 3.51 0.00213 116.98 176.210 924.3 5.5110E-02 90.6 6.5698E-02 108.0 176.408.8 | 12.7 0.00778 3.48 0.00213 116.98 174,746 913.8 5.5116E-02 89.8 6.599E-02 107.1 174,942.5 | 0.00781 3.46 0.00213 116.98 173.699 914.2 5.5110E-02 89.3 6.5698E-02 106.4 173.895.1 165 3.456.818 642.689 | 0.00783 3.45 0.00213 116.98 173,102 917.7 5.5116E-02 89.0 6.5698E-02 106.1 173,296.6 | 0.01389 9.03 0.00231 163.45 542,846 1,205.9 1.6535E-01 535.3 3.9419E-01 1,210.1 544,591.4 186 6,418,548 1,176,074 | 0.01360 9.14 0.00231 163.45 552,266 1,173.0 1.6535E-01 549.0 3.9419E-01 1,246.1 554,061.4 | 0.01364 9.14 0.00231 163.45 551,496 1,167.1 1.6835E-01 547.5 3.9419E-01 1,241.8 553,285.6 185 6,532,792 1,198,308 | 0.01366 9.17 0.00231 163.45 552,807 1,154.6 1,6533E-01 547.7 3,9419E-01 54,595.3 183 6,382,793 1,174,130 | 9.24 0.00231 163.45 556,581 1,140.6 1,6533E-01 551.2 3,9419E-01 3,9419E-01 184 6,237,719 1,152,671 | 9.28 0.00231 163.45 559.613 1,138.3 1,6535E-01 554.4 3,9419E-01 1,256.3 561,423.9 | 9.13 0.00231 163.45 550,152 1,142.6 1,6533E-01 545.1 3,9419E-01 3,9419E-01 184 6,003,036 1,115,224 | 0.01347 6.74 0.00232 163.45 434,815 1,229.8 1,6535E-01 479.8 3,9419E-01 1,144.0 436,438.8 | 39.4 0.01312 6.97 0.00232 163.45 449,819 1,184.3 1.6535E-01 496.4 3.9419E-01 1,183.4 451,499.0 | 0.01316 6.94 0.00232 163.45 447,886 1,177.6 1.6535E-01 494.3 3,9419E-01 1,178.3 449,558.6 185 6,490,652 1,185,218 | 39.3 0.01318 6.93 0.00232 163.45 447.073 1,163.6 1.6535E-01 493.4 3.9419E-01 1,176.2 448.742.6 | 0.01312 6.97 0.00232 163.45 449.853 1,149.9 1.6535E-01 496.4 3.9419E-01 1,183.5 451.533.3 | 39.4 0.01306 7.01 0.00232 163.45 452,619 1,150.2 1,6535E-01 499.5 3,9419E-01 1,190.8 454,309.8 | 39.3 0.01323 6.90 0.00232 163.45 445,081 1,156.3 1.6535E-01 491.2 3.9419E-01 1,171.0 446,742.6 |

Notes:

1. Particulate values exclude catalyst and other entrained particles.

2. Emission values do not include heavy metals (lead, mercury, etc.)

3. Differing fuel composition may change the calculated emissions.

4. CTG performance based on performance runs provided by SEI.

5. Fuel based on natural gas analysis provided by NTEC.

6. 35 ppm NOx control on 8000H gas turbine.

8. Stack SO2 content reported with no conversion to SO3.

9. Particulate emissions assume 100% conversion of SO2-SO3, and 100% cover 10. H2SO4 assumes 100% conversion of SO2-SO3, and 100% conversion of SO 11. Greenhouse Gas (GHC) emissions are based on EPA 40 CFR Part 98 emissions are based on EPA 40 CFR Part 98 emissions.

12. 20% margin in Fuel flow and 20% margin in exhaust flow are included.

13. Emissions reported on the basis of pounds per hour are for one combustion tu 14. Emissions estimates are for information only and are NOT guaranteed.

| Combustion Turbine Case # | | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 62 | 63 |
|--|------------------------------------|----------------------------------|------------------------------|------------------------------|------------------------------|-------------------------|------------------------------|----------------------|------------------------------|----------------------|
| | | | | | | Unfired Fuel Oil | | Unfired Fuel Oil | | Unfired Fuel Oil |
| | | Unfired Fuel Oil Evap OFF Min | Unfired Fuel Oil Evap OFF | Unfired Fuel Oil Evap OFF | Unfired Fuel Oil Evap OFF | Evap OFF | Unfired Fuel Oil Evap OFF | Evap OFF Maximum | Unfired Fuel Oil Evap OFF | Evap OFF Maximum |
| | | Ambient 1x75% | Winter Peak | Winter Average | Annual Average | Summer Average 1x75% | Summer Peak | Ambient 1x75% | Summer Peak | Ambient |
| Case Description | | CTG | 1x75% CTG | 1x75% CTG | 1x75% CTG | CTG | 1x75% CTG | CTG | 1xMECL CTG | 1xMECL CTG |
| Ambient Temperature | | -34.3 F | 7.9 F | 15.4 F | 39.1 F | 61 F | 76.8 F | 95.5 F | 76.8 F | 95.5 F |
| Gas Turbine Load | | 75% | 75% | 75% | 75% | 75% | 75% | 75% | 49% | 46% |
| Evaporative Cooling | | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF | OFF |
| Water Injection | | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON | INJECTION ON |
| Duct Firing Inlet Chiller | | OFF OFF | OFF OFF | OFF OFF | OFF OFF | OFF OFF | OFF OFF | OFF OFF | OFF OFF | OFF OFF |
| No. of Gas Turbines In Operation | | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Gas Turbine Fuel | | Fuel Oil | Fuel Oil | Fuel Oil | Fuel Oil | Fuel Oil | Fuel Oil | Fuel Oil | Fuel Oil | Fuel Oil |
| Duct Burner Fuel | | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| | | | | | | | | | | |
| Ambient Conditions | | | | | | | | | | |
| Temperature | degree F | -34.3 | 7.9 | 15.4 | 39.1 | 61 | 76.8 | 95.5 | 76.8 | 95.5 |
| Relative Humidity Wet Bulb Temperature | % degree F | 70% -34.5 | 69% 6.5 | 70% 13.5 | 70% 35.4 | 76% 56.4 | 62% 67.3 | 36% 73.6 | 62% 67.3 | 36% 73.6 |
| Pressure | psia | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 | 14.34 |
| Gas Turbine Generator Performance | pola | 11.01 | 11.01 | 11.01 | 11.01 | 11.01 | 11.01 | 11.01 | 11.01 | 11.01 |
| Electrical Output | kW | 178,707 | 194,008 | 193,733 | 194,160 | 195,081 | 190,691 | 177,262 | 127,127 | 118,174 |
| Heat Rate - LHV | Btu/kWh | 12,234 | 11,514 | 11,482 | 11,377 | 11,309 | 11,395 | 11,694 | 13,312 | 13,744 |
| Heat Rate - HHV | Btu/kWh | 13,138 | 12,365 | 12,330 | 12,218 | 12,145 | 12,237 | 12,558 | 14,296 | 14,759 |
| GTG Heat Input- LHV | MMBtu/hr | 2,186 | 2,234 | 2,224 | 2,209 | 2,206 | 2,173 | 2,073 | 1,692 | 1,624 |
| GTG Heat Input- HHV | MMBtu/hr | 2,348 | 2,399 | 2,389 | 2,372 | 2,369 | 2,334 | 2,226 | 1,817 | 1,744 |
| Water / Sprint Injection Rate (per HRSG) Exhaust Flow (per HRSG) | lb/hr lb/hr | 30,810 5,284,172 | 35,112 5,361,248 | 37,373 5,325,683 | 45,497 5,224,172 | 51,415 5,082,642 | 56,533 4,929,648 | 58,985 4,670,663 | 33,019 4,098,512 | 35,212 3,895,002 |
| Exhaust Flow (per FIRSG) Exhaust Temperature | degree F | 1,001 | 1,012 | 1,020 | 1,046 | 1,083 | 1,107 | 1,127 | 1,107 | 1,127 |
| Steam Turbine Generator Performance | 40g.00 I | .,501 | .,512 | .,320 | .,540 | .,300 | .,101 | ., .21 | .,101 | .,121 |
| Electrical Output | kW | 94,716 | 98,744 | 99,747 | 103,104 | 108,209 | 107,240 | 103,077 | 88,107 | 84,708 |
| Duct Burner Fuel Consumption | | | | | | | | | | |
| Heat Input, LHV (per HRSG) | MMBtu/hr | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Heat Input, HHV (per HRSG) | MMBtu/hr | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Stack Volumetric Analysis, Wet | 0/ | 0.000/ | 0.000/ | 0.000/ | 0.070/ | 0.000/ | 0.050/ | 0.050/ | 0.000/ | 0.000/ |
| Ar CO2 | % | 0.88% | 0.88% | 0.88% | 0.87% | 0.86% | 0.85% | 0.85% | 0.86% | 0.86% |
| H2O | % % | 4.56% 5.45% | 4.58% 5.71% | 4.59% 5.85% | 4.64% 6.51% | 4.74% 7.61% | 4.80% 8.39% | 4.82% 8.70% | 4.51% 7.60% | 4.55% 7.89% |
| N2 | % | 74.01% | 73.81% | 73.70% | 73.19% | 72.33% | 71.72% | 71.48% | 72.33% | 72.10% |
| 02 | % | 15.07% | 14.99% | 14.95% | 14.76% | 14.43% | 14.20% | 14.11% | 14.67% | 14.57% |
| Stack Emissions at Exit | | | | | | | | | | |
| NOx Emissions | | | | | | | | | | |
| NOx,@15% O2 Into SCR | ppmvd | 42.0 | 42.0 | 42.0 | 42.0 | 42.0 | 42.0 | 42.0 | 42.0 | 42.0 |
| NOx, as NO2 Into SCR (per HRSG) | lb/hr | 281.2 | 287.3 | 286.1 | 284.0 | 283.5 | 279.1 | 266.2 | 217.7 | 208.9 |
| NOx,@15% O2 Out of SCR | ppmvd | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| NOx, as NO2 Out of SCR (per HRSG) SCR NOx Removal Efficiency | lb/hr % | 40.2 85.7% | 41.0 85.7% | 40.9 85.7% | 40.6 85.7% | 40.5 85.7% | 39.9 85.7% | 38.0 85.7% | 31.1 85.7% | 29.8 85.7% |
| NH3 Emissions | 70 | 03.7% | 03.7% | 03.7% | 03.7% | 03.7% | 03.7% | 03.7% | 00.770 | 03.7% |
| NH3 Reacted with NOx (per HRSG) | lb/hr | 116.0 | 118.5 | 118.0 | 117.2 | 116.9 | 115.1 | 109.8 | 89.8 | 86.2 |
| NH3 slip @ 15% O2 | ppmvd | 10.0 | 10 | 10.0 | 10 | 10.9 | 10 | 10 | 10 | 10 |
| NH3 slip (per HRSG) | lb/hr | 24.8 | 25.3 | 25.2 | 25.0 | 25.0 | 24.6 | 23.5 | 19.2 | 18.4 |
| CO Emissions | | | | | | | | | | |
| CO into catalyst | ppmvd | 8.4 | 8.5 | 8.5 | 8.7 | 9.0 | 9.2 | 9.2 | 42.7 | 43.2 |
| CO into catalyst, @ 15% O2 | ppmvd | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 50.0 | 50.0 |
| CO into catalyst (per HRSG) | lb/hr ppmyd | 40.8 1.26 | 41.6 1.27 | 41.5 1.28 | 41.2 1.30 | 41.1 1.34 | 40.5 1.37 | 38.6 1.39 | 157.8 4.27 | 151.4 4.32 |
| CO out of catalyst CO out of catalyst, @ 15% O2 | ppmvd ppmvd | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 5.00 | 5.00 |
| CO out of catalyst (per HRSG) | lb/hr | 6.1 | 6.2 | 6.2 | 6.2 | 6.2 | 6.1 | 5.8 | 15.8 | 15.1 |
| CO Catalyst Removal Efficiency | % | 85.0% | 85.0% | 85.0% | 85.0% | 85.0% | 85.0% | 85.0% | 90.0% | 90.0% |
| SO2 Emissions | | | | | | | | | | |
| SO2 in Exh. Gas @ 15% O2 (assuming no conversion) | ppmvw | 0.361 | 0.360 | 0.360 | 0.357 | 0.353 | 0.350 | 0.349 | 0.353 | 0.352 |
| SO2 in Exh. Gas @ 15% O2 (assuming no conversion) | ppmvd | 0.382 | 0.382 | 0.382 | 0.382 | 0.382 | 0.382 | 0.382 | 0.382 | 0.382 |
| SO2 in Exhaust Gas (assuming no conversion) (per HRSG) | lb/hr | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.5 | 3.4 | 2.8 | 2.6 |
| SO2 in Exhaust Gas (assuming no conversion) (per HRSG) Volatile Organic Compounds | lb/MMBtu | 0.00152 | 0.00152 | 0.00152 | 0.00152 | 0.00152 | 0.00152 | 0.00152 | 0.00152 | 0.00152 |
| VOC @ 15% O2 | nnmvd | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| VOC @ 15% O2 VOC as CH4 (per HRSG) | ppmvd lb/hr | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.3 | 1.1 | 1.0 |
| VOC % Removal in Catalyst | % | 40% | 40% | 40% | 40% | 40% | 40% | 40% | 40% | 40% |
| Particulates | | | | | | | | 1010 | 1010 | |
| PM10, front including (NH4)2SO4 (per HRSG) | lb/hr | 22.3 | 22.5 | 22.5 | 22.4 | 22.4 | 22.3 | 22.0 | 20.7 | 20.5 |
| PM10, front & back including (NH4)2SO4 (per HRSG) | lb/hr | 37.3 | 37.5 | 37.5 | 37.4 | 37.4 | 37.3 | 37.0 | 35.7 | 35.5 |
| PM10, front & back including (NH4)2SO4 (per HRSG) | lb/MMBtu | 0.01591 | 0.01563 | 0.01569 | 0.01577 | 0.01579 | 0.01598 | 0.01660 | 0.01964 | 0.02033 |
| H2SO4 Emissions | | | | | | | | | | |
| H2SO4 in Exhaust Gas (per HRSG) | lb/hr | 5.45 | 5.57 | 5.55 | 5.51 | 5.50 | 5.42 | 5.17 | 4.22 | 4.05 |
| H2SO4 in Exhaust Gas | lb/MMBtu | 0.00232 | 0.00232 | 0.00232 | 0.00232 | 0.00232 | 0.00232 | 0.00232 | 0.00232 | 0.00232 |
| GHG Emissions CO2 in Exhaust Gas (per HRSG) | lb/MMBtu | 163.45 | 163.45 | 163.45 | 163.45 | 163.45 | 163.45 | 163.45 | 163.45 | 163.45 |
| CO2 in Exhaust Gas (per HRSG) CO2 in Exhaust Gas (per HRSG) | lb/MMBtu lb/hr | 163.45 351,785 | 163.45 359,429 | 163.45 357,909 | 163.45 355,437 | 163.45 354,976 | 163.45 349,638 | 333,538 | 163.45 272,292 | 163.45 261,330 |
| | lb/MWh (gross) | 1,286.6 | 1,227.8 | 1,219.5 | 1,195.7 | 1,170.4 | 1,173.6 | 1,189.8 | 1,265.1 | 1,288.1 |
| CH4 in Exhaust Gas (per HRSG) | lb/MMBtu | 1.6535E-01 | 1.6535E-01 | 1.6535E-01 | 1.6535E-01 | 1.6535E-01 | 1.6535E-01 | 1.6535E-01 | 1.6535E-01 | 1.6535E-01 |
| | lb/hr | 388.2 | 396.7 | 395.0 | 392.2 | 391.7 | 385.8 | 368.1 | 300.5 | 288.4 |
| CH4 in Exhaust Gas (per HRSG) | lb/MMBtu | 3.9419E-01 | 3.9419E-01 | 3.9419E-01 | 3.9419E-01 | 3.9419E-01 | 3.9419E-01 | 3.9419E-01 | 3.9419E-01 | 3.9419E-01 |
| N2O in Exhaust Gas (per HRSG) | He /he a | 925.5 | 945.6 | 941.6 | 935.1 | 933.9 | 919.9 | 877.5 | 716.4 | 687.5 |
| N2O in Exhaust Gas (per HRSG) N2O in Exhaust Gas (per HRSG) | lb/hr | 252,000,0 | 360,771.2 | 359,245.9 | 356,763.9 | 356,301.2 | 350,944.2 | 334,783.9 | 273,309.0 | 262,306.0 |
| N2O in Exhaust Gas (per HRSG) N2O in Exhaust Gas (per HRSG) GHG in Exhaust Gas (per HRSG) | lb/hr | 353,098.8 | | | | | | | | |
| N2O in Exhaust Gas (per HRSG) N2O in Exhaust Gas (per HRSG) GHG in Exhaust Gas (per HRSG) Stack Exit | lb/hr | | | | | | | | | |
| N2O in Exhaust Gas (per HRSG) N2O in Exhaust Gas (per HRSG) GHG in Exhaust Gas (per HRSG) Stack Exit Temperature | lb/hr degree F | 181 | 179 | 178 | 175 | 175 | 169 | 174 | 165 | 168 |
| N2O in Exhaust Gas (per HRSG) N2O in Exhaust Gas (per HRSG) GHG in Exhaust Gas (per HRSG) Stack Exit Temperature Flow Rate (per HRSG) | lb/hr degree F lb/hr | 181 5,284,172 | 5,361,248 | 5,325,683 | 5,224,172 | 5,082,642 | 4,929,648 | 4,670,663 | 4,098,512 | 3,895,002 |
| N2O in Exhaust Gas (per HRSG) N2O in Exhaust Gas (per HRSG) GHG in Exhaust Gas (per HRSG) Stack Exit Temperature Flow Rate (per HRSG) Flow Rate (per HRSG) | lb/hr degree F lb/hr scfm | 181 5,284,172 962,755 | 5,361,248 977,629 | 5,325,683 971,630 | 5,224,172 955,336 | 5,082,642 932,952 | 4,929,648 907,363 | 4,670,663 860,607 | 4,098,512 753,001 | 3,895,002 716,298 |
| N2O in Exhaust Gas (per HRSG) N2O in Exhaust Gas (per HRSG) GHG in Exhaust Gas (per HRSG) Stack Exit Temperature Flow Rate (per HRSG) | lb/hr degree F lb/hr | 181 5,284,172 | 5,361,248 | 5,325,683 | 5,224,172 | 5,082,642 | 4,929,648 | 4,670,663 | 4,098,512 | 3,895,002 |

- Notes:

 1. Particulate values exclude catalyst and other entrained particles.
 2. Emission values do not include heavy metals (lead, mercury, etc.)
 3. Differing fuel composition may change the calculated emissions.
 4. CTG performance based on performance runs provided by SEI.
 5. Fuel based on natural gas analysis provided by NTEC.
 6. 35 ppm NOx control on 8000H gas turbine.
 8. Stack SO2 content reported with no conversion to SO3.
 9. Particulate emissions assume 100% conversion of SO2-SO3, and 100% cove 10. HSO4 assumes 100% conversion of SO2-SO3, and 100% coversion of SO 11. Greenhouse Gas (GHG) emissions are based on EPA 40 CFR Part 98 emissi 12. 20% margin in Fuel flow and 20% margin in evaluate flow are included.
 13. Emissions reported on the basis of pounds per hour are for one combustion tu 14. Emissions estimates are for information only and are NOT guaranteed.

South Shore Energy, LLC - Nemadji Trail Energy Center Auxiliary Combustion Sources Emissions Calculations

Auxiliary Boiler

| Size | 100.00 | MMBtu/hr |
|-----------|--------|------------|
| HHV | 1,020 | Btu/cf |
| Operation | 8,760 | hours/year |

Auxiliary Boiler Stack Parameters

| | Height (ft) | Temp. (F) | Velocity (ft/sec) | Diameter (ft) | ACFM | Stack Discharge Type | Fuel |
|---|----------------|--------------|----------------------|------------------|--------|-------------------------|-------------|
| Г | 110.00 | 290.00 | 48.00 | 3.50 | 27,709 | Vertical | Natural Gas |

| | Emission Factors | | | Emissions | | | |
|--|------------------|----------|-------------------------------|-----------|--------|--|--|
| Pollutant | lb/MMcf | lb/MMBtu | Source | lb/hr | tpy | | |
| NO _X | | 0.011 | Vendor ^a | 1.1 | 4.8 | | |
| CO | | 0.0037 | BACT | 0.4 | 1.6 | | |
| PM/PM ₁₀ /PM _{2.5} | 7.6 | 0.01 | AP-42 ^b | 0.7 | 3.3 | | |
| SO ₂ | 0.6 | 0.0006 | AP-42 ^b | 0.06 | 0.3 | | |
| VOC | | 0.0027 | BACT | 0.3 | 1.2 | | |
| H ₂ SO ₄ Mist | | | Mass Balance | 9E-03 | 0.04 | | |
| CO ₂ | - | 117.0 | Federal Register ^c | 11,698 | 51,236 | | |
| CH₄ | - | 0.0022 | Federal Register ^c | 0.22 | 0.97 | | |
| N ₂ O | - | 0.00022 | Federal Register ^c | 0.022 | 0.097 | | |
| CO ₂ e | | | Federal Register ^c | 11,710 | 51,289 | | |

Natural Gas Heaters

| Size | 10.00 | MMBtu/hr |
|-------------------|-------|------------|
| HHV | 1,020 | Btu/cf |
| Operation | 8,760 | hours/year |
| Number of heaters | 2 | |

Natural Gas Heater Stack Parameters

| Height (ft) | Temp. (F) | Velocity (ft/sec) | Diameter (ft) | ACFM | Stack Discharge Type | Fuel |
|----------------|--------------|----------------------|------------------|-------|-------------------------|-------------|
| 15.00 | 750.00 | 25.00 | 1.67 | 3,272 | Vertical | Natural Gas |

| | Emission Factors | | | Emissions | | Emissions (2 | 2 heaters) |
|--|------------------|----------|-------------------------------|-----------|---------|--------------|------------|
| Pollutant | lb/MMcf | lb/MMBtu | Source | lb/hr | tpy | lb/hr | tpy |
| NO _X | 50.0 | 0.049 | AP-42 ^a | 0.5 | 2.1 | 1.0 | 4.3 |
| CO | 84.0 | 0.08 | AP-42 ^a | 0.8 | 3.6 | 1.6 | 7.2 |
| PM/PM ₁₀ /PM _{2.5} | 7.6 | 0.01 | AP-42 ^a | 0.07 | 0.3 | 0.1 | 0.7 |
| SO ₂ | 0.6 | 0.0006 | AP-42 ^a | 5.9E-03 | 0.03 | 0.01 | 0.05 |
| VOC | 5.5 | 0.005 | AP-42 ^a | 0.05 | 0.2 | 0.1 | 0.5 |
| H ₂ SO ₄ Mist | | | Mass Balance | 9.0E-04 | 3.9E-03 | 1.8E-03 | 7.9E-03 |
| CO ₂ | - | 117.0 | Federal Register ^b | 1,170 | 5,124 | 2,340 | 10,247 |
| CH₄ | | 0.0022 | Federal Register ^b | 0.022 | 0.10 | 0.04 | 0.19 |
| N ₂ O | - | 0.00022 | Federal Register ^b | 2.2E-03 | 0.010 | 0.00 | 0.02 |
| CO ₂ e | - | | Federal Register ^b | 1,171 | 5,129 | 2,342 | 10,258 |

⁽a) Ultra low-NOx burners (b) AP-42 Section 1.4 (7/98) (c) Federal Register - Subpart C of Part 98

⁽a) AP-42 Section 1.4 (7/98) (b) Federal Register - Subpart C of Part 98

South Shore Energy, LLC - Nemadji Trail Energy Center Auxiliary Combustion Sources Emissions Calculations

Emergency Diesel Fire Pump

| | 282.0 | HP |
|-----------|-------|------------|
| Size | 1.95 | MMBtu/hr |
| | 14.10 | gal/hr |
| Operation | 500 | hours/year |

Emergency Fire Pump Stack Parameters

| Height (ft) | Temp. (F) | Velocity (ft/sec) | Diameter (ft) | ACFM | Stack Discharge Type | Fuel |
|----------------|--------------|----------------------|------------------|-------|-------------------------|--------|
| 15.00 | 1,030 | 153.90 | 0.50 | 1,813 | Vertical | Diesel |

| | Emission Factors | | | Emissions | | | |
|--|------------------|---------|----------|-----------|-------------------------------|---------|---------|
| Pollutant | g/kw-hr | g/hp-hr | lb/hp-hr | lb/MMBtu | Source | lb/hr | tpy |
| NO_X | 4.0 | 3.0 | | | NSPS ^a | 1.9 | 0.5 |
| СО | 3.5 | 2.6 | | | NSPS ^a | 1.6 | 0.4 |
| PM/PM ₁₀ /PM _{2.5} | 0.2 | 0.15 | | | NSPS ^a | 0.09 | 0.02 |
| SO ₂ | | | 2.05E-03 | | AP-42 ^b | 0.6 | 0.1 |
| VOC | | 1.1 | 2.51E-03 | | AP-42 ^b | 0.7 | 0.2 |
| H ₂ SO ₄ Mist | | | | | Mass Balance | 0.09 | 0.02 |
| CO ₂ | | | | 163.1 | Federal Register ^c | 318.0 | 79.5 |
| CH₄ | | | | 0.0066 | Federal Register ^c | 0.013 | 3.2E-03 |
| N ₂ O | | | | 0.00132 | Federal Register ^c | 2.6E-03 | 6.4E-04 |
| CO₂e | | | | | Federal Register ^c | 319 | 80 |

(a) NSPS 40 CFR Part 60, Subapart IIII Limits

NSPS Limits - 40 CFR Part 60, Subapart IIII, (40 CFR 60 Table 4)

| | NOx + VOM | CO | PM |
|---------|-----------|-----|------|
| g/kW-hr | 4.0 | 3.5 | 0.20 |
| g/hp-hr | 3.0 | 2.6 | 0.15 |

⁽b) AP-42 Section 3.3 (10/96) (c) Federal Register - Subpart C of Part 98

South Shore Energy, LLC - Nemadji Trail Energy Center Auxiliary Combustion Sources Emissions Calculations

Emergency Diesel Generator

| | 1,112 | KW |
|----------------|--------|------------|
| Size | 1,490 | hp |
| | 150.0 | gal/hr |
| | 20.6 | MMBtu/hr |
| Operation | 500 | hours/year |
| Sulfur Content | 0.0015 | % |

137,000 Btu/gal

Emergency Diesel Generator Stack Parameters

| Height (ft) | Temp. (F) | Velocity (ft/sec) | Diameter (ft) | ACFM | Stack Discharge Type | Fuel |
|-------------|--------------|----------------------|------------------|-------|-------------------------|--------|
| 15.00 | 890.00 | 360.01 | 0.67 | 7,540 | Vertical | Diesel |

| | Emission Factors | | | Emissions | | | |
|--|------------------|---------|----------|-----------|-------------------------------|---------|---------|
| Pollutant | g/kw-hr | g/hp-hr | lb/hp-hr | lb/MMBtu | Source | lb/hr | tpy |
| NO_X | 6.4 | 4.8 | | | NSPS ^a | 15.7 | 3.9 |
| СО | 3.5 | 2.6 | | | NSPS ^a | 8.6 | 2.1 |
| PM/PM ₁₀ /PM _{2.5} | 0.2 | 0.15 | | | NSPS ^a | 0.5 | 0.1 |
| SO ₂ | | | 1.21E-05 | | AP-42 ^b | 0.02 | 4.5E-03 |
| VOC | | 0.32 | 7.05E-04 | | AP-42 ^b | 1.1 | 0.3 |
| H ₂ SO ₄ Mist | | | | | Mass Balance | 2.8E-03 | 6.9E-04 |
| CO ₂ | | | | 163.1 | Federal Register ^c | 3,351 | 838 |
| CH₄ | | | | 0.0066 | Federal Register ^c | 1.4E-01 | 3.4E-02 |
| N ₂ O | | | | 0.00132 | Federal Register ^c | 2.7E-02 | 6.8E-03 |
| CO ₂ e | | | | | Federal Register ^c | 3,362 | 841 |

(a) NSPS 40 CFR Part 60, Subapart IIII Limits

NSPS Limits - 40 CFR Part 60, Subapart IIII, (40 CFR 60.4202(a)(2) and 40 CFR 89.112 - Table 1)

| | NOx + VOM | CO | PM |
|---------|-----------|-----|------|
| g/kW-hr | 6.4 | 3.5 | 0.20 |
| g/hp-hr | 4.8 | 2.6 | 0.15 |

(b) AP-42 Section 3.4 (10/96) (c) Federal Register - Subpart C of Part 98

| Sulfuric Acid Mist | Conversion Percent | |
|---|--------------------|-------------------------|
| Assume 10% of SO ₂ is converted to SO ₃ | 10 | $SO_2 + 1/2 O_2 = SO_3$ |
| Assume 100% of SO ₃ is converted to H ₂ SO ₄ | 100 | $SO_3 + H_2O = H_2SO_4$ |

| Name | lb/hr SO ₂ | Ib/hr SO ₂ converted to SO ₃ | Ib/hr SO ₃ created | Ib/hr H ₂ SO ₄ created | tons/year H ₂ SO ₄ |
|----------------------------|-----------------------|---|----------------------------------|---|---|
| Auxiliary Boiler | 0.059 | 5.9E-03 | 7.4E-03 | 9.0E-03 | 3.9E-02 |
| Dew Point Heater | 5.9E-03 | 5.9E-04 | 7.4E-04 | 9.0E-04 | 3.9E-03 |
| Emergency Fire Pump | 0.58 | 5.8E-02 | 7.2E-02 | 8.9E-02 | 2.2E-02 |
| Emergency Diesel Generator | 0.02 | 0.00 | 0.00 | 0.00 | 6.9E-04 |

| Molecular Weights | | | | | | | | | |
|--------------------------------|------|--|--|--|--|--|--|--|--|
| SO ₂ | 64.1 | | | | | | | | |
| SO ₃ | 80.1 | | | | | | | | |
| H ₂ SO ₄ | 98.1 | | | | | | | | |
| | | | | | | | | | |

CO₂ Equivalent Ratios

| Gre | CO ₂ Equivalent Ratio | | |
|---------------------|-------------------------------------|------------------|---------------|
| Carbon Dioxide | 124-38-9 | CO ₂ | 1 |
| Methane | 74-82-8 | CH₄ | 25 |
| Nitrous Oxide | 10024-97-2 | N ₂ O | 298 |
| Hydrofluorocarbons | Various | CHF (various) | 12 - 11,700 |
| Perfluorocarbons | Various | CF (various) | 6500 - 17,340 |
| Sulfur Hexafluoride | 2551-62-4 | SF ₆ | 23,900 |
| Chlorofluorocarbons | Various | CCIF (various) | Not Available |

South Shore Energy, LLC - Nemadji Trail Energy Center Storage Tanks

| | | Size | VOC Emissions | 1 |
|---------------------------|-----------------|---------|------------------|-----------|
| Tank # | Material Stored | Gallons | lb/year | Tons/year |
| 1 - Day Tank | #2 Fuel Oil | 180,000 | 83.30 | 4.17E-02 |
| 2 - Diesel Generator Tank | #2 Fuel Oil | 1,700 | 0.48 | 2.40E-04 |
| 3 - Fire Pump Tank | #2 Fuel Oil | 350 | 0.1 | 5.00E-05 |
| | | | TOTAL: (tpy VOC) | 0.04 |

TANKS 4.0.9d Inputs

| | Day Tank | | Diesel Generator | Γank | Fire Pump Tank | |
|--------------------------------|--------------------------|-------|------------------------|-------|------------------------|-------|
| Description | Value Units | | Value | Units | Value | Units |
| Tank Type | Vertical Fixed Roof Tank | | Horizontal Tank | | Horizontal Tank | |
| Location (meteorological data) | Duluth, MN | | Duluth, MN | | Duluth, MN | |
| Tank Contents | Distillate Fuel Oil #2 | | Distillate Fuel Oil #2 | | Distillate Fuel Oil #2 | |
| Shell Height | 30.00 | ft | 8.04 | ft | 5.00 | ft |
| Diameter | 33.00 | ft | 6.00 | ft | 3.45 | ft |
| Avg. Liquid Height | 14.07 | | | | | |
| Volume | 180,042.51 | gal | 1,700 | gal | 350.0 | gal |
| Turnovers | 59.94 | | 20.83 | | 20.83 | |
| Net Throughput | 10,791,747.84 | gal | 35,360.00 | gal | 7291.55 | gal |
| Tank heated (y/n) | n | | n | | n | |
| Shell Color/Shade | White | | n | | n | |
| Shell Condition | Good | | White | | White | |
| Roof Color/Shade | White | | Good | | Good | |
| Roof Condition | Good | | | | | |
| Roof Type | Cone | | | | | |
| Roof Height | 5.00 | ft | | | | |
| Slope (Cone Roof) | 0.30 | ft/ft | | | | |
| Vacuum Settings (psig) | -0.03 | | -0.03 | | -0.03 | |
| Pressure Settings (psig) | 0.03 | | 0.03 | | 0.03 | |
| Working Loss | 69.18 | lb/yr | 0.34 | lb/yr | 0.07 | lb/yr |
| Breathing Loss | 14.11 | lb/yr | 0.14 | lb/yr | 0.03 | lb/yr |
| Total losses | 83.30 | lb/yr | 0.48 | lb/yr | 0.10 | lb/yr |
| Total Emissions | 4.17E-02 | tpy | 2.40E-04 | tpy | 5.00E-05 | tpy |

South Shore Energy, LLC - Nemadji Trail Energy Center Greenhouse Gas Emissions from SF_6 in Circuit Breakers

| Inputs | | | | | | | |
|---|--------|--|--|--|--|--|--|
| Number of 19 kV Generator Circuit Breakers | 2 | | | | | | |
| Quantity of SF ₆ in each 19 kV Breaker (lb) | 23.0 | | | | | | |
| Number of 345 kV Generator Circuit Breakers | 3 | | | | | | |
| Quantity of SF ₆ in each 345 kV Breaker (lb) | 687.0 | | | | | | |
| Global Warming Potential of SF6 (100yr) | 22,800 | | | | | | |

Fugitive Emissions of SF6 due to leakage

| | Number of Units | Quantity of SF ₆ per Breaker (lbs) | Emissions of SF ₆ Per Breaker ^a (lbs/yr) | Total SF ₆ Emissions (lbs/yr) | Global Warming Potential | Total CO₂e Emissions (tons/yr) |
|-----------------|--------------------|---|--|--|--------------------------------|--------------------------------------|
| 19 kV Breakers | 2 | 23.0 | 0.12 | 0.23 | 22,800 | 2.6 |
| 345 kV Breakers | 3 | 687.0 | 3.44 | 10.31 | 22,800 | 117.5 |
| Total | | | | 10.5 | | 120 |

⁽a) Based on a maximum SF₆ leakage rate of 0.5% per year

South Shore Energy, LLC - Nemadji Trail Energy Center Emissions from Paved Haul Roads

Paved Haul Road Emissions $E = k * (sL)^{0.91} * (W)^{1.02}$ Equation 1 from AP 42 Section where E is the particulate emission factor having the units matching k Equation 1 from AP 42 Section 13.2.1.3.

| Parameter | Value | Description of parameter |
|-----------|-----------|---|
| sL | 2.4 | Ubiquitous Silt Loading Default Value, g/m ² |
| W | see below | Mean vehicle weight [(loaded truck weight + unloaded truck weight)/2], tons |
| VMT | see below | Vehicle miles traveled (length traveled round trip) |
| VMT/hr | see below | Vehicle miles traveled per hour = VMT*maximum trips per hour |
| VMT/yr | see below | Vehicle miles traveled per year = VMT*maximum trips per year |

| | k |
|------------|----------|
| | (lb/VMT) |
| PM2.5 | 0.00054 |
| PM10 | 0.0022 |
| PM30 (TSP) | 0.011 |

Constant k, lb/VMT is from AP 42 Table 13.2.1-1 Notes:

| | | | Max# | Max # | VMT - Len | gth (round | Truck | Weight [□] | Factor "E" | Factor "F" | Factor "E" | Traveled | Travalad | Emi | ssions | Emis | sions | Emiss | sions | | | | | |
|---------------------------|--------------|-------|------------|--------------|------------|-------------|----------|---------------------|------------|------------|------------|----------|---------------------|----------------|-------------------------|-------------------|--------------|--------------|--------------|--------|------------|----------|-------------|-----------|
| | Vehicle Type | Paved | | | tri | p) | Loaded | Unloaded | | 1 dotor L | | | Traveled VMT/yr | Uncontrolled | Uncontrolled | Uncontrolled | Uncontrolled | Uncontrolled | Uncontrolled | | | | | |
| | | • • | rrips/nour | Trips/nour T | rrips/nour | i rips/nour | mps/nour | Trips/hour Trips | Trips/yr | meters | (miles) | tons | tons ID PIVI/VIVI I | ID PIVI/VIVI I | Ib PM10/VMT lb PM2.5/VI | ID PIVIZ.5/VIVI I | /VMT VMT/hr | VIVI I/yI | lb PM/hr | PM tpy | lb PM10/hr | PM10 tpy | lb PM2.5/hr | PM2.5 tpy |
| Miscellaneous Deliveries | generic haul | | | | | | | | | | | | | | | | | | | | | | | |
| paved (single-trip: loop) | truck | yes | 6 | 520 | 837 | 0.52 | 40 | 15 | 0.72 | 0.14 | 0.04 | 3.12 | 270.40 | 2.24 | 0.10 | 0.45 | 0.02 | 0.11 | 0.005 | | | | | |

⁽a) On average less than 10 trucks per week are expected for delivery or removal; therefore, 10 trucks per week * 52 weeks per year = 520 trips per year

⁽b) Based on generic truck weight of the trucks that will be traveling onsite

| | VOC | CO ₂ e |
|---|------|-------------------|
| Total Emissions from Piping Fugitives (tpy) | 10.4 | 976.6 |

| Natural Gas | | | | | VOC ^D | | | | | | |
|------------------|-------------|----------|---------------------------------------|---------------------------------|--|-------------------------------|---------------------------------|--|--------------|--|--|
| Natural Gas | Natural Gas | | | | | | | CO₂e ^{c,d} | | | |
| Equipment Type | Service | Quantity | Factor ^a (kg/hr/source) | Maximum emissions (lb/hr) | Maximum theoretical emissions (tpy) | Potential to emit (tpy) | Maximum emissions (lb/hr) | Maximum theoretical emissions (tpy) | Potential to | | |
| Connectors | Natural Gas | 279 | 2.00E-04 | 0.01 | 0.04 | 0.04 | 3.00 | 13.13 | 13.13 | | |
| Flanges | Natural Gas | 465 | 3.90E-04 | 0.03 | 0.12 | 0.12 | 9.75 | 42.68 | 42.68 | | |
| Open Ended Lines | Natural Gas | 30 | 2.00E-03 | 0.01 | 0.04 | 0.04 | 3.22 | 14.12 | 14.12 | | |
| Valves | Natural Gas | 856 | 4.50E-03 | 0.59 | 2.60 | 2.60 | 207.00 | 906.65 | 906.65 | | |
| | | | Total | 0.64 | 2.80 | 2.80 | 222.97 | 976.59 | 976.59 | | |

⁽a) 1995 Protocol for Equipment Leak Emission Estimates- EPA-453/R-95-017

93.00% minimum wt% methane

(c) Since methane is GHG, the maximum CO₂e is calculated at the maximum methane content.

97.50% maximum wt% methane

(d) Methane Global Warming Potential (40 CFR 98) was applied

25

| Fuel Oil | | | | | VOC ^b | | | |
|------------------|-----------|----------|---------------------------------------|---------------------------------|--|-------------------------------|--|--|
| 1 401 011 | i uci oli | | | | | | | |
| Equipment Type | Service | Quantity | Factor ^a (kg/hr/source) | Maximum emissions (lb/hr) | Maximum theoretical emissions (tpy) | Potential to emit (tpy) | | |
| Connectors | Light Oil | 52 | 2.10E-04 | 0.02 | 0.11 | 0.11 | | |
| Flanges | Light Oil | 420 | 1.10E-04 | 0.10 | 0.45 | 0.45 | | |
| Open Ended Lines | Light Oil | 0 | 1.40E-03 | 0.00 | 0.00 | 0.00 | | |
| Valves | Light Oil | 291 | 2.50E-03 | 1.60 | 7.02 | 7.02 | | |
| | | | Total | 1.73 | 7.58 | 7.58 | | |

⁽a) 1995 Protocol for Equipment Leak Emission Estimates- EPA-453/R-95-017

(b) Assume all emissions are VOC

Note: The 1995 Protocol for Equipment Leak Emission Rates is the most relevant calculation reference and is a reputable reference document that is widely referenced.

⁽b) Since methane is not a VOC, the maximum VOC is calculated at the minimum methane content.

South Shore Energy, LLC - Nemadji Trail Energy Center Combined Cycle HAPs Emissions - New Emission Sources

Hours of Operation Combustion Turbine Natural Gas Hours = 8,760 hours per year hours per year Combustion Turbine Fuel Oil Hours = Duct Burner = hours per year Auxillary Boiler = hours per year Natural Gas Heater = 8,760 hours per year Emergency Diesel Fire Pump = Emergency Diesel Generator = 500 500 hours per year hours per year

Natural Gas Usage 1,020 MMBtu/MMcf mmBtu/hr mmCF/hr Combustion Turbine (Natural Gas) = Combustion Turbine (Fuel Oil) = 3,021 0.987 Duct Burner = 1,006 100.0 Auxillary Boiler = 0.098 20.0 2 Natural Gas Heaters Natural Gas Heaters = 0.020 Emergency Diesel Fire Pump =

Total Facility: Hazardous Air Pollutants Emissions

| | Maximum |
|---------------------------|-----------|
| | Potential |
| | Emissions |
| HAP | tpy |
| 1st Maximum: Formaldehyde | 3.28 |
| 2nd Maximum: Toluene | 2.09 |
| 3rd Maximum: Xylene | 1.03 |
| All HAPs | 9.33 |

| | | | Natural | l Gas - Internal C | ombustion | Fuel O | il - Internal Coml | bustion | | | Natural G | ias- External C | Combustion | | | | | Fue | el Oil | | | |
|------------------------------|------------|--------|----------|--------------------|-------------------|----------|--------------------|-----------------|-----------------|--------------------|---------------------|--------------------|------------------------|------------|-------------------------|-----------------|---------------|----------------------------|-----------------|---------------|---------------|--------------------|
| | CAS | | C | Combustion Turk | bine ^a | Co | ombustion Turbi | ne ^a | Emission Factor | Duct E | Burner ^b | Auxillaı | ry Boiler ^b | Natural Ga | as Heaters ^b | Emission Factor | Emergency Die | sel Fire Pump ^c | Emission Factor | Emergency Die | sel Generator | r ^d Tot |
| Chemical | | POM? | lb/MMBtu | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | lb/MMcf | lb/hr | tpy | lb/hr | tpy | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | l tp |
| -Methylnaphthalene | 97-57-6 | POM | | | ., | | | 1,2 | 2.4E-05 | 2.4E-05 | 0.0E+00 | 2.4E-06 | 1.0E-05 | 4.7E-07 | 2.1E-06 | | | | | | | 1.2E |
| Methylchloranthrene | 56-49-5 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | | | | | | | 9.3E |
| 12-Dimethylbenz(a)anthracene | | POM | | | | | | | 1.6E-05 | 1.6E-05 | 0.0E+00 | 1.6E-06 | 6.9E-06 | 3.1E-07 | 1.4E-06 | | | | | | | 8.2 |
| cenaphthene | 83-32-9 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 1.42E-06 | 2.8E-06 | 6.9E-07 | 4.68E-06 | 9.6E-05 | 2.4E-05 | 2.6 |
| cenaphthylene | 203-96-8 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 5.06E-06 | 9.9E-06 | 2.5E-06 | 9.23E-06 | 1.9E-04 | 4.7E-05 | 5.1 |
| cetaldehyde | 75-07-0 | | 4.0E-05 | 1.5E-01 | 6.4E-01 | | | | | | | | | | | 7.67E-04 | 1.5E-03 | 3.7E-04 | 2.52E-05 | 5.2E-04 | 1.3E-04 | 6.4 |
| crolein | 107-02-8 | | 6.4E-06 | 2.3E-02 | 1.0E-01 | | | | | | | | | | | 9.25E-05 | 1.8E-04 | 4.5E-05 | 7.88E-06 | 1.6E-04 | 4.0E-05 | 1.0 |
| nthracene | 120-12-7 | POM | | | | | | | 2.4E-06 | 2.4E-06 | 0.0E+00 | 2.4E-07 | 1.0E-06 | 4.7E-08 | 2.1E-07 | 1.87E-06 | 3.6E-06 | 9.1E-07 | 1.23E-06 | 2.5E-05 | 6.3E-06 | 8.5 |
| rsenic | 7440-38-2 | | | | | 1.1E-05 | 3.3E-02 | 0.0E+00 | 2.0E-04 | 2.0E-04 | 0.0E+00 | 2.0E-05 | 8.6E-05 | 3.9E-06 | 1.7E-05 | | | | | | | 1.0 |
| enz(a)anthracene | 56-55-3 | POM | | | | 2 00 | 0.02 02 | 0.02 00 | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 1.68E-06 | 3.3E-06 | 8.2E-07 | 6.22E-07 | 1.3E-05 | 3.2E-06 | 4.9 |
| enzene | 71-43-2 | | 1.2E-05 | 4.4E-02 | 1.9E-01 | 5.5E-05 | 1.7E-01 | 0.0E+00 | 2.1E-03 | 2.1E-03 | 0.0E+00 | 2.1E-04 | 9.0E-04 | 4.1E-05 | 1.8E-04 | 9.33E-04 | 1.8E-03 | 4.5E-04 | 7.76E-04 | 1.6E-02 | 4.0E-03 | 2.0 |
| enzo(a)pyrene | 50-32-8 | POM | 1.22 00 | 7.72 02 | 1.02 01 | 0.0L 00 | 1.72 01 | 0.02.100 | 1.2E-06 | 1.2E-06 | 0.0E+00 | 1.2E-07 | 5.2E-07 | 2.4E-08 | 1.0E-07 | 1.88E-07 | 3.7E-07 | 9.2E-08 | 2.57E-07 | 5.3E-06 | 1.3E-06 | 2.0 |
| enzo(b)fluoranthene | 205-99-2 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 9.91E-08 | 1.9E-07 | 4.8E-08 | 1.11E-06 | 2.3E-05 | 5.7E-06 | 6.7 |
| enzo(g,h,l)perylene | 191-24-2 | POM | | | | | | | 1.2E-06 | 1.2E-06 | 0.0E+00 | 1.2E-07 | 5.2E-07 | 2.4E-08 | 1.0E-07 | 4.89E-07 | 9.5E-07 | 2.4E-07 | 5.56E-07 | 1.1E-05 | 2.9E-06 | 3.7 |
| enzo(k)fluoranthene | 205-82-3 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 1.55E-07 | 3.0E-07 | 7.6E-08 | 2.18E-07 | 4.5E-06 | 1.1E-06 | 2.1 |
| ervllium | 7440-41-7 | I OIVI | | | | 3.1E-07 | 9.4E-04 | 0.0E+00 | 1.2E-05 | 1.2E-05 | 0.0E+00 | 1.2E-06 | 5.2E-06 | 2.4E-07 | 1.0E-06 | 1.33L=01 | 3.0L-01 | 7.0L-00 | 2.10L=01 | 4.3L-00 | 1.12-00 | 6.2 |
| 3-Butadiene | 106-99-0 | | 4.3E-07 | 1.6E-03 | 6.9E-03 | 1.6E-05 | 9.4E-04 4.8E-02 | 0.0E+00 | 1.2E-03 | 1.2E-05 | 0.0E+00 | 1.2E-00 | 5.2E-00 | 2.46-07 | 1.0E-00 | 3.91E-05 | 7.6E-05 | 1.9E-05 | | | $\overline{}$ | 6.9 |
| admium | 7440-43-7 | | 4.3L-07 | 1.0L-03 | 0.9L=03 | 4.8E-06 | 1.5E-02 | 0.0E+00 | 1.1E-03 | 1.1E-03 | 0.0E+00 | 1.1E-04 | 4.7E-04 | 2.2E-05 | 9.4E-05 | 3.91L-03 | 7.0L-03 | 1.9L-03 | | | $\overline{}$ | 5.7 |
| hromium | 7440-43-7 | | | | | 1.1E-05 | 3.3E-02 | 0.0E+00 | 1.4E-03 | 1.4E-03 | 0.0E+00 | 1.4E-04 | 6.0E-04 | 2.7E-05 | 1.2E-04 | | | | | | _ | 7.2 |
| | | DOM | | | | 1.1E-05 | 3.3E-02 | 0.0⊑+00 | 1.4E-03 | 1.4E-03 1.8E-06 | 0.0E+00 | 1.4E-04 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.2E-04 1.5E-07 | 3.53E-07 | 6.9E-07 | 1.7E-07 | 1.53E-06 | 3.1E-05 | 7.9E-06 | |
| hrysene | 218-01-9 | POM | | | | | | | | | | | | | | 3.53E-07 | 6.9E-07 | 1./E-0/ | 1.53E-06 | 3.1E-05 | 7.9E-06 | 9.0 |
| obalt | 7440-48-4 | 2011 | | | | | | | 8.4E-05 | 8.3E-05 | 0.0E+00 | 8.2E-06 | 3.6E-05 | 1.6E-06 | 7.2E-06 | | 4.45.00 | 0.05.05 | 2 125 25 | 7.15.00 | 4 | 4.3 |
| ibenzo(a,h)anthracene | 53-70-3 | POM | | | | | | | 1.2E-06 | 1.2E-06 | 0.0E+00 | 1.2E-07 | 5.2E-07 | 2.4E-08 | 1.0E-07 | 5.83E-07 | 1.1E-06 | 2.8E-07 | 3.46E-07 | 7.1E-06 | 1.8E-06 | 2.7 |
| ichlorobenzene | 25321-22-6 | | | | | | | | 1.2E-03 | 1.2E-03 | 0.0E+00 | 1.2E-04 | 5.2E-04 | 2.4E-05 | 1.0E-04 | | | | | | | 6.2 |
| thyl benzene | 100-41-4 | | 3.2E-05 | 1.2E-01 | 5.1E-01 | | | | | | | | | | | | | | | | | 5.1 |
| luoranthene | 206-44-0 | POM | | | | | | | 3.0E-06 | 3.0E-06 | 0.0E+00 | 2.9E-07 | 1.3E-06 | 5.9E-08 | 2.6E-07 | 7.61E-06 | 1.5E-05 | 3.7E-06 | 4.03E-06 | 8.3E-05 | 2.1E-05 | 2.6 |
| luorene | 86-73-7 | POM | | | | | | | 2.8E-06 | 2.8E-06 | 0.0E+00 | 2.7E-07 | 1.2E-06 | 5.5E-08 | 2.4E-07 | 2.92E-05 | 5.7E-05 | 1.4E-05 | 1.28E-05 | 2.6E-04 | 6.6E-05 | 8.11 |
| ormaldehyde | 50-00-0 | | 2.0E-04 | 7.4E-01 | 3.2E+00 | 2.8E-04 | 8.5E-01 | 0.0E+00 | 7.5E-02 | 7.4E-02 | 0.0E+00 | 7.4E-03 | 3.2E-02 | 1.5E-03 | 6.4E-03 | 1.18E-03 | 2.3E-03 | 5.8E-04 | 7.89E-05 | 1.6E-03 | 4.1E-04 | 3.3E |
| lexane | 110-54-3 | | | | | | | | 1.8E+00 | 1.8E+00 | 0.0E+00 | 1.8E-01 | 7.7E-01 | 3.5E-02 | 1.5E-01 | | | | | | | 9.3 |
| ideno(1,2,3-cd)pyrene | 193-39-5 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 3.75E-07 | 7.3E-07 | 1.8E-07 | 4.14E-07 | 8.5E-06 | 2.1E-06 | 3.2 |
| langanese | 7439-96-5 | | | | | 7.9E-04 | 2.4E+00 | 0.0E+00 | 3.8E-04 | 3.7E-04 | 0.0E+00 | 3.7E-05 | 1.6E-04 | 7.5E-06 | 3.3E-05 | | | | | | | 2.0 |
| 1ercury | 7439-97-6 | | | | | 1.2E-06 | 3.6E-03 | 0.0E+00 | 2.6E-04 | 2.6E-04 | 0.0E+00 | 2.5E-05 | 1.1E-04 | 5.1E-06 | 2.2E-05 | | | | | | | 1.3E |
| aphthalene | 91-20-3 | | 1.3E-06 | 4.8E-03 | 2.1E-02 | 3.5E-05 | 1.1E-01 | 0.0E+00 | 6.1E-04 | 6.0E-04 | 0.0E+00 | 6.0E-05 | 2.6E-04 | 1.2E-05 | 5.2E-05 | 8.48E-05 | 1.7E-04 | 4.1E-05 | 1.30E-04 | 2.7E-03 | 6.7E-04 | 2.2 |
| lickel | 7440-02-0 | | | | | 4.6E-06 | 1.4E-02 | 0.0E+00 | 2.1E-03 | 2.1E-03 | 0.0E+00 | 2.1E-04 | 9.0E-04 | 4.1E-05 | 1.8E-04 | | | | | | | 1.18 |
| AH | | | 2.2E-06 | 8.1E-03 | 3.5E-02 | 4.0E-05 | 1.2E-01 | 0.0E+00 | | | | | | | | | | | | | | 3.5 |
| henanathrene | 85-01-8 | POM | | | | | | 1 | 1.7E-05 | 1.7E-05 | 0.0E+00 | 1.7E-06 | 7.3E-06 | 3.3E-07 | 1.5E-06 | 2.94E-05 | 5.7E-05 | 1.4E-05 | 4.08E-05 | 8.4E-04 | 2.1E-04 | 2.3 |
| ropylene | 1 22 2 . 0 | | | | | | | | = | | | | 1112 | | | 2.58E-03 | 5.0E-03 | 1.3E-03 | 2.79E-03 | 5.7E-02 | 1.4E-02 | 1.6 |
| roplylene Oxide | 75-56-9 | | 2.9E-05 | 1.1E-01 | 4.7E-01 | | | | | | | | | | | 2.002.00 | 0.02 00 | | 202 00 | <u> </u> | | 4.7 |
| vrene | 129-00-0 | POM | 2.02 00 | | 7.7 = 01 | | | | 5.0E-06 | 4.9E-06 | 0.0E+00 | 4.9E-07 | 2.1E-06 | 9.8E-08 | 4.3E-07 | 4.78E-06 | 9.3E-06 | 2.3E-06 | 3.71E-06 | 7.6E-05 | 1.9E-05 | 2.4 |
| | 7782-49-2 | FOW | | | | 2.5E-05 | 7.6E-02 | 0.0E+00 | 2.4E-05 | 2.4E-05 | 0.0E+00 | 2.4E-06 | 1.0E-05 | 4.7E-07 | 2.1E-06 | 4.70E-00 | 9.3E-00 | Z.JE-00 | 3.7 TE-00 | 7.02-03 | 1.9E-03 | 1.2 |
| elenium | | | 4.05.04 | 4.05.04 | 0.45+00 | 2.5E-U5 | 7.0E-UZ | 0.0⊑+00 | | | | | | | | 4.005.04 | 0.05.04 | 0.05.04 | 0.045.04 | F 0F 00 | 4.45.60 | |
| oluene | 108-88-3 | | 1.3E-04 | 4.8E-01 | 2.1E+00 | | | | 3.4E-03 | 3.4E-03 | 0.0E+00 | 3.3E-04 | 1.5E-03 | 6.7E-05 | 2.9E-04 | 4.09E-04 | 8.0E-04 | 2.0E-04 | 2.81E-04 | 5.8E-03 | 1.4E-03 | 2.1 |
| ylene | 1330-20-7 | | 6.4E-05 | 2.3E-01 | 1.0E+00 | | | | | | | | | | | 2.85E-04 | 5.6E-04 | 1.4E-04 | 1.93E-04 | 4.0E-03 | 9.9E-04 | 1.0 |
| | | TOTAL | | 1.90 | 8.34 | | 3.85 | 0.00 | | 1.86 | 0.00 | 0.19 | 0.81 | 0.04 | 1.6E-01 | | 1.3E-02 | 3.1E-03 | | | | 9. |

(a) Emission factors for combustion turbines from AP-42 Section 3.1, Updated 2/2000. Formaldehyde emission factor from Sims Roy EPA Memo "Hazardous Air Pollutant (HAP) Emission Control Technology for New Stationary Combustion Turbines" 8/21/2001.

⁽c) Emission factors from AP-42 Section 3.3, Updated 10/1996 (d) Emission factors from AP-42 Section 3.4, Updated 10/1996

| | | | Natural G | ias - Internal Co | mbustion | Fuel C | il - Internal Com | bustion | | | Natural G | as- External Co | ombustion | | | | | Fue | el Oil | | | |
|----------|-----|------|-----------|-------------------|-----------------|----------|-------------------|-----------------|-----------------|---------|---------------------|-----------------|-----------------------|------------|------------------------|-----------------|----------------|----------------------------|------------------------|----------------|---------------------------|---------|
| | | | Co | mbustion Turbi | ne ^a | | mbustion Turbi | ne ^a | Emission Factor | Duct B | Burner ^b | | / Boiler ^b | Natural Ga | s Heaters ^b | Emission Factor | Emergency Dies | sel Fire Pump ^c | Emission Factor | Emergency Dies | el Generator ^d | Total |
| Chemical | CAS | POM? | lb/MMBtu | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | lb/mmCF | lb/hr | tpy | lb/hr | tpy | lb/hr | tpy | lb/mmCF | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | tpy |
| Lead | | | | | | 1.4E-05 | 4.2E-02 | 0.0E+00 | 5.0E-04 | 4.9E-04 | 0.0E+00 | 4.9E-05 | 2.1E-04 | 9.8E-06 | 4.3E-05 | | | | | | | 2.6E-04 |

⁽a) Emission factors for combustion turbines from AP-42 Section 3.1, Updated 2/2000. Formaldehyde emission factor from Sims Roy EPA Memo "Hazardous Air Pollutant (HAP) Emission Control Technology for New Stationary Combustion Turbines" 8/21/2001.

⁽b) Emission factors from AP-42 Section 1.4, Updated 7/1998

⁽b) Emission factors from AP-42 Section 1.4, Updated 7/1998

⁽c) Emission factors from AP-42 Section 3.3, Updated 10/1996 (d) Emission factors from AP-42 Section 3.4, Updated 10/1996

South Shore Energy, LLC - Nemadji Trail Energy Center Combined Cycle HAPs Emissions - New Emission Sources

Hours of Operation Combustion Turbine Natural Gas Hours = hours per year hours per year Combustion Turbine Fuel Oil Hours = Duct Burner = hours per year Auxillary Boiler = hours per year Natural Gas Heater = 8,760 hours per year Emergency Diesel Fire Pump = Emergency Diesel Generator = hours per year hours per year

| Natural Gas Usage | | | |
|------------------------------------|----------|---------|-----------------------|
| _ | mmBtu/hr | mmCF/hr | 1,020 MMBtu/MMcf |
| Combustion Turbine (Natural Gas) = | 3,665 | | |
| Combustion Turbine (Fuel Oil) = | 3,021 | | |
| Duct Burner = | 1,006 | 0.987 | |
| Auxillary Boiler = | 100.0 | 0.098 | |
| Natural Gas Heater = | 20.0 | 0.020 | 2 Natural Gas Heaters |
| Emergency Diesel Fire Pump = | 1.95 | | |
| Emergency Diesel Generator = | 20.6 | | |

Total Facility: Hazardous Air Pollutants Emissions

| | Maximum Potential |
|---------------------------|----------------------|
| | Emissions |
| HAP | tpy |
| 1st Maximum: Hexane | 8.71 |
| 2nd Maximum: Formaldehyde | 0.36 |
| 3rd Maximum: Toluene | 0.02 |
| All HAPs | 9.16 |

| | | | Natural | Gas - Internal C | Combustion | Fuel C | il - Internal Comb | oustion | | | Natural G | as- External C | ombustion | | | | | Fue | el Oil | | | 1 |
|---------------------------------------|------------|-------|----------|------------------|-------------------|----------|--------------------|-----------------|--------------------|--------------------|---------------------|--------------------|-----------------------|--------------------|-------------------------|-----------------|---------------|----------------------------|-----------------|---------------|----------------------------|-------------------|
| | CAS | | C | Combustion Turl | bine ^a | Co | ombustion Turbi | ne ^a | Emission Factor | Duct | Burner ^b | Auxillar | y Boiler ^b | Natural Ga | as Heaters ^b | Emission Factor | Emergency Die | sel Fire Pump ^c | Emission Factor | Emergency Die | sel Generator ^o | r ^d To |
| Chemical | | POM? | lb/MMBtu | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | lb/MMcf | lb/hr | tpy | lb/hr | tpy | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | t |
| lethylnaphthalene | 97-57-6 | POM | | | | | | 1. | 2.4E-05 | 2.4E-05 | 1.0E-04 | 2.4E-06 | 1.0E-05 | 4.7E-07 | 2.1E-06 | | | 1.5 | | | 1.5 | 1.2 |
| lethylchloranthrene | 56-49-5 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.8E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | | | | | | | 8.7 |
| 2-Dimethylbenz(a)anthracene | | POM | | | | | | | 1.6E-05 | 1.6E-05 | 6.9E-05 | 1.6E-06 | 6.9E-06 | 3.1E-07 | 1.4E-06 | | | | | | | 7.7 |
| enaphthene | 83-32-9 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.8E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 1.42E-06 | 2.8E-06 | 6.9E-07 | 4.68E-06 | 9.6E-05 | 2.4E-05 | 3. |
| naphthylene | 203-96-8 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.8E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 5.06E-06 | 9.9E-06 | 2.5E-06 | 9.23E-06 | 1.9E-04 | 4.7E-05 | 5. |
| taldehyde | 75-07-0 | | 4.0E-05 | 1.5E-01 | 0.0E+00 | | | | | | | | | | | 7.67E-04 | 1.5E-03 | 3.7E-04 | 2.52E-05 | 5.2E-04 | 1.3E-04 | 5. |
| olein | 107-02-8 | | 6.4E-06 | 2.3E-02 | 0.0E+00 | | | | | | | | | | | 9.25E-05 | 1.8E-04 | 4.5E-05 | 7.88E-06 | 1.6E-04 | 4.0E-05 | 8. |
| hracene | 120-12-7 | POM | | | | | | | 2.4E-06 | 2.4E-06 | 1.0E-05 | 2.4E-07 | 1.0E-06 | 4.7E-08 | 2.1E-07 | 1.87E-06 | 3.6E-06 | 9.1E-07 | 1.23E-06 | 2.5E-05 | 6.3E-06 | 1. |
| senic | 7440-38-2 | | | | | 1.1E-05 | 3.3E-02 | 0.0E+00 | 2.0E-04 | 2.0E-04 | 8.6E-04 | 2.0E-05 | 8.6E-05 | 3.9E-06 | 1.7E-05 | | | | | | | 9. |
| nz(a)anthracene | 56-55-3 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.8E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 1.68E-06 | 3.3E-06 | 8.2E-07 | 6.22E-07 | 1.3E-05 | 3.2E-06 | 1. |
| nzene | 71-43-2 | | 1.2E-05 | 4.4E-02 | 0.0E+00 | 5.5E-05 | 1.7E-01 | 0.0E+00 | 2.1E-03 | 2.1E-03 | 9.1E-03 | 2.1E-04 | 9.0E-04 | 4.1E-05 | 1.8E-04 | 9.33E-04 | 1.8E-03 | 4.5E-04 | 7.76E-04 | 1.6E-02 | 4.0E-03 | 1. |
| nzo(a)pyrene | 50-32-8 | POM | | | | | | | 1.2E-06 | 1.2E-06 | 5.2E-06 | 1.2E-07 | 5.2E-07 | 2.4E-08 | 1.0E-07 | 1.88E-07 | 3.7E-07 | 9.2E-08 | 2.57E-07 | 5.3E-06 | 1.3E-06 | 7. |
| nzo(b)fluoranthene | 205-99-2 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.8E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 9.91E-08 | 1.9E-07 | 4.8E-08 | 1.11E-06 | 2.3E-05 | 5.7E-06 | 1. |
| nzo(q,h,l)perylene | 191-24-2 | POM | | | | | | | 1.2E-06 | 1.2E-06 | 5.2E-06 | 1.2E-07 | 5.2E-07 | 2.4E-08 | 1.0E-07 | 4.89E-07 | 9.5E-07 | 2.4E-07 | 5.56E-07 | 1.1E-05 | 2.9E-06 | 8. |
| nzo(k)fluoranthene | 205-82-3 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.8E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 1.55E-07 | 3.0E-07 | 7.6E-08 | 2.18E-07 | 4.5E-06 | 1.1E-06 | 9. |
| vilium | 7440-41-7 | | | | | 3.1E-07 | 9.4E-04 | 0.0E+00 | 1.2E-05 | 1.2E-05 | 5.2E-05 | 1.2E-06 | 5.2E-06 | 2.4E-07 | 1.0E-06 | 1.002 01 | 0.02 01 | 1.02 00 | 2.102 01 | | 2 00 | 5. |
| -Butadiene | 106-99-0 | | 4.3E-07 | 1.6E-03 | 0.0E+00 | 1.6E-05 | 4.8E-02 | 0.0E+00 | 1.22 00 | 1.22 00 | 0.EE 00 | 1.22 00 | O.EL OO | 2.42 07 | 1.02 00 | 3.91E-05 | 7.6E-05 | 1.9E-05 | | | | 1. |
| dmium | 7440-43-7 | | 1.02 07 | 1.02 00 | 0.02.00 | 4.8E-06 | 1.5E-02 | 0.0E+00 | 1.1E-03 | 1.1E-03 | 4.8E-03 | 1.1E-04 | 4.7E-04 | 2.2E-05 | 9.4E-05 | 0.012 00 | 1.02 00 | 1.02 00 | | | | 5. |
| romium | 7440-47-3 | | | | | 1.1E-05 | 3.3E-02 | 0.0E+00 | 1.4E-03 | 1.4E-03 | 6.0E-03 | 1.4E-04 | 6.0E-04 | 2.7E-05 | 1.2E-04 | | | | | | 1 | 6. |
| rysene | 218-01-9 | POM | | | | 1.1L-03 | 3.3L-02 | 0.02100 | 1.8E-06 | 1.8E-06 | 7.8E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 3.53E-07 | 6.9E-07 | 1.7E-07 | 1.53E-06 | 3.1E-05 | 7.9E-06 | 1. |
| balt | 7440-48-4 | FOW | | | | | | | 8.4E-05 | 8.3E-05 | 3.6E-04 | 8.2E-06 | 3.6E-05 | 1.6E-06 | 7.2E-06 | 3.33E-01 | 0.9E-07 | 1.7 E-07 | 1.55E-00 | 3. IE-03 | 7.9E-00 | 4. |
| | 53-70-3 | POM | | | | | | | 1.2E-06 | 1.2E-06 | 5.2E-06 | 1.2E-07 | 5.2E-07 | 2.4E-08 | 1.0E-07 | 5.83E-07 | 1.1E-06 | 2.8E-07 | 3.46E-07 | 7.1E-06 | 1.8E-06 | 7.9 |
| penzo(a,h)anthracene chlorobenzene | 25321-22-6 | POW | | | | | | | 1.2E-06 1.2E-03 | 1.2E-06 1.2E-03 | 5.2E-06 5.2E-03 | 1.2E-07 1.2E-04 | 5.2E-07 5.2E-04 | 2.4E-06 2.4E-05 | 1.0E-07 1.0E-04 | 5.03E-07 | 1.1E-00 | 2.0E-07 | 3.40⊑-07 | 7.1E-00 | 1.0E-00 | 5.8 |
| | 100-41-4 | | 2.05.05 | 1.2E-01 | 0.0E+00 | | | | 1.2E-03 | 1.2E-03 | 5.2E-03 | 1.2E-04 | 5.2E-04 | 2.4E-05 | 1.0E-04 | | | | | | | 0.0 |
| nyl benzene | 206-44-0 | POM | 3.2E-05 | 1.2E-01 | 0.0E+00 | | | | 3.0E-06 | 3.0E-06 | 1.3E-05 | 2.9E-07 | 1.3E-06 | 5.9E-08 | 2.6E-07 | 7.61E-06 | 1.5E-05 | 3.7E-06 | 4.03E-06 | 8.3E-05 | 2.1E-05 | 3.9 |
| uoranthene | | | | | | | | | | | | | | | | | | | | | | |
| iorene | 86-73-7 | POM | 0.05.04 | 7.45.04 | 0.05.00 | 0.05.04 | 0.55.04 | 0.05.00 | 2.8E-06 | 2.8E-06 | 1.2E-05 | 2.7E-07 | 1.2E-06 | 5.5E-08 | 2.4E-07 | 2.92E-05 | 5.7E-05 | 1.4E-05 | 1.28E-05 | 2.6E-04 | 6.6E-05 | 9.4 |
| rmaldehyde | 50-00-0 | | 2.0E-04 | 7.4E-01 | 0.0E+00 | 2.8E-04 | 8.5E-01 | 0.0E+00 | 7.5E-02 | 7.4E-02 | 3.2E-01 | 7.4E-03 | 3.2E-02 | 1.5E-03 | 6.4E-03 | 1.18E-03 | 2.3E-03 | 5.8E-04 | 7.89E-05 | 1.6E-03 | 4.1E-04 | 3.6 |
| xane | 110-54-3 | BOM | | | | | | | 1.8E+00 | 1.8E+00 | 7.8E+00 | 1.8E-01 | 7.7E-01 | 3.5E-02 | 1.5E-01 | 0.755.07 | 7.05.07 | 4.05.07 | 4.445.07 | 0.55.00 | 0.45.00 | 8.7 |
| leno(1,2,3-cd)pyrene | 193-39-5 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.8E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 3.75E-07 | 7.3E-07 | 1.8E-07 | 4.14E-07 | 8.5E-06 | 2.1E-06 | 1.1 |
| inganese | 7439-96-5 | | | | | 7.9E-04 | 2.4E+00 | 0.0E+00 | 3.8E-04 | 3.7E-04 | 1.6E-03 | 3.7E-05 | 1.6E-04 | 7.5E-06 | 3.3E-05 | | | | | | | 1.8 |
| ercury | 7439-97-6 | | | | | 1.2E-06 | 3.6E-03 | 0.0E+00 | 2.6E-04 | 2.6E-04 | 1.1E-03 | 2.5E-05 | 1.1E-04 | 5.1E-06 | 2.2E-05 | | | | | | | 1.3 |
| phthalene | 91-20-3 | | 1.3E-06 | 4.8E-03 | 0.0E+00 | 3.5E-05 | 1.1E-01 | 0.0E+00 | 6.1E-04 | 6.0E-04 | 2.6E-03 | 6.0E-05 | 2.6E-04 | 1.2E-05 | 5.2E-05 | 8.48E-05 | 1.7E-04 | 4.1E-05 | 1.30E-04 | 2.7E-03 | 6.7E-04 | 3. |
| ckel | 7440-02-0 | | | | | 4.6E-06 | 1.4E-02 | 0.0E+00 | 2.1E-03 | 2.1E-03 | 9.1E-03 | 2.1E-04 | 9.0E-04 | 4.1E-05 | 1.8E-04 | | | | | | | 1.0 |
| \H | | | 2.2E-06 | 8.1E-03 | 0.0E+00 | 4.0E-05 | 1.2E-01 | 0.0E+00 | | | | | | | | | | | | | | 0.0 |
| enanathrene | 85-01-8 | POM | | | | | | | 1.7E-05 | 1.7E-05 | 7.3E-05 | 1.7E-06 | 7.3E-06 | 3.3E-07 | 1.5E-06 | 2.94E-05 | 5.7E-05 | 1.4E-05 | 4.08E-05 | 8.4E-04 | 2.1E-04 | 3.1 |
| ppylene | | | | | | | | | | | | | | | | 2.58E-03 | 5.0E-03 | 1.3E-03 | 2.79E-03 | 5.7E-02 | 1.4E-02 | 1.6 |
| pplylene Oxide | 75-56-9 | | 2.9E-05 | 1.1E-01 | 0.0E+00 | | | | | | | | | | | | | | | | | 0.0 |
| ene | 129-00-0 | POM | | | | | | | 5.0E-06 | 4.9E-06 | 2.2E-05 | 4.9E-07 | 2.1E-06 | 9.8E-08 | 4.3E-07 | 4.78E-06 | 9.3E-06 | 2.3E-06 | 3.71E-06 | 7.6E-05 | 1.9E-05 | 4. |
| lenium | 7782-49-2 | | | | | 2.5E-05 | 7.6E-02 | 0.0E+00 | 2.4E-05 | 2.4E-05 | 1.0E-04 | 2.4E-06 | 1.0E-05 | 4.7E-07 | 2.1E-06 | 52 55 | 0.02 00 | 2.02.00 | 02 00 | | | 1 |
| uene | 108-88-3 | | 1.3E-04 | 4.8E-01 | 0.0E+00 | 2.02.00 | 7.02.02 | 0.02.00 | 3.4E-03 | 3.4E-03 | 1.5E-02 | 3.3E-04 | 1.5E-03 | 6.7E-05 | 2.9E-04 | 4.09E-04 | 8.0E-04 | 2.0E-04 | 2.81E-04 | 5.8E-03 | 1.4E-03 | 1. |
| ene | 1330-20-7 | | 6.4E-05 | 2.3E-01 | 0.0E+00 | | | | J.4L-03 | J.4L-03 | 1.JL=02 | J.JL=04 | 1.52-03 | 0.7 L=03 | 2.3L=04 | 2.85E-04 | 5.6E-04 | 1.4E-04 | 1.93E-04 | 4.0E-03 | 9.9E-04 | 1. |
| IOIIO | 1330-20-7 | TOTAL | | 1.90 | 0.02+00 | | 3.85 | 0.00 | | 1.86 | 8.16 | 0.19 | 0.81 | 0.04 | 1.6E-01 | 2.00L=04 | 1.3E-02 | 3.1E-03 | 1.33L=04 | 4.01-03 | 3.3∟-04 | 1. |

(a) Emission factors for combustion turbines from AP-42 Section 3.1, Updated 2/2000. Formaldehyde emission factor from Sims Roy EPA Memo "Hazardous Air Pollutant (HAP) Emission Control Technology for New Stationary Combustion Turbines" 8/21/2001.

| | | | Natural G | as - Internal Co | mbustion | Fuel O | il - Internal Com | bustion | | | Natural G | as- External Co | ombustion | | | | | Fue | l Oil | | | |
|----------|-----|------|-----------|------------------|-----------------|----------|-------------------|-----------------|-----------------|---------|---------------------|-----------------|-----------------------|-------------|------------------------|-----------------|----------------|----------------------------|------------------------|-----------------|--------------------------|---------|
| | | | Co | mbustion Turbi | ne ^a | | mbustion Turbi | ne ^a | Emission Factor | Duct B | Burner ^b | | / Boiler ^b | Natural Gas | s Heaters ^b | Emission Factor | Emergency Dies | sel Fire Pump ^c | Emission Factor | Emergency Diese | l Generator ^d | Total |
| Chemical | CAS | POM? | lb/MMBtu | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | lb/mmCF | lb/hr | tpy | lb/hr | tpy | lb/hr | tpy | lb/mmCF | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | tpy |
| Lead | | | | | | 1.4E-05 | 4.2E-02 | 0.0E+00 | 5.0E-04 | 4.9E-04 | 2.2E-03 | 4.9E-05 | 2.1E-04 | 9.8E-06 | 4.3E-05 | | | | | | | 2.4E-03 |

⁽a) Emission factors for combustion turbines from AP-42 Section 3.1, Updated 2/2000. Formaldehyde emission factor from Sims Roy EPA Memo "Hazardous Air Pollutant (HAP) Emission Control Technology for New Stationary Combustion Turbines" 8/21/2001.

⁽b) Emission factors from AP-42 Section 1.4, Updated 7/1998

⁽c) Emission factors from AP-42 Section 3.3, Updated 10/1996 (d) Emission factors from AP-42 Section 3.4, Updated 10/1996

⁽b) Emission factors from AP-42 Section 1.4, Updated 7/1998 (c) Emission factors from AP-42 Section 3.3, Updated 10/1996 (d) Emission factors from AP-42 Section 3.4, Updated 10/1996

South Shore Energy, LLC - Nemadji Trail Energy Center Combined Cycle HAPs Emissions - New Emission Sources

Hours of Operation Combustion Turbine Natural Gas Hours = hours per year hours per year Combustion Turbine Fuel Oil Hours = Duct Burner = 8,260 hours per year Auxillary Boiler = hours per year Natural Gas Heater = 8,760 hours per year

| Emergency Diesel Fire Pump = | 500 | hours per year | |
|------------------------------------|----------|----------------|-----------------------|
| Emergency Diesel Generator = | 500 | hours per year | |
| | | | |
| atural Gas Usage | | | |
| _ | mmBtu/hr | mmCF/hr | 1,020 MMBtu/MMcf |
| | | | |
| Combustion Turbine (Natural Gas) = | 3,665 | | |
| Combustion Turbine (Fuel Oil) = | 3,021 | | |
| Duct Burner = | 1,006 | 0.987 | |
| Auxillary Boiler = | 100.0 | 0.098 | |
| Natural Gas Heater = | 20.0 | 0.020 | 2 Natural Gas Heaters |

Total Facility: Hazardous Air Pollutants Emissions

| | Maximum |
|---------------------------|-----------|
| | Potential |
| | Emissions |
| HAP | tpy |
| 1st Maximum: Hexane | 8.26 |
| 2nd Maximum: Manganese | 0.60 |
| 3rd Maximum: Formaldehyde | 0.56 |
| All HAPs | 9.65 |

| Natural Gas Heater = | 20.0 | 0.020 | 2 | Natural Gas Hea | aters | | | | | | | | | | | | | | | | | |
|--------------------------------|------------|-------|----------|------------------|-------------------|----------|--------------------|------------------|-----------------|---------|---------------------|-----------------|-----------------------|------------|-------------------------|-----------------|---------------|----------------|-----------------|---------------|---------------|---------------------|
| Emergency Diesel Fire Pump = | 1.95 | | | | | | | | | | | | | | | | | | | | | |
| Emergency Diesel Generator = | 20.6 | | | | | | | | | | | | | | | | | | | | | |
| | | | Natural | Gas - Internal C | Combustion | I Fuel C | Dil - Internal Com | bustion | I | | Natural C | Gas- External C | ombustion | | | | | Fu | el Oil | | | ٦ |
| | CAS | | C | Combustion Tur | bine ^a | C | ombustion Turbi | ine ^a | Emission Factor | Duct | Burner ^b | Auxilla | y Boiler ^b | Natural Ga | as Heaters ^b | Emission Factor | Emergency Die | esel Fire Pump | Emission Factor | Emergency Die | sel Generator | r ^d Tota |
| Chemical | | POM? | lb/MMBtu | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | lb/MMcf | lb/hr | tpv | l lb/hr | tpy | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | tpv |
| 2-Methylnaphthalene | 97-57-6 | POM | | | 47 | | | 77 | 2.4E-05 | 2.4E-05 | 9.8E-05 | 2.4E-06 | 1.0E-05 | 4.7E-07 | 2.1E-06 | | | 47 | | 14.1 | +7 | 1.1E- |
| 3-Methylchloranthrene | 56-49-5 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.3E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | | | | | | | 8.3E- |
| 7.12-Dimethylbenz(a)anthracene | | POM | | | | | | | 1.6E-05 | 1.6E-05 | 6.5E-05 | 1.6E-06 | 6.9E-06 | 3.1E-07 | 1.4E-06 | | | | | | | 7.3E- |
| Acenaphthene | 83-32-9 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.3E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 1.42E-06 | 2.8E-06 | 6.9E-07 | 4.68E-06 | 9.6E-05 | 2.4E-05 | 3.3E- |
| Acenaphthylene | 203-96-8 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.3E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 5.06E-06 | 9.9E-06 | 2.5E-06 | 9.23E-06 | 1.9E-04 | 4.7E-05 | 5.8E- |
| Acetaldehyde | 75-07-0 | | 4.0E-05 | 1.5E-01 | 0.0E+00 | | | | | | | | | | | 7.67E-04 | 1.5E-03 | 3.7E-04 | 2.52E-05 | 5.2E-04 | 1.3E-04 | 5.0E- |
| Acrolein | 107-02-8 | | 6.4E-06 | 2.3E-02 | 0.0E+00 | | | | | | | | | | | 9.25E-05 | 1.8E-04 | 4.5E-05 | 7.88E-06 | 1.6E-04 | 4.0E-05 | 8.6E-0 |
| Anthracene | 120-12-7 | POM | | | | | | | 2.4E-06 | 2.4E-06 | 9.8E-06 | 2.4E-07 | 1.0E-06 | 4.7E-08 | 2.1E-07 | 1.87E-06 | 3.6E-06 | 9.1E-07 | 1.23E-06 | 2.5E-05 | 6.3E-06 | 1.8E-0 |
| Arsenic | 7440-38-2 | | | | | 1.1E-05 | 3.3E-02 | 8.3E-03 | 2.0E-04 | 2.0E-04 | 8.1E-04 | 2.0E-05 | 8.6E-05 | 3.9E-06 | 1.7E-05 | | | | | | | 9.2E-0 |
| Benz(a)anthracene | 56-55-3 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.3E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 1.68E-06 | 3.3E-06 | 8.2E-07 | 6.22E-07 | 1.3E-05 | 3.2E-06 | 1.2E-0 |
| Benzene | 71-43-2 | | 1.2E-05 | 4.4E-02 | 0.0E+00 | 5.5E-05 | 1.7E-01 | 4.2E-02 | 2.1E-03 | 2.1E-03 | 8.6E-03 | 2.1E-04 | 9.0E-04 | 4.1E-05 | 1.8E-04 | 9.33E-04 | 1.8E-03 | 4.5E-04 | 7.76E-04 | 1.6E-02 | 4.0E-03 | 5.6E-0 |
| Benzo(a)pyrene | 50-32-8 | POM | | | | | | | 1.2E-06 | 1.2E-06 | 4.9E-06 | 1.2E-07 | 5.2E-07 | 2.4E-08 | 1.0E-07 | 1.88E-07 | 3.7E-07 | 9.2E-08 | 2.57E-07 | 5.3E-06 | 1.3E-06 | 6.9E-0 |
| Benzo(b)fluoranthene | 205-99-2 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.3E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 9.91E-08 | 1.9E-07 | 4.8E-08 | 1.11E-06 | 2.3E-05 | 5.7E-06 | 1.4E-0 |
| Benzo(g,h,l)perylene | 191-24-2 | POM | | | | | | | 1.2E-06 | 1.2E-06 | 4.9E-06 | 1.2E-07 | 5.2E-07 | 2.4E-08 | 1.0E-07 | 4.89E-07 | 9.5E-07 | 2.4E-07 | 5.56E-07 | 1.1E-05 | 2.9E-06 | 8.6E-0 |
| Benzo(k)fluoranthene | 205-82-3 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.3E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 1.55E-07 | 3.0E-07 | 7.6E-08 | 2.18E-07 | 4.5E-06 | 1.1E-06 | 9.5E-0 |
| Beryllium | 7440-41-7 | | | | | 3.1E-07 | 9.4E-04 | 2.3E-04 | 1.2E-05 | 1.2E-05 | 4.9E-05 | 1.2E-06 | 5.2E-06 | 2.4E-07 | 1.0E-06 | | | | | | | 2.9E-0 |
| 1,3-Butadiene | 106-99-0 | | 4.3E-07 | 1.6E-03 | 0.0E+00 | 1.6E-05 | 4.8E-02 | 1.2E-02 | | | | | | | | 3.91E-05 | 7.6E-05 | 1.9E-05 | | | | 1.2E-0 |
| Cadmium | 7440-43-7 | | | | | 4.8E-06 | 1.5E-02 | 3.6E-03 | 1.1E-03 | 1.1E-03 | 4.5E-03 | 1.1E-04 | 4.7E-04 | 2.2E-05 | 9.4E-05 | | | | | | | 8.7E-0 |
| | 7440-47-3 | | | | | 1.1E-05 | 3.3E-02 | 8.3E-03 | 1.4E-03 | 1.4E-03 | 5.7E-03 | 1.4E-04 | 6.0E-04 | 2.7E-05 | 1.2E-04 | | | | | | | 1.5E-0 |
| Chrysene | 218-01-9 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.3E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 3.53E-07 | 6.9E-07 | 1.7E-07 | 1.53E-06 | 3.1E-05 | 7.9E-06 | 1.6E-0 |
| Cobalt | 7440-48-4 | | | | | | | | 8.4E-05 | 8.3E-05 | 3.4E-04 | 8.2E-06 | 3.6E-05 | 1.6E-06 | 7.2E-06 | | | | | | | 3.9E-0 |
| Dibenzo(a,h)anthracene | 53-70-3 | POM | | | | | | | 1.2E-06 | 1.2E-06 | 4.9E-06 | 1.2E-07 | 5.2E-07 | 2.4E-08 | 1.0E-07 | 5.83E-07 | 1.1E-06 | 2.8E-07 | 3.46E-07 | 7.1E-06 | 1.8E-06 | 7.6E-0 |
| Dichlorobenzene | 25321-22-6 | | | | | | | | 1.2E-03 | 1.2E-03 | 4.9E-03 | 1.2E-04 | 5.2E-04 | 2.4E-05 | 1.0E-04 | | | | | | | 5.5E-0 |
| Ethyl benzene | 100-41-4 | | 3.2E-05 | 1.2E-01 | 0.0E+00 | | | | | | | | | | | | | | | | | 0.0E+ |
| Fluoranthene | 206-44-0 | POM | | | | | | | 3.0E-06 | 3.0E-06 | 1.2E-05 | 2.9E-07 | 1.3E-06 | 5.9E-08 | 2.6E-07 | 7.61E-06 | 1.5E-05 | 3.7E-06 | 4.03E-06 | 8.3E-05 | 2.1E-05 | 3.8E-0 |
| Fluorene | 86-73-7 | POM | | | | | | | 2.8E-06 | 2.8E-06 | 1.1E-05 | 2.7E-07 | 1.2E-06 | 5.5E-08 | 2.4E-07 | 2.92E-05 | 5.7E-05 | 1.4E-05 | 1.28E-05 | 2.6E-04 | 6.6E-05 | 9.3E-0 |
| Formaldehyde | 50-00-0 | | 2.0E-04 | 7.4E-01 | 0.0E+00 | 2.8E-04 | 8.5E-01 | 2.1E-01 | 7.5E-02 | 7.4E-02 | 3.1E-01 | 7.4E-03 | 3.2E-02 | 1.5E-03 | 6.4E-03 | 1.18E-03 | 2.3E-03 | 5.8E-04 | 7.89E-05 | 1.6E-03 | 4.1E-04 | 5.6E-0 |
| Hexane | 110-54-3 | | | | | | | | 1.8E+00 | 1.8E+00 | 7.3E+00 | 1.8E-01 | 7.7E-01 | 3.5E-02 | 1.5E-01 | | | | | | | 8.3E+ |
| Indeno(1,2,3-cd)pyrene | 193-39-5 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 7.3E-06 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 3.75E-07 | 7.3E-07 | 1.8E-07 | 4.14E-07 | 8.5E-06 | 2.1E-06 | 1.1E-(|
| Manganese | 7439-96-5 | | | | | 7.9E-04 | 2.4E+00 | 6.0E-01 | 3.8E-04 | 3.7E-04 | 1.5E-03 | 3.7E-05 | 1.6E-04 | 7.5E-06 | 3.3E-05 | | | | | | | 6.0E-0 |
| Mercury | 7439-97-6 | | | | | 1.2E-06 | 3.6E-03 | 9.1E-04 | 2.6E-04 | 2.6E-04 | 1.1E-03 | 2.5E-05 | 1.1E-04 | 5.1E-06 | 2.2E-05 | | | | | | | 2.1E-0 |
| Naphthalene | 91-20-3 | | 1.3E-06 | 4.8E-03 | 0.0E+00 | 3.5E-05 | 1.1E-01 | 2.6E-02 | 6.1E-04 | 6.0E-04 | 2.5E-03 | 6.0E-05 | 2.6E-04 | 1.2E-05 | 5.2E-05 | 8.48E-05 | 1.7E-04 | 4.1E-05 | 1.30E-04 | 2.7E-03 | 6.7E-04 | 3.0E-0 |
| Nickel | 7440-02-0 | | | | | 4.6E-06 | 1.4E-02 | 3.5E-03 | 2.1E-03 | 2.1E-03 | 8.6E-03 | 2.1E-04 | 9.0E-04 | 4.1E-05 | 1.8E-04 | | | | | | | 1.3E-0 |
| PAH | | | 2.2E-06 | 8.1E-03 | 0.0E+00 | 4.0E-05 | 1.2E-01 | 3.0E-02 | | | | | | | | | | | | | | 3.0E-0 |
| Phenanathrene | 85-01-8 | POM | | | | | | | 1.7E-05 | 1.7E-05 | 6.9E-05 | 1.7E-06 | 7.3E-06 | 3.3E-07 | 1.5E-06 | 2.94E-05 | 5.7E-05 | 1.4E-05 | 4.08E-05 | 8.4E-04 | 2.1E-04 | 3.0E-0 |
| Propylene | | | | | | | | | | | | | | | | 2.58E-03 | 5.0E-03 | 1.3E-03 | 2.79E-03 | 5.7E-02 | 1.4E-02 | 1.6E-0 |
| Proplylene Oxide | 75-56-9 | | 2.9E-05 | 1.1E-01 | 0.0E+00 | | | | | | | | | | | | | | | | | 0.0E+ |
| Pyrene | 129-00-0 | POM | | | | | | | 5.0E-06 | 4.9E-06 | 2.0E-05 | 4.9E-07 | 2.1E-06 | 9.8E-08 | 4.3E-07 | 4.78E-06 | 9.3E-06 | 2.3E-06 | 3.71E-06 | 7.6E-05 | 1.9E-05 | 4.4E-0 |
| | 7782-49-2 | | | | | 2.5E-05 | 7.6E-02 | 1.9E-02 | 2.4E-05 | 2.4E-05 | 9.8E-05 | 2.4E-06 | 1.0E-05 | 4.7E-07 | 2.1E-06 | | | | | | 1 | 1.9E-0 |
| Toluene | 108-88-3 | | 1.3E-04 | 4.8E-01 | 0.0E+00 | | | | 3.4E-03 | 3.4E-03 | 1.4E-02 | 3.3E-04 | 1.5E-03 | 6.7E-05 | 2.9E-04 | 4.09E-04 | 8.0E-04 | 2.0E-04 | 2.81E-04 | 5.8E-03 | 1.4E-03 | 1.7E-0 |
| Xylene | 1330-20-7 | | 6.4E-05 | 2.3E-01 | 0.0E+00 | | | | 0.72 00 | 0.42 00 | 1.72 02 | 0.02 04 | 1.02 00 | 0.7 2 00 | 2.02 0-7 | 2.85E-04 | 5.6E-04 | 1.4E-04 | 1.93E-04 | 4.0E-03 | 9.9E-04 | 1.1E-(|
| . y | | TOTAL | | 1.90 | 0.00 | | 3.85 | 0.96 | | | 7.69 | 0.19 | 0.81 | 0.04 | | | 1.3E-02 | | | | 1 0.02 01 | 9.65 |

(a) Emission factors for combustion turbines from AP-42 Section 3.1, Updated 2/2000. Formaldehyde emission factor from Sims Roy EPA Memo "Hazardous Air Pollutant (HAP) Emission Control Technology for New Stationary Combustion Turbines" 8/21/2001.

⁽c) Emission factors from AP-42 Section 3.3, Updated 10/1996 (d) Emission factors from AP-42 Section 3.4, Updated 10/1996

| | | | Natural G | ias - Internal Co | mbustion | Fuel O | il - Internal Com | bustion | | | Natural G | as- External Co | ombustion | | | | | Fue | el Oil | | | i . |
|----------|-----|------|-----------|-------------------|-----------------|----------|-------------------|-----------------|-----------------|---------|---------------------|-----------------|-----------------------|-------------|------------------------|-----------------|----------------|----------------------------|------------------------|-----------------|---------------------------|---------|
| | | | Co | mbustion Turbi | ne ^a | | ombustion Turbi | ne ^a | Emission Factor | Duct B | Burner ^b | | / Boiler ^b | Natural Gas | s Heaters ^b | Emission Factor | Emergency Dies | sel Fire Pump ^c | Emission Factor | Emergency Diese | el Generator ^d | Total |
| Chemical | CAS | POM? | lb/MMBtu | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | lb/mmCF | lb/hr | tpy | lb/hr | tpy | lb/hr | tpy | lb/mmCF | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | tpy |
| Lead | | | | | | 1.4E-05 | 4.2E-02 | 1.1E-02 | 5.0E-04 | 4.9E-04 | 2.0E-03 | 4.9E-05 | 2.1E-04 | 9.8E-06 | 4.3E-05 | | | | | | | 2.3E-03 |

⁽a) Emission factors for combustion turbines from AP-42 Section 3.1, Updated 2/2000. Formaldehyde emission factor from Sims Roy EPA Memo "Hazardous Air Pollutant (HAP) Emission Control Technology for New Stationary Combustion Turbines" 8/21/2001.

⁽b) Emission factors from AP-42 Section 1.4, Updated 7/1998

⁽b) Emission factors from AP-42 Section 1.4, Updated 7/1998 (c) Emission factors from AP-42 Section 3.3, Updated 10/1996 (d) Emission factors from AP-42 Section 3.4, Updated 10/1996

Hours of Operation

Combustion Turbine Natural Gas Hours = 8,260 hours per year
Combustion Turbine Fuel Oil Hours = 500 hours per year
Duct Burner = 0 hours per year
Auxillary Boiler = 8,760 hours per year
Natural Gas Heater = 8,760 hours per year
Emergency Diesel Fire Pump = 500 hours per year
Emergency Diesel Generator = 500 hours per year

Natural Gas Usage

1,020 MMBtu/MMcf mmCF/hr mmBtu/hr Combustion Turbine (Natural Gas) = Combustion Turbine (Fuel Oil) = 3,021 Duct Burner = 0.987 Auxillary Boiler = 100.0 0.098 Natural Gas Heater = 0.020 20.0 2 Natural Gas Heaters Emergency Diesel Fire Pump = 1.95 Emergency Diesel Generator =

Total Facility: Hazardous Air Pollutants Emissions

| | Maximum Potential Emissions |
|---------------------------|-----------------------------------|
| HAP | tpy |
| 1st Maximum: Formaldehyde | 3.31 |
| 2nd Maximum: Toluene | 1.97 |
| 3rd Maximum: Xylene | 0.97 |
| All HAPs | 9.82 |

| | | | Natura | l Gas - Internal C | Combustion | Fuel O | il - Internal Coml | bustion | | | Natural G | as- External C | combustion | | | | | Fue | l Oil | | | |
|--------------------------------|------------|-------|----------|--------------------|-------------------|----------|--------------------|-----------------|-----------------|----------|---------------------|----------------|-----------------------|-----------|-------------------------|-----------------|---------------|----------------------------|------------------------|---------------|----------------------------|----|
| | CAS | | (| Combustion Tur | bine ^a | Co | mbustion Turbi | ne ^a | Emission Factor | Duct E | Burner ^b | Auxillar | y Boiler ^b | Natural G | as Heaters ^b | Emission Factor | Emergency Die | sel Fire Pump ^c | Emission Factor | Emergency Die | sel Generator ^c | rd |
| Chemical | | POM? | lb/MMBtu | lb/hr | tpv | lb/MMBtu | lb/hr | tpy | lb/MMcf | lb/hr | tpv | lb/hr | tpv | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | lb/MMBtu | lb/hr | tpy | |
| 2-Methylnaphthalene | 97-57-6 | POM | | | 1.7 | | | 1, | 2.4E-05 | 2.4E-05 | 0.0E+00 | 2.4E-06 | 1.0E-05 | 4.7E-07 | 2.1E-06 | | | 1, | | | 17 | |
| 3-Methylchloranthrene | 56-49-5 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | | | | | | | |
| 7.12-Dimethylbenz(a)anthracene | | POM | | | | | | | 1.6E-05 | 1.6E-05 | 0.0E+00 | 1.6E-06 | 6.9E-06 | 3.1E-07 | 1.4E-06 | | | | | | | |
| Acenaphthene | 83-32-9 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 1.42E-06 | 2.8E-06 | 6.9E-07 | 4.68E-06 | 9.6E-05 | 2.4E-05 | - |
| Acenaphthylene | 203-96-8 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 5.06E-06 | 9.9E-06 | 2.5E-06 | 9.23E-06 | 1.9E-04 | 4.7E-05 | _ |
| Acetaldehyde | 75-07-0 | | 4.0E-05 | 1.5E-01 | 6.1E-01 | | | | | | | | | | | 7.67E-04 | 1.5E-03 | 3.7E-04 | 2.52E-05 | 5.2E-04 | 1.3E-04 | _ |
| Acrolein | 107-02-8 | | 6.4E-06 | 2.3E-02 | 9.7E-02 | | | | | | | | | | | 9.25E-05 | 1.8E-04 | 4.5E-05 | 7.88E-06 | 1.6E-04 | 4.0E-05 | _ |
| Anthracene | 120-12-7 | POM | | _,,,_, | V = V= | | | | 2.4E-06 | 2.4E-06 | 0.0E+00 | 2.4E-07 | 1.0E-06 | 4.7E-08 | 2.1E-07 | 1.87E-06 | 3.6E-06 | 9.1E-07 | 1.23E-06 | 2.5E-05 | 6.3E-06 | _ |
| Arsenic | 7440-38-2 | | | | | 1.1E-05 | 3.3E-02 | 8.3E-03 | 2.0E-04 | 2.0E-04 | 0.0E+00 | 2.0E-05 | 8.6E-05 | 3.9E-06 | 1.7E-05 | | | | | | | |
| Benz(a)anthracene | 56-55-3 | POM | | | | | V. V. V. | 1.02 10 | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 1.68E-06 | 3.3E-06 | 8.2E-07 | 6.22E-07 | 1.3E-05 | 3.2E-06 | - |
| Benzene | 71-43-2 | | 1.2E-05 | 4.4E-02 | 1.8E-01 | 5.5E-05 | 1.7E-01 | 4.2E-02 | 2.1E-03 | 2.1E-03 | 0.0E+00 | 2.1E-04 | 9.0E-04 | 4.1E-05 | 1.8E-04 | 9.33E-04 | 1.8E-03 | 4.5E-04 | 7.76E-04 | 1.6E-02 | 4.0E-03 | _ |
| Benzo(a)pyrene | 50-32-8 | POM | | | | | | | 1.2E-06 | 1.2E-06 | 0.0E+00 | 1.2E-07 | 5.2E-07 | 2.4E-08 | 1.0E-07 | 1.88E-07 | 3.7E-07 | 9.2E-08 | 2.57E-07 | 5.3E-06 | 1.3E-06 | _ |
| Benzo(b)fluoranthene | 205-99-2 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 9.91E-08 | 1.9E-07 | 4.8E-08 | 1.11E-06 | 2.3E-05 | 5.7E-06 | _ |
| Benzo(a.h.l)pervlene | 191-24-2 | POM | | | | | | | 1.2E-06 | 1.2E-06 | 0.0E+00 | 1.2E-07 | 5.2E-07 | 2.4E-08 | 1.0E-07 | 4.89E-07 | 9.5E-07 | 2.4E-07 | 5.56E-07 | 1.1E-05 | 2.9E-06 | _ |
| Benzo(k)fluoranthene | 205-82-3 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 1.55E-07 | 3.0E-07 | 7.6E-08 | 2.18E-07 | 4.5E-06 | 1.1E-06 | _ |
| Bervllium | 7440-41-7 | | | | | 3.1E-07 | 9.4E-04 | 2.3E-04 | 1.2E-05 | 1.2E-05 | 0.0E+00 | 1.2E-06 | 5.2E-06 | 2.4E-07 | 1.0E-06 | | | | | | | |
| 1.3-Butadiene | 106-99-0 | | 4.3E-07 | 1.6E-03 | 6.5E-03 | 1.6E-05 | 4.8E-02 | 1.2E-02 | ,, | ,, | 7.0 | | , | | | 3.91E-05 | 7.6E-05 | 1.9E-05 | | | | ī |
| Cadmium | 7440-43-7 | | | | 7.02 77 | 4.8E-06 | 1.5E-02 | 3.6E-03 | 1.1E-03 | 1.1E-03 | 0.0E+00 | 1.1E-04 | 4.7E-04 | 2.2E-05 | 9.4E-05 | 0.0 | | 1.0 = 40 | | | | |
| Chromium | 7440-47-3 | | | | | 1.1E-05 | 3.3E-02 | 8.3E-03 | 1.4E-03 | 1.4E-03 | 0.0E+00 | 1.4E-04 | 6.0E-04 | 2.7E-05 | 1.2E-04 | | | | | | | |
| Chrysene | 218-01-9 | POM | | | | | V.U. V. | 0.02 00 | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 3.53E-07 | 6.9E-07 | 1.7E-07 | 1.53E-06 | 3.1E-05 | 7.9E-06 | - |
| Cobalt | 7440-48-4 | | | | | | | | 8.4E-05 | 8.3E-05 | 0.0E+00 | 8.2E-06 | 3.6E-05 | 1.6E-06 | 7.2E-06 | 0.00= 0. | | = 4. | | 4= 44 | | |
| Dibenzo(a.h)anthracene | 53-70-3 | POM | | | | | | | 1.2E-06 | 1.2E-06 | 0.0E+00 | 1.2E-07 | 5.2E-07 | 2.4E-08 | 1.0E-07 | 5.83E-07 | 1.1E-06 | 2.8E-07 | 3.46E-07 | 7.1E-06 | 1.8E-06 | - |
| Dichlorobenzene | 25321-22-6 | | | | | | | | 1.2E-03 | 1.2E-03 | 0.0E+00 | 1.2E-04 | 5.2E-04 | 2.4E-05 | 1.0E-04 | 0.002 01 | 1112 00 | 2.02 01 | 0.102 01 | 1112 00 | 1.02 00 | |
| Ethyl benzene | 100-41-4 | | 3.2E-05 | 1.2E-01 | 4.8E-01 | | | | 1122 00 | 1.22 00 | 0.02 - 00 | 1122 01 | 0.22 01 | 2.12 00 | 1.02 01 | | | | | | | Ē |
| Fluoranthene | 206-44-0 | POM | | | | | | | 3.0E-06 | 3.0E-06 | 0.0E+00 | 2.9E-07 | 1.3E-06 | 5.9E-08 | 2.6E-07 | 7.61E-06 | 1.5E-05 | 3.7E-06 | 4.03E-06 | 8.3E-05 | 2.1E-05 | - |
| Fluorene | 86-73-7 | POM | | | | | | | 2.8E-06 | 2.8E-06 | 0.0E+00 | 2.7E-07 | 1.2E-06 | 5.5E-08 | 2.4E-07 | 2.92E-05 | 5.7E-05 | 1.4E-05 | 1.28E-05 | 2.6E-04 | 6.6E-05 | - |
| Formaldehvde | 50-00-0 | | 2.0E-04 | 7.4E-01 | 3.1E+00 | 2.8E-04 | 8.5E-01 | 2.1E-01 | 7.5E-02 | 7.4E-02 | 0.0E+00 | 7.4E-03 | 3.2E-02 | 1.5E-03 | 6.4E-03 | 1.18E-03 | 2.3E-03 | 5.8E-04 | 7.89E-05 | 1.6E-03 | 4.1E-04 | - |
| Hexane | 110-54-3 | | | | V | | 0.02 0. | | 1.8E+00 | 1.8E+00 | 0.0E+00 | 1.8E-01 | 7.7E-01 | 3.5E-02 | 1.5E-01 | | | 0.02 | | | | |
| Indeno(1,2,3-cd)pyrene | 193-39-5 | POM | | | | | | | 1.8E-06 | 1.8E-06 | 0.0E+00 | 1.8E-07 | 7.7E-07 | 3.5E-08 | 1.5E-07 | 3.75E-07 | 7.3E-07 | 1.8E-07 | 4.14E-07 | 8.5E-06 | 2.1E-06 | - |
| Manganese | 7439-96-5 | | | | | 7.9E-04 | 2.4E+00 | 6.0E-01 | 3.8E-04 | 3.7E-04 | 0.0E+00 | 3.7E-05 | 1.6E-04 | 7.5E-06 | 3.3E-05 | | | | | | | |
| Mercury | 7439-97-6 | | | | | 1.2E-06 | 3.6E-03 | 9.1E-04 | 2.6E-04 | 2.6E-04 | 0.0E+00 | 2.5E-05 | 1.1E-04 | 5.1E-06 | 2.2E-05 | | | | | | | |
| Naphthalene | 91-20-3 | | 1.3E-06 | 4.8E-03 | 2.0E-02 | 3.5E-05 | 1.1E-01 | 2.6E-02 | 6.1E-04 | 6.0E-04 | 0.0E+00 | 6.0E-05 | 2.6E-04 | 1.2E-05 | 5.2E-05 | 8.48E-05 | 1.7E-04 | 4.1E-05 | 1.30E-04 | 2.7E-03 | 6.7E-04 | - |
| Nickel | 7440-02-0 | | 1.02 00 | 4.0L 00 | 2.02 02 | 4.6E-06 | 1.4E-02 | 3.5E-03 | 2.1E-03 | 2.1E-03 | 0.0E+00 | 2.1E-04 | 9.0E-04 | 4.1E-05 | 1.8E-04 | 0.40L 00 | 1.7 = 04 | 4.12 00 | 1.002 04 | 2.12 00 | 0.7 2 04 | |
| PAH | 7.440-02-0 | | 2.2E-06 | 8.1E-03 | 3.3E-02 | 4.0E-05 | 1.4E-02 1.2E-01 | 3.0E-02 | Z.1L-03 | 2.12-00 | 0.02100 | 2.12-04 | 0.0L-04 | 4.1L-03 | 1.52-04 | | | | | | | £. |
| Phenanathrene | 85-01-8 | POM | 2.21-00 | 0.1L-03 | 0.0L-02 | 7.0L-03 | 1.2L-01 | J.UL-UZ | 1.7E-05 | 1.7E-05 | 0.0E+00 | 1.7E-06 | 7.3E-06 | 3.3E-07 | 1.5E-06 | 2.94E-05 | 5.7E-05 | 1.4E-05 | 4.08E-05 | 8.4E-04 | 2.1E-04 | 4 |
| Propylene | 00-01-0 | 1 OW | | | | | | | 1.7 = 00 | 1.7 = 03 | 0.02.00 | 1.7 L-00 | 7.52-00 | J.JL-01 | 1.52-00 | 2.58E-03 | 5.0E-03 | 1.4E-03 | 2.79E-03 | 5.7E-02 | 1.4E-02 | _ |
| Proplylene Oxide | 75-56-9 | | 2.9E-05 | 1.1E-01 | 4.4E-01 | | | | | | | | | | | 2.002-00 | J.UL-03 | 1.02-00 | 2.731-00 | J./ L-UZ | 1.7L-02 | |
| Pyrene | 129-00-0 | POM | 2.91-03 | 1.1L=01 | 4.4L=01 | | | | 5.0E-06 | 4.9E-06 | 0.0E+00 | 4.9E-07 | 2.1E-06 | 9.8E-08 | 4.3E-07 | 4.78E-06 | 9.3E-06 | 2.3E-06 | 3.71E-06 | 7.6E-05 | 1.9E-05 | 4 |
| , | | FOW | | | | 2.55.05 | 7.65.00 | 1.05.00 | | | | | | | | 4.70E-00 | 9.3E-00 | 2.3E-00 | 3.1 IE-00 | 7.0E-05 | 1.9E-05 | - |
| Selenium | 7782-49-2 | | 4.05.04 | 4.05.04 | 0.05.00 | 2.5E-05 | 7.6E-02 | 1.9E-02 | 2.4E-05 | 2.4E-05 | 0.0E+00 | 2.4E-06 | 1.0E-05 | 4.7E-07 | 2.1E-06 | 4.005.04 | 0.05.04 | 0.05.04 | 0.045.04 | 5.05.00 | 4.45.00 | 4 |
| Toluene | 108-88-3 | | 1.3E-04 | 4.8E-01 | 2.0E+00 | | | | 3.4E-03 | 3.4E-03 | 0.0E+00 | 3.3E-04 | 1.5E-03 | 6.7E-05 | 2.9E-04 | 4.09E-04 | 8.0E-04 | 2.0E-04 | 2.81E-04 | 5.8E-03 | 1.4E-03 | _ |
| Xylene | 1330-20-7 | | 6.4E-05 | 2.3E-01 | 9.7E-01 | | | | | | | | | | | 2.85E-04 | 5.6E-04 | 1.4E-04 | 1.93E-04 | 4.0E-03 | 9.9E-04 | _ |
| | | TOTAL | | l 1.90 | l 7.86 | | 3.85 | 0.96 | | 1.86 | 0.00 | 0.19 | I 0.81 | 0.04 | 1.6E-01 | | 1.3E-02 | 3.1E-03 | | | | |

(a) Emission factors for combustion turbines from AP-42 Section 3.1, Updated 2/2000. Formaldehyde emission factor from Sims Roy EPA Memo "Hazardous Air Pollutant (HAP) Emission Control Technology for New Stationary Combustion Turbines" 8/21/20 (b) Emission factors from AP-42 Section 1.4, Updated 7/1998

Total (b) Emission factors from AP-42 Section 1.4, Updated 7/1998 tpy (c) Emission factors from AP-42 Section 3.3, Updated 10/1996 0.00025765 (d) Emission factors from AP-42 Section 3.4, Updated 10/1996

(a) Emission factors for om AP-42 Section 1.4, Updated 7/1998

(c) Emission factors from AP-42 Section 1.4, Updated 7/1998 (c) Emission factors from AP-42 Section 3.3, Updated 10/1996

(d) Emission factors from AP-42 Section 3.4, Updated 10/1996

South Shore Energy, LLC - Nemadji Trail Energy Center Q/D Analysis for Federal Class I Areas

Nemadji River Site

| | | | Natural Gas Duct Firing |
|---------------------------------------|--------|------------------------|-------------------------|
| | | Operation | Operation |
| | | Q/D (Based on max | Q/D (Based on max |
| | | 24-hr for 365 days per | 24-hr for 365 days per |
| Class I Area | D (km) | year) | year) |
| Rainbow Lake Wilderness | 60 | 9.9 | 7.3 |
| Boundary Waters Canoe Area Wilderness | 126 | 4.7 | 3.5 |
| Voyageurs National Park | 182 | 3.3 | 2.4 |
| Isle Royale National Park | 237 | 2.5 | 1.9 |
| Forest County Potawatomi Community | 261 | 2.3 | 1.7 |

| | Fuel Oil Duct Firing 2 | 4-hr Max Emissions | Natural Gas Duct firi | ng 24-hr Max Emissions |
|--------------------------------|--------------------------------|---------------------|--------------------------------|--------------------------|
| | Max Emissions in | | Max Emissions in | |
| | 24-hr period | Max 24-hour for 365 | 24-hr period | Max 24-hour for 365 Days |
| Pollutant | (lb/24-hr period) ^a | Days Per Year (tpy) | (lb/24-hr period) ^a | Per Year (tpy) |
| NO _x | 1,569.0 | 286.3 | 1,109.3 | 202.4 |
| PM ₁₀ | 1,322.3 | 241.3 | 901.9 | 164.6 |
| SO2 | 145.8 | 26.6 | 156.1 | 28.5 |
| H ₂ SO ₄ | 222.9 | 40.7 | 236.8 | 43.2 |
| | Q duct firing fuel oil= | 594.9 | Q natural gas duct firing= | 438.7 |

Scenario 1: Worst-Case Fuel Oil Turbine Operation With Duct firing

| Pollutant | Turbine Fuel Oil Duct Firing (lb/24-hour period) ^a | Auxiliary Boiler (lb/24-hour period) ^b | Haul Road Fugitives Cooling Tower (lb/24-hour period) | Natural Gas Heater #1 or #2 (lb/24-hour period) ^c |
|--------------------------------|---|--|---|--|
| NO _x | 1,555.0 | 2.20 | 0.00 | 11.76 |
| PM ₁₀ | 1,308.3 | 1.49 | 10.74 | 1.79 |
| SO2 | 145.6 | 0.12 | 0.00 | 0.14 |
| H ₂ SO ₄ | 222.8 | 0.02 | 0.00 | 0.02 |

- (a) Turbine NOx emissions will be monitored via NOx CEMs and will not exceed 1,555 lb/24-hr while duct firing and combusting fuel oil. In addition, fuel oil is limited to fuel consumption equivalent of 500 hours per year, however emissions are based on 8,760 hours per
- year.
 (b) The auxiliary boiler will operate maximum 2 hours in a 24-hr period when fuel oil duct firing occurs
- (c) One natural gas heater will operate at a time (one is back-up)

Scenario 2: Worst-Case Natural Gas Turbine Operation With Duct firing

| Pollutant | Turbine Natural Gas Duct Firing (Ib/24-hour period) ^a | Auxiliary Boiler (lb/24-hour period) | Haul Road Fugitives Cooling Tower (Ib/24-hour period) | Natural Gas Heater #1 or #2 (Ib/24-hour period) ^b |
|--------------------------------|--|---|---|--|
| NO _x | 1,071.1 | 26.40 | 0.00 | 11.76 |
| PM ₁₀ | 871.5 | 17.88 | 10.74 | 1.79 |
| SO2 | 154.5 | 1.41 | 0.00 | 0.14 |
| H ₂ SO ₄ | 236.6 | 0.22 | 0.00 | 0.02 |

- (a) Includes one start-up per day.
- (b) One natural gas heater will operate at a time (one is back-up)

lb/hr emissions

| | Turbine Fuel Oil Duct Firing | Turbine Natural Gas Duct Firing | Auxiliary Boiler | Haul Road Fugitives | Natural Gas Heater |
|--------------------------------|------------------------------|---------------------------------|------------------|---------------------|-----------------------|
| Pollutant | (lb/hr) | (lb/hr) | (lb/hr) | (lb/hr) | (lb/hr) |
| NO _x | a | 33.5 | 1,1 | 0.00 | 0.5 |
| PM ₁₀ | 54.5 | 36.3 | 0.7 | 0.45 | 0.07 |
| SO2 | 6.1 | 6.4 | 0.06 | 0.00 | 5.9E-03 |
| H ₂ SO ₄ | 9.3 | 9.9 | 9.0E-03 | 0.00 | 9.0E-04 |

(a) 24-hr emissions will be less than 1,555 lbs for the combustion turbine while combusting fuel oil and duct firing.

Ib/start-up emissions

| Pollutant | Fuel Oil Start-up Emissions (Ib/cold start) ^{a,b} | Natural Gas Start-up Emissions (Ib/cold start) ^{a,b} |
|--------------------------------|--|---|
| NO _x | 860.0 | 335.0 |
| PM ₁₀ | 78.9 | 43.6 |
| SO2 | 9.2 | 10.2 |
| H ₂ SO ₄ | 14.0 | 15.6 |

- (a) Start-up emissions based on vendor load and start-up profiles (b) Start-up emissions are 2 hours.

South Shore Energy, LLC - Nemadji Trail Energy Center NR 445 Analysis

| Pollutant | Stack Height | E _{Unot} | E _{Unobstructed} | | ed + E _{Fugitive}) | E- | Total | NR 445 Thresholds | | In compliance with NR 445 Thresholds? | |
|---------------------------|-----------------|-------------------|---------------------------|---------------|------------------------------|---------------|---------|--------------------|---------|---------------------------------------|--------|
| Politiani | Class | lb/hr | lb/yr | avg. lb/hr | lb/yr | avg. lb/hr | lb/yr | 1-hr/24-hr avg. | Annual | 1-hr/24-hr avg. | Annual |
| Benzene (71-43-2) | <25 | | | | 141 | | 141 | | 228 | | Yes |
| Delizelle (7 1-43-2) | 25<40 | | | | 333 | | 333 | | 936 | | Yes |
| Ethylbenzene (100-41-4) | <25 | | | 0.018 | 124 | 0.018 | 124 | 23.3 | 177,688 | Yes | Yes |
| Euryiberizerie (100-41-4) | 25<40 | | | 0.7 | 333 | 0.7 | 333 | 90.6 | 730,000 | Yes | Yes |
| Hexane (110-54-3) | <25 | | | 0.034 | 263 | 0.034 | 263 | 9.47 | 35,538 | Yes | Yes |
| Hexaile (110-54-5) | 25<40 | | | 0.7 | 333 | 0.7 | 333 | 36.8 | 146,000 | Yes | Yes |
| Toluene (108-88-3) | <25 | | | 0.034 | 263 | 0.034 | 263 | 10.1 | 17,075 | Yes | Yes |
| Toluette (106-66-3) | 25<40 | | | 0.7 | 333 | 0.7 | 333 | 39.3 | 292,000 | Yes | Yes |
| Vylone (1220-20-7) | <25 | | | 0.060 | | 0.060 | | 23.3 | | Yes | |
| Xylene (1330-20-7) | 25<40 | | | 0.7 | | 0.7 | | 90.6 | | Yes | |
| Ammonia (7664-41-7) | >75 | 62 | 543,120 | | | 62 | 543,120 | 28.2 | 612,587 | No | Yes |

Sources:

Xylene (1330-20-7)

WDNR Memo. Chapter NR 445 Compliance Demonstration Method for Non-exempt Potential Emissions from Non-vertical or Obstructed Stacks and Non-exempt Potential Fugitive Emissions. October 20, 2005.

NR 445, Wis. Adm. Code - Control of Hazardous Pollutants

| F Fmissions from Pining | Fugitives | Broakdowi | ` | | | | | | | |
|---|----------------|-----------------------|-------|------|-----------------------|-------|------------|-----------------------|------------|-------------|
| E _{Fugitive} Emissions from Piping | VOC (lb/hr) | VOC (lb/yr) | 1 | | | | | | | |
| Natural Gas | | 1b/yr 5,609 | | | | | | | | |
| Fuel Oil 1.73 15,153 | | | | | | | | | | |
| | | E _{Fugitive} | | | E _{Fugitive} | | Total | E _{Fugitive} | 4x (E | Fugitive) |
| Pollutant | | Natural Gas | ; | | Fuel Oil | | Fuel Oil + | Natural Gas | Fuel Oil + | Natural Gas |
| Pollutarit | wt% | lb/hr | lb/yr | wt% | lb/hr | lb/yr | lb/hr | lb/yr | lb/hr | lb/yr |
| Benzene (71-43-2) | 0.08% | 0.00051 | 4.5 | 0.2% | 0.003 | 30 | 0.004 | 35 | 0.016 | 139 |
| Ethylbenzene (100-41-4) | | | | 0.2% | 0.003 | 30 | 0.003 | 30.306 | 0.014 | 121 |
| Hexane (110-54-3) | 0.08% | 0.00051 | 4.5 | 0.4% | 0.01 | 60.61 | 0.01 | 65 | 0.030 | 260 |
| Toluene (108-88-3) | 0.08% | 0.00051 | 4.5 | 0.4% | 0.01 | 61 | 0.01 | 65 | 0.030 | 260 |
| | | | | | | | | | | |

0.01

0.8%

121

0.01

121

0.055

485



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TANKS 4.P.P

issions Report - Detail ForP at P Tank InPentification anP Physical CharacteristicsP

IPentificationP

NTEC Turb ne D esel TFnkF DulufhF on:F

User IdenF CFy:F SF e:F W sFons nF

CompFny:F Type oFTFnk:F DesFr pFon:F

NTECF VerF I F xed RooFTFnkF 180,000 gFllon bF kup Ruel F nk For Furb nesF

Tank DiP ensionsP Shell He ghF(F):F

30.00F DF mefer (F):F

L qu d He ghF(F):F

Avg. L qu d He ghF(F):F

Volume (gFllons):F

Turnovers:F 33.00F 28.14F 14.07F 180,042.51F 59.94F 10,791,747.84F

NeFThroughpuf(gFl/yr):F Is TFnk HeF ed (y/n):F NF

aint CharacteristicsP

Shell Color/ShFde:F Shell CondFonF WhFe/WhFeF GoodF WhFe/WhFeF RooFColor/ShFde:F RooFCondFon:F GoodF

Roof CharacteristicsP

ConeF

Type:F He ghF(F)F Slope (F/F) (Cone Roof)F 5.00F 0.30F

Breather Vent SettingsP

VF uum SeF ngs (ps g):F Pressure SeF ngs (ps g)F -0.03F 0.03F

MeFerologF IDF used n Emssons CFI ulF ons: Dulufh, MnnesoF (Avg A mospherF Pressure = 13.98 psF)F

S 4.0 Report Page 2 of

TANKS 4.P.P issions Report - Detail ForP at P LiquiP Contents of Storage TankP

NTPC Turbine Diesel Tank - Vertical FixeP Roof TankP Duluth, WisconsinP

| , | | DF Temp | ly L qu d Su perF ure (de | ırF.F g F)F | L qu dF BulkF TempF | VFpo | r Pressure (| psF)F | VFporF Mol.F | L qu dF MFssF | VFporF MFssF | Mol.F | BFs s for VFpor PressureF |
|-------------------------|--------|------------|------------------------------|----------------|---------------------------|---------|--------------|---------|-----------------|------------------|-----------------|---------|-------------------------------------|
| M xFure/ComponenF | Mon hF | Avg.F | M n.F | MFx.F | (deg F)F | Avg.F | M n.F | MFx.F | We gh .F | rF .F | rF .F | We ghF | CFIFuIF onsF |
| D sRIF e uel o I no. 2F | AIIF | 40.03F | 35.22F | 44.84F | 38.46F | 0.0031F | 0.0031F | 0.0038F | 130.0000F | | | 188.00F | OpFon 1: VP40 = .0031 VP50 = .0045F |

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TANKS 4.P.P issions Report - Detail ForP at P Detail Calculations (AP-42)P

NTPC Turbine Diesel Tank - Vertical FixeP Roof TankP Duluth, WisconsinP

| AnnuFl Em ss on CFIF ulF onsF | |
|--|------------------------------|
| SF nd ng Losses (lb):F | 14.1127F |
| VFpor SpF e Volume (Fu F):F | 15,050.4043F |
| VFpor DensFy (lb/Fu F):F | 0.0001F |
| VFpor SpF e ExpFns on F or:F | 0.0342F |
| Ven ed VFpor SF urF on F or:F | 0.9971F |
| TENK VENNE SAF A VALUMANE | |
| TFnk VFpor SpF e Volume:F VFpor SpF e Volume (Fu F):F | 15,050.4043F |
| TFnk DF me er (F):F | 33.0000F |
| VEnor SpE e QuE de (E):E | 17.5967F |
| VFpor SpF e OuF ge (F):F TFnk Shell He gh (F):F | 30.0000F |
| AverFge L qu d He gh (F):F | 14.0700F |
| Roo OuF ge (F):F | 1.6667F |
| Roo OuF ge (Cone Roo)F | |
| Roo OuF ge (F):F | 1.6667F |
| Roo Hegh (F):F | 5.0000F |
| Roo Slope (F/F):F | 0.3000F |
| Shell RFd us (F):F | 16.5000F |
| VFpor DensFyF | |
| VFpor DensFy (lb/Fu F):F | 0.0001F |
| VFpor MoleFulFr We gh (lb/lb-mole):F | 130.0000F |
| VFpor Pressure F DF ly AverFge L qu dF | |
| SurF e TemperF ure (psF):F | 0.0031F |
| DF ly Avg. L qu d SurF e Temp. (deg. R):F | 499.7017F |
| DF ly AverFge Amb en Temp. (deg. F):F | 38.4417F |
| IdeFl GFs ConsF n RF | |
| (psF FuF / (lb-mol-deg R)):F | 10.731F |
| L qu d Bulk TemperF ure (deg. R):F | 498.1317F |
| TFnk PF n SolFr AbsorpF nFe (Shell):F TFnk PF n SolFr AbsorpF nFe (Roo):F | 0.1700F |
| TFnk PF n SolFr AbsorpF nFe (Roo):F DF ly ToF I SolFr InsulF onF | 0.1700F |
| F or (B u/sqF dFy):F | 1,175.5647F |
| VFpor SpF e ExpFns on F orF | |
| VFpor SpF e ExpFns on F orF VFpor SpF e ExpFns on F or:F | 0.0342F |
| DF ly VFpor TemperF ure RFnge (deg. R):F | 19.2277F |
| DF ly VFpor Pressure RFnge (psF):F | 0.0007F |
| BreF her Ven Press. SeF ng RFnge(psF):F | 0.0600F |
| VFpor Pressure F DF ly AverFge L qu dF | |
| SurF e TemperF ure (psF):F | 0.0031F |
| VFpor Pressure F DF ly M n mum L qu dF | |
| SurF e TemperF ure (psF):F | 0.0031F |
| VFpor Pressure F DF ly MFx mum L qu dF | |
| SurF e TemperF ure (psF):F | 0.0038F |
| DF ly Avg. L qu d SurF e Temp. (deg R):F | 499.7017F |
| DF ly Avg. L qu d SurF e Temp. (deg R):F DF ly M n. L qu d SurF e Temp. (deg R):F DF ly MFx. L qu d SurF e Temp. (deg R):F | 494.8947F |
| DF ly MFx. L qu d SurF e Temp. (deg R):F | 504.5086F |
| DF ly Amb en Temp. RFnge (deg. R).F | 18.9333F |
| Ven ed VFpor SF urF on F orF Ven ed VFpor SF urF on F or:F | 0.00745 |
| ven ea v-por SHurt on Hor:H | 0.9971F |
| VFpor Pressure F DF ly AverFge L qu d:F | |
| SurF e TemperF ure (psF):F VFpor SpF e OuF ge (F):F | 0.0031F 17.5967F |
| | |
| Working Losses (lb):F | 69.1835F 130.0000F |
| VFpor MoleFulFr We gh (lb/lb-mole):F VFpor Pressure F DF ly AverFge L qu dF | 130.0000F |
| | 0.0031F |
| SurF e TemperFure (psF):F | |
| AnnuFl Ne Throughpu (gFl/yr.):F AnnuFl Turnovers:F | 10,791,747.8413F 59.9400F |
| | |
| Turnover F or:F | 0.6672F |
| MFx mum L qu d Volume (gFl):F | 180,042.5065F |
| MFx mum L qu d He gh (F):F | 28.1400F |
| TFnk DF me er (F):F Work ng Loss ProduF F or:F | 33.0000F 1.0000F |
| | 1.50001 |
| ToF I Losses (lb):F | 83.2962F |
| | |

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TANKS 4.P.P issions Report - Detail ForP at P InPiviPual Tank P ission TotalsP

issions Report for: Annual P

NTPC Turbine Diesel Tank - Vertical FixeP Roof TankP Duluth, WisconsinP

Losses(lbs)F

 Componen®F
 Working LossF
 BreFining LossF
 ToFIEmissionsF

 DisFIIF eitled of no. 2F
 69.18F
 14.11F
 83.30F

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TANKS 4.P.P

issions Report - Detail ForP at P Tank InPentification anP Physical CharacteristicsP

IPentificationP

User IdenD CDy:D SD e:D on:D NTEC F re Pump TDnkD Super orD W sDons nD CompDny:D Type o TDnk:D esDr pDon:D NTECD Hor zonDI TDnkD 350 gDlon d esel DnkD

Tank DiP ensionsP
Shell Leng h (D):D
me er (D):D
Volume (gDlons):D
Turnovers:D 5.00D 3.45D 350.00D Ne Throughpu (gDl/yr):D Is TDnk HeD ed (y/n):D Is TDnk Underground (y/n):D 7,291.55D

ND

aint CharacteristicsP Shell Color/ShDde:D

WhDe/WhDeD Shell CondDonD GoodD

Breather Vent SettingsP VD uum SeDngs (ps g):D Pressure SeDngs (ps g)D -0.03D

 $\label{eq:main_model} \mbox{Me erologD ID} \quad \mbox{used n Em ss ons CD ulD ons: Dulu h, MnnesoD (Avg A mospherD Pressure = 13.98 psD)D}$

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TANKS 4.P.P issions Report - Detail ForP at P LiquiP Contents of Storage TankP

NTPC Fire PuP p Tank - Horizontal TankP Superior, WisconsinP

| , | L qu dD ly L qu d Sur .D BulkD TemperDure (deg F)D TempD | | | | | | | V porD Mol.D | L qu dD M ssD | V porD M ssD | Mol.D | B ss or VDpor PressureD | |
|----------------------|--|---------|-------|--------|----------|---------|---------|-----------------|------------------|-----------------|--------|-------------------------|-------------------------------------|
| M x ure/ComponenD | Mon hl | D Avg.D | M n.D | M x.D | (deg F)D | Avg.D | M n.D | M x.D | We gh .D | FrD .D | FrD .D | We ghD | C I ulD onsD |
| s IIDe uel o I no. 2 | AIID | 40.03D | 35.22 | 44.84D | 38.46D | 0.0031D | 0.0031D | 0.0038D | 130.0000D | | | 188.00D | OpDon 1: VP40 = .0031 VP50 = .0045D |

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TANKS 4.P.P issions Report - Detail ForP at P Detail Calculations (AP-42)P

NTPC Fire PuP p Tank - Horizontal TankP Superior, WisconsinP

| AnnuDl Em ss on CDID uID onsD | |
|--|-------------|
| SD nd ng Losses (lb):D | 0.0280D |
| VDpor SpD e Volume (Du D):D | 29.8059D |
| VDpor DensDy (lb/Du D):D | 0.0001D |
| VDpor SpD e ExpDns on FD or:D | 0.0342 |
| Ven ed VDpor SDurD on FD or:D | 0.9997D |
| TDnk VDpor SpD e Volume:D | |
| VDpor SpD e Volume (Du D):D | 29.8059D |
| TDnk D me er (D):D | 3.4520D |
| EDeD ve D me er (D):D | 4.6891D |
| VDpor SpD e OuD ge (D):D | 1.7260D |
| TDnk Shell Leng h (D):D | 5.0000D |
| VDpor DensD/D | |
| VDpor DensDy (lb/Du D):D | 0.0001D |
| VDpor MoleDuIDr We gh (lb/lb-mole):D | 130.0000D |
| VDpor Pressure D D ly AverDge L qu dD | |
| SurD e TemperDure (psD):D | 0.0031D |
| D ly Avg. L qu d SurD e Temp. (deg. R):D | 499.7017D |
| D ly AverDge Amb en Temp. (deg. F):D | 38.4417D |
| IdeDI GDs ConsDn RD | |
| (psD DiD/ (lb-mol-deg R)):D | 10.731D |
| L qu d Bulk TemperDure (deg. R):D | 498.1317D |
| TDnk PDn SolDr AbsorpDn e (Shell):D | 0.1700D |
| D ly ToDI SolDr InsulD onD | 4 475 50470 |
| FD or (B u/sqDdDy):D | 1,175.5647D |
| V por SpD e ExpDns on FD_orD | |
| VDpor SpD e ExpDns on FD or:D | 0.0342 |
| D ly VDpor TemperDure RDnge (deg. R):D | 19.2277D |
| D ly VDpor Pressure RDnge (psD):D | 0.0007D |
| BreDher Ven Press. SeDng RDnge(psD):D | 0.0600D |
| VDpor Pressure D D Iy AverDge L qu dD | 0.0004D |
| SurD e TemperDure (psD):D | 0.0031D |
| VDpor Pressure D D ly M n mum L qu dD | 0.0031D |
| SurD e TemperDure (psD):D VDpor Pressure D D Iy MDx mum L qu dD | 0.0031D |
| SurD e TemperDure (psD):D | 0.0038D |
| D ly Avg. L qu d SurD e Temp. (deg R):D | 499.7017D |
| D ly M n. L qu d SurD e Temp. (deg R):D | 494.8947D |
| D ly MDx. L qu d SurD e Temp. (deg R):D | 504.5086D |
| D ly Amb en Temp. RDnge (deg. R):D | 18.9333D |
| | |
| Ven ed VDpor SDurD on FD orD Ven ed VDpor SDurD on FD or:D | 0.9997D |
| VDpor Pressure D D ly AverDge L qu d:D | 0.33311 |
| SurD e TemperDure (psD):D | 0.0031D |
| VDpor SpD e OuD ge (D):D | 1.7260D |
| | |
| Work ng Losses (lb):D | 0.0701D |
| VDpor MoleDulDr We gh (lb/lb-mole):D | 130.0000D |
| VDpor Pressure D D ly AverDge L qu dD | |
| SurD e TemperDuré (psD):D | 0.0031D |
| AnnuDl Ne Throughpu (gDl/yr.):D | 7,291.5500D |
| AnnuDl Turnovers:D | 20.8330D |
| Turnover FD or:D | 1.0000D |
| TDnk D me er (D):D | 3.4520D |
| Work ng Loss ProduD FD or:D | 1.0000D |
| | |
| ToDI Losses (lb):D | 0.0981D |
| | |

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TANKS 4.P.P issions Report - Detail ForP at P InPiviPual Tank P ission TotalsP

issions Report for: Annual P

NTPC Fire PuP p Tank - Horizontal TankP Superior, WisconsinP

Losses(lbs)D

 Componen sD
 Work ng LossD
 BreDh ng LossD
 ToDI Em ss onsD

 sDIDe uel ol no. 2
 0.07D
 0.03D
 0.10D

Page 1 of S 4.0 Report

TANKS 4.P.P

issions Report - Detail ForP at P Tank InPentification anP Physical CharacteristicsP

IPentificationP

User Iden1 C1y:1 S1 e:1 NTEC Gen T1nk1 Super or1 W s1ons n1 Comp1ny:1 Type o1T1nk:1 Des1r p1on:1 NTEC1 Hor zon1 I T1nk1 ,700 g1llon d esel 1 nk1

Tank DiP ensionsP
Shell Leng 1 (1):1
D1 me1er (1):1
Volume (g1llons):1
Turnovers:1 8.041 6.001 ,700.001 Ne1Throughpu1(g1l/yr):1 Is T1nk He1 ed (y/n):1 Is T1nk Underground (y/n):1 35,360.001

N1

aint CharacteristicsP Shell Color/Sh1de:1 Wh1e/Wh1e1 Shell Cond1 on1

Breather Vent SettingsP V uum Se1 ngs (ps g):1 Pressure Se1 ngs (ps g)1 -0.031

Me1erolog1 I D1 used n Em ss ons C1I ul1 ons: Dulu1h, M nneso1 (Avg A mospher1 Pressure = 13.98 ps1)1

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TANKS 4.P.P issions Report - Detail ForP at P LiquiP Contents of Storage TankP

NTPC Gen Tank - Horizontal TankP Superior, WisconsinP

| | | D1 Tem | ly L qu d Su per1 ure (de | ır11 g F)1 | L qu d1 Bulk1 Temp1 | V po | r Pressure | (ps1)1 | V por1 Mol.1 | L qu d1 M ss1 | V por1 M ss1 | Mol.1 | B s s for V por Pressure1 |
|--------------------------|--------|-----------|------------------------------|---------------|---------------------------|--------|------------|---------|-----------------|------------------|-----------------|--------|-------------------------------------|
| M x1ure/Componen1 | Mon h1 | Avg.1 | M n.1 | M x.1 | (deg F)1 | Avg.1 | M n.1 | M x.1 | We gh11 | Fr1 .1 | Fr1 .1 | We gh1 | C I ul1 ons1 |
| D s1ll1 e uel o l no. 21 | All1 | 40.031 | 35.221 | 44.841 | 38.461 | 0.0031 | 0.0031 | 0.00381 | 30.00001 | | | 88.001 | Op1on 1: VP40 = .0031 VP50 = .00451 |

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TANKS 4.P.P issions Report - Detail ForP at P Detail Calculations (AP-42)P

NTPC Gen Tank - Horizontal TankP Superior, WisconsinP

| Annual Emission California | |
|--|--------------------|
| Annu1 Em ss on C1I1 ul1 ons1 | 0.4004 |
| S1 nd ng Losses (lb):1 | 0.1361 |
| V por Sp1 e Volume (1u 1):1 V por Dens1y (lb/1u 1):1 | 44.75741 0.0001 |
| v por Density (ID/10 1):1 | |
| V por Sp1 e Exp1ns on F1 or:1 | 0.03421 |
| Ven ed V por S1 ur1 on F1 or:1 | 0.99951 |
| T1nk V por Sp1 e Volume:1 V por Sp1 e Volume (1u 1):1 | 44.75741 |
| | 6.00001 |
| T1nk D1 me er (1):1 | 7.83821 |
| E1e1 ve D1 me er (1):1 | 3.00001 |
| V por Sp1 e Ou1 ge (1):1 T1nk Shell Leng h (1):1 | 8.03801 |
| V por Dens1y1 | |
| V por Dens1y (lb/1u 1):1 | 0.0001 |
| V por Mole1ul1r We gh (lb/lb-mole):1 | 30.00001 |
| V por Pressure 1 D1 ly Aver1ge L qu d1 | |
| Sur1 e Temper1 ure (ps1):1 | 0.0031 |
| D1 ly Avg. L qu d Sur1 e Temp. (deg. R):1 | 499.70171 |
| D1 ly Aver1ge Amb en Temp. (deg. F):1 | 38 44171 |
| Ide1I G1s Cons1 n R1 | |
| (ps1 1u1 / (lb-mol-deg R)):1 | 0.731 |
| L qu d Bulk Temper1 ure (deg. R):1 | 498.13171 |
| T1nk P1 n Sol1r Absorp1 n1e (Shell):1 | 0.17001 |
| D1 ly To1 Sol1r Insul1 on1 F1 or (B u/sq1 d1y):1 | ,175.56471 |
| V por Sp1 e Exp1ns on F1 or1 | |
| V por Sp1 e Exp1ns on F1 or:1 | 0.03421 |
| D1 ly V por Temper1 ure R1nge (deg. R):1 | 9.22771 |
| D1 ly V por Pressure R1nge (ps1):1 | 0.00071 |
| Bre1 her Ven Press. Se1 ng R1nge(ps1):1 | 0.06001 |
| V por Pressure 1 D1 ly Aver1ge L qu d1 | |
| Sur1 e Temper1 ure (ps1):1 | 0.0031 |
| V por Pressure 1 D1 ly M n mum L qu d1 | |
| Sur1 e Temper1 uré (ps1):1 | 0.0031 |
| V por Pressure 1 D1 ly M1x mum L qu d1 | |
| Sur1 e Temper1 uré (ps1):1 | 0.00381 |
| D1 ly Avg. L qu d Sur1 e Temp. (deg R):1 | 499.70171 |
| D1 lý M n. L qu d Sur1 e Temp. (deg R):1 | 494.89471 |
| D1 ly M1x. L qu d Sur1 e Temp. (deg R):1 | 504.50861 |
| D1 ly Amb en Temp. R1nge (deg. R):1 | 8.93331 |
| Ven ed V por S1 ur1 on F1 or1 | |
| Ven ed V por S1 ur1 on F1 or:1 | 0.99951 |
| V por Pressure 1 D1 ly Aver1ge L qu d:1 | |
| Sur1 e Temper1 ure (ps1):1 | 0.0031 |
| V por Sp1 e Ou1 ge (1):1 | 3.00001 |
| Mark and Lancas (lb.):1 | 0.33981 |
| Work ng Losses (lb):1 V por Mole1ul1r We gh (lb/lb-mole):1 | 30.00001 |
| V por Pressure 1 D1 ly Aver1ge L qu d1 | 30.00001 |
| Sur1 e Temper1 ure (ps1):1 | 0.0031 |
| | 35,360.00001 |
| Annu1 Ne Throughpu (g1l/yr.):1 | |
| Annu1l Turnovers:1 | 20.80001 |
| Turnover F1 or:1 | .00001 |
| T1nk D1 me er (1):1 | 6.00001 |
| Work ng Loss Produ1 F1 or:1 | .00001 |
| To1 I Losses (lb):1 | 0.47581 |
| • • | |

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TANKS 4.P.P issions Report - Detail ForP at P InPiviPual Tank P ission TotalsP

issions Report for: Annual P

NTPC Gen Tank - Horizontal TankP Superior, WisconsinP

Losses(lbs)1

 Components1
 Working Loss1
 Bre1 hing Loss1
 To1 | Emissions1

 Distill eituel oil no. 21
 0.341
 0.141
 0.481



| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре | Turbine Model |
|----------|---|---|----------------|------------|--|-------------|-----------------------|----------|--------|------------------------------|
| | | | Nitrogen Oxide | | | | | | | |
| CA-1192 | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | MW | SCR/DLN | 160 | lb/hr | BACT | |
| CA-1192 | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | MW | SCR/DLN | 160 | lb/hr | BACT | |
| MI-0423 | INDECK NILES, LLC | INDECK NILES, LLC | 1/4/2017 | 8,322 | MMBtu/hr | SCR/DLN | 0.034 | lb/MMBtu | BACT | |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | 2,147 | MMBtu/hr | SCR/DLN | 0.082 | lb/MMBtu | BACT | |
| LA-0224 | ARSENAL HILL POWER PLANT | SOUTHWEST ELECTRIC POWER COMPANY (SWEPCO) | 3/20/2008 | 2,110 | MMBtu/hr | GCP | 0.190 | lb/MMBtu | BACT | |
| CA-1178 | APPLIED ENERGY LLC | APPLIED ENERGY LLC | 3/20/2009 | 2,234 | MMBtu/hr | SCR | 2.0 | | BACT | |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | | SCR | | ppm | BACT | |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | | SCR | | ppm | BACT | |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | | SCR | | ppm | BACT | |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | | SCR | | ppm | BACT | |
| | | | | 180 | | | | | BACT | + |
| | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | | | SCR/DLN | | ppm | | |
| CA-1192 | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | | SCR/DLN | | ppm | BACT | |
| CA-1192 | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | | SCR/DLN | | ppm | BACT | |
| CA-1192 | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | | SCR/DLN | | ppm | BACT | |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | SCR/DLN | 2.0 | ppm | BACT | |
| CA-1212 | PALMDALE HYBRID POWER PROJECT | CITY OF PALMDALE | 10/18/2011 | 154 | MW | SCR/DLN | 2.0 | ppm | BACT | |
| FL-0303 | FPL WEST COUNTY ENERGY CENTER UNIT 3 | FLORIDA POWER AND LIGHT COMPANY (FP&L) | 7/30/2008 | 2,333 | MMBtu/hr | SCR/DLN | 2.0 | ppm | BACT | |
| FL-0304 | CANE ISLAND POWER PARK | FLORIDA MUNICIPAL POWER AGENCY (FMPA | 9/8/2008 | 1,860 | MMBtu/hr | SCR | | ppm | BACT | GE 7241 FA CTG |
| FL-0337 | POLK POWER STATION | TAMPA ELECTRIC COMPANY | 10/14/2012 | | | SCR/DLN | | ppm | BACT | |
| FL-0356 | OKEECHOBEE CLEAN ENERGY CENTER | FLORIDA POWER & LIGHT | 3/9/2016 | | | SCR/DLN/WI | | ppm | BACT | GE 7HA.02 |
| IA-0107 | MARSHALLTOWN GENERATING STATION | INTERSTATE POWER AND LIGHT | 4/14/2014 | | MMBtu/hr | SCR/DLN | | ppm | BACT | GE TIM.02 |
| IA-0107 | MARSHALLTOWN GENERATING STATION | INTERSTATE FOWER AND LIGHT | 4/14/2014 | | MMBtu/hr | SCR/LNB | | ppm | BACT | Siemens SGT6-5000F |
| | | | | | | · · | | | | |
| ID-0018 | LANGLEY GULCH POWER PLANT | IDAHO POWER COMPANY | 6/25/2010 | | MMBtu/hr | SCR/DLN/GCP | | ppm | BACT | Siemens SGT6-5000F |
| IN-0158 | ST. JOSEPH ENEGRY CENTER, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 2,300 | MMBtu/hr | SCR/DLN | 2.0 | ppm | BACT | |
| | | | | | | | | | | SGT-8000H VERSION 1.4- |
| | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | | SCR/DLN/GCP | | ppm | BACT | OPTIMIZED |
| MD-0046 | KEYS ENERGY CENTER | KEYS ENERGY CENTER, LLC | 10/31/2014 | 235 | MW | SCR/DLN/GCP | | ppm | BACT | SGT6-500FEE |
| MI-0405 | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | 2,486 | MMBtu/hr | SCR/DLN | 2.0 | ppm | BACT | |
| MI-0405 | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | 2,237 | MMBtu/hr | SCR/DLN | 2.0 | ppm | BACT | |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | 2,147 | MMBtu/hr | SCR/DLN | 2.0 | ppm | BACT | |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | 2,807 | MMBtu/hr | SCR/DLN | | ppm | BACT | |
| | | | | | | , | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 5 579 | MMBtu/hr | SCR/DLN | 2.0 | ppm | BACT | 2 Siemens SGT-8000H |
| 011 0002 | CHECON CEETIN ENERGY CENTER | 7.110.10.10, 00, 1110. | 0,10,2015 | 3,373 | ······································ | JOHN DEIT | 2.0 | pp | 5,10. | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | E E70 | MMBtu/hr | SCR/DLN | 2.0 | ppm | BACT | 2 Siemens SGT-8000H |
| UH-0332 | OREGON CLEAN ENERGY CENTER | ARCADIS, 03, INC. | 0/10/2013 | 3,379 | IVIIVIBLU/III | JCK/ DLN | 2.0 | ppiii | BACI | |
| 011 0252 | ODECON CLEAN ENERGY CENTER | ABCARIC US INC | 6/40/2042 | 5.004 | /1 | CCD /D1 N | 2.0 | | D 4 CT | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 6,004 | MMBtu/hr | SCR/DLN | 2.0 | ppm | BACT | 2 Siemens SGT-8000H |
| | | | 1 | | | | | | | Mitsubishi M501 GAC units or |
| | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 799 | | SCR/DLN | | ppm | BACT | 2 Siemens SGT-8000H |
| | CHOUTEAU POWER PLANT | ASSOCIATED ELECTRIC COOPERATIVE INC | 1/23/2009 | | MMBtu/hr | SCR/DLN | | ppm | BACT | SIEMENS V84.3A |
| OK-0154 | MOORELAND GENERATING STA | WESTERN FARMERS ELECTRIC COOPERATIVE | 7/2/2013 | 360 | MW | SCR/DLN | 2.0 | ppm | BACT | Siemens SGT6-5000F5 |
| OK-0154 | MOORELAND GENERATING STA | WESTERN FARMERS ELECTRIC COOPERATIVE | 7/2/2013 | 360 | MW | SCR/DLN | 2.0 | ppm | BACT | Siemens SGT6-5000F5 |
| OR-0048 | CARTY PLANT | PORTLAND GENERAL ELECTRIC | 12/29/2010 | 2,866 | MMBtu/hr | SCR | 2.0 | ppm | BACT | |
| OR-0050 | TROUTDALE ENERGY CENTER, LLC | TROUTDALE ENERGY CENTER, LLC | 3/5/2014 | 2,988 | MMBtu/hr | DLN/WI | 2.0 | ppm | BACT | Mitsubishi M501-GAC |
| PA-0278 | MOXIE LIBERTY LLC/ASYLUM POWER PLT | MOXIE ENERGY LLC | 10/10/2012 | | MMBtu/hr | SCR/DLN | | ppm | BACT | G or HA |
| PA-0286 | MOXIE ENERGY LLC/PATRIOT GENERATION PLT | MOXIE ENERGY LLC | 1/31/2013 | 472 | , | SCR | | ppm | BACT | 1 |
| TN-0162 | JOHNSONVILLE COGENERATION | TENNESSEE VALLEY AUTHORITY | 4/19/2016 | | MMBtu/hr | SCR/GCP | | ppm | BACT | |
| 3202 | | | .,, | 1,555 | | 22.,700. | 2.0 | r F | 1 | GE 7FA, GE 7FB, AND SIEMENS |
| TX-0546 | PATTILLO BRANCH POWER PLANT | PATTILLO BRANCH POWER COMPANY LLC | 6/17/2009 | 350 | N/1\A/ | SCR | 2.0 | ppm | BACT | SGT6-5000F. |
| 17-0340 | TATTLES BRANCH FOWER FLAINT | TATTILLO BRANCH FOWER CONFAINT LLC | 0/1//2003 | 330 | 14144 | JUN | 2.0 | Phili | שאכו | |
| TV 05 47 | NATURAL CAS SIRED DOWER CONSTANTION SASTER | LAMAR ROWER BARTNERS !! ! C | 6/22/2006 | 25. | | 665 | | L | DACT | GE 7FAS OR 250 MW |
| | NATURAL GAS-FIRED POWER GENERATION FACILITY | LAMAR POWER PARTNERS II LLC | 6/22/2009 | 250 | | SCR | | ppm | BACT | MITSUBISHI 501GS |
| TX-0548 | MADISON BELL ENERGY CENTER | MADISON BELL PARTNERS LP | 8/18/2009 | 275 | | SCR | | ppm | BACT | GE PG7121(EA |
| TX-0600 | THOMAS C. FERGUSON POWER PLANT | LOWER COLORADO RIVER AUTHORITY | 9/1/2011 | 390 | | SCR/DLN | | ppm | BACT | GE 7FA |
| TX-0620 | ES JOSLIN POWER PLANT | CALHOUN PORT AUTHORITY | 9/12/2012 | 195 | MW | SCR | 2.0 | ppm | BACT | GE 7FA |
| TX-0678 | FREEPORT LNG PRETREATMENT FACILITY | FREEPORT LNG DEVELOPMENT LP | 7/16/2014 | 87 | MW | SCR | 2.0 | ppm | BACT | |
| | · | | | | 1 | · · | 1 | | | |
| | | | 1 | | | | | | | |
| | | | | j | | | | | | Siemens Model F5, GE7Fa, and |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре | Turbine Model |
|---------|---|---|--------------|------------|----------|--------------------|-----------------------|----------|------|-------------------------------|
| | | | | | | | | | | GE 7FA.04; (2 Siemens SGT6- |
| | | | | | | | | | | 5000F(4; or (3 Siemens SGT6- |
| TX-0708 | LA PALOMA ENERGY CENTER | LA PALOMA ENERGY CENTER, LLC | 2/7/2013 | 650 | MW | SCR | 2.0 | ppm | BACT | 5000F(5. |
| TX-0709 | SAND HILL ENERGY CENTER | CITY OF AUSTIN | 9/13/2013 | 174 | MW | SCR | | ppm | BACT | GE 7FA |
| TX-0710 | VICTORIA POWER STATION | VICTORIA WLE L.P. | 12/1/2014 | 197 | MW | SCR | 2.0 | ppm | BACT | GE 7FA.04 |
| TX-0712 | TRINIDAD GENERATING FACILITY | SOUTHERN POWER COMPANY | 11/20/2014 | 497 | MW | SCR | 2.0 | ppm | BACT | MHI J model |
| TX-0713 | TENASKA BROWNSVILLE GENERATING STATION | TENASKA BROWNSVILLE PARTNERS, LLC | 4/29/2014 | 274 | MW | SCR | 2.0 | ppm | BACT | |
| TX-0714 | S R BERTRON ELECTRIC GENERATING STATION | NRG TEXAS POWER LLC | 12/19/2014 | 240 | MW | SCR | | ppm | BACT | Siemens Model F5 (SF5 |
| TX-0730 | COLORADO BEND ENERGY CENTER | COLORADO BEND II POWER, LLC | 4/1/2015 | 1,100 | MW | SCR/OxCat | 2.0 | ppm | BACT | GE Model 7HA.02 |
| | | | | | | | | | | Siemens SCC6-5000 CTGs and |
| | | | | | | | | | | a SST6-5000 ST, or two GE 7FA |
| TX-0767 | LON C. HILL POWER STATION | LON C. HILL, L.P. | 10/2/2015 | 195 | MW | SCR | 2.0 | ppm | BACT | CTGs and a D-11 ST. |
| TX-0773 | FGE EAGLE PINES PROJECT | FGE EAGLE PINES, LLC | 11/4/2015 | 321 | MW | SCR | 2.0 | ppm | BACT | Alstom GT36 |
| TX-0788 | NECHES STATION | APEX TEXAS POWER LLC | 3/24/2016 | 231 | MW | SCR | | ppm | BACT | Siemens or GE |
| TX-0789 | DECORDOVA STEAM ELECTRIC STATION | DECORDOVA II POWER COMPANY LLC | 3/8/2016 | 231 | MW | SCR | | ppm | BACT | Siemens or GE |
| TX-0819 | GAINES COUNTY POWER PLANT | SOUTHWESTERN PUBLIC SERVICE COMPANY | 4/28/2017 | 426 | MW | SCR/DLN | _ | ppm | BACT | Siemens SGT6-5000F5 |
| | WARREN COUNTY POWER PLANT - DOMINION | VIRGINIA ELECTRIC AND POWER COMPANY | 12/17/2010 | | MMBtu/hr | SCR/DLN | | ppm | BACT | MHI M501 GAC |
| | | MOUNDSVILLE POWER, LLC | 11/21/2014 | | MMBtu/hr | SCR/DLN | _ | ppm | BACT | GE Frame 7FA.04 |
| | HIGH DESERT POWER PROJECT | HIGH DESERT POWER PROJECT LLC | 3/11/2010 | | MW | SCR/DLN | | ppm | BACT | oz manie mno |
| GA-0138 | LIVE OAKS POWER PLANT | LIVE OAKS COMPANY, LLC | 4/8/2010 | 600 | MW | SCR/DLN | | ppm | BACT | SGT6-5000F. |
| | THETFORD GENERATING STATION | CONSUMERS ENERGY COMPANY | 7/25/2013 | | MMBtu/hr | SCR/LNB | _ | ppm | BACT | 5010 500011 |
| MI-0412 | | HOLLAND BOARD OF PUBLIC WORKS | 12/4/2013 | 647 | MMBtu/hr | SCR/DLN | _ | ppm | BACT | |
| MI-0424 | | HOLLAND BOARD OF PUBLIC WORKS | 12/5/2016 | | MMBtu/hr | SCR/DLN | | ppm | BACT | |
| | FILER CITY STATION | FILER CITY STATION LIMITED PARTNERSHIP | 11/17/2017 | | MMBtu/hr | SCR/DLN | | ppm | BACT | |
| | | DUKE ENERGY HANGING ROCK, LLC | 12/18/2012 | | MW | SCR/DLN | | ppm | BACT | GE 7FA |
| | DUKE ENERGY HANGING ROCK ENERGY | DUKE ENERGY HANGING ROCK, LLC | 12/18/2012 | 172 | | SCR/DLN | | ppm | BACT | GE 7FA |
| LA-0224 | | SOUTHWEST ELECTRIC POWER COMPANY (SWEPCO) | 3/20/2008 | | MMBtu/hr | SCR/DLN SCR/LNB | | ppm | BACT | GE /FA |
| | INTERNATIONAL STATION POWER PLANT | CHUGACH ELECTRIC ASSOCIATION | 12/20/2010 | | MW | SCR/DLN | | | BACT | |
| LA-0136 | PLAQUEMINE COGENERATION FACILITY | | 7/23/2008 | | MMBtu/hr | SCR/DLN SCR/DLN | | ppm | BACT | GE FRAME 7 FA |
| | - | THE DOW CHEMICAL COMPANY | | | | | | ppm | | GE FRAIVIE / FA |
| LA-0308 | MORGAN CITY POWER PLANT | LOUISIANA ENERGY AND POWER AUTHORITY (LEPA) | 9/26/2013 | | MMBtu/hr | SCR/WI | | ppm | BACT | CE 754 |
| TX-0698 | BAYPORT COMPLEX | AIR LIQUIDE LARGE INDUSTRIES U.S., L.P. | 9/5/2013 | | MW | DLN, CLEC | | ppm | BACT | GE 7EA |
| MI-0402 | SUMPTER POWER PLANT | WOLVERINE POWER SUPPLY COOPERATIVE INC. | 11/17/2011 | | MW | LNB | | ppm | BACT | |
| | ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | | MMBtu/hr | SCR/DLN | | ppm | BACT | |
| LA-0313 | ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | | MMBtu/hr | SCR/DLN | 15.0 | | BACT | |
| | THETFORD GENERATING STATION | CONSUMERS ENERGY COMPANY | 7/25/2013 | | MMBtu/hr | SCR/LNB | 78.4 | | BACT | |
| PA-0296 | BERKS HOLLOW ENERGY ASSOC LLC/ONTELAUNEE | BERKS HOLLOW ENERGY ASSOC LLC | 12/17/2013 | | MMBtu/hr | SCR | 131.6 | tpy | BACT | |
| | I | | Carbon Monox | | | | | lu / | T | |
| | INDECK NILES, LLC | INDECK NILES, LLC | 1/4/2017 | | MMBtu/hr | OxCat/GCP | _ | lb/MMBtu | BACT | |
| PA-0296 | BERKS HOLLOW ENERGY ASSOC LLC/ONTELAUNEE | BERKS HOLLOW ENERGY ASSOC LLC | 12/17/2013 | | MMBtu/hr | OxCat | _ | | BACT | |
| | THETFORD GENERATING STATION | CONSUMERS ENERGY COMPANY | 7/25/2013 | | MMBtu/hr | OxCat/GCP | | lb/MMBtu | BACT | |
| OK-0169 | PSO COMANCHE POWER STATION | PUBLIC SERVICE COMPANY OF OKLAHOMA | 10/8/2015 | | MMBtu/hr | DLN | 0.079 | lb/MMBtu | BACT | |
| | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | | MMBtu/hr | OxCat | | lb/MMBtu | BACT | |
| MI-0412 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | | 12/4/2013 | | MMBtu/hr | OxCat/GCP | | lb/MMBtu | BACT | |
| | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | | 12/5/2016 | | MMBtu/hr | OxCat/GCP | | lb/MMBtu | BACT | |
| LA-0224 | ARSENAL HILL POWER PLANT | SOUTHWEST ELECTRIC POWER COMPANY (SWEPCO) | 3/20/2008 | 2,110 | MMBtu/hr | GCP | 0.747 | lb/MMBtu | BACT | |
| MI-0405 | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | | MMBtu/hr | GCP | 1.396 | | BACT | |
| CT-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | 2,639 | MMBtu/hr | OxCat | _ | lb/MMBtu | BACT | |
| CT-0151 | KLEEN ENERGY SYSTEMS, LLC | KLEEN ENERGY SYSTEMS, LLC | 2/25/2008 | 2,142 | MMBtu/hr | OxCat | 0.9 | ppm | BACT | SIEMENS SGT6-5000F |
| CT-0157 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | 2,420 | MMBtu/hr | OxCat | 0.9 | ppm | BACT | GE 7HA.01 |
| CT-0158 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | 2,420 | MMBtu/hr | OxCat | 0.9 | ppm | BACT | GE 7HA.01 |
| CT-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | 2,969 | MMBtu/hr | OxCat | 0.9 | ppm | BACT | Mitsubishi M501JAC |
| NJ-0082 | WEST DEPTFORD ENERGY STATION | WEST DEPTFORD ENERGY ASSOCIATES | 7/18/2014 | 2,362 | MMBtu/hr | OxCat/GCP/Fuel | _ | ppm | BACT | Siemens F |
| | - | **** | , | ,.,_ | | , , | 1 | ĺ | | Never built. Proposed Model |
| CA-1192 | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | MW | OxCat | 1.5 | ppm | BACT | GE 7241 FA |
| | | | | | | | | | | Never built. Proposed Model |
| | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | MW | OxCat | 1.5 | ppm | BACT | GE 7241 FA |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре | Turbine Model |
|--------------------|--|--|------------------------|------------|----------|------------------|-----------------------|------------|--------------|--------------------------------|
| | | | | | | | | | | Never built. In 2011, proposed |
| | | | | | | | | | | turbines were GE. Currently |
| | | | | | | | | | | proposed turbines are Siemens |
| | PALMDALE HYBRID POWER PROJECT | CITY OF PALMDALE | 10/18/2011 | | MW | OxCat | | ppm | BACT | STG6-5000F |
| NJ-0082 | WEST DEPTFORD ENERGY STATION | WEST DEPTFORD ENERGY ASSOCIATES | 7/18/2014 | | MMBtu/hr | OxCat/GCP/Fuel | | ppm | BACT | Siemens F |
| | WARREN COUNTY POWER PLANT - DOMINION | VIRGINIA ELECTRIC AND POWER COMPANY | 12/17/2010 | , | MMBtu/hr | OxCat/GCP | | ppm | BACT | MHI M501 GAC |
| GA-0127 | PLANT MCDONOUGH COMBINED CYCLE | SOUTHERN COMPANY/GEORGIA POWER | 1/7/2008 | | MW | OxCat | | ppm | BACT | MITSUBISHI MODEL M501G |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | | MW | OxCat | | ppm | BACT | |
| CA-1191 CA-1192 | VICTORVILLE 2 HYBRID POWER PROJECT AVENAL ENERGY PROJECT | CITY OF VICTORVILLE AVENAL POWER CENTER LLC | 3/11/2010 6/21/2011 | | MW | OxCat OxCat | | ppm ppm | BACT BACT | |
| CA-1192 | AVENAL ENERGY PROJECT AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC AVENAL POWER CENTER LLC | 6/21/2011 | | MW | OxCat | | ppm | BACT | + |
| GA-0138 | LIVE OAKS POWER PLANT | LIVE OAKS COMPANY, LLC | 4/8/2010 | | MW | OxCat/GCP | | ppm | BACT | SGT6-5000F. |
| IA-0107 | MARSHALLTOWN GENERATING STATION | INTERSTATE POWER AND LIGHT | 4/14/2014 | | MMBtu/hr | OxCat | | ppm | BACT | 3010-30001. |
| IA-0107 | MARSHALLTOWN GENERATING STATION | INTERSTATE POWER AND LIGHT | 4/14/2014 | 2,258 | | OxCat | | ppm | BACT | Siemens SGT6-5000F |
| ID-0018 | LANGLEY GULCH POWER PLANT | IDAHO POWER COMPANY | 6/25/2010 | | MMBtu/hr | OxCat, DLN, GCP | | ppm | BACT | Siemens SGT6-5000F |
| | ST. JOSEPH ENEGRY CENTER, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | | MMBtu/hr | OxCat | | ppm | BACT | Siemens sere seee. |
| | ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | | MMBtu/hr | OxCat, DLN, GCP | | ppm | BACT | |
| LA-0313 | ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | | MMBtu/hr | OxCat, DLN, GCP | | ppm | BACT | |
| | CPV ST. CHARLES | CPV MARYLAND, LLC | 4/23/2014 | | MW | OxCat/GCP | | ppm | BACT | GE F class |
| | | | ,,=0,=0=1 | | | | | PP | | SGT-8000H VERSION 1.4- |
| MD-0045 | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | MW | OxCat/GCP | 2.0 | ppm | BACT | OPTIMIZED |
| | KEYS ENERGY CENTER | KEYS ENERGY CENTER, LLC | 10/31/2014 | | MW | OxCat/GCP | | ppm | BACT | SGT6-500FEE |
| | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | | MMBtu/hr | OxCat | | ppm | BACT | 55.15.55.12 |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | | MMBtu/hr | OxCat | | ppm | BACT | |
| NJ-0074 | WEST DEPTFORD ENERGY | LS POWER | 5/6/2009 | 2,014 | | OxCat | | ppm | BACT | |
| NJ-0079 | WOODBRIDGE ENERGY CENTER | CPV SHORE, LLC | 7/25/2012 | 4,692 | | OxCat/GCP | | ppm | BACT | GE |
| NJ-0079 | WOODBRIDGE ENERGY CENTER | CPV SHORE, LLC | 7/25/2012 | 4,692 | | OxCat/GCP/Fuel | | ppm | BACT | GE 7FA |
| NJ-0080 | HESS NEWARK ENERGY CENTER | HESS NEWARK ENERGY CENTER, LLC | 11/1/2012 | 4,595 | | OxCat/GCP/Fuel | | ppm | BACT | GE |
| NJ-0080 | HESS NEWARK ENERGY CENTER | HESS NEWARK ENERGY CENTER, LLC | 11/1/2012 | 4,595 | | OxCat | | ppm | BACT | GE |
| | | , | ,,, | , | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | OxCat/GCP/Fuel | 2.0 | ppm | BACT | 5000F |
| | | | | | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | OxCat, GCP, Fuel | 2.0 | ppm | BACT | 5000F |
| | | | | | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | OxCat, GCP, Fuel | 2.0 | ppm | BACT | 5000F |
| | | | | | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | OxCat, GCP, Fuel | 2.0 | ppm | BACT | 5000F |
| NJ-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | MW | OxCat/GCP | 2.0 | ppm | BACT | GE 7HA.02 |
| NJ-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | MW | OxCat/GCP | 2.0 | ppm | BACT | GE 7HA.02 |
| NY-0104 | CPV VALLEY ENERGY CENTER | CPV VALLEY LLC | 8/1/2013 | 2,234 | MMBtu/hr | OxCat/GCP | 2.0 | ppm | BACT | |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 5,579 | MMBtu/hr | OxCat | 2.0 | ppm | BACT | 2 Siemens SGT-8000H |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 5,579 | MMBtu/hr | OxCat | 2.0 | ppm | BACT | 2 Siemens SGT-8000H |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 6,004 | MMBtu/hr | OxCat | 2.0 | ppm | BACT | 2 Siemens SGT-8000H |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 799 | MW | OxCat | 2.0 | ppm | BACT | 2 Siemens SGT-8000H |
| | MOORELAND GENERATING STA | WESTERN FARMERS ELECTRIC COOPERATIVE | 7/2/2013 | | MW | OxCat/GCP | | ppm | BACT | Siemens SGT6-5000F5 |
| | MOORELAND GENERATING STA | WESTERN FARMERS ELECTRIC COOPERATIVE | 7/2/2013 | 360 | | OxCat/GCP | | ppm | BACT | Siemens SGT6-5000F5 |
| | MOXIE LIBERTY LLC/ASYLUM POWER PL T | MOXIE ENERGY LLC | 10/10/2012 | | MMBtu/hr | OxCat | | ppm | BACT | F Class |
| PA-0286 | MOXIE ENERGY LLC/PATRIOT GENERATION PLT | MOXIE ENERGY LLC | 1/31/2013 | 472 | | OxCat | | ppm | BACT | |
| TN-0162 | JOHNSONVILLE COGENERATION | TENNESSEE VALLEY AUTHORITY | 4/19/2016 | 1,339 | MMBtu/hr | OxCat/GCP | 2.0 | ppm | BACT | |
| | | | | | | | | | | GE 7FA, GE 7FB, AND SIEMENS |
| TX-0546 | PATTILLO BRANCH POWER PLANT | PATTILLO BRANCH POWER COMPANY LLC | 6/17/2009 | 350 | MW | OxCat | 2.0 | ppm | BACT | SGT6-5000F. |
| | | | | | | | | | | SGT6-5000F CTGs or four GE |
| TX-0590 | KING POWER STATION | PONDERA CAPITAL MANAGEMENT GP INC | 8/5/2010 | 1,350 | MW | OxCat/GCP | 2.0 | ppm | BACT | Frame 7FA CTGs |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре | Turbine Model |
|---------|---|--|-------------|------------|----------|-----------|----------------|-------|------|-------------------------------|
| | | | | | | | | | | 6: 14 1155 0575 |
| | | | 0 /00 /00 | 1 | | | | | | Siemens Model F5, GE7Fa, and |
| 1X-0689 | CEDAR BAYOU ELECTRIC GENERATION STATION | NRG TEXAS POWER | 8/29/2014 | 225 | MW | OxCat | 2.0 | ppm | BACT | Mitsubishi Heavy Industry G |
| | | | | İ | | | | | | GE 7FA.04; (2 Siemens SGT6- |
| | | | | l | | | | | | 5000F(4; or (3 Siemens SGT6- |
| | LA PALOMA ENERGY CENTER | LA PALOMA ENERGY CENTER, LLC | 2/7/2013 | 650 | | OxCat | | ppm | BACT | 5000F(5. |
| | SAND HILL ENERGY CENTER | CITY OF AUSTIN | 9/13/2013 | 174 | | OxCat | | ppm | BACT | GE 7FA |
| TX-0713 | TENASKA BROWNSVILLE GENERATING STATION | TENASKA BROWNSVILLE PARTNERS, LLC | 4/29/2014 | 274 | MW | OxCat | 2.0 | ppm | BACT | |
| | | | | İ | | | | | | Siemens SCC6-5000 CTGs and |
| | | | | İ | | | | | | a SST6-5000 ST, or two GE 7FA |
| | LON C. HILL POWER STATION | LON C. HILL, L.P. | 10/2/2015 | 195 | | OxCat | | ppm | BACT | CTGs and a D-11 ST. |
| | FGE EAGLE PINES PROJECT | FGE EAGLE PINES, LLC | 11/4/2015 | 321 | | OxCat | | ppm | BACT | Alstom GT36 |
| | GAINES COUNTY POWER PLANT | SOUTHWESTERN PUBLIC SERVICE COMPANY | 4/28/2017 | 426 | | SCR/DLN | | ppm | BACT | Siemens SGT6-5000F5 |
| | MOUNDSVILLE COMBINED CYCLE POWER PLANT | MOUNDSVILLE POWER, LLC | 11/21/2014 | 2,420 | MMBtu/hr | OxCat/GCP | 2.0 | ppm | BACT | GE 7FA.04 |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | OxCat | 3.0 | ppm | BACT | |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | OxCat | 3.0 | ppm | BACT | |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | OxCat | 3.0 | ppm | BACT | |
| LA-0254 | NINEMILE POINT ELECTRIC GENERATING PLANT | ENTERGY LOUISIANA LLC | 8/16/2011 | 7,146 | MMBtu/hr | OxCat/GCP | 3.0 | ppm | BACT | |
| OR-0050 | TROUTDALE ENERGY CENTER, LLC | TROUTDALE ENERGY CENTER, LLC | 3/5/2014 | 2,988 | MMBtu/hr | OxCat/GCP | 3.3 | ppm | BACT | Mitsubishi M501-GAC |
| CA-1209 | HIGH DESERT POWER PROJECT | HIGH DESERT POWER PROJECT LLC | 3/11/2010 | 190 | MW | OxCat | 4.0 | ppm | BACT | |
| MI-0410 | THETFORD GENERATING STATION | CONSUMERS ENERGY COMPANY | 7/25/2013 | 2,587 | MMBtu/hr | OxCat/GCP | 4.0 | ppm | BACT | |
| MI-0412 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | HOLLAND BOARD OF PUBLIC WORKS | 12/4/2013 | 647 | MMBtu/hr | OxCat/GCP | 4.0 | ppm | BACT | |
| MI-0424 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | HOLLAND BOARD OF PUBLIC WORKS | 12/5/2016 | 554 | MMBtu/hr | OxCat/GCP | | ppm | BACT | |
| MI-0427 | FILER CITY STATION | FILER CITY STATION LIMITED PARTNERSHIP | 11/17/2017 | 1,935 | MMBtu/hr | OxCat/GCP | 4.0 | ppm | BACT | |
| TX-0600 | THOMAS C. FERGUSON POWER PLANT | LOWER COLORADO RIVER AUTHORITY | 9/1/2011 | 390 | | OxCat/GCP | | ppm | BACT | GE 7FA |
| TX-0618 | CHANNEL ENERGY CENTER LLC | CHANNEL ENERGY CENTER LLC | 10/15/2012 | 180 | MW | GCP | 4.0 | ppm | BACT | Siemens 501F |
| | | | | | | | | | | |
| TX-0619 | DEER PARK ENERGY CENTER | DEER PARK ENERGY CENTER LLC | 9/26/2012 | 180 | MW | GCP | 4.0 | ppm | BACT | Siemens/Westinghouse 501F |
| | | CALHOUN PORT AUTHORITY | 9/12/2012 | 195 | | GCP | | ppm | BACT | GE 7FA |
| | FREEPORT LNG PRETREATMENT FACILITY | FREEPORT LNG DEVELOPMENT LP | 7/16/2014 | | MW | OxCat | | ppm | BACT | |
| | VICTORIA POWER STATION | VICTORIA WLE L.P. | 12/1/2014 | 197 | | OxCat | | ppm | BACT | GE 7FA.04 |
| | TRINIDAD GENERATING FACILITY | SOUTHERN POWER COMPANY | 11/20/2014 | 497 | | OxCat | | ppm | BACT | MHI J model |
| | S R BERTRON ELECTRIC GENERATING STATION | NRG TEXAS POWER LLC | 12/19/2014 | 240 | | OxCat | | ppm | BACT | Siemens Model F5 (SF5 |
| TX-0730 | COLORADO BEND ENERGY CENTER | COLORADO BEND II POWER, LLC | 4/1/2015 | 1,100 | | SCR/OxCat | | ppm | BACT | GE Model 7HA.02 |
| TX-0788 | NECHES STATION | APEX TEXAS POWER LLC | 3/24/2016 | 231 | | OxCat | | ppm | BACT | Siemens or GE |
| | DECORDOVA STEAM ELECTRIC STATION | DECORDOVA II POWER COMPANY LLC | 3/8/2016 | | MW | OxCat | | ppm | BACT | Siemens or GE |
| | OKEECHOBEE CLEAN ENERGY CENTER | FLORIDA POWER & LIGHT | 3/9/2016 | | MMBtu/hr | GCP | | ppm | BACT | GE 7HA.02 |
| | FPL WEST COUNTY ENERGY CENTER UNIT 3 | FLORIDA POWER & EIGHT FLORIDA POWER AND LIGHT COMPANY (FP&L) | 7/30/2008 | | MMBtu/hr | GCP | | ppm | BACT | GE 711A.02 |
| FL-0303 | CANE ISLAND POWER PARK | FLORIDA MUNICIPAL POWER AGENCY (FMPA | 9/8/2008 | | MMBtu/hr | GCP | | ppm | BACT | GE 7241 FA CTG |
| | | DUKE ENERGY HANGING ROCK, LLC | 12/18/2012 | 1,800 | MW | GCP/Fuel | | ppm | BACT | GE 7FA |
| | | DUKE ENERGY HANGING ROCK, LLC | 12/18/2012 | 172 | | GCP/Fuel | | | BACT | GE 7FA |
| | DUKE ENERGY HANGING ROCK ENERGY | | | | | | | ppm | | |
| | CHOUTEAU POWER PLANT MIDLAND COGENERATION VENTURE | ASSOCIATED ELECTRIC COOPERATIVE INC MIDLAND COGENERATION VENTURE | 1/23/2009 | | MMBtu/hr | GCP | | ppm | BACT | SIEMENS V84.3A |
| | | | 4/23/2013 | | MMBtu/hr | | | ppm | BACT | |
| GA-0127 | PLANT MCDONOUGH COMBINED CYCLE | SOUTHERN COMPANY/GEORGIA POWER | 1/7/2008 | 254 | | OxCat | | ppm | BACT | |
| LA-0224 | ARSENAL HILL POWER PLANT | SOUTHWEST ELECTRIC POWER COMPANY (SWEPCO) | 3/20/2008 | | MMBtu/hr | GCP | | ppm | BACT | |
| MI-0405 | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | 2,486 | MMBtu/hr | GCP | 10.5 | ppm | BACT | |
| | | | | | | | | | | GE 7FAS OR 250 MW |
| | | LAMAR POWER PARTNERS II LLC | 6/22/2009 | 250 | | GCP | | ppm | BACT | MITSUBISHI 501GS |
| | BAYPORT COMPLEX | AIR LIQUIDE LARGE INDUSTRIES U.S., L.P. | 9/5/2013 | | MW | DLN, CLEC | | ppm | BACT | GE 7EA |
| TX-0727 | CEDAR BAYOU ELECTRIC GENERATING STATION | NRG TEXAS POWER LLC | 3/31/2015 | 187 | | OxCat | | ppm | BACT | |
| TX-0548 | MADISON BELL ENERGY CENTER | MADISON BELL PARTNERS LP | 8/18/2009 | | MW | GCP | | ppm | BACT | GE PG7121(EA |
| LA-0136 | PLAQUEMINE COGENERATION FACILITY | THE DOW CHEMICAL COMPANY | 7/23/2008 | 2,876 | MMBtu/hr | GCP | 25.0 | ppm | BACT | GE FRAME 7 FA |
| | | | | 1 | | | | | | Never built. Proposed Model |
| CA-1192 | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | MW | Fuel | 11.8 | lb/hr | BACT | GE 7241 FA |
| | | | 1 | 1 |] | 1 | | | 1 | Never built. No turbine |
| | | | 1 | 1 | 1 | 1 | | | 1 | specified in Application for |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | Fuel | 12.0 | lb/hr | BACT | Certification of Project |
| | | | | 1 | | | | | | Never built. No turbine |
| | | | | | | | | | | |
| | | | | | | | | | | specified in Application for |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Type | Turbine Model |
|---------|---|--|---------------|------------|----------|---------------------------------|-----------------------|------------|------|--|
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | | Fuel | 13.5 | | BACT | GE 7FA |
| CA-1211 | COLOGA GENERATING STATION | FACILIC GAS & ELECTRIC CONFART | 3/11/2011 | 1/2 | 10100 | ruei | 13.5 | 15/111 | BACI | Never built. No turbine specified in Application for |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | Fuel | 18.0 | lb/hr | BACT | Certification of Project |
| CA 1131 | VICTORVILLE 2 ITTBRID TO WERT ROSECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | 10100 | i dei | 10.0 | 15/111 | BACI | Never built. No turbine |
| | | | | | | | | | | specified in Application for |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 15/ | MW | Fuel | 18.0 | lb/hr | BACT | Certification of Project |
| TX-0620 | ES JOSLIN POWER PLANT | CALHOUN PORT AUTHORITY | 9/12/2012 | | MW | GCP/Fuel | | lb/hr | BACT | GE 7FA |
| | CHANNEL ENERGY CENTER LLC | CHANNEL ENERGY CENTER LLC | 10/15/2012 | | MW | GCP/Fuel | | lb/hr | BACT | Siemens 501F |
| 1V-0019 | CHANNEL ENERGY CENTER LLC | CHANNEL ENERGY CENTER LLC | 10/13/2012 | 180 | IVIVV | GCF/Fuel | 27.0 | 10/111 | BACI | Siemens 301F |
| TX-0619 | DEED DADY ENERGY CENTER | DEED DADK ENERGY CENTER I.I.C | 9/26/2012 | 100 | N 4147 | CCD/EI | 27.0 | 11- /1 | BACT | Ci |
| | DEER PARK ENERGY CENTER | DEER PARK ENERGY CENTER LLC | | | MW | GCP/Fuel | | lb/hr | | Siemens/Westinghouse 501F |
| | THE EMPIRE DISTRICT ELECTRIC COMPANY | THE EMPIRE DISTRICT ELECTRIC COMPANY | 7/14/2015 | | MW | DLN | 30.2 | , | BACT | 05.44 1.1704.00 |
| | COLORADO BEND ENERGY CENTER | COLORADO BEND II POWER, LLC | 4/1/2015 | 1,100 | | GCP | 43.0 | | BACT | GE Model 7HA.02 |
| MI-0423 | INDECK NILES, LLC | INDECK NILES, LLC | 1/4/2017 | 8,322 | MMBtu/hr | GCP/Fuel/Inlet Air Filter | 0.0012 | lb/MMBtu | BACT | |
| | | | | | | | | | | GE7FA.05 OR Siemens SGT6 |
| | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | | MMBtu/hr | Fuel | 0.0022 | | BACT | 5000F |
| | FILER CITY STATION | FILER CITY STATION LIMITED PARTNERSHIP | 11/17/2017 | 1,935 | | GCP/Fuel/Inlet Air Filter | 0.0025 | lb/MMBtu | BACT | |
| NJ-0082 | WEST DEPTFORD ENERGY STATION | WEST DEPTFORD ENERGY ASSOCIATES | 7/18/2014 | 2,362 | MMBtu/hr | Fuel | 0.0025 | lb/MMBtu | BACT | Siemens |
| | | | | | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | Fuel | 0.0027 | lb/MMBtu | BACT | 5000F |
| | | | | | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | Fuel | 0.0027 | lb/MMBtu | BACT | 5000F |
| MI-0410 | THETFORD GENERATING STATION | CONSUMERS ENERGY COMPANY | 7/25/2013 | | MMBtu/hr | Fuel | 0.0033 | | BACT | |
| | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | | MMBtu/hr | GCP | 0.0040 | | BACT | |
| | MOXIE LIBERTY LLC/ASYLUM POWER PL T | MOXIE ENERGY LLC | 10/10/2012 | | MMBtu/hr | Fuel | 0.0040 | | BACT | |
| | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | | MMBtu/hr | GCP | 0.0042 | | BACT | + |
| | PALMDALE HYBRID POWER PROJECT | CITY OF PALMDALE | 10/18/2011 | | MW | Fuel | 0.0042 | | BACT | |
| | | | | | | | | - | | C: |
| | WEST DEPTFORD ENERGY STATION | WEST DEPTFORD ENERGY ASSOCIATES | 7/18/2014 | | MMBtu/hr | Fuel | 0.0048 | | BACT | Siemens |
| MD-0041 | CPV ST. CHARLES | CPV MARYLAND, LLC | 4/23/2014 | | MW | GCP/Fuel | 0.0050 | | BACT | GE F class |
| | JOHNSONVILLE COGENERATION | TENNESSEE VALLEY AUTHORITY | 4/19/2016 | | MMBtu/hr | OxCat/GCP | 0.0050 | | BACT | |
| | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | | MMBtu/hr | GCP | 0.0060 | | BACT | |
| MI-0412 | | HOLLAND BOARD OF PUBLIC WORKS | 12/4/2013 | | MMBtu/hr | GCP/Fuel | 0.0070 | | BACT | |
| MI-0424 | | HOLLAND BOARD OF PUBLIC WORKS | 12/5/2016 | | MMBtu/hr | GCP/Fuel | 0.0070 | | BACT | |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | | MMBtu/hr | GCP | 0.0073 | lb/MMBtu | BACT | |
| | CPV VALLEY ENERGY CENTER | CPV VALLEY LLC | 8/1/2013 | | MMBtu/hr | Fuel | 0.0073 | | BACT | |
| IN-0158 | ST. JOSEPH ENEGRY CENTER, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 2,300 | MMBtu/hr | GCP/Fuel | 0.0078 | lb/MMBtu | BACT | |
| IA-0107 | MARSHALLTOWN GENERATING STATION | INTERSTATE POWER AND LIGHT | 4/14/2014 | 2,258 | MMBtu/hr | None | 0.0100 | lb/MMBtu | BACT | Siemens SGT6-5000F |
| IA-0107 | MARSHALLTOWN GENERATING STATION | INTERSTATE POWER AND LIGHT | 4/14/2014 | 2,258 | MMBtu/hr | None | 0.0100 | lb/MMBtu | BACT | |
| LA-0224 | ARSENAL HILL POWER PLANT | SOUTHWEST ELECTRIC POWER COMPANY (SWEPCO) | 3/20/2008 | 2,110 | MMBtu/hr | GCP/Fuel | 0.0115 | lb/MMBtu | BACT | |
| DE-0024 | GARRISON ENERGY CENTER | GARRISON ENERGY CENTER, LLC/ CALPINE CORPORATION | 1/30/2013 | 2,260 | MMBtu/hr | Fuel | 0.0122 | lb/MMBtu | BACT | |
| | | Volatil | e Organic Con | npounds | | | | | | |
| TX-0756 | CCI CORPUS CHRISTI CONDENSATE SPLITTER FACILITY | CASTLETON COMMODITIES INTERNATIONAL (CCI) CORPU | 6/19/2015 | | MMBtu/hr | GCP/Fuel | 0.005 | LB/100 SCF | BACT | |
| OH-0356 | DUKE ENERGY HANGING ROCK ENERGY | DUKE ENERGY HANGING ROCK, LLC | 12/18/2012 | | MW | GCP | 3.2 | <u> </u> | BACT | GE 7FA |
| OH-0356 | DUKE ENERGY HANGING ROCK ENERGY | DUKE ENERGY HANGING ROCK, LLC | 12/18/2012 | | MW | GCP | 7.3 | | BACT | GE 7FA |
| | WARREN COUNTY POWER PLANT - DOMINION | VIRGINIA ELECTRIC AND POWER COMPANY | 12/17/2010 | | MMBtu/hr | OxCat/GCP | | lb/MMBtu | BACT | MHI M501 GAC |
| | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | | MMBtu/hr | GCP | 0.0018 | | BACT | |
| | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | | MMBtu/hr | GCP | 0.0040 | | BACT | † |
| | ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | 3,625 | | OxCat, DLN, GCP | 0.0040 | ., | BACT | 1 |
| | ST. CHARLES POWER STATION ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | 3,625 | | OxCat, DLN, GCP OxCat, DLN, GCP | 0.0169 | | BACT | + |
| | ARSENAL HILL POWER PLANT | SOUTHWEST ELECTRIC POWER COMPANY (SWEPCO) | | | MMBtu/hr | GCP | 0.0169 | | BACT | + |
| | | | 3/20/2008 | | | | | | _ | + |
| | | HOLLAND BOARD OF PUBLIC WORKS | 12/4/2013 | 647 | | OxCat/GCP | 0.3074 | | BACT | CIENTERIC VOA 2A |
| | CHOUTEAU POWER PLANT | ASSOCIATED ELECTRIC COOPERATIVE INC | 1/23/2009 | 1,882 | | GCP | 0.3 | | BACT | SIEMENS V84.3A |
| CT-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | | MMBtu/hr | OxCat | | ppm | BACT | Mitsubishi M501JAC |
| CT-0157 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | | MMBtu/hr | OxCat | | ppm | BACT | 1 |
| | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | | MMBtu/hr | OxCat | | ppm | BACT | |
| | OKEECHOBEE CLEAN ENERGY CENTER | FLORIDA POWER & LIGHT | 3/9/2016 | 3,096 | | GCP | | ppm | BACT | GE 7HA.02 |
| FL-0364 | SEMINOLE GENERATING STATION | SEMINOLE ELECTRIC COOPERATIVE, INC. | 3/21/2018 | 3,514 | MMBtu/hr | OxCat | 1.0 | ppm | BACT | GE 7HA.02 |
| IA-0107 | MARSHALLTOWN GENERATING STATION | INTERSTATE POWER AND LIGHT | 4/14/2014 | 2,258 | MMBtu/hr | OxCat | 1.0 | ppm | BACT | Siemens SGT6-5000F |
| | | | | | | | | 1 - | | |
| IA-0107 | MARSHALLTOWN GENERATING STATION | INTERSTATE POWER AND LIGHT | 4/14/2014 | 2,258 | MMBtu/hr | None | 1.0 | ppm | BACT | |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре | Turbine Model |
|-----------|---|---|------------------|------------|----------|-----------------|-----------------------|--------------|-------|-------------------------------|
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | | MW | OxCat | | ppm | BACT | 2 Siemens SGT-8000H |
| PA-0286 | MOXIE ENERGY LLC/PATRIOT GENERATION PLT | MOXIE ENERGY LLC | 1/31/2013 | 472 | | OxCat | | ppm | BACT | |
| TX-0714 | S R BERTRON ELECTRIC GENERATING STATION | NRG TEXAS POWER LLC | 12/19/2014 | | MW | OxCat | | ppm | BACT | Siemens Model F5 (SF5 |
| | FPL WEST COUNTY ENERGY CENTER UNIT 3 | FLORIDA POWER AND LIGHT COMPANY (FP&L) | 7/30/2008 | | MMBtu/hr | None | | ppm | BACT | |
| FL-0337 | POLK POWER STATION | TAMPA ELECTRIC COMPANY | 10/14/2012 | 1,160 | | Fuel | _ | ppm | BACT | |
| LA-0254 | NINEMILE POINT ELECTRIC GENERATING PLANT | ENTERGY LOUISIANA LLC | 8/16/2011 | | MMBtu/hr | GCP | | ppm | BACT | |
| CT-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | 2,639 | MMBtu/hr | OxCat | 1.6 | ppm | BACT | 14" 1:1:14504 040 " |
| 011 0252 | ODEGON CLEAN ENERGY CENTER | ADDADIG UG ING | 6/40/2042 | | /1 | 0.01 | | | DA CT | Mitsubishi M501 GAC units or |
| | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 6,004 | MMBtu/hr | OxCat | | ppm | BACT | 2 Siemens SGT-8000H |
| | APPLIED ENERGY LLC | APPLIED ENERGY LLC | 3/20/2009 | | | OxCat | | ppm | BACT | |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | | MW | None | | ppm | BACT | 5075 50005 |
| GA-0138 | LIVE OAKS POWER PLANT | LIVE OAKS COMPANY, LLC | 4/8/2010 | | MW | OxCat/GCP | | ppm | BACT | SGT6-5000F. |
| ID-0018 | LANGLEY GULCH POWER PLANT | IDAHO POWER COMPANY | 6/25/2010 | | MMBtu/hr | OxCat, DLN, GCP | | ppm | BACT | Siemens SGT6-5000F |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | | MMBtu/hr | OxCat | | ppm | BACT | |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | 2,807 | MMBtu/hr | OxCat | 2.0 | ppm | BACT | |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 5,579 | MMBtu/hr | OxCat | 2.0 | ppm | BACT | 2 Siemens SGT-8000H |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | | MMBtu/hr | OxCat | | ppm | BACT | 2 Siemens SGT-8000H |
| OR-0050 | TROUTDALE ENERGY CENTER, LLC | TROUTDALE ENERGY CENTER, LLC | 3/5/2014 | 2,988 | MMBtu/hr | OxCat/GCP | 2.0 | ppm | BACT | Mitsubishi M501-GAC |
| | | | | | | | | | | GE 7FA, GE 7FB, AND SIEMENS |
| TX-0546 | PATTILLO BRANCH POWER PLANT | PATTILLO BRANCH POWER COMPANY LLC | 6/17/2009 | | MW | OxCat | | ppm | BACT | SGT6-5000F. |
| TX-0600 | THOMAS C. FERGUSON POWER PLANT | LOWER COLORADO RIVER AUTHORITY | 9/1/2011 | | MW | OxCat/GCP | | ppm | BACT | GE 7FA |
| TX-0618 | CHANNEL ENERGY CENTER LLC | CHANNEL ENERGY CENTER LLC | 10/15/2012 | 180 | MW | GCP | 2.0 | ppm | BACT | Siemens 501F |
| | | | | | | | | | | |
| TX-0619 | DEER PARK ENERGY CENTER | DEER PARK ENERGY CENTER LLC | 9/26/2012 | | MW | GCP/Fuel | | ppm | BACT | Siemens/Westinghouse 501F |
| TX-0620 | ES JOSLIN POWER PLANT | CALHOUN PORT AUTHORITY | 9/12/2012 | | MW | GCP/Fuel | | ppm | BACT | GE 7FA |
| TX-0678 | FREEPORT LNG PRETREATMENT FACILITY | FREEPORT LNG DEVELOPMENT LP | 7/16/2014 | 87 | MW | OxCat | 2.0 | ppm | BACT | |
| | | | | | | | | | | GE 7FA.04; (2 Siemens SGT6- |
| | | | | | | | | | | 5000F(4; or (3 Siemens SGT6- |
| | LA PALOMA ENERGY CENTER | LA PALOMA ENERGY CENTER, LLC | 2/7/2013 | | MW | OxCat | | ppm | BACT | 5000F(5. |
| | SAND HILL ENERGY CENTER | CITY OF AUSTIN | 9/13/2013 | | MW | None | | ppm | BACT | GE 7FA |
| TX-0713 | TENASKA BROWNSVILLE GENERATING STATION | TENASKA BROWNSVILLE PARTNERS, LLC | 4/29/2014 | 274 | MW | OxCat | 2.0 | ppm | BACT | |
| | | | | | | | | | | Siemens SCC6-5000 CTGs and |
| | | | | | | | | | | a SST6-5000 ST, or two GE 7FA |
| TX-0767 | LON C. HILL POWER STATION | LON C. HILL, L.P. | 10/2/2015 | | MW | OxCat | 2.0 | ppm | BACT | CTGs and a D-11 ST. |
| TX-0773 | FGE EAGLE PINES PROJECT | FGE EAGLE PINES, LLC | 11/4/2015 | | MW | OxCat | 2.0 | ppm | BACT | Alstom GT36 |
| TX-0788 | NECHES STATION | APEX TEXAS POWER LLC | 3/24/2016 | 231 | MW | OxCat | 2.0 | ppm | BACT | Siemens or GE |
| TX-0789 | DECORDOVA STEAM ELECTRIC STATION | DECORDOVA II POWER COMPANY LLC | 3/8/2016 | | MW | OxCat | 2.0 | ppm | BACT | Siemens or GE |
| WV-0025 | MOUNDSVILLE COMBINED CYCLE POWER PLANT | MOUNDSVILLE POWER, LLC | 11/21/2014 | 2,420 | MMBtu/hr | OxCat/GCP | 2.0 | ppm | BACT | GE Frame 7FA.04 |
| TX-0548 | MADISON BELL ENERGY CENTER | MADISON BELL PARTNERS LP | 8/18/2009 | 275 | MW | GCP | 2.5 | ppm | BACT | GE PG7121(EA |
| TX-0819 | GAINES COUNTY POWER PLANT | SOUTHWESTERN PUBLIC SERVICE COMPANY | 4/28/2017 | 426 | MW | OxCat/GCP | 3.5 | ppm | BACT | Siemens SGT6-5000F5 |
| MI-0412 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | HOLLAND BOARD OF PUBLIC WORKS | 12/4/2013 | 647 | MMBtu/hr | OxCat/GCP | 4.0 | ppm | BACT | |
| MI-0423 | INDECK NILES, LLC | INDECK NILES, LLC | 1/4/2017 | 8,322 | MMBtu/hr | OxCat/GCP | 4.0 | ppm | BACT | |
| MI-0424 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | HOLLAND BOARD OF PUBLIC WORKS | 12/5/2016 | 554 | MMBtu/hr | OxCat/GCP | 4.0 | ppm | BACT | |
| | | | | | | | | | | GE 7FAS OR 250 MW |
| TX-0547 | NATURAL GAS-FIRED POWER GENERATION FACILITY | LAMAR POWER PARTNERS II LLC | 6/22/2009 | 250 | MW | GCP | 4.0 | ppm | BACT | MITSUBISHI 501GS |
| TX-0710 | VICTORIA POWER STATION | VICTORIA WLE L.P. | 12/1/2014 | 197 | MW | OxCat | 4.0 | ppm | BACT | GE 7FA.04 |
| TX-0712 | TRINIDAD GENERATING FACILITY | SOUTHERN POWER COMPANY | 11/20/2014 | 497 | MW | OxCat | 4.0 | ppm | BACT | MHI J model |
| TX-0730 | COLORADO BEND ENERGY CENTER | COLORADO BEND II POWER, LLC | 4/1/2015 | 1,100 | MW | SCR/OxCat | 4.0 | ppm | BACT | GE Model 7HA.02 |
| LA-0224 | ARSENAL HILL POWER PLANT | SOUTHWEST ELECTRIC POWER COMPANY (SWEPCO) | 3/20/2008 | 2,110 | MMBtu/hr | GCP | 4.9 | ppm | BACT | |
| CT-0151 | KLEEN ENERGY SYSTEMS, LLC | KLEEN ENERGY SYSTEMS, LLC | 2/25/2008 | 2,142 | MMBtu/hr | OxCat | 5.0 | ppm | BACT | SIEMENS SGT6-5000F |
| OK-0154 | MOORELAND GENERATING STA | WESTERN FARMERS ELECTRIC COOPERATIVE | 7/2/2013 | 360 | MW | OxCat/GCP | | ppm | BACT | Siemens SGT6-5000F5 |
| OK-0154 | MOORELAND GENERATING STA | WESTERN FARMERS ELECTRIC COOPERATIVE | 7/2/2013 | 360 | MW | OxCat/GCP | 5.0 | ppm | BACT | Siemens SGT6-5000F5 |
| | ST. JOSEPH ENEGRY CENTER, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | | MMBtu/hr | None | | tpy | BACT | |
| 1111-0128 | | • | | | | | - | | • | |
| IN-0158 | | | PM10 | | | | | | | |
| | CANE ISLAND POWER PARK | FLORIDA MUNICIPAL POWER AGENCY (FMPA | PM10 9/8/2008 | 1,860 | MMBtu/hr | Fuel | 2.0 | GR S/100 SCF | BACT | GE 7241 FA CTG |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре | Turbine Model |
|----------|---|--------------------------------------|-------------|------------|---------------------|---------------------------|-----------------------|----------------|-------|-------------------------------|
| | | | | | | | | | | Never built. Proposed Model |
| CA-1192 | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | MW | Fuel | 8.9 | lb/hr | BACT | GE 7241 FA |
| | | | | | | | | | | Never built. Proposed Model |
| CA-1192 | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | MW | Fuel | 8.9 | lb/hr | BACT | GE 7241 FA |
| CA-1198 | MORRO BAY POWER PLANT | DYNERGY MORRO BAY LLC | 9/25/2008 | 180 | MW | Fuel | 11.0 | lb/hr | BACT | GE Frame 7, Model PG7241 |
| CA-1198 | MORRO BAY POWER PLANT | DYNERGY MORRO BAY LLC | 9/25/2008 | 180 | MW | Fuel | 11.0 | lb/hr | BACT | GE Frame 7, Model PG7241 |
| MD-0046 | KEYS ENERGY CENTER | KEYS ENERGY CENTER, LLC | 10/31/2014 | 235 | MW | GCP/Fuel | 11.0 | lb/hr | BACT | SGT6-500FEE |
| | | | | | | | | | | SGT6-5000F CTGs or four GE |
| TX-0590 | KING POWER STATION | PONDERA CAPITAL MANAGEMENT GP INC | 8/5/2010 | 1,350 | MW | Fuel | 11.1 | lb/hr | BACT | Frame 7FA CTGs |
| NJ-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | MW | Fuel | 11.7 | lb/hr | BACT | GE 7HA.02 |
| | | | | | | | | | | Never built. Proposed Model |
| CA-1192 | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | MW | Fuel | 11.8 | lb/hr | BACT | GE 7241 FA |
| | | | | | | | | | | Never built. Proposed Model |
| CA-1192 | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | MW | Fuel | 11.8 | lb/hr | BACT | GE 7241 FA |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 799 | MW | Fuel | 13.3 | lb/hr | BACT | 2 Siemens SGT-8000H |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | Fuel | 13.5 | lb/hr | BACT | GE 7FA |
| OH-0356 | DUKE ENERGY HANGING ROCK ENERGY | DUKE ENERGY HANGING ROCK, LLC | 12/18/2012 | | MW | Fuel | | lb/hr | BACT | GE 7FA |
| | | | | | | | | | | Siemens SCC6-5000 CTGs and |
| | | | | | | | | | 1 | a SST6-5000 ST, or two GE 7FA |
| TX-0767 | LON C. HILL POWER STATION | LON C. HILL, L.P. | 10/2/2015 | 195 | MW | GCP/Fuel | 16.0 | lb/hr | BACT | CTGs and a D-11 ST. |
| | | | ,-, | | | 55.7.25. | | , | | SGT-8000H VERSION 1.4- |
| MD-0045 | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | MW | GCP/Fuel | 17.9 | lb/hr | BACT | OPTIMIZED |
| TX-0620 | ES JOSLIN POWER PLANT | CALHOUN PORT AUTHORITY | 9/12/2012 | | MW | GCP/Fuel | | lb/hr | BACT | GE 7FA |
| | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | | MW | None | | lb/hr | BACT | GE 7HA.02 |
| TX-0788 | NECHES STATION | APEX TEXAS POWER LLC | 3/24/2016 | | MW | GCP/Fuel | | lb/hr | BACT | Siemens or GE |
| | DUKE ENERGY HANGING ROCK ENERGY | DUKE ENERGY HANGING ROCK, LLC | 12/18/2012 | | MW | Fuel | | lb/hr | BACT | GE 7FA |
| TX-0773 | FGE EAGLE PINES PROJECT | FGE EAGLE PINES, LLC | 11/4/2015 | | MW | None | | lb/hr | BACT | Alstom GT36 |
| TX-0618 | CHANNEL ENERGY CENTER LLC | CHANNEL ENERGY CENTER LLC | 10/15/2012 | | MW | GCP/Fuel | | lb/hr | BACT | Siemens 501F |
| 177 0020 | CHANNEL ENERGY CENTER EEG | CHANNEL ENERGY CENTER LEC | 10/13/2012 | 100 | | 00.7. uc. | 27.0 | , | 57101 | Siemens so I |
| TX-0619 | DEER PARK ENERGY CENTER | DEER PARK ENERGY CENTER LLC | 9/26/2012 | 180 | MW | GCP/Fuel | 27.0 | lb/hr | BACT | Siemens/Westinghouse 501F |
| | THE EMPIRE DISTRICT ELECTRIC COMPANY | THE EMPIRE DISTRICT ELECTRIC COMPANY | 7/14/2015 | | MW | DLN | | lb/hr | BACT | Siemens, Westinghouse 501. |
| | EAGLE MOUNTAIN STEAM ELECTRIC STATION | EAGLE MOUNTAIN POWER COMPANY LLC | 6/18/2015 | | MW | None | | lb/hr | BACT | Siemens or GE |
| | DECORDOVA STEAM ELECTRIC STATION | DECORDOVA II POWER COMPANY LLC | 3/8/2016 | | MW | GCP/Fuel | | lb/hr | BACT | Siemens or GE |
| OR-0050 | TROUTDALE ENERGY CENTER, LLC | TROUTDALE ENERGY CENTER, LLC | 3/5/2014 | | MMBtu/hr | Fuel | | lb/hr | BACT | Mitsubishi M501-GAC |
| TX-0730 | COLORADO BEND ENERGY CENTER | COLORADO BEND II POWER, LLC | 4/1/2015 | 1,100 | | GCP | | lb/hr | BACT | GE Model 7HA.02 |
| 17. 0750 | COLONADO DEND ENEROT CENTER | COLONADO BEND II I OWEN, EEC | 4/1/2015 | 1,100 | 10100 | GCI | 43.0 | 15/111 | BACI | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 5 570 | MMBtu/hr | . Fuel | 0.0018 | lb/MMBtu | BACT | 2 Siemens SGT-8000H |
| 011 0332 | ONEGON CLEAN ENERGY CENTER | ARCADIS, 03, INC. | 0/10/2015 | 3,373 | IVIIVIDEA/III | ruci | 0.0010 | ID/ IVIIVIDEA | BACI | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 5 570 | MMBtu/hr | Fuel | 0.0020 | lb/MMBtu | BACT | 2 Siemens SGT-8000H |
| 011-0332 | OREGON CLEAN ENERGY CENTER | ARCADIS, 03, INC. | 0/10/2013 | 3,373 | IVIIVIDEU/III | ruei | 0.0020 | ID/IVIIVIDEA | DACI | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 6 004 | MMBtu/hr | Fuel | 0.0033 | lb/MMBtu | BACT | 2 Siemens SGT-8000H |
| MI-0423 | INDECK NILES, LLC | INDECK NILES, LLC | 1/4/2017 | | | GCP/Fuel/Inlet Air Filter | 0.0023 | | BACT | 2 Siemens 3G1-8000H |
| VA-0315 | WARREN COUNTY POWER PLANT - DOMINION | VIRGINIA ELECTRIC AND POWER COMPANY | 12/17/2010 | 2,996 | | Fuel | 0.0024 | lb/MMBtu | BACT | MHI M501 GAC |
| VA-0313 | WARREIN COUNTY FOWER FLANT - DOMINION | VIRGINIA ELECTRIC AND FOWER COMPANY | 12/17/2010 | 2,990 | IVIIVIBLU/III | ruei | 0.0027 | ID/IVIIVIBLU | BACI | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 2 022 | MMBtu/hr | . Fuel | 0.0032 | lb/MMBtu | BACT | 5000F |
| 143-0061 | F3EG F033IE EEC SEWAREN GENERATING STATION | F3EG F033IL EEC | 3/7/2014 | 3,323 | IVIIVIBLU/III | ruei | 0.0032 | ID/IVIIVIBLU | BACI | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 2 022 | MMBtu/hr | · Fuel | 0.0022 | lb/MMBtu | BACT | 5000F |
| 143-0001 | F3EG F033IL LEC SEWAREN GENERATING STATION | F3EG F033IL EEC | 3/7/2014 | 3,323 | IVIIVIBLU/III | ruei | 0.0033 | ID/IVIIVIBLU | BACI | GE7FA.05 OR Siemens SGT6 |
| NII 0001 | DEFC FOSSIL LLC SENVADENI CENEDATING STATIONI | DEEC LOSSILLIC | 2/7/2014 | 2 022 | 1 4 1 4 D + 1 / b = | Fuel | 0.0036 | Ib /NANAD+ | DACT | |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | | Fuel | | | BACT | 5000F |
| LA-0254 | NINEMILE POINT ELECTRIC GENERATING PLANT | ENTERGY LOUISIANA LLC | 8/16/2011 | /,146 | MMBtu/hr | GCP/Fuel | 0.0037 | lb/MMBtu | BACT | CEZEA OF OR Signature COTS |
| NII 0004 | DOEG FOCCIL LIG CENTA DENI GENERATING CTATIO | DCEC FOCCII II C | 2/7/26: | 2.000 | NANAD: " | | 2 222- | II- /8 48 45 : | DACT | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | | MMBtu/hr | Fuel | 0.0037 | | BACT | 5000F |
| NJ-0079 | WOODBRIDGE ENERGY CENTER | CPV SHORE, LLC | 7/25/2012 | | MMBtu/hr | GCP/Fuel | 0.0041 | | BACT | GE |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | | MMBtu/hr | GCP | 0.0042 | | BACT | |
| NJ-0082 | WEST DEPTFORD ENERGY STATION | WEST DEPTFORD ENERGY ASSOCIATES | 7/18/2014 | | MMBtu/hr | Fuel | 0.0042 | | BACT | Siemens |
| CA-1212 | PALMDALE HYBRID POWER PROJECT | CITY OF PALMDALE | 10/18/2011 | | MW | Fuel | 0.0048 | - | BACT | + |
| CT-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | 2,639 | | GCP | 0.0050 | lb/MMBtu | BACT | |
| MI-0405 | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | 2,237 | MMBtu/hr | GCP | 0.0060 | lb/MMBtu | BACT | |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре | Turbine Model |
|---|---|---|---|--|----------------------------|--|--|----------------------------------|------------------------------|--|
| | · | | | | | | | | | GE Energy 7F Series 5 Rapid |
| MA-0039 | SALEM HARBOR STATION REDEVELOPMENT | FOOTPRINT POWER SALEM HARBOR DEVELOPMENT LP | 1/30/2014 | 2,449 | MMBtu/hr | None | 0.0062 | lb/MMBtu | BACT | Response |
| MI-0410 | THETFORD GENERATING STATION | CONSUMERS ENERGY COMPANY | 7/25/2013 | 2,587 | MMBtu/hr | r Fuel | 0.0066 | lb/MMBtu | BACT | |
| MI-0427 | FILER CITY STATION | FILER CITY STATION LIMITED PARTNERSHIP | 11/17/2017 | 1,935 | MMBtu/hr | GCP/Fuel/Inlet Air Filter | 0.0066 | lb/MMBtu | BACT | |
| NJ-0082 | WEST DEPTFORD ENERGY STATION | WEST DEPTFORD ENERGY ASSOCIATES | 7/18/2014 | | MMBtu/hr | r Fuel | 0.0069 | lb/MMBtu | BACT | Siemens |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | | MMBtu/hr | r GCP | 0.0073 | | BACT | |
| MD-0041 | CPV ST. CHARLES | CPV MARYLAND, LLC | 4/23/2014 | | MW | GCP/Fuel | 0.0080 | | BACT | GE F-class advanced |
| MI-0405 | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | | MMBtu/hr | r GCP | 0.0080 | | BACT | |
| CO-0073 | PUEBLO AIRPORT GENERATING STATION | BLACK HILLS ELECTRIC GENERATION, LLC | 7/22/2010 | | MMBtu/hr | GCP/Fuel | 0.0115 | | BACT | |
| MI-0412 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | HOLLAND BOARD OF PUBLIC WORKS | 12/4/2013 | 647 | | GCP/Fuel | 0.0140 | | BACT | |
| MI-0424 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | | 12/5/2016 | | MMBtu/hr | GCP/Fuel | 0.0140 | | BACT | |
| CT-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | | MMBtu/hr | GCP | 0.0440 | lb/MMBtu | BACT | |
| | T | | /10 (filterable | | I | | | T | | |
| FL-0337 | POLK POWER STATION | TAMPA ELECTRIC COMPANY | 10/14/2012 | 1,160 | | GCP | | GR S/100 SCF | BACT | |
| NJ-0080 | HESS NEWARK ENERGY CENTER | HESS NEWARK ENERGY CENTER, LLC | 11/1/2012 | 4,595 | | Fuel | 0.0024 | | BACT | GE |
| OR-0048 | CARTY PLANT | PORTLAND GENERAL ELECTRIC | 12/29/2010 | | MMBtu/hr | Fuel | 0.0025 | | BACT | |
| NJ-0080 | HESS NEWARK ENERGY CENTER | HESS NEWARK ENERGY CENTER, LLC | 11/1/2012 | | MMBtu/hr | r Fuel | 0.0029 | | BACT | GE |
| | BERKS HOLLOW ENERGY ASSOC LLC/ONTELAUNEE | BERKS HOLLOW ENERGY ASSOC LLC | 12/17/2013 | | MMBtu/hr | None | 0.0036 | | BACT | |
| LA-0313 | ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | 3,625 | | GCP/Fuel | 0.0048 | | BACT | |
| LA-0313 | ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | | MMBtu/hr | GCP/Fuel | 0.0048 | | BACT | |
| CT-0151 | KLEEN ENERGY SYSTEMS, LLC | KLEEN ENERGY SYSTEMS, LLC | 2/25/2008 | | MMBtu/hr | None | 0.0051 | | BACT | SIEMENS SGT6-5000F |
| AK-0073 | INTERNATIONAL STATION POWER PLANT | CHUGACH ELECTRIC ASSOCIATION | 12/20/2010 | | MW | Fuel | 0.0066 | | BACT | |
| IN-0158 | ST. JOSEPH ENEGRY CENTER, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | | MMBtu/hr | GCP/Fuel | 0.0078 | ., | BACT | |
| LA-0136 | PLAQUEMINE COGENERATION FACILITY | THE DOW CHEMICAL COMPANY | 7/23/2008 | | MMBtu/hr | Fuel | 0.0116 | | BACT | GE FRAME 7 FA |
| LA-0308 | MORGAN CITY POWER PLANT | LOUISIANA ENERGY AND POWER AUTHORITY (LEPA) | 9/26/2013 | | MMBtu/hr | GCP/Fuel | 0.0198 | lb/MMBtu | BACT | |
| 51,0056 | Toursellanes disant enemoy ornites | Islanda nowen a Hour | PM2.5 (total | | 1 4 4 4 D ; /I | | 2.0 | CD 5/400 565 | Inacr | Lor 7114 00 |
| FL-0356 | OKEECHOBEE CLEAN ENERGY CENTER | FLORIDA POWER & LIGHT | 3/9/2016 | 3,096 | MMBtu/hr | Fuel | 2.0 | GR S/100 SCF | BACT | GE 7HA.02 |
| TV 0500 | WING DOWED STATION | DONIDED A CADITAL AAAANA CEAAFAIT OD ING | 0/5/2010 | 4 250 | | - 1 | | | DAGT | SGT6-5000F CTGs or four GE |
| TX-0590 | KING POWER STATION | PONDERA CAPITAL MANAGEMENT GP INC | 8/5/2010 | 1,350 | | Fuel | | lb/hr | BACT BACT | Frame 7FA CTGs |
| NJ-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | MW | Fuel | 11./ | lb/hr | BACI | GE 7HA.02 |
| | | | | | | | | | | Never built. No turbine |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | Fuel | 12.0 | lb/hr | BACT | specified in Application for Certification of Project |
| CA-1191 | VICTORVILLE 2 HTBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | IVIVV | ruei | 12.0 | ID/III | BACI | Never built. No turbine |
| | | | | | | | | | | |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | Fuel | 12.0 | lb/hr | BACT | specified in Application for Certification of Project |
| TX-0678 | FREEPORT LNG PRETREATMENT FACILITY | FREEPORT LNG DEVELOPMENT LP | 7/16/2014 | | MW | None | | lb/hr | BACT | GE 7EA |
| 17-0078 | FREEFORT ENG FRETREATIVIENT FACILITY | FREEFORT LING DEVELOPINIENT LF | 7/10/2014 | 67 | IVIVV | None | 13.2 | 10/111 | BACI | Siemens SCC6-5000 CTGs and |
| | | | | | | | | | | a SST6-5000 ST, or two GE 7FA |
| TX-0767 | LON C. HILL POWER STATION | LON C. HILL, L.P. | 10/2/2015 | 105 | MW | GCP/Fuel | 16.0 | lb/hr | BACT | CTGs and a D-11 ST. |
| 17-0/0/ | LON C. HILL FOWER STATION | LON C. HILL, L.F. | 10/2/2013 | 193 | IVIVV | GCF/Fuel | 10.0 | 10/111 | BACI | CTGS and a D-11 31. |
| | | | | | | | | | | SIEMENS H-CLASS (SGT-8000H |
| MD-0045 | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | MW | GCP/Fuel | 17 9 | lb/hr | BACT | VERSION 1.4-OPTIMIZED |
| IVID 0043 | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, EEC | 11/13/2013 | 200 | 10.00 | Geryruer | 17.5 | 15/111 | DACI | Never built. No turbine |
| | | | | | | | | | | specified in Application for |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | Fuel | 18.0 | lb/hr | BACT | Certification of Project |
| CK 1151 | VICTORVILLE 2 ITTERIO I OWER I ROSECI | CITT OF VICTORVILLE | 3/11/2010 | 154 | 10.00 | ruci | 10.0 | 15/111 | DACI | Never built. No turbine |
| | | | | | | | | | | specified in Application for |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | Fuel | 18.0 | lb/hr | BACT | Certification of Project |
| | | | | | MW | None | | lb/hr | BACT | GE 7FA |
| TX-0620 | | CALHOUN PORT AUTHORITY | 9/12/2012 | | | | | | | GE 7HA.02 |
| TX-0620 | ES JOSLIN POWER PLANT | CALHOUN PORT AUTHORITY STONEGATE POWER. LLC | 9/12/2012 7/19/2016 | | | | 18.3 | lb/hr | BACT | |
| TX-0620 | | CALHOUN PORT AUTHORITY STONEGATE POWER, LLC APEX TEXAS POWER LLC | 7/19/2016 3/24/2016 | 663 | MW | None | | lb/hr lb/hr | BACT BACT | |
| TX-0620 NJ-0085 TX-0788 | ES JOSLIN POWER PLANT MIDDLESEX ENERGY CENTER, LLC NECHES STATION | STONEGATE POWER, LLC APEX TEXAS POWER LLC | 7/19/2016 3/24/2016 | 663 231 | MW MW | None GCP/Fuel | 19.4 | lb/hr | BACT | Siemens or GE |
| TX-0620 NJ-0085 TX-0788 TX-0773 | ES JOSLIN POWER PLANT MIDDLESEX ENERGY CENTER, LLC NECHES STATION FGE EAGLE PINES PROJECT | STONEGATE POWER, LLC APEX TEXAS POWER LLC FGE EAGLE PINES, LLC | 7/19/2016 3/24/2016 11/4/2015 | 663 231 321 | MW MW MW | None GCP/Fuel None | 19.4 21.4 | lb/hr lb/hr | BACT BACT | Siemens or GE Alstom GT36 |
| TX-0620 NJ-0085 TX-0788 TX-0773 OK-0154 | ES JOSLIN POWER PLANT MIDDLESEX ENERGY CENTER, LLC NECHES STATION FGE EAGLE PINES PROJECT MOORELAND GENERATING STA | STONEGATE POWER, LLC APEX TEXAS POWER LLC FGE EAGLE PINES, LLC WESTERN FARMERS ELECTRIC COOPERATIVE | 7/19/2016 3/24/2016 11/4/2015 7/2/2013 | 663 231 321 360 | MW MW MW | None GCP/Fuel None GCP/Fuel | 19.4 21.4 22.1 | lb/hr lb/hr lb/hr | BACT BACT BACT | Siemens or GE Alstom GT36 Siemens SGT6-5000F5 |
| TX-0620 NJ-0085 TX-0788 TX-0773 OK-0154 OK-0154 | ES JOSLIN POWER PLANT MIDDLESEX ENERGY CENTER, LLC NECHES STATION FGE EAGLE PINES PROJECT MOORELAND GENERATING STA MOORELAND GENERATING STA | STONEGATE POWER, LLC APEX TEXAS POWER LLC FGE EAGLE PINES, LLC WESTERN FARMERS ELECTRIC COOPERATIVE WESTERN FARMERS ELECTRIC COOPERATIVE | 7/19/2016 3/24/2016 11/4/2015 7/2/2013 7/2/2013 | 663 231 321 360 360 | MW MW MW MW | None GCP/Fuel None GCP/Fuel GCP/Fuel | 19.4 21.4 22.1 22.2 | lb/hr lb/hr lb/hr lb/hr | BACT BACT BACT BACT | Siemens or GE Alstom GT36 Siemens SGT6-5000F5 Siemens SGT6-5000F5 |
| TX-0620 NJ-0085 TX-0788 TX-0773 OK-0154 | ES JOSLIN POWER PLANT MIDDLESEX ENERGY CENTER, LLC NECHES STATION FGE EAGLE PINES PROJECT MOORELAND GENERATING STA | STONEGATE POWER, LLC APEX TEXAS POWER LLC FGE EAGLE PINES, LLC WESTERN FARMERS ELECTRIC COOPERATIVE | 7/19/2016 3/24/2016 11/4/2015 7/2/2013 | 663 231 321 360 360 | MW MW MW | None GCP/Fuel None GCP/Fuel | 19.4 21.4 22.1 22.2 | lb/hr lb/hr lb/hr | BACT BACT BACT | Siemens or GE Alstom GT36 Siemens SGT6-5000F5 |
| TX-0620 NJ-0085 TX-0788 TX-0773 OK-0154 OK-0154 TX-0618 | ES JOSLIN POWER PLANT MIDDLESEX ENERGY CENTER, LLC NECHES STATION FGE EAGLE PINES PROJECT MOORELAND GENERATING STA MOORELAND GENERATING STA CHANNEL ENERGY CENTER LLC | STONEGATE POWER, LLC APEX TEXAS POWER LLC FGE EAGLE PINES, LLC WESTERN FARMERS ELECTRIC COOPERATIVE WESTERN FARMERS ELECTRIC COOPERATIVE CHANNEL ENERGY CENTER LLC | 7/19/2016 3/24/2016 11/4/2015 7/2/2013 7/2/2013 10/15/2012 | 663 231 321 360 360 180 | MW MW MW MW MW | None GCP/Fuel None GCP/Fuel GCP/Fuel GCP/Fuel | 19.4 21.4 22.1 22.2 27.0 | lb/hr lb/hr lb/hr lb/hr | BACT BACT BACT BACT | Siemens or GE Alstom GT36 Siemens SGT6-5000F5 Siemens SGT6-5000F5 Siemens SGT6-500F5 |
| TX-0620 NJ-0085 TX-0788 TX-0773 OK-0154 OK-0154 | ES JOSLIN POWER PLANT MIDDLESEX ENERGY CENTER, LLC NECHES STATION FGE EAGLE PINES PROJECT MOORELAND GENERATING STA MOORELAND GENERATING STA | STONEGATE POWER, LLC APEX TEXAS POWER LLC FGE EAGLE PINES, LLC WESTERN FARMERS ELECTRIC COOPERATIVE WESTERN FARMERS ELECTRIC COOPERATIVE | 7/19/2016 3/24/2016 11/4/2015 7/2/2013 7/2/2013 | 663 231 321 360 360 180 | MW MW MW MW | None GCP/Fuel None GCP/Fuel GCP/Fuel | 19.4 21.4 22.1 22.2 27.0 27.0 | lb/hr lb/hr lb/hr lb/hr | BACT BACT BACT BACT | Siemens or GE Alstom GT36 Siemens SGT6-5000F5 Siemens SGT6-5000F5 |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Type | Turbine Model |
|--|--|--|---|--------------------|----------------|---------------------------|------------------|------------------------|--------------|------------------------------------|
| TX-0789 | DECORDOVA STEAM ELECTRIC STATION | DECORDOVA II POWER COMPANY LLC | 3/8/2016 | 231 | | GCP/Fuel | 35.5 | | BACT | Siemens or GE |
| TX-0789 | COLORADO BEND ENERGY CENTER | COLORADO BEND II POWER, LLC | 4/1/2015 | 1,100 | | GCP/Fuel | 43.0 | • | BACT | GE Model 7HA.02 |
| MI-0423 | INDECK NILES, LLC | INDECK NILES, LLC | 1/4/2017 | 8,322 | | GCP/Fuel/Inlet Air Filter | 0.0024 | • | BACT | GE Model 7HA.02 |
| VA-0315 | WARREN COUNTY POWER PLANT - DOMINION | VIRGINIA ELECTRIC AND POWER COMPANY | 12/17/2010 | 2,996 | | Fuel | 0.0024 | • | BACT | MHI M501 GAC |
| PA-0315 | BERKS HOLLOW ENERGY ASSOC LLC/ONTELAUNEE | BERKS HOLLOW ENERGY ASSOC LLC | 12/17/2010 | 3,046 | MMBtu/hi | None None | 0.0027 | lb/MMBtu | BACT | MHI MS01 GAC |
| | NINEMILE POINT ELECTRIC GENERATING PLANT | | 8/16/2011 | | | r GCP/Fuel | 0.0036 | | BACT | |
| LA-0254 | | ENTERGY LOUISIANA LLC | | | MMBtu/h | | | | | CF F 75A 04 |
| WV-0025 | MOUNDSVILLE COMBINED CYCLE POWER PLANT | MOUNDSVILLE POWER, LLC | 11/21/2014 | | | GCP/Fuel/Inlet Air Filter | 0.0037 | | BACT | GE Frame 7FA.04 |
| CT-0157 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | | MMBtu/h | None | 0.0040 0.0040 | | BACT | |
| CT-0158 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | | MMBtu/hi | None | | • | | |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | 2,147 | | GCP | 0.0042 | lb/MMBtu | BACT | 6: |
| NJ-0082 | WEST DEPTFORD ENERGY STATION | WEST DEPTFORD ENERGY ASSOCIATES | 7/18/2014 | 2,362 | | Fuel | 0.0042 | lb/MMBtu | BACT | Siemens |
| CT-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | 2,969 | | GCP | 0.0044 | lb/MMBtu | BACT | |
| CA-1212 | PALMDALE HYBRID POWER PROJECT | CITY OF PALMDALE | 10/18/2011 | | MW | Fuel | 0.0048 | | BACT | |
| CT-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | 2,639 | MMBtu/h | GCP | 0.0050 | lb/MMBtu | BACT | |
| MI-0405 | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | 2,237 | MMBtu/h | GCP | 0.0060 | lb/MMBtu | BACT | |
| | | | | | | | | | | GE Energy 7F Series 5 Rapid |
| MA-0039 | SALEM HARBOR STATION REDEVELOPMENT | FOOTPRINT POWER SALEM HARBOR DEVELOPMENT LP | 1/30/2014 | | MMBtu/h | None | 0.0062 | ., | BACT | Response |
| MI-0402 | SUMPTER POWER PLANT | WOLVERINE POWER SUPPLY COOPERATIVE INC. | 11/17/2011 | | MW | None | 0.0066 | - | BACT | 1 |
| MI-0410 | THETFORD GENERATING STATION | CONSUMERS ENERGY COMPANY | 7/25/2013 | 2,587 | | Fuel | 0.0066 | • | BACT | |
| MI-0427 | FILER CITY STATION | FILER CITY STATION LIMITED PARTNERSHIP | 11/17/2017 | | | GCP/Fuel/Inlet Air Filter | 0.0066 | - | BACT | |
| NJ-0082 | WEST DEPTFORD ENERGY STATION | WEST DEPTFORD ENERGY ASSOCIATES | 7/18/2014 | 2,362 | MMBtu/h | r Fuel | 0.0069 | lb/MMBtu | BACT | Siemens |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | 2,807 | MMBtu/h | r GCP | 0.0073 | lb/MMBtu | BACT | |
| MI-0405 | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | 2,486 | MMBtu/h | GCP | 0.0080 | lb/MMBtu | BACT | |
| MI-0412 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | HOLLAND BOARD OF PUBLIC WORKS | 12/4/2013 | 647 | MMBtu/h | GCP/Fuel | 0.0140 | lb/MMBtu | BACT | |
| MI-0424 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | HOLLAND BOARD OF PUBLIC WORKS | 12/5/2016 | 554 | MMBtu/h | GCP/Fuel | 0.0140 | lb/MMBtu | BACT | |
| | | PM | 2.5 (filterable | only) | | • | <u>-</u> | | • | • |
| | | | | | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hi | r Fuel | 0.0025 | lb/MMBtu | BACT | 5000F |
| LA-0313 | ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | | MMBtu/hi | GCP/Fuel | 0.0048 | | BACT | |
| LA-0313 | ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | | MMBtu/hi | GCP/Fuel | 0.0048 | | BACT | |
| IN-0158 | ST. JOSEPH ENEGRY CENTER, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | | MMBtu/hi | GCP/Fuel | 0.0078 | | BACT | |
| LA-0308 | MORGAN CITY POWER PLANT | LOUISIANA ENERGY AND POWER AUTHORITY (LEPA) | 9/26/2013 | | MMBtu/hi | GCP/Fuel | 0.0198 | | BACT | |
| | | Gree | enhouse Gase | s - CO2 | | , | | | | |
| CT-0158 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | 2,420 | MMBtu/hi | r None | 809 | lb/MW-hr | BACT | GE HA.01 |
| | | , | , , , , , , , | , - | , | | | , | | |
| TX-0761 | SR BERTRON ELECTRIC GENERATING STATION | NRG TEXAS POWER | 9/15/2015 | 301 | MMBtu/h | None | 825 | lb/MW-hr | BACT | GE 7HA, GE7FA, MHI510G, SF5 |
| | | | 0,10,1010 | | | | | , | | |
| TX-0762 | CEDAR BAYOU ELECTRIC GENERATING STATION | NRG TEXAS POWER | 9/15/2015 | 301 | MMBtu/hi | None | 825 | lb/MW-hr | BACT | GE 7HA, GE7FA, MHI510G, SF5 |
| | KEYS ENERGY CENTER | KEYS ENERGY CENTER, LLC | 10/31/2014 | | MW | None | 869 | | BACT | SGT6-500FEE |
| TX-0730 | COLORADO BEND ENERGY CENTER | COLORADO BEND II POWER, LLC | 4/1/2015 | 1,100 | | GCP | | lb/MW-hr | BACT | GE Model 7HA.02 |
| TX-0730 | DEER PARK ENERGY CENTER LLC | CALPIINE CO - DEER PARK ENERGY CENTER(DPEC) LLC | 11/29/2012 | | MW | None | 920 | | BACT | Siemens Model FD3 |
| TX-0632 | DEER PARK ENERGY CENTER LLC | CALPIINE CO - DEER PARK ENERGY CENTER(DPEC) LLC | 11/29/2012 | | MW | None | 920 | - | BACT | Siemens Model FD3 |
| TX-0632 | CHANNEL ENERGY ENERGY CENTER, LLC | CALPINE CORPORATION-CHANNEL ENERGY CENTER, LLC | 11/29/2012 | | MW | None | 920 | , | BACT | Siemens Model FD2 |
| TX-0633 | CHANNEL ENERGY ENERGY CENTER, LLC | CALPINE CORPORATION-CHANNEL ENERGY CENTER, LLC | 11/29/2012 | | MW | None | 920 | • | BACT | Siemens Model FD2 |
| 17-0022 | CHANNEL ENERGY ENERGY CENTER, LLC | CALPINE CORPORATION-CHANNEL ENERGY CENTER, LLC | 11/29/2012 | 100 | IVIVV | None | 920 | ID/IVIVV-III | BACI | |
| TV 0664 | LON C HILL DOWER STATION | ION C HILL ID | 10/28/2014 | 700 | N.41A/ | None | 920 | lb/84\A/ b= | BACT | Siemens SGT6-5000F or GE 7FA.04 |
| TX-0664 | LON C. HILL POWER STATION | LON C. HILL, LP | 10/28/2014 | 700 | MW | None | 920 | lb/MW-hr | BACI | |
| NII 0001 | DOEC FOSCIL LLC CENTA DENI CENTEDATINIC CTATIONI | DOES FORSIL ITS | 2/7/2014 | 2 022 | 0.40.4D+/b | | 025 | II- /A ANA/ I | DACT | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/h | None | 925 | lb/MW-hr | BACT | 5000F |
| | 2000 2000 110 051114 2511 0511 1511 | Design to a | 2/=/22 | | | l | | 11. /5.45.47.1 | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | | None | 925 | | BACT | 5000F |
| | MARSHALLTOWN GENERATING STATION | INTERSTATE POWER AND LIGHT | 4/14/2014 | 2,258 | | None | 951 | lb/MW-hr | BACT | Siemens SGT6-5000F |
| IA-0107 | | | 4/14/2014 | 2,258 | MMBtu/h | None | 951 | lb/MW-hr | BACT | Siemens SGT6-5000F |
| IA-0107 | MARSHALLTOWN GENERATING STATION | INTERSTATE POWER AND LIGHT | | | | | | | | |
| | | BERKS HOLLOW ENERGY ASSOC LLC | 12/17/2013 | | MMBtu/h | None | 1,000 | lb/MW-hr | BACT | GE H class |
| IA-0107 PA-0296 | MARSHALLTOWN GENERATING STATION BERKS HOLLOW ENERGY ASSOC LLC/ONTELAUNEE | BERKS HOLLOW ENERGY ASSOC LLC Greenhou | 12/17/2013 se Gase - CO2 | Equivalents | | | , | | | |
| IA-0107 PA-0296 MD-0041 | MARSHALLTOWN GENERATING STATION BERKS HOLLOW ENERGY ASSOC LLC/ONTELAUNEE CPV ST. CHARLES | BERKS HOLLOW ENERGY ASSOC LLC Greenhou CPV MARYLAND, LLC | 12/17/2013 se Gase - CO2 4/23/2014 | Equivalents 725 | MW | None | 7,109 | BTU/KW-HR | BACT | GE F class |
| IA-0107 PA-0296 | MARSHALLTOWN GENERATING STATION BERKS HOLLOW ENERGY ASSOC LLC/ONTELAUNEE | BERKS HOLLOW ENERGY ASSOC LLC Greenhou | 12/17/2013 se Gase - CO2 | Equivalents 725 | | None | , | BTU/KW-HR | | |
| IA-0107 PA-0296 MD-0041 | MARSHALLTOWN GENERATING STATION BERKS HOLLOW ENERGY ASSOC LLC/ONTELAUNEE CPV ST. CHARLES | BERKS HOLLOW ENERGY ASSOC LLC Greenhou CPV MARYLAND, LLC | 12/17/2013 se Gase - CO2 4/23/2014 | 725 2,969 | MW | None | 7,109 | BTU/KW-HR BTU/KW-HR | BACT | GE F class |
| IA-0107 PA-0296 MD-0041 CT-0161 | MARSHALLTOWN GENERATING STATION BERKS HOLLOW ENERGY ASSOC LLC/ONTELAUNEE CPV ST. CHARLES KILLINGLY ENERGY CENTER | BERKS HOLLOW ENERGY ASSOC LLC Greenhou CPV MARYLAND, LLC NTE CONNECTICUT, LLC | 12/17/2013 se Gase - CO2 4/23/2014 6/30/2017 | 725 2,969 | MW MMBtu/hi | None Fuel | 7,109 7,273 | BTU/KW-HR BTU/KW-HR | BACT BACT | GE F class Mitsubishi J Class |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре | Turbine Model |
|---------|---|--|-----------------|------------|---------------------------------------|-----------|-----------------------|--------------|-------|---|
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 5,579 | MMBtu/hr | GCP | 57.07 | lb/MMBtu | BACT | 2 Siemens SGT-8000H |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 5,579 | MMBtu/hr | GCP | 57.07 | lb/MMBtu | BACT | 2 Siemens SGT-8000H |
| MI-0423 | INDECK NILES, LLC | INDECK NILES, LLC | 1/4/2017 | 8,322 | MMBtu/hr | GCP | 57.53 | lb/MMBtu | BACT | H Class? |
| TX-0612 | THOMAS C. FERGUSON POWER PLANT | LOWER COLORADO RIVER AUTHORITY | 11/10/2011 | 1,746 | MMBtu/hr | GCP | 87.85 | lb/MMBtu | BACT | GE 7FA |
| DE-0024 | GARRISON ENERGY CENTER | GARRISON ENERGY CENTER, LLC/ CALPINE CORPORATION | 1/30/2013 | 2,260 | MMBtu/hr | Fuel | 101.66 | lb/MMBtu | BACT | GE 7FA |
| PA-0278 | MOXIE LIBERTY LLC/ASYLUM POWER PL T | MOXIE ENERGY LLC | 10/10/2012 | 3,277 | MMBtu/hr | GCP | 103.12 | lb/MMBtu | BACT | F Class |
| PA-0296 | BERKS HOLLOW ENERGY ASSOC LLC/ONTELAUNEE | BERKS HOLLOW ENERGY ASSOC LLC | 12/17/2013 | 3,046 | MMBtu/hr | None | 103.50 | lb/MMBtu | BACT | GE H class |
| MI-0427 | FILER CITY STATION | FILER CITY STATION LIMITED PARTNERSHIP | 11/17/2017 | 1,935 | MMBtu/hr | GCP | 117.10 | lb/MMBtu | BACT | |
| MI-0412 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | HOLLAND BOARD OF PUBLIC WORKS | 12/4/2013 | 647 | MMBtu/hr | GCP | 119.67 | lb/MMBtu | BACT | İ |
| MI-0410 | THETFORD GENERATING STATION | CONSUMERS ENERGY COMPANY | 7/25/2013 | | MMBtu/hr | None | 122.34 | | BACT | İ |
| MI-0424 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | HOLLAND BOARD OF PUBLIC WORKS | 12/5/2016 | | MMBtu/hr | GCP | 128.71 | lb/MMBtu | BACT | |
| IA-0107 | MARSHALLTOWN GENERATING STATION | INTERSTATE POWER AND LIGHT | 4/14/2014 | 2,258 | | None | 133.33 | lb/MMBtu | BACT | Siemens SGT6-5000F |
| IA-0107 | MARSHALLTOWN GENERATING STATION | INTERSTATE POWER AND LIGHT | 4/14/2014 | | MMBtu/hr | None | 133.33 | | BACT | Siemens SGT6-5000F |
| W(010) | THE WASHINGTON OF THE STATE OF | THE TOWER THE ENGINEER PROPERTY OF THE PROPERT | 1,21,2021 | 2,230 | · · · · · · · · · · · · · · · · · · · | 110110 | 155.55 | 15/11111514 | 57.0. | Siemens serie sees. |
| | | | | | | | | | | Never built. In 2011, proposed |
| | | | | | | | | | | turbines were GE. Currently |
| | | | | | | | | | | |
| CA 1212 | DALMONIE LIVERID DOWER PROJECT | CITY OF DALMOALE | 10/18/2011 | 154 | N 4147 | None | 774 | lb/MW-hr | DACT | proposed turbines are Siemens STG6-5000F |
| | PALMDALE HYBRID POWER PROJECT | CITY OF PALMDALE | | | MW | None | | • | BACT | |
| WV-0025 | MOUNDSVILLE COMBINED CYCLE POWER PLANT | MOUNDSVILLE POWER, LLC | 11/21/2014 | 2,420 | MMBtu/hr | Fuel | 792 | lb/MW-hr | BACT | GE Frame 7FA.04 |
| | | | . / / | | | | | | | GE Energy 7F Series 5 Rapid |
| MA-0039 | SALEM HARBOR STATION REDEVELOPMENT | FOOTPRINT POWER SALEM HARBOR DEVELOPMENT LP | 1/30/2014 | 2,449 | MMBtu/hr | None | 825 | lb/MW-hr | BACT | Response |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | | MW | GCP | 840 | • | BACT | 2 Siemens SGT-8000H |
| FL-0356 | OKEECHOBEE CLEAN ENERGY CENTER | FLORIDA POWER & LIGHT | 3/9/2016 | 3,096 | MMBtu/hr | Fuel | 850 | lb/MW-hr | BACT | GE 7HA.02 |
| | | | | | | | | | | SGT-8000H VERSION 1.4- |
| | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | | MW | None | 865 | lb/MW-hr | BACT | OPTIMIZED |
| | ROCKWOOD ENERGY CENTER | ROCKWOOD ENERGY CENTER, LLC | 3/18/2016 | 1,127 | | GCP | 865 | | BACT | GE 7FA.0 |
| TX-0773 | FGE EAGLE PINES PROJECT | FGE EAGLE PINES, LLC | 11/4/2015 | | MW | GCP/Fuel | 886 | | BACT | Alstom GT36 |
| NJ-0080 | HESS NEWARK ENERGY CENTER | HESS NEWARK ENERGY CENTER, LLC | 11/1/2012 | 4,595 | MMBtu/hr | GCP | 887 | lb/MW-hr | BACT | GE |
| NJ-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | MW | Fuel | 888 | lb/MW-hr | BACT | GE 7HA.02 |
| NJ-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | MW | Fuel | 888 | lb/MW-hr | BACT | GE 7HA.02 |
| TX-0748 | FGE POWER, FGE TEXAS PROJECT | FGE POWER, LLC | 4/28/2014 | 231 | MW | None | 889 | lb/MW-hr | BACT | Alstom GT24 |
| TX-0791 | ROCKWOOD ENERGY CENTER | ROCKWOOD ENERGY CENTER, LLC | 3/18/2016 | 889 | MW | GCP | 901 | lb/MW-hr | BACT | GE 7FA.0 |
| TX-0805 | EAGLE MOUNTAIN STEAM ELECTRIC STATION | EAGLE MOUNTAIN POWER COMPANY | 7/19/2016 | 462 | MW | GCP | 917 | lb/MW-hr | BACT | |
| TX-0788 | NECHES STATION | APEX TEXAS POWER LLC | 3/24/2016 | 231 | MW | GCP | 924 | | BACT | Siemens or GE |
| NJ-0079 | WOODBRIDGE ENERGY CENTER | CPV SHORE, LLC | 7/25/2012 | 4,692 | MMBtu/hr | GCP | 925 | lb/MW-hr | BACT | GE |
| TX-0791 | ROCKWOOD ENERGY CENTER | ROCKWOOD ENERGY CENTER, LLC | 3/18/2016 | 889 | MW | GCP | 929 | lb/MW-hr | BACT | MHI 501GAC |
| TX-0791 | ROCKWOOD ENERGY CENTER | ROCKWOOD ENERGY CENTER, LLC | 3/18/2016 | | MW | GCP | 929 | | BACT | MHI 501GAC |
| | AUSTIN ENERGY, SAND HILL ENERGY CENTER | CITY OF AUSTIN | 9/29/2014 | | MW | None | 930 | | BACT | GE 7FA.04 |
| TX-0787 | TRINIDAD GENERATING FACILITY | SOUTHERN POWER | 3/1/2016 | | MW | GCP | 937 | lb/MW-hr | BACT | |
| | ROCKWOOD ENERGY CENTER | ROCKWOOD ENERGY CENTER, LLC | 3/18/2016 | | MW | GCP | 944 | | BACT | GE 7FA.0 |
| | WEST DEPTFORD ENERGY STATION | WEST DEPTFORD ENERGY ASSOCIATES | 7/18/2014 | | MMBtu/hr | GCP/Fuel | 947 | | BACT | Siemens |
| | SUMPTER POWER PLANT | WOLVERINE POWER SUPPLY COOPERATIVE INC. | 11/17/2011 | | MW | None | 954 | | BACT | |
| | GAINES COUNTY POWER PLANT | SOUTHWESTERN PUBLIC SERVICE COMPANY | 4/28/2017 | | MW | Fuel | 960 | , | BACT | Siemens SGT6-5000F5 |
| TX-0813 | ROCKWOOD ENERGY CENTER | ROCKWOOD ENERGY CENTER, LLC | 3/18/2016 | | MW | GCP | 965 | | BACT | Siemens SCC6-8000H(1.4 |
| | DECORDOVA STEAM ELECTRIC STATION (DECORDOVA ST | , | 10/4/2016 | | MW | GCP/Fuel | 966 | | BACT | GE 7FA |
| MI-0405 | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | | MMBtu/hr | GCP/Fuel | 995 | | BACT | SE /1A |
| MI-0405 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | | MMBtu/hr | GCP/Fuel | 1,000 | | BACT | |
| | | | 11/1/2013 | - | - | | | - | | |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | | | MMBtu/hr | GCP | 1,000 | • | BACT | Sigmons SCT6 FOODE |
| | MOORELAND GENERATING STA | WESTERN FARMERS ELECTRIC COOPERATIVE | 7/2/2013 | 360 | | GCP | 1,000 | lb/MW-hr | BACT | Siemens SGT6-5000F5 |
| | MOORELAND GENERATING STA | WESTERN FARMERS ELECTRIC COOPERATIVE | 7/2/2013 | | MW | GCP | 1,000 | | BACT | Siemens SGT6-5000F5 |
| OR-0050 | TROUTDALE ENERGY CENTER, LLC | TROUTDALE ENERGY CENTER, LLC | 3/5/2014 | | MMBtu/hr | GCP/Fuel | 1,000 | - / | BACT | Mitsubishi M501-GAC |
| | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | | MMBtu/hr | GCP/Fuel | 1,071 | | BACT | |
| TN-0162 | JOHNSONVILLE COGENERATION | TENNESSEE VALLEY AUTHORITY | 4/19/2016 | | MMBtu/hr | OxCat/GCP | 1,800 | | BACT | |
| TX-0766 | GOLDEN PASS LNG EXPORT TERMINAL | GOLDEN PASS PRODUCTS, LLC | 9/11/2015 | | MW | GCP | 614,533 | tpy | BACT | GE Frame 7 |
| KS-0029 | THE EMPIRE DISTRICT ELECTRIC COMPANY | THE EMPIRE DISTRICT ELECTRIC COMPANY | 7/14/2015 | | MW | None | 1,022,756 | tpy | BACT | |
| | | | Sulfuric Acid N | | | | | | | |
| | S R BERTRON ELECTRIC GENERATING STATION | NRG TEXAS POWER LLC | 12/19/2014 | _ | MW | None | | GR S/100 SCF | BACT | Siemens Model F5 (SF5 |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре | Turbine Model |
|---------|--|--|------------------------|------------|----------|--------------|----------------|----------------|--------------|-------------------------------|
| | ST. JOSEPH ENEGRY CENTER, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 2,300 | MMBtu/hr | Fuel | | GR S/100 SCF | BACT | |
| | NECHES STATION | APEX TEXAS POWER LLC | 3/24/2016 | | MW | GCP/Fuel | | GR S/100 SCF | BACT | Siemens or GE |
| FL-0356 | OKEECHOBEE CLEAN ENERGY CENTER | FLORIDA POWER & LIGHT | 3/9/2016 | 3.096 | MMBtu/hr | Fuel | 2.00 | GR S/100 SCF | BACT | GE 7HA.02 |
| | COLORADO BEND ENERGY CENTER | COLORADO BEND II POWER, LLC | 4/1/2015 | 1,100 | | GCP | 2.00 | GR S/100 SCF | BACT | GE Model 7HA.02 |
| TX-0789 | DECORDOVA STEAM ELECTRIC STATION | DECORDOVA II POWER COMPANY LLC | 3/8/2016 | 231 | MW | GCP/Fuel | 5.00 | GR S/100 SCF | BACT | Siemens or GE |
| OH-0356 | DUKE ENERGY HANGING ROCK ENERGY | DUKE ENERGY HANGING ROCK, LLC | 12/18/2012 | 172 | MW | Fuel | 0.18 | lb/hr | BACT | GE 7FA |
| OH-0356 | DUKE ENERGY HANGING ROCK ENERGY | DUKE ENERGY HANGING ROCK, LLC | 12/18/2012 | 172 | MW | Fuel | 0.23 | lb/hr | BACT | GE 7FA |
| MD-0041 | CPV ST. CHARLES | CPV MARYLAND, LLC | 4/23/2014 | 725 | MW | Fuel | 2.20 | lb/hr | BACT | GE F class |
| TX-0773 | FGE EAGLE PINES PROJECT | FGE EAGLE PINES, LLC | 11/4/2015 | 321 | MW | Fuel | 2.37 | lb/hr | BACT | Alstom GT36 |
| NJ-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | MW | Fuel | 3.61 | lb/hr | BACT | GE 7HA.02 |
| NJ-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | MW | Fuel | 4.26 | lb/hr | BACT | GE 7HA.02 |
| | | | | | | | | | | SGT-8000H VERSION 1.4- |
| MD-0045 | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | MW | None | 4.60 | lb/hr | BACT | OPTIMIZED |
| TX-0600 | THOMAS C. FERGUSON POWER PLANT | LOWER COLORADO RIVER AUTHORITY | 9/1/2011 | 390 | MW | Fuel | 13.68 | lb/hr | BACT | GE 7FA |
| TX-0751 | EAGLE MOUNTAIN STEAM ELECTRIC STATION | EAGLE MOUNTAIN POWER COMPANY LLC | 6/18/2015 | 210 | MW | None | 15.56 | lb/hr | BACT | Siemens or GE |
| VA-0315 | WARREN COUNTY POWER PLANT - DOMINION | VIRGINIA ELECTRIC AND POWER COMPANY | 12/17/2010 | 2,996 | MMBtu/hr | Fuel | 0.00030 | lb/MMBtu | BACT | MHI M501 GAC |
| LA-0313 | ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | 3,625 | MMBtu/hr | Fuel | 0.00033 | lb/MMBtu | BACT | |
| LA-0313 | ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | 3,625 | MMBtu/hr | Fuel | 0.00033 | lb/MMBtu | BACT | |
| CT-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | 2,969 | MMBtu/hr | Fuel | 0.00050 | lb/MMBtu | BACT | |
| MI-0423 | INDECK NILES, LLC | INDECK NILES, LLC | 1/4/2017 | 8,322 | MMBtu/hr | GCP/Fuel | 0.00055 | lb/MMBtu | BACT | |
| | | | | | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | Fuel | 0.00070 | lb/MMBtu | BACT | 5000F |
| NY-0104 | CPV VALLEY ENERGY CENTER | CPV VALLEY LLC | 8/1/2013 | 2,234 | MMBtu/hr | Fuel | 0.00070 | lb/MMBtu | BACT | |
| | | | | | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | Fuel | 0.00071 | lb/MMBtu | BACT | 5000F |
| | | | | | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | Fuel | 0.00071 | lb/MMBtu | BACT | 5000F |
| | | | | | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | Fuel | 0.00075 | lb/MMBtu | BACT | 5000F |
| CT-0157 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | 2,420 | MMBtu/hr | None | 0.00087 | lb/MMBtu | BACT | |
| CT-0158 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | 2,420 | MMBtu/hr | Fuel | 0.00087 | lb/MMBtu | BACT | |
| LA-0224 | ARSENAL HILL POWER PLANT | SOUTHWEST ELECTRIC POWER COMPANY (SWEPCO) | 3/20/2008 | 2,110 | MMBtu/hr | SCR/Fuel | 0.00088 | lb/MMBtu | BACT | |
| | | | | | | | | | | GE Energy 7F Series 5 Rapid |
| MA-0039 | SALEM HARBOR STATION REDEVELOPMENT | FOOTPRINT POWER SALEM HARBOR DEVELOPMENT LP | 1/30/2014 | 2,449 | MMBtu/hr | None | 0.00100 | lb/MMBtu | BACT | Response |
| IA-0107 | MARSHALLTOWN GENERATING STATION | INTERSTATE POWER AND LIGHT | 4/14/2014 | 2,258 | MMBtu/hr | None | 0.00320 | lb/MMBtu | BACT | Siemens SGT6-5000F |
| IA-0107 | MARSHALLTOWN GENERATING STATION | INTERSTATE POWER AND LIGHT | 4/14/2014 | 2,258 | MMBtu/hr | None | 0.00320 | lb/MMBtu | BACT | |
| DE-0024 | GARRISON ENERGY CENTER | GARRISON ENERGY CENTER, LLC/ CALPINE CORPORATION | 1/30/2013 | 2,260 | MMBtu/hr | None | 0.01075 | lb/MMBtu | BACT | |
| | | | PM10 | | | | | | | |
| FL-0304 | CANE ISLAND POWER PARK | FLORIDA MUNICIPAL POWER AGENCY (FMPA | 9/8/2008 | 1,860 | MMBtu/hr | Fuel | 2.0 | GR S/100 SCF | BACT | GE 7241 FA CTG |
| FL-0356 | OKEECHOBEE CLEAN ENERGY CENTER | FLORIDA POWER & LIGHT | 3/9/2016 | 3,096 | MMBtu/hr | Fuel | 2.0 | GR S/100 SCF | BACT | |
| | | | | | | | | | | Never built. Proposed Model |
| CA-1192 | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | MW | Fuel | 8.9 | lb/hr | BACT | GE 7241 FA |
| | | | | | | | | | | Never built. Proposed Model |
| | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | | MW | Fuel | | lb/hr | BACT | GE 7241 FA |
| | MORRO BAY POWER PLANT | DYNERGY MORRO BAY LLC | 9/25/2008 | | MW | Fuel | | lb/hr | BACT | GE Frame 7, Model PG7241 |
| | MORRO BAY POWER PLANT | DYNERGY MORRO BAY LLC | 9/25/2008 | 180 | | Fuel | | lb/hr | BACT | GE Frame 7, Model PG7241 |
| MD-0046 | KEYS ENERGY CENTER | KEYS ENERGY CENTER, LLC | 10/31/2014 | 235 | MW | GCP/Fuel | 11.0 | lb/hr | BACT | SGT6-500FEE |
| | | | | | | | | | | SGT6-5000F CTGs or four GE |
| TX-0590 | KING POWER STATION | PONDERA CAPITAL MANAGEMENT GP INC | 8/5/2010 | 1,350 | | Fuel | 11.1 | | BACT | Frame 7FA CTGs |
| NJ-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | MW | Fuel | 11.7 | lb/hr | BACT | GE 7HA.02 |
| | | | | | | | | | | Never built. Proposed Model |
| CA-1192 | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | MW | Fuel | 11.8 | lb/hr | BACT | GE 7241 FA |
| | | | | | 1 | | | | | Never built. Proposed Model |
| CA-1192 | AVENAL ENERGY PROJECT | AVENAL POWER CENTER LLC | 6/21/2011 | 180 | MW | Fuel | 11.8 | lb/hr | BACT | GE 7241 FA |
| _ | | | | | | | | | | Mitsubishi M501 GAC units or |
| | | | | | | | | | | |
| | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 799 | | Fuel | 13.3 | lb/hr | BACT | 2 Siemens SGT-8000H |
| | OREGON CLEAN ENERGY CENTER COLUSA GENERATING STATION | ARCADIS, US, INC. PACIFIC GAS & ELECTRIC COMPANY | 6/18/2013 3/11/2011 | | MW | Fuel Fuel | | lb/hr lb/hr | BACT BACT | 2 Siemens SGT-8000H GE 7FA |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Type | Turbine Model |
|-------------------------------|---|---|--|-------------------------------|----------------------------|---------------------------|-------------------------|--|----------------------|-------------------------------|
| | · | · | | | | | | | | Siemens SCC6-5000 CTGs and |
| | | | | | | | | | | a SST6-5000 ST, or two GE 7FA |
| TX-0767 | LON C. HILL POWER STATION | LON C. HILL, L.P. | 10/2/2015 | 195 | MW | GCP/Fuel | 16.0 | lb/hr | BACT | CTGs and a D-11 ST. |
| | | | , , | | | , | | , | | SGT-8000H VERSION 1.4- |
| MD-0045 | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | MW | GCP/Fuel | 17.9 | lb/hr | BACT | OPTIMIZED |
| | ES JOSLIN POWER PLANT | CALHOUN PORT AUTHORITY | 9/12/2012 | | MW | GCP/Fuel | | lb/hr | BACT | GE 7FA |
| | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | | MW | None | | lb/hr | BACT | GE 7HA.02 |
| TX-0788 | NECHES STATION | APEX TEXAS POWER LLC | 3/24/2016 | | MW | GCP/Fuel | | lb/hr | BACT | Siemens or GE |
| | DUKE ENERGY HANGING ROCK ENERGY | DUKE ENERGY HANGING ROCK, LLC | 12/18/2012 | | MW | Fuel | | lb/hr | BACT | GE 7FA |
| | | | | | | | | | | |
| TX-0773 | FGE EAGLE PINES PROJECT | FGE EAGLE PINES, LLC | 11/4/2015 | | MW | None . | | lb/hr | BACT | Alstom GT36 |
| TX-0618 | CHANNEL ENERGY CENTER LLC | CHANNEL ENERGY CENTER LLC | 10/15/2012 | 180 | MW | GCP/Fuel | 27.0 | lb/hr | BACT | Siemens 501F |
| | | | | | | /- | | , | | |
| TX-0619 | DEER PARK ENERGY CENTER | DEER PARK ENERGY CENTER LLC | 9/26/2012 | | MW | GCP/Fuel | | lb/hr | BACT | Siemens/Westinghouse 501F |
| | THE EMPIRE DISTRICT ELECTRIC COMPANY | THE EMPIRE DISTRICT ELECTRIC COMPANY | 7/14/2015 | | MW | DLN | | lb/hr | BACT | |
| | EAGLE MOUNTAIN STEAM ELECTRIC STATION | EAGLE MOUNTAIN POWER COMPANY LLC | 6/18/2015 | | MW | None | 35.5 | | BACT | Siemens or GE |
| TX-0789 | DECORDOVA STEAM ELECTRIC STATION | DECORDOVA II POWER COMPANY LLC | 3/8/2016 | | MW | GCP/Fuel | | lb/hr | BACT | Siemens or GE |
| OR-0050 | TROUTDALE ENERGY CENTER, LLC | TROUTDALE ENERGY CENTER, LLC | 3/5/2014 | 2,988 | MMBtu/hr | r Fuel | 42.3 | lb/hr | BACT | Mitsubishi M501-GAC |
| TX-0730 | COLORADO BEND ENERGY CENTER | COLORADO BEND II POWER, LLC | 4/1/2015 | 1,100 | MW | GCP | 43.0 | lb/hr | BACT | GE Model 7HA.02 |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 5,579 | MMBtu/hr | Fuel | 0.0018 | lb/MMBtu | BACT | 2 Siemens SGT-8000H |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 5.579 | MMBtu/hr | Fuel | 0.0020 | lb/MMBtu | BACT | 2 Siemens SGT-8000H |
| | | | 5, 25, 2525 | 0,0.10 | | | | , | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 6 004 | MMBtu/hr | Fuel | 0.0023 | lb/MMBtu | BACT | 2 Siemens SGT-8000H |
| | INDECK NILES, LLC | INDECK NILES, LLC | 1/4/2017 | 8,322 | | GCP/Fuel/Inlet Air Filter | | lb/MMBtu | BACT | 2 5/6/11/6/13 5/6/1 6/6/6/11 |
| | WARREN COUNTY POWER PLANT - DOMINION | VIRGINIA ELECTRIC AND POWER COMPANY | 12/17/2010 | | MMBtu/hr | | 0.0024 | | BACT | MHI M501 GAC |
| VA-0313 | WARREN COUNTY FOWER FLANT - DOMINION | VIRGINIA ELECTRIC AND FOWER CONFANT | 12/17/2010 | 2,990 | IVIIVIBLU/III | ruei | 0.0027 | ID/ IVIIVIBLU | BACI | GE7FA.05 OR Siemens SGT6 |
| | DOTO TOCOU LLO CENTADEN CENTEDATINO CTATION | DOEG FOCCII I I G | 2/7/2044 | 2 022 | /1 | - 1 | 0.0000 | 11 /2 42 40 1 | DA CT | |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | Fuel | 0.0032 | lb/MMBtu | BACT | 5000F |
| | | | - /- / | | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | Fuel | 0.0033 | lb/MMBtu | BACT | 5000F |
| | | | | | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | Fuel | 0.0036 | lb/MMBtu | BACT | 5000F |
| LA-0254 | NINEMILE POINT ELECTRIC GENERATING PLANT | ENTERGY LOUISIANA LLC | 8/16/2011 | 7,146 | MMBtu/hr | GCP/Fuel | 0.0037 | lb/MMBtu | BACT | |
| | | | | | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | r Fuel | 0.0037 | lb/MMBtu | BACT | 5000F |
| NJ-0079 | WOODBRIDGE ENERGY CENTER | CPV SHORE, LLC | 7/25/2012 | 4,692 | MMBtu/hr | GCP/Fuel | 0.0041 | lb/MMBtu | BACT | GE |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | 2,147 | MMBtu/hr | GCP | 0.0042 | lb/MMBtu | BACT | |
| NJ-0082 | WEST DEPTFORD ENERGY STATION | WEST DEPTFORD ENERGY ASSOCIATES | 7/18/2014 | 2,362 | MMBtu/hr | Fuel | 0.0042 | lb/MMBtu | BACT | Siemens |
| CA-1212 | PALMDALE HYBRID POWER PROJECT | CITY OF PALMDALE | 10/18/2011 | 154 | MW | Fuel | 0.0048 | lb/MMBtu | BACT | |
| CT-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | 2,639 | MMBtu/hr | GCP | 0.0050 | lb/MMBtu | BACT | |
| | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | | MMBtu/hr | | 0.0060 | | BACT | |
| | | | , , , , , , | , , | , | | | , | | GE Energy 7F Series 5 Rapid |
| MA-0039 | SALEM HARBOR STATION REDEVELOPMENT | FOOTPRINT POWER SALEM HARBOR DEVELOPMENT LP | 1/30/2014 | 2 449 | MMBtu/hr | None | 0.0062 | lb/MMBtu | BACT | Response |
| | THETFORD GENERATING STATION | CONSUMERS ENERGY COMPANY | 7/25/2013 | | MMBtu/hr | Fuel | 0.0066 | | BACT | пезропае |
| | FILER CITY STATION | FILER CITY STATION LIMITED PARTNERSHIP | 11/17/2017 | | | GCP/Fuel/Inlet Air Filter | 0.0066 | | BACT | |
| | WEST DEPTFORD ENERGY STATION | WEST DEPTFORD ENERGY ASSOCIATES | 7/18/2014 | | MMBtu/hr | Fuel | 0.0069 | - | BACT | Ciamans |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | | MMBtu/hr | GCP | 0.0003 | | BACT | Siemens |
| | | | | | | | | lb/MMBtu | | CE E alare advanced |
| MD-0041 | CPV ST. CHARLES | CPV MARYLAND, LLC | 4/23/2014 | | MW | GCP/Fuel | 0.0080 | | BACT | GE F-class advanced |
| | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | | MMBtu/hr | GCP /5 | 0.0080 | | BACT | + |
| CO-0073 | PUEBLO AIRPORT GENERATING STATION | BLACK HILLS ELECTRIC GENERATION, LLC | 7/22/2010 | | MMBtu/hr | GCP/Fuel | 0.0115 | - | BACT | + |
| MI-0412 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | HOLLAND BOARD OF PUBLIC WORKS | 12/4/2013 | | MMBtu/hr | | 0.0140 | | BACT | |
| | | HOLLAND BOARD OF PUBLIC WORKS | 12/5/2016 | | MMBtu/hr | GCP/Fuel | 0.0140 | | BACT | 1 |
| MI-0424 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | i | | | | GCP | 0.0440 | III / N A N A D + | BACT | 1 |
| MI-0424 CT-0161 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | | MMBtu/hr | GCP | 0.0440 | lb/MMBtu | BACI | |
| CT-0161 | KILLINGLY ENERGY CENTER | PN | 110 (filterable | only) | | | | | • | |
| CT-0161 | | | 110 (filterable 10/14/2012 | | | GCP | 2.0 | GR S/100 SCF | BACT | |
| CT-0161 | KILLINGLY ENERGY CENTER | PN | 110 (filterable | only) 1,160 | | GCP | 2.0 | | • | GE |
| CT-0161 FL-0337 | KILLINGLY ENERGY CENTER POLK POWER STATION | TAMPA ELECTRIC COMPANY | 110 (filterable 10/14/2012 | only) 1,160 | MW MMBtu/hr | GCP | 2.0 | GR S/100 SCF | BACT | GE |
| CT-0161 FL-0337 NJ-0080 | KILLINGLY ENERGY CENTER POLK POWER STATION HESS NEWARK ENERGY CENTER | TAMPA ELECTRIC COMPANY HESS NEWARK ENERGY CENTER, LLC | 110 (filterable 10/14/2012 11/1/2012 | only) 1,160 4,595 | MW MMBtu/hr MMBtu/hr | GCP Fuel | 2.0 0.0024 | GR S/100 SCF lb/MMBtu | BACT BACT | GE GE |
| FL-0337 NJ-0080 OR-0048 | KILLINGLY ENERGY CENTER POLK POWER STATION HESS NEWARK ENERGY CENTER CARTY PLANT | TAMPA ELECTRIC COMPANY HESS NEWARK ENERGY CENTER, LLC PORTLAND GENERAL ELECTRIC | 110 (filterable 10/14/2012 11/1/2012 12/29/2010 | only) 1,160 4,595 2,866 4,595 | MW MMBtu/hr MMBtu/hr | GCP Fuel Fuel | 2.0 0.0024 0.0025 | GR S/100 SCF lb/MMBtu lb/MMBtu lb/MMBtu | BACT BACT BACT | |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре | Turbine Model |
|-----------|--|---|--------------|------------|---------------|---------------------------|-----------------------|---------------|-------|-------------------------------|
| LA-0313 | ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | 3,625 | MMBtu/hr | GCP/Fuel | 0.0048 | lb/MMBtu | BACT | |
| CT-0151 | KLEEN ENERGY SYSTEMS, LLC | KLEEN ENERGY SYSTEMS, LLC | 2/25/2008 | 2,142 | MMBtu/hr | r None | 0.0051 | lb/MMBtu | BACT | SIEMENS SGT6-5000F |
| AK-0073 | INTERNATIONAL STATION POWER PLANT | CHUGACH ELECTRIC ASSOCIATION | 12/20/2010 | 45 | MW | Fuel | 0.0066 | lb/MMBtu | BACT | |
| IN-0158 | ST. JOSEPH ENEGRY CENTER, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 2,300 | MMBtu/hr | GCP/Fuel | 0.0078 | lb/MMBtu | BACT | |
| LA-0136 | PLAQUEMINE COGENERATION FACILITY | THE DOW CHEMICAL COMPANY | 7/23/2008 | 2,876 | MMBtu/hr | r Fuel | 0.0116 | lb/MMBtu | BACT | GE FRAME 7 FA |
| LA-0308 | MORGAN CITY POWER PLANT | LOUISIANA ENERGY AND POWER AUTHORITY (LEPA) | 9/26/2013 | 607 | MMBtu/hr | GCP/Fuel | 0.0198 | lb/MMBtu | BACT | |
| · · | | , , | PM2.5 (total |) | <u> </u> | . , | | | • | • |
| FL-0356 | OKEECHOBEE CLEAN ENERGY CENTER | FLORIDA POWER & LIGHT | 3/9/2016 | | MMBtu/hr | r Fuel | 2.0 | GR S/100 SCF | BACT | GE 7HA.02 |
| | | | | | | | | | | SGT6-5000F CTGs or four GE |
| TX-0590 | KING POWER STATION | PONDERA CAPITAL MANAGEMENT GP INC | 8/5/2010 | 1,350 | MW | Fuel | 11.1 | lb/hr | BACT | Frame 7FA CTGs |
| NJ-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | MW | Fuel | 11.7 | lb/hr | BACT | GE 7HA.02 |
| | | | | | | | | | | Never built. No turbine |
| | | | | | | | | | | specified in Application for |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | Fuel | 12.0 | lb/hr | BACT | Certification of Project |
| | | | | | | | | | | Never built. No turbine |
| | | | | | | | | | | specified in Application for |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | Fuel | 12.0 | lb/hr | BACT | Certification of Project |
| TX-0678 | FREEPORT LNG PRETREATMENT FACILITY | FREEPORT LNG DEVELOPMENT LP | 7/16/2014 | | MW | None | | lb/hr | BACT | GE 7EA |
| | | | | | | | | | | Siemens SCC6-5000 CTGs and |
| | | | | | | | | | | a SST6-5000 ST, or two GE 7FA |
| TX-0767 | LON C. HILL POWER STATION | LON C. HILL, L.P. | 10/2/2015 | 195 | MW | GCP/Fuel | 16.0 | lb/hr | BACT | CTGs and a D-11 ST. |
| | | , | , , | | | , | | , | | |
| | | | | | | | | | | SIEMENS H-CLASS (SGT-8000H |
| MD-0045 | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | MW | GCP/Fuel | 17.9 | lb/hr | BACT | VERSION 1.4-OPTIMIZED |
| | | | | | | 20.7.20. | | , | | Never built. No turbine |
| | | | | | | | | | | specified in Application for |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | Fuel | 18.0 | lb/hr | BACT | Certification of Project |
| | | | 0,11,1010 | | | | | , | | Never built. No turbine |
| | | | | | | | | | | specified in Application for |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | Fuel | 18.0 | lb/hr | BACT | Certification of Project |
| TX-0620 | ES JOSLIN POWER PLANT | CALHOUN PORT AUTHORITY | 9/12/2012 | | MW | None | | lb/hr | BACT | GE 7FA |
| | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | | MW | None | | lb/hr | BACT | GE 7HA.02 |
| | NECHES STATION | APEX TEXAS POWER LLC | 3/24/2016 | | MW | GCP/Fuel | | lb/hr | BACT | Siemens or GE |
| TX-0773 | FGE EAGLE PINES PROJECT | FGE EAGLE PINES, LLC | 11/4/2015 | | MW | None | | lb/hr | BACT | Alstom GT36 |
| OK-0154 | MOORELAND GENERATING STA | WESTERN FARMERS ELECTRIC COOPERATIVE | 7/2/2013 | | MW | GCP/Fuel | 22.1 | | BACT | Siemens SGT6-5000F5 |
| OK-0154 | MOORELAND GENERATING STA | WESTERN FARMERS ELECTRIC COOPERATIVE | 7/2/2013 | | MW | GCP/Fuel | | lb/hr | BACT | Siemens SGT6-5000F5 |
| TX-0618 | CHANNEL ENERGY CENTER LLC | CHANNEL ENERGY CENTER LLC | 10/15/2012 | | MW | GCP/Fuel | | lb/hr | BACT | Siemens 501F |
| 17.0010 | CHAINTEE ENERGY CENTER EEG | CHANNEL ENERGY CENTER LEG | 10/10/2012 | 100 | | 00171 001 | 27.0 | , | 27101 | Siemens 301 |
| TX-0619 | DEER PARK ENERGY CENTER | DEER PARK ENERGY CENTER LLC | 9/26/2012 | 180 | MW | None | 27.0 | lb/hr | BACT | Siemens/Westinghouse 501F |
| TX-0600 | THOMAS C. FERGUSON POWER PLANT | LOWER COLORADO RIVER AUTHORITY | 9/1/2011 | | MW | Fuel | | lb/hr | BACT | GE 7FA |
| | EAGLE MOUNTAIN STEAM ELECTRIC STATION | EAGLE MOUNTAIN POWER COMPANY LLC | 6/18/2015 | | MW | None | | lb/hr | BACT | Siemens or GE |
| | DECORDOVA STEAM ELECTRIC STATION | DECORDOVA II POWER COMPANY LLC | 3/8/2016 | | MW | GCP/Fuel | | lb/hr | BACT | Siemens or GE |
| TX-0783 | COLORADO BEND ENERGY CENTER | COLORADO BEND II POWER, LLC | 4/1/2015 | 1,100 | | GCP | | lb/hr | BACT | GE Model 7HA.02 |
| MI-0423 | INDECK NILES, LLC | INDECK NILES, LLC | 1/4/2017 | 8.322 | | GCP/Fuel/Inlet Air Filter | 0.0024 | • | BACT | |
| VA-0315 | WARREN COUNTY POWER PLANT - DOMINION | VIRGINIA ELECTRIC AND POWER COMPANY | 12/17/2010 | -,- | MMBtu/hr | Fuel | 0.0024 | , | BACT | MHI M501 GAC |
| PA-0296 | BERKS HOLLOW ENERGY ASSOC LLC/ONTELAUNEE | BERKS HOLLOW ENERGY ASSOC LLC | 12/17/2013 | | MMBtu/hr | None | 0.0027 | • | BACT | |
| LA-0254 | NINEMILE POINT ELECTRIC GENERATING PLANT | ENTERGY LOUISIANA LLC | 8/16/2011 | 7,146 | | | 0.0037 | lb/MMBtu | BACT | + |
| | MOUNDSVILLE COMBINED CYCLE POWER PLANT | MOUNDSVILLE POWER, LLC | 11/21/2014 | | | GCP/Fuel/Inlet Air Filter | 0.0037 | | BACT | GE Frame 7FA.04 |
| CT-0157 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | | MMBtu/hr | None | 0.0037 | , | BACT | 221101110711104 |
| CT-0157 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | | MMBtu/hr | None | 0.0040 | | BACT | + |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | | MMBtu/hr | r GCP | 0.0040 | • | BACT | + |
| NJ-0082 | WEST DEPTFORD ENERGY STATION | WEST DEPTFORD ENERGY ASSOCIATES | 7/18/2014 | 2,362 | | r Fuel | 0.0042 | lb/MMBtu | BACT | Siemens |
| CT-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | 2,969 | | | 0.0042 | | BACT | 5.6615 |
| CA-1212 | PALMDALE HYBRID POWER PROJECT | CITY OF PALMDALE | 10/18/2011 | | MW | Fuel | 0.0044 | | BACT | + |
| CT-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | | MMBtu/hr | r GCP | 0.0048 | | BACT | + |
| MI-0405 | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | | MMBtu/hr | r GCP | | lb/MMBtu | BACT | + |
| 1911-0403 | MIDDING COGENERATION VENTURE | INTEGRAL COOLINERATION VENTURE | 4/23/2013 | 2,237 | iviiviotu/III | ULF | 0.0000 | IS/ IVIIVIBLU | DACI | GE Energy 7F Series 5 Rapid |
| MA-0039 | SALEM HARBOR STATION REDEVELOPMENT | FOOTPRINT POWER SALEM HARBOR DEVELOPMENT LP | 1/30/2014 | 2 440 | MMBtu/hr | n None | 0.0062 | lb/MMBtu | BACT | Response |
| MI-0402 | SUMPTER POWER PLANT | WOLVERINE POWER SUPPLY COOPERATIVE INC. | 1/30/2014 | | MW | None | 0.0062 | • | BACT | пеэропзе |
| | THETFORD GENERATING STATION | CONSUMERS ENERGY COMPANY | 7/25/2013 | | MMBtu/hr | | | lb/MMBtu | BACT | + |
| 1711-0410 | THE FFORD GENERATING STATION | CONSCIVIENS ENERGY CONTRAINT | //25/2013 | 2,587 | iviivibtu/fi | ruei | 0.0066 | ID/IVIIVIBLU | DACI | i |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре | Turbine Model |
|---------|---|---|-------------------|------------|----------|---------------------------|-----------------------|-----------|------|------------------------------|
| MI-0427 | FILER CITY STATION | FILER CITY STATION LIMITED PARTNERSHIP | 11/17/2017 | 1,935 | MMBtu/hr | GCP/Fuel/Inlet Air Filter | 0.0066 | lb/MMBtu | BACT | |
| NJ-0082 | WEST DEPTFORD ENERGY STATION | WEST DEPTFORD ENERGY ASSOCIATES | 7/18/2014 | 2,362 | MMBtu/hr | Fuel | 0.0069 | lb/MMBtu | BACT | Siemens |
| MI-0406 | RENAISSANCE POWER LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | 2,807 | MMBtu/hr | GCP | 0.0073 | lb/MMBtu | BACT | |
| MI-0405 | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | 2,486 | MMBtu/hr | GCP | 0.0080 | lb/MMBtu | BACT | |
| MI-0412 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | HOLLAND BOARD OF PUBLIC WORKS | 12/4/2013 | 647 | MMBtu/hr | GCP/Fuel | 0.0140 | lb/MMBtu | BACT | |
| MI-0424 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | HOLLAND BOARD OF PUBLIC WORKS | 12/5/2016 | 554 | MMBtu/hr | GCP/Fuel | 0.0140 | lb/MMBtu | BACT | |
| | | PN | /12.5 (filterable | only) | | | | | | |
| | | | | | | | | | | GE7FA.05 OR Siemens SGT6 |
| NJ-0081 | PSEG FOSSIL LLC SEWAREN GENERATING STATION | PSEG FOSSIL LLC | 3/7/2014 | 3,923 | MMBtu/hr | Fuel | 0.0025 | lb/MMBtu | BACT | 5000F |
| LA-0313 | ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | 3,625 | MMBtu/hr | GCP/Fuel | 0.0048 | lb/MMBtu | BACT | |
| LA-0313 | ST. CHARLES POWER STATION | ENTERGY LOUISIANA, LLC | 8/31/2016 | 3,625 | MMBtu/hr | GCP/Fuel | 0.0048 | lb/MMBtu | BACT | |
| IN-0158 | ST. JOSEPH ENEGRY CENTER, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 2,300 | MMBtu/hr | GCP/Fuel | 0.0078 | lb/MMBtu | BACT | |
| LA-0308 | MORGAN CITY POWER PLANT | LOUISIANA ENERGY AND POWER AUTHORITY (LEPA) | 9/26/2013 | 607 | MMBtu/hr | GCP/Fuel | 0.0198 | lb/MMBtu | BACT | |
| | | | Opacity | | | | | | | |
| IA-0107 | MARSHALLTOWN GENERATING STATION | INTERSTATE POWER AND LIGHT | 4/14/2014 | 2,258 | MMBtu/hr | None | 0 | % OPACITY | BACT | Siemens SGT6-5000F |
| MI-0405 | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | 2,237 | MMBtu/hr | GCP | 5 | % OPACITY | BACT | |
| MI-0405 | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | 2,486 | MMBtu/hr | GCP | 5 | % OPACITY | BACT | |
| FL-0303 | FPL WEST COUNTY ENERGY CENTER UNIT 3 | FLORIDA POWER AND LIGHT COMPANY (FP&L) | 7/30/2008 | 2,333 | MMBtu/hr | None | 10 | % OPACITY | BACT | |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 5,579 | MMBtu/hr | Fuel | 10 | % OPACITY | BACT | 2 Siemens SGT-8000H |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 5,579 | MMBtu/hr | Fuel | 10 | % OPACITY | BACT | 2 Siemens SGT-8000H |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 6,004 | MMBtu/hr | Fuel | 10 | % OPACITY | BACT | 2 Siemens SGT-8000H |
| | | | | | | | | | | Mitsubishi M501 GAC units or |
| OH-0352 | OREGON CLEAN ENERGY CENTER | ARCADIS, US, INC. | 6/18/2013 | 799 | MW | Fuel | 10 | % OPACITY | BACT | 2 Siemens SGT-8000H |

Table D-1a Addendum: RBLC Tables for Combined Cycle Turbines (Natural Gas) UPDATED DATA: November 2018 to October 2021

| DDICID | Facility Name | Common None | Downit Data | Thursday Haite | Control | Emission | Harita | Toma | Turbine |
|--------------------|--|--|-------------|---------------------------------|---|----------|---------------------|--------------|--|
| RBLC ID | Facility Name | Company Name | Permit Date | Throughput Units | Controls ⁴ | Limit | Units | Туре | Model |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | Nitrogen Oxides 576 MMBtu/hr | DLN/GCP | 17 | PPMV @ 15% O2 | BACT | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 431 MMBtu/hr | DLN/GCP | | PPMV @ 15% O2 | BACT | \vdash |
| | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 386 MMBtu/hr | DLN/GCP | | PPMV @ 15% O2 | BACT | \vdash |
| | PLANT BARRY | ALABAMA POWER COMPANY | 11/09/2020 | 744 MW | SCR | | PPM | BACT | |
| LA-0364 | FG LA COMPLEX | FG LA LLC | 01/06/2020 | 2222 mm btu/h | DLN/SCR | | PPMVD | BACT | \vdash |
| | BIG CAJUN I POWER PLANT | | 06/27/2019 | 1679 MM BTU/hr | DLN/WI | | PPMV | BACT | \vdash |
| | BIG CAJUN I POWER PLANT | LOUISIANA GENERATING, LLC LOUISIANA GENERATING, LLC | 06/27/2019 | 1679 MM BTU/hr | DLN/WI | | PPMV | BACT | \vdash |
| MI-0439 | JACKSON GENERATING STATION | | 04/02/2019 | | SI/GCP/CBF | | PPM | | |
| MI-0439 | | CONSUMERS ENERGY COMPANY | | 420 MW 667 MMBTU/H | | | PPM | BACT | |
| MI-0441 | LBWLERICKSON STATION LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | | DLN/SCR DLN/GCP | | | BACT BACT | ⊢—— |
| | | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 MMBTU/H | , | | PPM PPM | | \vdash |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 MMBTU/H | DLN/SCR | | | BACT | |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | 625 MW | DLN/SCR/GCP | | PPM | BACT | + |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 3421 MMBTU/H | DLN/SCR | | PPM | BACT | - |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | DLN/GCP | | PPM | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | DLN/SCR | | LB/H | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | DLN/SCR | | LB/H | BACT | |
| NJ-0088 | COGEN TECH LINDEN VENTURE LP | COGEN TECH LINDEN VENTURE LP | 07/30/2019 | 21042 MMCubic ft/yr | SCR/DLN/CBF | | LB/H | BACT | |
| *TX-0908 | NEWMAN POWER STATION | EL PASO ELECTRIC COMPANY | 08/27/2021 | 230 MW | DLN/SCR | | PPMVD | BACT | |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 MMCF/YR | DLN/SCR | | PPMVD 15% O2 | BACT | |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 MMCF/YR | DLN/SCR | | LB/TURBINE/CAL. DAY | BACT | |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 MMCF/YR | DLN/SCR | 60 | LB/TURBINE/EVENT | BACT | |
| *VA-0334 | DOMINION ENERGY - BRUNSWICK | VIRGINIA ELECTRIC AND POWER COMPANY | 12/01/2020 | 3442 MMBTU/H | DLN/SCR | 604 | LBS | BACT | ı |
| *VA-0334 | DOMINION ENERGY - BRUNSWICK | VIRGINIA ELECTRIC AND POWER COMPANY | 12/01/2020 | 3442 MMBTU/H | DLN/SCR | 604 | LBS | BACT | i |
| | | | | Carbon Monoxide | | | | | |
| | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 576 MMBtu/hr | OxCat/GCP | 5 | PPMV @ 15% O2 | BACT | İ |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 431 MMBtu/hr | OxCat/GCP | 5 | PPMV @ 15% O2 | BACT | i |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 386 MMBtu/hr | GCP/CBF | 15 | PPMV @ 15% O2 | BACT | |
| *AL-0328 | PLANT BARRY | ALABAMA POWER COMPANY | 11/09/2020 | 744 MW | OxCat | 23.8 | LB/HR | BACT | |
| IL-0130 | JACKSON ENERGY CENTER | JACKSON GENERATION, LLC | 12/31/2018 | 3864 mmBtu/hr | OxCat | 2 | PPMV | BACT | |
| LA-0364 | FG LA COMPLEX | FG LA LLC | 01/06/2020 | 2222 mm btu/h | CBP/catalytic oxidation | 4 | PPMVD | BACT | |
| *LA-0365 | BIG CAJUN I POWER PLANT | LOUISIANA GENERATING, LLC | 06/27/2019 | 1679 MM BTU/hr | | 25 | PPMV | BACT | |
| *LA-0365 | BIG CAJUN I POWER PLANT | LOUISIANA GENERATING, LLC | 06/27/2019 | 1679 MM BTU/hr | | 25 | PPMV | BACT | |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 MMBTU/H | OxCat/GCP | 4 | PPM | BACT | |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 MMBTU/H | DLN/GCP | 9 | LB/H | BACT | |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 MMBTU/H | OxCat/GCP | 4 | PPM | BACT | |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | 625 MW | OxCat/GCP | 2 | PPM | BACT | |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 3421 MMBTU/H | OxCat/GCP | 4 | PPM | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | DLN/GCP | 9 | LB/H | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | OxCat/GCP | | PPM | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | OxCat/GCP | | PPM | BACT | |
| *TX-0908 | NEWMAN POWER STATION | EL PASO ELECTRIC COMPANY | 08/27/2021 | 230 MW | OxCat | | PPMVD | BACT | |
| *TX-0915 | UNIT 5 | NRG CEDAR BAYOU LLC | 03/17/2021 | 0 | OxCat | | PPMVD | BACT | |
| *TX-0915 | UNIT 5 | NRG CEDAR BAYOU LLC | 03/17/2021 | 14552539 MMBTU/YR | OxCat | | PPMVD | BACT | |
| VA-0313 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 MMCF/YR | OxCat/GCP | | PPMVD @ 15% O2 | BACT | |
| VA-0332 VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 MMCF/YR | OxCat/GCP | | LB/TURBINE/DAY | BACT | \vdash |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 MMCF/YR | OxCat/GCP | | LB/TURBINE/EVENT | BACT | \vdash |
| *VA-0334 | DOMINION ENERGY - BRUNSWICK | VIRGINIA ELECTRIC AND POWER COMPANY | 12/01/2020 | 3442 MMBTU/H | OxCat/GCP OxCat/GCP | | LBS | BACT | \vdash |
| | DOMINION ENERGY - BRUNSWICK DOMINION ENERGY - BRUNSWICK | VIRGINIA ELECTRIC AND POWER COMPANY | 12/01/2020 | 3442 MMBTU/H | OxCat/GCP OxCat/GCP | | LBS | BACT | \vdash |
| | | VIRGINIA ELECTRIC AND POWER COMPANY | , , , , | 3442 IVIIVIBTU/H | 1 | 416 | LD3 | DACI | |

⁽a) SCR = selective catalytic reduction, DLN = dry, low-NOx burners, WI = water injection, GCP = good combustion practices, CBF = clean burning fuels, OxCat = oxidation catalyst

Table D-1a Addendum: RBLC Tables for Combined Cycle Turbines (Natural Gas) UPDATED DATA: November 2018 to October 2021

| | | | | | | Emission | | | Turbine |
|----------|------------------------------|--|-------------|------------------------------------|--------------------------------|----------|------------------|------|----------|
| RBLC ID | Facility Name | Company Name | Permit Date | Throughput Units | Controls ^A | Limit | Units | Туре | Model |
| | | <u> </u> | | /olatile Organic Compounds | | <u> </u> | • | | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 576 MMBtu/hr | OxCat/GCP | 0.0022 | LB/MMBTU | BACT | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 431 MMBtu/hr | OxCat/GCP | 0.0022 | LB/MMBTU | BACT | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 386 MMBtu/hr | GCP/CBF | 0.0022 | LB/MMBTU | BACT | |
| *AL-0328 | PLANT BARRY | ALABAMA POWER COMPANY | 11/09/2020 | 744 MW | OxCat | 13.6 | LB/HR | BACT | |
| LA-0364 | FG LA COMPLEX | FG LA LLC | 01/06/2020 | 2222 mm btu/h | OxCat/GCP | 4 | PPMVD | BACT | |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 MMBTU/H | OxCat/GCP | 3 | PPM | BACT | |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 MMBTU/H | GCP | 5 | LB/H | BACT | |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 MMBTU/H | OxCat/GCP | 3 | PPM | BACT | |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | 625 MW | OxCat/GCP | | LB/MMBTU | BACT | |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 3421 MMBTU/H | GCP/CBF/Inlet Air Conditioning | | PPM | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | GCP | | LB/H | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | OxCat/GCP | | PPM | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | OxCat/GCP | | PPM | BACT | |
| *TX-0908 | NEWMAN POWER STATION | EL PASO ELECTRIC COMPANY | 08/27/2021 | 230 MW | OxCat/GCP/CBF | | PPMVD | BACT | |
| *TX-0915 | UNIT 5 | NRG CEDAR BAYOU LLC | 03/17/2021 | 0 | OxCat | | PPMVD | BACT | |
| *TX-0915 | UNIT 5 | NRG CEDAR BAYOU LLC | 03/17/2021 | 14552539 MMBTU/YR | OxCat | | PPMVD | BACT | |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 MMCF/YR | OxCat/GCP | | PPMVD @ 15% O2 | BACT | |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 MMCF/YR | OxCat/GCP | 216 | LB/TURBINE/EVENT | BACT | |
| | | | | PM ₁₀ (total) | | | | | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 576 MMBtu/hr | GCP/CBF | 0.0063 | LB/MMBTU | BACT | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 431 MMBtu/hr | GCP/CBF | 0.0063 | LB/MMBTU | BACT | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 386 MMBtu/hr | GCP/CBF | 0.007 | LB/MMBTU | BACT | |
| *AL-0328 | PLANT BARRY | ALABAMA POWER COMPANY | 11/09/2020 | 744 MW | | 0.004 | LB/MMBTU | BACT | |
| LA-0364 | FG LA COMPLEX | FG LA LLC | 01/06/2020 | 2222 mm btu/h | GCP/CBF | 12.46 | LB/H | BACT | |
| *LA-0365 | BIG CAJUN I POWER PLANT | LOUISIANA GENERATING, LLC | 06/27/2019 | 1679 MM BTU/hr | Good Combustion Controls | 19 | LB/HR | BACT | |
| *LA-0365 | BIG CAJUN I POWER PLANT | LOUISIANA GENERATING, LLC | 06/27/2019 | 1679 MM BTU/hr | Good Combustion Controls | 19 | LB/HR | BACT | |
| MI-0439 | JACKSON GENERATING STATION | CONSUMERS ENERGY COMPANY | 04/02/2019 | 420 MW | Inlet Air Filters/GCP/CBF | 4.9 | LB/H | BACT | |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 MMBTU/H | inlet air conditioning/CBF/GCP | 6.02 | LB/H | BACT | |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 MMBTU/H | inlet air conditioning/CBF/GCP | 4.5 | LB/H | BACT | |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 MMBTU/H | inlet air conditioning/CBF/GCP | 6.02 | LB/H | BACT | |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | 625 MW | GCP/CBF | 0.006 | LB/MMBTU | BACT | |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 3421 MMBTU/H | inlet air conditioning/CBF/GCP | 19.8 | LB/H | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | inlet air conditioning/CBF/GCP | 4.5 | LB/H | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | inlet air conditioning/CBF/GCP | 6.02 | LB/H | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | inlet air conditioning/CBF/GCP | 6.02 | LB/H | BACT | |
| NJ-0088 | COGEN TECH LINDEN VENTURE LP | COGEN TECH LINDEN VENTURE LP | 07/30/2019 | 21042 MMCubic ft/yr | CBF | 11.58 | LB/H | BACT | |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 MMCF/YR | GCP/CBF | 0.0052 | LB/MMBTU | BACT | |
| | | | | PM ₁₀ (filterable only) | | | | | |
| *TX-0915 | UNIT 5 | NRG CEDAR BAYOU LLC | 03/17/2021 | 0 | CBF | 0 | | BACT | |
| *TX-0915 | UNIT 5 | NRG CEDAR BAYOU LLC | 03/17/2021 | 14552539 MMBTU/YR | CBF | 0 | | BACT | |
| | | | | PM _{2.5} (total) | | | | | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 576 MMBtu/hr | GCP/CBF | 0.0063 | LB/MMBTU | BACT | T |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 431 MMBtu/hr | GCP/CBF | | LB/MMBTU | BACT | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 386 MMBtu/hr | GCP/CBF | | LB/MMBTU | BACT | \vdash |
| LA-0364 | FG LA COMPLEX | FG LA LLC | 01/06/2020 | 2222 mm btu/h | GCP/CBF | 12.46 | | BACT | |
| MI-0439 | JACKSON GENERATING STATION | CONSUMERS ENERGY COMPANY | 04/02/2019 | 420 MW | Inlet Air Filters/GCP/CBF | 4.9 | | BACT | + |
| MI-0433 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 MMBTU/H | inlet air conditioning/CBF/GCP | | LB/H | BACT | |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 MMBTU/H | inlet air conditioning/CBF/GCP | 4.5 | | BACT | + |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 MMBTU/H | inlet air conditioning/CBF/GCP | 6.02 | | BACT | |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | 625 MW | GCP/CBF | | LB/MMBTU | BACT | |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 3421 MMBTU/H | inlet air conditioning/CBF/GCP | | LB/H | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | inlet air conditioning/CBF/GCP | 4.5 | | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | inlet air conditioning/CBF/GCP | 6.02 | | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 MMBTU/H | inlet air conditioning/CBF/GCP | 6.02 | | BACT | ++ |
| NJ-0088 | COGEN TECH LINDEN VENTURE LP | COGEN TECH LINDEN VENTURE LP | 07/30/2019 | 21042 MMCubic ft/yr | CBF | 11.58 | | BACT | +1 |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 MMCF/YR | GCP/CBF | | LB/MMBTU | BACT | +1 |
| 1.1 0552 | C.T.C.G.T.O.WINTT TOWER EEC | C. II C. II II I I I I I I I I I I I I I | 30/24/2013 | 33000 11111111 1111 | 00.700. | 0.0032 | 25, | DACI | |

(a) SCR = selective catalytic reduction, DLN = dry, low-NOx burners, WI = water injection, GCP = good combustion practices, CBF = clean burning fuels, OxCat = oxidation catalyst

Table D-1a Addendum: RBLC Tables for Combined Cycle Turbines (Natural Gas) UPDATED DATA: November 2018 to October 2021

| | | | | | | | Emission | | | Turbine |
|----------|------------------------------|--|-------------|---------------------------|-----------------------------|---|----------|--------------|------|---------|
| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls ^A | Limit | Units | Туре | Model |
| | | | | PM _{2.5} (filter | able only) | | | | | |
| *AL-0328 | PLANT BARRY | ALABAMA POWER COMPANY | 11/09/2020 | 744 | MW | | 0.004 | LB/MMBTU | BACT | |
| *TX-0908 | NEWMAN POWER STATION | EL PASO ELECTRIC COMPANY | 08/27/2021 | 230 | MW | GCP/CBF | 0 | | BACT | |
| *TX-0915 | UNIT 5 | NRG CEDAR BAYOU LLC | 03/17/2021 | 0 | | CBF | 0 | | BACT | |
| *TX-0915 | UNIT 5 | NRG CEDAR BAYOU LLC | 03/17/2021 | 14552539 | MMBTU/YR | CBF | 0 | | BACT | |
| | | | | Greenhouse | Gases - CO ₂ | | · | • | • | |
| *AL-0328 | PLANT BARRY | ALABAMA POWER COMPANY | 11/09/2020 | 744 | MW | Efficient Design | 1000 | LB/MWH | BACT | |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 | MMBTU/H | CBF/GCP/energy efficiency measures. | 1000 | LB/MW-H | BACT | |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 | MMBTU/H | CBF/GCP/energy efficiency measures. | 1000 | LB/MW-H | BACT | |
| | | | Gree | nhouse Gases | - CO ₂ Equivalen | ts | | | | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 576 | MMBtu/hr | GCP/CBF | 117.1 | LB/MMBTU | BACT | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 431 | MMBtu/hr | GCP/CBF | 117.1 | LB/MMBTU | BACT | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 386 | MMBtu/hr | GCP/CBF | 117.1 | LB/MMBTU | BACT | 1 |
| IL-0130 | JACKSON ENERGY CENTER | JACKSON GENERATION, LLC | 12/31/2018 | 3864 | mmBtu/hr | GCP | 4733910 | TONS/YEAR | BACT | 1 |
| LA-0364 | FG LA COMPLEX | FG LA LLC | 01/06/2020 | 2222 | mm btu/h | CBF/GCP/energy-efficient design options | 1096666 | TONS/YR | BACT | 1 |
| MI-0439 | JACKSON GENERATING STATION | CONSUMERS ENERGY COMPANY | 04/02/2019 | 420 | MW | CBF/GCP/energy efficiency measures | 1000257 | T/YR | BACT | |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 | MMBTU/H | CBF/GCP/energy efficiency measures | 430349 | T/YR | BACT | |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 667 | MMBTU/H | CBF/GCP/energy efficiency measures | 430349 | T/YR | BACT | |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | 625 | MW | Energy efficiency measures | 2739722 | T/YR | BACT | |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 3421 | MMBTU/H | GCP/CBF/Inlet Air Conditioning | 1911481 | T/YR | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 | MMBTU/H | CBF/GCP/energy efficiency measures | 430349 | T/YR | BACT | |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 667 | MMBTU/H | CBF/GCP/energy efficiency measures | 430349 | T/YR | BACT | |
| *TX-0908 | NEWMAN POWER STATION | EL PASO ELECTRIC COMPANY | 08/27/2021 | 230 | MW | GCP/CBF | 0 | | BACT | |
| *TX-0915 | UNIT 5 | NRG CEDAR BAYOU LLC | 03/17/2021 | 0 | | CBF | 0 | | BACT | |
| *TX-0915 | UNIT 5 | NRG CEDAR BAYOU LLC | 03/17/2021 | 14552539 | MMBTU/YR | CBF | 0 | | BACT | |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 | MMCF/YR | Energy efficient combustion practices/CBF | 812 | LB/CO2E/MW-H | BACT | |
| | | | | Sulfuric A | | _ | | | | |
| IL-0130 | JACKSON ENERGY CENTER | JACKSON GENERATION, LLC | 12/31/2018 | | mmBtu/hr | | | POUNDS/HOUR | BACT | |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | 625 | | CBF | | LB/MMBTU | BACT | |
| | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | | MMBTU/H | GCP/CBF | | LB/H | BACT | |
| NJ-0088 | COGEN TECH LINDEN VENTURE LP | COGEN TECH LINDEN VENTURE LP | 07/30/2019 | | MMCubic ft/yr | CBF | 3.45 | LB/H | BACT | |
| *TX-0908 | NEWMAN POWER STATION | EL PASO ELECTRIC COMPANY | 08/27/2021 | 230 | MW | GCP/CBF | 0 | | BACT | |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 | MMCF/YR | CBF | 0.0012 | LB/MMBTU | BACT | |
| | | | | Opa | | | | | | |
| MI-0439 | JACKSON GENERATING STATION | CONSUMERS ENERGY COMPANY | 04/02/2019 | 420 | MW | Inlet Air Filters/GCP/CBF | 10 | % | BACT | |

⁽a) SCR = selective catalytic reduction, DLN = dry, low-NOx burners, WI = water injection, GCP = good combustion practices, CBF = clean burning fuels, OxCat = oxidation catalyst

| | | | | | | | Emission | | | |
|----------|--------------------------------|--------------------------------|-------------|----------------|-----------|---|----------|----------------|------|-----------------------|
| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Limit | Units | Туре | Turbine Model |
| <u> </u> | <u> </u> | <u> </u> | | Nitroger | Oxides | | • | • | | • |
| | | | | | | WATER INJECTION AND SELECTIVE | | | | |
| T-0151 | KLEEN ENERGY SYSTEMS, LLC | KLEEN ENERGY SYSTEMS, LLC | 2/25/2008 | 15,119 | GAL/H | CATALYTIC REDUCTION | 48.4 | LB/H | LAER | SIEMENS SGT6-5000F |
| | | | | | | Selective catalytic Reduction Systems and | | | | |
| NJ-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 720 | H/YR | Dry Low NOx | 4 | PPMVD@15% O2 | LAER | GE 7HA.02 |
| | | | | | | Water injection and selective catalytic | | | | |
| IY-0104 | CPV VALLEY ENERGY CENTER | CPV VALLEY LLC | 8/1/2013 | - | | reduction. | 6 | PPMVD @ 15% O2 | LAER | F Class |
| | | | | Carbon N | 1onoxide | | | | | |
| Γ-0151 | KLEEN ENERGY SYSTEMS, LLC | KLEEN ENERGY SYSTEMS, LLC | 2/25/2008 | 2,117 | MMBtu/hr | OxCat | 1.8 | ppm | BACT | SIEMENS SGT6-5000F |
| T-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | 2,639 | MMBtu/hr | OxCat | 1.8 | ppm | BACT | Mitsubishi M501JAC |
| T-0157 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | 805 | MW | OxCat | 2 | ppm | BACT | GE 7HA.01 |
| T-0158 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | 805 | MW | OxCat | 2 | ppm | BACT | GE 7HA.01 |
| J-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | MW | OXCAT/GCP | 2 | ppm | BACT | GE 7HA.02 |
| Y-0104 | CPV VALLEY ENERGY CENTER | CPV VALLEY LLC | 8/1/2013 | 2,234 | MMBtu/hr | OXCAT/GCP | 2 | ppm | BACT | F class |
| A-0127 | PLANT MCDONOUGH COMBINED CYCLE | SOUTHERN COMPANY/GEORGIA POWER | 1/7/2008 | 254 | MW | OxCat | 9 | ppm | BACT | Mitsubishi MHI 501-GI |
| | | • | | Greenhou | ise Gases | | | | | |
| J-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | MW | Fuel | 888 | lb/MW-hr | BACT | GE 7HA.02 |
| | | | | Sulfuric A | | | | | | |
| T-0157 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | 805 | MW | Fuel | 2.31 | lb/hr | BACT | |
| T-0158 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | 805 | | Fuel | 2.31 | lb/hr | BACT | |
| J-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | MW | Fuel | 4.27 | lb/hr | BACT | GE 7HA.02 |
| T-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | 2,639 | MMBtu/hr | Fuel | 0.0005 | lb/MMBtu | BACT | |
| Y-0104 | CPV VALLEY ENERGY CENTER | CPV VALLEY LLC | 8/1/2013 | 2,234 | MMBtu/hr | Fuel | 0.0005 | lb/MMBtu | BACT | |
| | | | | Particulat | | | | | | |
| J-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | MW | Fuel | 34.3 | lb/hr | BACT | GE 7HA.02 |
| Y-0104 | CPV VALLEY ENERGY CENTER | CPV VALLEY LLC | 8/1/2013 | 2,234 | MMBtu/hr | Fuel | 0.0368 | lb/MMBtu | BACT | |
| | | | | PM | | | | | | |
| J-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | 663 | | Fuel | | lb/hr | BACT | GE 7HA.02 |
| T-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | | MMBtu/hr | | 0.0168 | lb/MMBtu | BACT | |
| T-0151 | KLEEN ENERGY SYSTEMS, LLC | KLEEN ENERGY SYSTEMS, LLC | 2/25/2008 | 2,117 | MMBtu/hr | None | 0.02692 | lb/MMBtu | BACT | SIEMENS SGT6-5000F |
| | | | | PM | | | | | | |
| | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | 805 | | None | 42.6 | | BACT | |
| J-0085 | MIDDLESEX ENERGY CENTER, LLC | STONEGATE POWER, LLC | 7/19/2016 | | MW | Fuel | | lb/hr | BACT | GE 7HA.02 |
| | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | | MMBtu/hr | GCP | | lb/MMBtu | BACT | |
| T-0157 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | 805 | MW | None | 42.6 | lb/hr | BACT | |
| | | | | Volatile Organ | | | | | | |
| T-0157 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | 805 | MW | OxCat | 2 | ppm | BACT | GE 7HA.01 |
| T-0158 | CPV TOWANTIC, LLC | CPV TOWANTIC, LLC | 11/30/2015 | 805 | MW | OxCat | 2 | ppm | BACT | GE 7HA.01 |
| T-0161 | KILLINGLY ENERGY CENTER | NTE CONNECTICUT, LLC | 6/30/2017 | | MMBtu/hr | | 2 | ppm | BACT | Mitsubishi M501JAC |
| T-0151 | KLEEN ENERGY SYSTEMS, LLC | KLEEN ENERGY SYSTEMS, LLC | 2/25/2008 | 2,117 | MMBtu/hr | OxCat | 3.6 | ppm | BACT | SIEMENS SGT6-5000F |

Table D-1b Addendum: RBLC Tables for Combined Cycle Turbines (Fuel Oil) UPDATED DATA: November 2018 to October 2021

| | | | | | | | Emission | | | Turbine |
|---------|------------------------------|------------------------------|-------------------|------------|----------|-----------|----------|-------|------|---------|
| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Limit | Units | Туре | Model |
| | | | Carbon I | Monoxide | | | | | | |
| NJ-0088 | COGEN TECH LINDEN VENTURE LP | COGEN TECH LINDEN VENTURE LP | 07/30/2019 | 14.78 | MMGAL/YR | OxCat/CBF | 18.4 | LB/H | BACT | |
| | | | PM ₁₀ | (total) | | | | | | |
| NJ-0088 | COGEN TECH LINDEN VENTURE LP | COGEN TECH LINDEN VENTURE LP | 07/30/2019 | 14.78 | MMGAL/YR | CBF | 49.17 | LB/H | BACT | |
| | | | PM _{2.5} | (total) | | | | | | |
| NJ-0088 | COGEN TECH LINDEN VENTURE LP | COGEN TECH LINDEN VENTURE LP | 07/30/2019 | 14.78 | MMGAL/YR | CBF | 49.17 | LB/H | BACT | |
| | | | Sulfuric | Acid Mist | | | | | | |
| NJ-0088 | COGEN TECH LINDEN VENTURE LP | COGEN TECH LINDEN VENTURE LP | 07/30/2019 | 14.78 | MMGAL/YR | CBF | 4.8 | LB/H | BACT | |

⁽a) SCR = selective catalytic reduction, DLN = dry, low-NOx burners, WI = water injection, GCP = good combustion practices, CBF = clean burning fuels, OxCat = oxidation catalyst

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре | Turbine Model |
|--------------------|--|--|------------------|------------|----------|-------------|-------------------|----------------------|-------|------------------------|
| | | Nitrogen | Oxides - Startup | /Shutdown | | | | • | • | • |
| | | | | | | | | | | SGT-8000H VERSION 1.4- |
| MD-0045 | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | MW | SCR/DLN | 23 | lb/event | BACT | OPTIMIZED |
| MI-0427 | FILER CITY STATION | FILER CITY STATION LIMITED PARTNERSHIP | 11/17/2017 | | MMBtu/hr | SCR/DLN | 32 | lb/event | BACT | |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | SCR | 40 | lb/event | BACT | |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | SCR | 40 | lb/event | BACT | |
| MI-0412 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | HOLLAND BOARD OF PUBLIC WORKS | 12/4/2013 | 647 | MMBtu/hr | SCR/DLN | 44 | lb/event | BACT | |
| MI-0424 | HOLLAND BOARD OF PUBLIC WORKS - EAST 5TH STREET | HOLLAND BOARD OF PUBLIC WORKS | 12/5/2016 | 554 | MMBtu/hr | SCR/DLN | 44 | lb/event | BACT | |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | SCR | 57 | lb/event | BACT | |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | SCR | 57 | lb/event | BACT | |
| CA-1212 | PALMDALE HYBRID POWER PROJECT | CITY OF PALMDALE | 10/18/2011 | 110 | MMBtu/hr | SCR/DLN | 57 | lb/event | BACT | |
| MD-0046 | KEYS ENERGY CENTER | KEYS ENERGY CENTER, LLC | 10/31/2014 | 235 | MW | SCR/DLN | 60 | lb/event | BACT | SGT6-500FEE |
| MD-0046 | KEYS ENERGY CENTER | KEYS ENERGY CENTER, LLC | 10/31/2014 | 235 | MW | SCR/DLN/GCP | 71 | lb/event | BACT | SGT6-500FEE |
| MD-0046 | KEYS ENERGY CENTER | KEYS ENERGY CENTER, LLC | 10/31/2014 | 235 | MW | SCR/DLN/GCP | 83 | lb/event | BACT | SGT6-500FEE |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | SCR | 96 | lb/event | BACT | |
| CA-1212 | PALMDALE HYBRID POWER PROJECT | CITY OF PALMDALE | 10/18/2011 | 154 | MW | SCR/DLN | | lb/event | BACT | |
| CA-1209 | HIGH DESERT POWER PROJECT | HIGH DESERT POWER PROJECT LLC | 3/11/2010 | 190 | | SCR/DLN | | lb/event | BACT | |
| OF CELOS | THE PERSON FOR THE PE | INOT BESENT FOWENT NOSECT EEC | 3/11/2010 | 150 | | 301,9211 | J. | 10,000.10 | 57.6. | SGT-8000H VERSION 1.4- |
| MD-0045 | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | MW | SCR/DLN/GCP | 105 | lb/event | BACT | OPTIMIZED |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | | SCR/DLN | | lb/event | BACT | OF THIVITZED |
| CA-1211 | COLOSA GENERATING STATION | PACIFIC GAS & ELECTRIC CONIPAINT | 3/11/2011 | 1/2 | IVIVV | 3CR/DLN | 115 | ib/event | BACI | SGT-8000H VERSION 1.4- |
| MD-0045 | MATTAWOMAN ENERGY CENTER | MAATTAMONAAN ENERGY LLC | 11/12/2015 | 200 | MW | CCD/DIN/CCD | 122 | Un /nn.ah | BACT | |
| | | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | | SCR/DLN/GCP | | lb/event | _ | OPTIMIZED |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | SCR | 142 | lb/event | BACT | |
| | | | | | | | | | | SGT-8000H VERSION 1.4- |
| | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | MW | SCR/DLN/GCP | | lb/event | BACT | OPTIMIZED |
| | MIDLAND COGENERATION VENTURE | MIDLAND COGENERATION VENTURE | 4/23/2013 | 2,237 | | SCR/DLN | | lb/event | BACT | |
| MD-0046 | KEYS ENERGY CENTER | KEYS ENERGY CENTER, LLC | 10/31/2014 | 235 | | SCR/DLN/GCP | 245 | | BACT | SGT6-500FEE |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | SCR/DLN | | lb/event | BACT | |
| IN-0158 | ST. JOSEPH ENEGRY CENTER, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 2,300 | MMBtu/hr | None | | lb/event | BACT | |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | SCR/DLN | 456 | lb/event | BACT | |
| OK-0129 | CHOUTEAU POWER PLANT | ASSOCIATED ELECTRIC COOPERATIVE INC | 1/23/2009 | 1,882 | MMBtu/hr | DLN | 568 | lb/event | BACT | SIEMENS V84.3A |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | SCR/DLN | 779 | lb/event | BACT | |
| CA-1209 | HIGH DESERT POWER PROJECT | HIGH DESERT POWER PROJECT LLC | 3/11/2010 | 190 | MW | SCR/DLN | 3,541 | lb/event | BACT | |
| | | Carbon M | onoxide - Startu | p/Shutdown | | | | | | |
| MD-0046 | KEYS ENERGY CENTER | KEYS ENERGY CENTER, LLC | 10/31/2014 | 235 | MW | OxCat/GCP | 60 | lb/event | BACT | SGT6-500FEE |
| | | | | | | | | | | SGT-8000H VERSION 1.4- |
| MD-0045 | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | MW | OxCat/GCP | 156 | lb/event | BACT | OPTIMIZED |
| CA-1209 | HIGH DESERT POWER PROJECT | HIGH DESERT POWER PROJECT LLC | 3/11/2010 | 190 | MW | OxCat | 183 | lb/event | BACT | |
| CA-1209 | HIGH DESERT POWER PROJECT | HIGH DESERT POWER PROJECT LLC | 3/11/2010 | 190 | MW | OxCat | | lb/event | BACT | |
| MD-0046 | KEYS ENERGY CENTER | KEYS ENERGY CENTER, LLC | 10/31/2014 | 235 | MW | OxCat/GCP | 269 | lb/event | BACT | SGT6-500FEE |
| MD-0046 | KEYS ENERGY CENTER | KEYS ENERGY CENTER, LLC | 10/31/2014 | 235 | MW | OxCat/GCP | | lb/event | BACT | SGT6-500FEE |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | OxCat | 329 | | BACT | |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | | OxCat | | lb/event | BACT | |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | | | OxCat | | lb/event | BACT | |
| CA-1212 | PALMDALE HYBRID POWER PROJECT | CITY OF PALMDALE | 10/18/2011 | 110 | MMBtu/hr | OxCat | 337 | lb/event | BACT | |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | OxCat | | lb/event | BACT | _ |
| CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2010 | 154 | MW | OxCat | | lb/event | BACT | |
| CA-1191 CA-1212 | PALMDALE HYBRID POWER PROJECT | CITY OF VICTORVILLE CITY OF PALMDALE | 10/18/2011 | | MW | OxCat | 410 | lb/event | BACT | 1 |
| CA-1212 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | | | OxCat | | lb/event | BACT | |
| A-1211 CA-1191 | VICTORVILLE 2 HYBRID POWER PROJECT | CITY OF VICTORVILLE | 3/11/2011 | 154 | | OxCat | 674 | | BACT | |
| CA-1191 CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2010 | 172 | MW | OxCat | 680 | lb/event lb/event | BACT | |
| | | | | | | | | | _ | + |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | OxCat | 791 | lb/event | BACT | CCTC F00F== |
| ИD-0046 | KEYS ENERGY CENTER | KEYS ENERGY CENTER, LLC | 10/31/2014 | 235 | MW | OxCat/GCP | 1,064 | lb/event | BACT | SGT6-500FEE |
| | | | 1 | | | | | l | 1 | SGT-8000H VERSION 1.4- |
| 1D-0045 | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | MW | OxCat/GCP | 1,216 | lb/event | BACT | OPTIMIZED |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | OxCat | 1,356 | lb/event | BACT | |
| | | | 1 | | | | | | 1 | SGT-8000H VERSION 1.4- |
| | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | MW | OxCat/GCP | 1,461 | lb/event | BACT | OPTIMIZED |
| | FILER CITY STATION | FILER CITY STATION LIMITED PARTNERSHIP | 11/17/2017 | 4 025 | MMBtu/hr | OxCat/GCP | 4.500 | lb/event | BACT | 1 |

| | | | | | | | Emission | | | |
|---|-------------------------------|-------------------------------------|--------------------|------------|----------|-----------|----------|----------|------|-------------------------------------|
| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Limit | Units | Type | Turbine Model |
| OK-0129 | CHOUTEAU POWER PLANT | ASSOCIATED ELECTRIC COOPERATIVE INC | 1/23/2009 | 1,882 | MMBtu/hr | GCP | 1,596 | lb/event | BACT | SIEMENS V84.3A |
| OK-0157 | CHOUTEAU POWER PLANT | ASSOCIATED ELECTRIC COOPERATIVE INC | 9/5/2013 | 182 | MMBtu/hr | None | 1,750 | lb/event | BACT | |
| MD-0045 | MATTAWOMAN ENERGY CENTER | MATTAWOMAN ENERGY, LLC | 11/13/2015 | 286 | MW | OxCat/GCP | 1.772 | lb/event | BACT | SGT-8000H VERSION 1.4- OPTIMIZED |
| | ST. JOSEPH ENEGRY CENTER, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | | MMBtu/hr | | | lb/event | BACT | |
| OK-0157 | CHOUTEAU POWER PLANT | ASSOCIATED ELECTRIC COOPERATIVE INC | 9/5/2013 | | MW | GCP | 4,500 | lb/event | BACT | |
| | <u> </u> | Particulate N | latter - Startu | p/Shutdown | | | | | | • |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | Fuel | 6.0 | lb/event | BACT | |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | Fuel | 12.8 | lb/event | BACT | |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | Fuel | 30.8 | lb/event | BACT | |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | Fuel | 48.8 | lb/event | BACT | |
| | | | -Startup/Shut | | | | | | | |
| | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | | MW | Fuel | | lb/event | BACT | |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | Fuel | 12.8 | lb/event | BACT | |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | Fuel | 30.8 | lb/event | BACT | |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | | MW | Fuel | 48.0 | lb/event | BACT | |
| | | Volatile Organic C | | | | | | | | |
| CA-1211 COLUSA GENERATING STATION PACIFIC GAS & ELECTRIC COMPANY 3/ | | | | | MW | None | | lb/event | BACT | |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | None | 38.0 | lb/event | BACT | |
| | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | | MW | None | | lb/event | BACT | |
| CA-1211 | COLUSA GENERATING STATION | PACIFIC GAS & ELECTRIC COMPANY | 3/11/2011 | 172 | MW | None | 106.7 | lb/event | BACT | |

Table D-1c Addendum: RBLC Tables for Combined Cycle Turbines (Startup/Shutdown) UPDATED DATA: November 2018 to October 2021

| | | | | | | | Emission | | | Turbine |
|---------|------------------------|------------------------|--------------------|------------|---------|-----------|----------|------------------|------|---------|
| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Limit | Units | Type | Model |
| | | N | litrogen Oxide | es | | | | | | |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 | MMCF/YR | DLN/SCR | 60 | LB/TURBINE/EVENT | BACT | |
| | | Ca | arbon Monoxi | de | | | | | | |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 | MMCF/YR | OxCat/GCP | 444 | LB/TURBINE/EVENT | BACT | |
| | | Volatile | Organic Com | pounds | | | | | | • |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 35000 | MMCF/YR | OxCat/GCP | 216 | LB/TURBINE/EVENT | BACT | |

⁽a) SCR = selective catalytic reduction, DLN = dry, low-NOx burners, WI = water injection, GCP = good combustion practices, CBF = clean burning fuels, OxCat = oxidation catalyst

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|---------|--|-------------|-------------|----------|------------------|-----------------------|----------|----------|
| | | Carl | on Monoxide | | | | • | |
| OK-0168 | Seminole Generating Station | 5/5/2015 | 40.4 | MMBtu/hr | GCP | 0.0075 | lb/MMBtu | BACT-PSD |
| IA-0107 | Marshalltown Generating Station | 4/14/2014 | 60.1 | MMBtu/hr | Ox Cat | 0.0164 | lb/MMBtu | BACT-PSD |
| MD-0040 | CPV St Charles | 11/12/2008 | 93 | MMBtu/hr | None | 0.0200 | lb/MMBtu | BACT-PSD |
| MD-0041 | CPV St. Charles | 4/23/2014 | 93 | MMBtu/hr | GCP | 0.0200 | lb/MMBtu | BACT-PSD |
| NJ-0080 | Hess Newark Energy Center | 11/1/2012 | 100 | MMBtu/hr | Clean Fuels | 0.0245 | lb/MMBtu | BACT-PSD |
| IN-0263 | Midwest Fertilizer Company LLC | 3/23/2017 | 218.6 | MMBtu/hr | GCP | 0.0354 | lb/MMBtu | BACT-PSD |
| IN-0173 | Midwest Fertilizer Corporation | 6/4/2014 | 218.6 | MMBtu/hr | GCP | 0.0354 | lb/MMBtu | BACT-PSD |
| IN-0180 | Midwest Fertilizer Corporation | 6/4/2014 | 218.6 | MMBtu/hr | GCP | 0.0354 | lb/MMBtu | BACT-PSD |
| IN-0179 | Ohio Valley Resources, LLC | 9/25/2013 | 218 | MMBtu/hr | GCP | 0.0354 | lb/MMBtu | BACT-PSD |
| OH-0354 | Kraton Polymers U.S. LLC | 1/15/2013 | 249 | MMBtu/hr | GCP, Clean fuels | 0.0360 | lb/MMBtu | BACT-PSD |
| WI-0259 | Manitowoc Public Utilities | 4/16/2012 | 33 | MMBtu/hr | None | 0.0360 | lb/MMBtu | BACT-PSD |
| NJ-0084 | PSEG Fossil LLC Sewaren Generating Station | 3/10/2016 | 80 | | GCP, Clean fuels | 0.0360 | lb/MMBtu | BACT-PSD |
| MI-0406 | Renaissance Power LLC | 11/1/2013 | | | GCP | | lb/MMBtu | BACT-PSD |
| AR-0121 | El Dorado Chemical Company | 11/18/2013 | 240 | MMBtu/hr | GCP | 0.0370 | lb/MMBtu | BACT-PSD |
| LA-0240 | Flopam Inc. | 6/14/2010 | 25.1 | MMBtu/hr | GCP | 0.0370 | lb/MMBtu | BACT-PSD |
| FL-0318 | Highlands Ethanol Facility | 12/10/2009 | | MMBtu/hr | None | | lb/MMBtu | BACT-PSD |
| LA-0314 | Indorama Lake Charles Facility | 8/3/2016 | 229 | MMBtu/hr | GCP | 0.0370 | lb/MMBtu | BACT-PSD |
| MD-0045 | Mattawoman Energy Center | 11/13/2015 | 42 | MMBtu/hr | GCP | 0.0370 | lb/MMBtu | BACT-PSD |
| | Olefins Plant | 8/8/2014 | | | GCP | | lb/MMBtu | BACT-PSD |
| GA-0127 | Plant Mcdonough Combined Cycle | 1/7/2008 | 200 | MMBtu/hr | None | | lb/MMBtu | BACT-PSD |
| | S R Bertron Electric Generating Station | 12/19/2014 | | MMBtu/hr | LNB | | lb/MMBtu | BACT-PSD |
| | Middlesex Energy Center, LLC | 7/19/2016 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD |
| | Cheyenne Prairie Generating Station | 7/16/2014 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| NY-0103 | Cricket Valley Energy Center | 2/3/2016 | 60 | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| | Woodbridge Energy Center | 7/25/2012 | | MMBtu/hr | GCP, Clean fuels | | lb/MMBtu | BACT-PSD |
| | Direct Reduction Iron Plant | 1/27/2011 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| | Direct Reduction Iron Plant | 1/27/2011 | | | GCP | | lb/MMBtu | BACT-PSD |
| | Suwannee Mill | 9/5/2012 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| | Filer City Station | 11/17/2017 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| | Indeck Niles, LLC | 1/4/2017 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| | Moundsville Combined Cycle Power Plant | 11/21/2014 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| | Mount Vernon Mill | 3/25/2010 | | MMBtu/hr | None | | lb/MMBtu | BACT-PSD |
| | Ponca City Refinery | 2/9/2009 | | MMBtu/hr | Ultra LNB, GCP | | lb/MMBtu | BACT-PSD |
| | Republic Steel | 7/18/2012 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| | Thyssenkrupp Stainless USA, LLC | 3/25/2010 | | MMBtu/hr | None | | lb/MMBtu | BACT-PSD |
| | Troutdale Energy Center, LLC | 3/5/2014 | | | LNB, FGR | | lb/MMBtu | BACT-PSD |
| | Ammonia Production Facility | 3/27/2013 | | | GCP | | lb/MMBtu | BACT-PSD |
| | Oregon Clean Energy Center | 6/18/2013 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| AR-0138 | Nucor Corporation - Nucor Steel, Arkansas | 2/17/2012 | 50.4 | MMBtu/hr | GCP | 0.0610 | lb/MMBtu | BACT-PSD |

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|---------|---|-------------|------------|----------|-----------------------------|-----------------------|----------|----------|
| SC-0112 | Nucor Steel - Berkeley | 5/5/2008 | 50.21 | MMBtu/hr | GCP, Clean fuels | 0.0610 | lb/MMBtu | BACT-PSD |
| NY-0104 | CPV Valley Energy Center | 8/1/2013 | 73.5 | MMBtu/hr | GCP | 0.0721 | lb/MMBtu | BACT-PSD |
| OK-0148 | Buffalo Creek Processing Plant | 9/12/2012 | 11.04 | MMBtu/hr | None | 0.0740 | lb/MMBtu | BACT-PSD |
| OH-0336 | Campbell Soup Company | 12/14/2010 | | | None | 0.0750 | lb/MMBtu | BACT-PSD |
| IA-0108 | Iowa State University Power Plant | 11/7/2013 | 213.6 | MMBtu/hr | None | 0.0750 | lb/MMBtu | BACT-PSD |
| MI-0410 | Thetford Generating Station | 7/25/2013 | 100 | MMBtu/hr | GCP | 0.0750 | lb/MMBtu | BACT-PSD |
| MI-0412 | Holland Board of Public Works - East 5th Street | 12/4/2013 | 55 | MMBtu/hr | GCP | 0.0770 | lb/MMBtu | BACT-PSD |
| MI-0424 | Holland Board of Public Works - East 5th Street | 12/5/2016 | 83.5 | MMBtu/hr | GCP | 0.0770 | lb/MMBtu | BACT-PSD |
| MI-0412 | Holland Board of Public Works - East 5th Street | 12/4/2013 | 95 | MMBtu/hr | GCP | 0.0770 | lb/MMBtu | BACT-PSD |
| AL-0307 | Alloys Plant | 10/9/2015 | 17.5 | MMBtu/hr | GCP | 0.0800 | lb/MMBtu | BACT-PSD |
| AL-0307 | Alloys Plant | 10/9/2015 | 24.59 | MMBtu/hr | GCP | 0.0800 | lb/MMBtu | BACT-PSD |
| MD-0046 | Keys Energy Center | 10/31/2014 | 93 | MMBtu/hr | GCP | 0.0800 | lb/MMBtu | BACT-PSD |
| FL-0356 | Okeechobee Clean Energy Center | 3/9/2016 | 99.8 | MMBtu/hr | GCP | 0.0800 | lb/MMBtu | BACT-PSD |
| OH-0323 | Titan Tire Corporation of Bryan | 6/5/2008 | 50.4 | MMBtu/hr | None | 0.0800 | lb/MMBtu | BACT-PSD |
| LA-0314 | Indorama Lake Charles Facility | 8/3/2016 | 248 | MMBtu/hr | GCP | 0.0820 | lb/MMBtu | BACT-PSD |
| AR-0140 | Big River Steel LLC | 9/18/2013 | 24.5 | MMBtu/hr | GCP, Clean fuels | 0.0824 | lb/MMBtu | BACT-PSD |
| AR-0140 | Big River Steel LLC | 9/18/2013 | 51.2 | MMBtu/hr | GCP, Clean fuels | 0.0824 | lb/MMBtu | BACT-PSD |
| AR-0140 | Big River Steel LLC | 9/18/2013 | 67 | MMBtu/hr | GCP, Clean fuels | 0.0824 | lb/MMBtu | BACT-PSD |
| OK-0135 | Pryor Plant Chemical | 2/23/2009 | 80 | MMBtu/hr | GCP | 0.0825 | lb/MMBtu | BACT-PSD |
| IN-0158 | St. Joseph Energy Center, LLC | 12/3/2012 | 80 | MMBtu/hr | GCP | 0.0830 | lb/MMBtu | BACT-PSD |
| OH-0315 | New Steel International, Inc., Haverhill | 5/6/2008 | 50.4 | MMBtu/hr | None | 0.0839 | lb/MMBtu | BACT-PSD |
| OH-0310 | American Municipal Power Generating Station | 10/8/2009 | 150 | MMBtu/hr | None | 0.0840 | lb/MMBtu | BACT-PSD |
| TX-0576 | Pipe Manufacturing Steel Mini Mill | 4/19/2010 | 40 | MMBtu/hr | GCP | 0.0842 | lb/MMBtu | BACT-PSD |
| CA-1192 | Avenal Energy Project | 6/21/2011 | 37.4 | MMBtu/hr | Ultra LNB, GCP, Clean fuels | 50.0000 | ppm | BACT-PSD |
| TX-0731 | Corpus Christi Terminal Condensate Splitter | 4/10/2015 | 129 | MMBtu/hr | GCP | 50.0000 | ppm | BACT-PSD |
| TX-0751 | Eagle Mountain Steam Electric Station | 6/18/2015 | 73.3 | MMBtu/hr | None | 50.0000 | ppm | BACT-PSD |
| AK-0083 | Kenai Nitrogen Operations | 1/6/2015 | 50 | MMBtu/hr | None | 50.0000 | ppm | BACT-PSD |
| AK-0083 | Kenai Nitrogen Operations | 1/6/2015 | 243 | MMBtu/hr | None | 50.0000 | ppm | BACT-PSD |
| CA-1212 | Palmdale Hybrid Power Project | 10/18/2011 | 40 | MMBtu/hr | None | 50.0000 | ppm | BACT-PSD |
| | Palmdale Hybrid Power Project | 10/18/2011 | 110 | MMBtu/hr | None | 50.0000 | ppm | BACT-PSD |
| TX-0772 | Port of Beaumont Petroleum Transload Terminal (PBPTT) | 11/6/2015 | 13.2 | MMBtu/hr | GCP | 50.0000 | ppm | BACT-PSD |
| TX-0772 | Port of Beaumont Petroleum Transload Terminal (PBPTT) | 11/6/2015 | 40 | MMBtu/hr | GCP | 50.0000 | ppm | BACT-PSD |
| TX-0772 | Port of Beaumont Petroleum Transload Terminal (PBPTT) | 11/6/2015 | | | GCP | | ppm | BACT-PSD |
| CA-1191 | Victorville 2 Hybrid Power Project | 3/11/2010 | | | None | | ppm | BACT-PSD |
| CA-1191 | Victorville 2 Hybrid Power Project | 3/11/2010 | | | None | 50.0000 | ppm | BACT-PSD |
| TX-0708 | La Paloma Energy Center | 2/7/2013 | 150 | MMBtu/hr | GCP | 75.0000 | ppm | BACT-PSD |

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|---------|---|---------------|---------------|--------------|------------------|-----------------------|----------|----------|
| | | Greenhouse | Gases - Carbo | n Dioxide | | | | |
| IN-0263 | Midwest Fertilizer Company LLC | 3/23/2017 | 218.6 | MMBtu/hr | GCP | 0.0568 | lb/MMBtu | BACT-PSD |
| IN-0173 | Midwest Fertilizer Corporation | 6/4/2014 | 218.6 | MMBtu/hr | GCP | 116.8824 | lb/MMBtu | BACT-PSD |
| IN-0180 | Midwest Fertilizer Corporation | 6/4/2014 | 218.6 | MMBtu/hr | GCP | 116.8824 | lb/MMBtu | BACT-PSD |
| AR-0140 | Big River Steel LLC | 9/18/2013 | 24.5 | MMBtu/hr | GCP | 117.0000 | lb/MMBtu | BACT-PSD |
| AR-0140 | Big River Steel LLC | 9/18/2013 | 51.2 | MMBtu/hr | GCP | 117.0000 | lb/MMBtu | BACT-PSD |
| AR-0121 | El Dorado Chemical Company | 11/18/2013 | 240 | MMBtu/hr | GCP | 117.0000 | lb/MMBtu | BACT-PSD |
| NY-0116 | Fab 8, Luther Forest Technology Campus | 3/29/2013 | | | GCP, Clean fuels | 118.0000 | lb/MMBtu | BACT-PSD |
| NY-0116 | Fab 8, Luther Forest Technology Campus | 3/29/2013 | | | GCP, Clean fuels | 160.0000 | lb/MMBtu | BACT-PSD |
| IN-0179 | Ohio Valley Resources, LLC | 9/25/2013 | 218 | MMBtu/hr | GCP | 546.8807 | lb/MMBtu | BACT-PSD |
| | Gree | enhouse Gases | - Carbon Diox | ide Equivale | nts | | | |
| KS-0029 | The Empire District Electric Company | 7/14/2015 | 18.6 | MMBtu/hr | None | 116.8741 | lb/MMBtu | BACT-PSD |
| AR-0140 | Big River Steel LLC | 9/18/2013 | 67 | MMBtu/hr | GCP | 117.0000 | lb/MMBtu | BACT-PSD |
| OK-0148 | Buffalo Creek Processing Plant | 9/12/2012 | 11.04 | MMBtu/hr | None | 117.0000 | lb/MMBtu | BACT-PSD |
| OR-0050 | Troutdale Energy Center, LLC | 3/5/2014 | 39.8 | MMBtu/hr | Clean Fuels | 117.0000 | lb/MMBtu | BACT-PSD |
| OR-0050 | Troutdale Energy Center, LLC | 3/5/2014 | 39.8 | MMBtu/hr | Clean Fuels | 117.0000 | lb/MMBtu | BACT-PSD |
| TX-0814 | Ammonia And Urea Plant | 1/5/2017 | 240 | MMBtu/hr | GCP | 117.0653 | lb/MMBtu | BACT-PSD |
| MI-0427 | Filer City Station | 11/17/2017 | 182 | MMBtu/hr | GCP | 117.0982 | lb/MMBtu | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | 1/4/2017 | 182 | MMBtu/hr | GCP, Clean fuels | 117.0982 | lb/MMBtu | BACT-PSD |
| WY-0075 | Cheyenne Prairie Generating Station | 7/16/2014 | 25.06 | MMBtu/hr | GCP | 117.1162 | lb/MMBtu | BACT-PSD |
| AR-0121 | El Dorado Chemical Company | 11/18/2013 | 240 | MMBtu/hr | GCP | 117.4001 | lb/MMBtu | BACT-PSD |
| MI-0424 | Holland Board of Public Works - East 5th Street | 12/5/2016 | 83.5 | MMBtu/hr | GCP | 118.3469 | lb/MMBtu | BACT-PSD |
| MI-0412 | Holland Board of Public Works - East 5th Street | 12/4/2013 | 95 | MMBtu/hr | GCP | 118.3634 | lb/MMBtu | BACT-PSD |
| MI-0412 | Holland Board of Public Works - East 5th Street | 12/4/2013 | 55 | MMBtu/hr | GCP | 118.3645 | lb/MMBtu | BACT-PSD |
| TX-0772 | Port of Beaumont Petroleum Transload Terminal (PBPTT) | 11/6/2015 | 13.2 | MMBtu/hr | GCP | 118.4793 | lb/MMBtu | BACT-PSD |
| TX-0772 | Port of Beaumont Petroleum Transload Terminal (PBPTT) | 11/6/2015 | 40 | MMBtu/hr | GCP | 118.4817 | lb/MMBtu | BACT-PSD |
| NY-0103 | Cricket Valley Energy Center | 2/3/2016 | 60 | MMBtu/hr | GCP, Clean fuels | 119.0000 | lb/MMBtu | BACT-PSD |
| MA-0039 | Salem Harbor Station Redevelopment | 1/30/2014 | 80 | MMBtu/hr | None | 119.0000 | lb/MMBtu | BACT-PSD |
| TX-0812 | Crude Oil Processing Facility | 10/31/2016 | 104 | MMBtu/hr | GCP | 120.3021 | lb/MMBtu | BACT-PSD |
| WV-0025 | Moundsville Combined Cycle Power Plant | 11/21/2014 | 100 | MMBtu/hr | Clean Fuels | 120.8100 | lb/MMBtu | BACT-PSD |
| IA-0108 | Iowa State University Power Plant | 11/7/2013 | 213.6 | MMBtu/hr | None | 121.3723 | lb/MMBtu | BACT-PSD |
| AK-0083 | Kenai Nitrogen Operations | 1/6/2015 | 243 | MMBtu/hr | None | 490.6173 | lb/MMBtu | BACT-PSD |
| AK-0083 | Kenai Nitrogen Operations | 1/6/2015 | 50 | MMBtu/hr | None | 2,384.4000 | lb/MMBtu | BACT-PSD |

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|---------|---|-------------|-----------------|----------|-----------------------------|-----------------------|----------|----------|
| | · | | furic Acid Mist | | • | | | |
| IA-0107 | Marshalltown Generating Station | 4/14/2014 | 60.1 | MMBtu/hr | None | 0.0001 | lb/MMBtu | BACT-PSD |
| MD-0040 | CPV St Charles | 11/12/2008 | 93 | MMBtu/hr | None | 0.0001 | lb/MMBtu | BACT-PSD |
| OH-0352 | Oregon Clean Energy Center | 6/18/2013 | 99 | MMBtu/hr | Clean Fuels | 0.0001 | lb/MMBtu | BACT-PSD |
| NJ-0085 | Middlesex Energy Center, LLC | 7/19/2016 | 97.5 | MMBtu/hr | Clean Fuels | 0.0001 | lb/MMBtu | BACT-PSD |
| NY-0103 | Cricket Valley Energy Center | 2/3/2016 | 60 | MMBtu/hr | Clean Fuels | 0.0001 | lb/MMBtu | BACT-PSD |
| NY-0104 | CPV Valley Energy Center | 8/1/2013 | 73.5 | MMBtu/hr | Clean Fuels | 0.0002 | lb/MMBtu | BACT-PSD |
| NJ-0084 | PSEG Fossil LLC Sewaren Generating Station | 3/10/2016 | 80 | MMBtu/hr | Clean Fuels | 0.0003 | lb/MMBtu | BACT-PSD |
| MA-0039 | Salem Harbor Station Redevelopment | 1/30/2014 | 80 | MMBtu/hr | None | 0.0009 | lb/MMBtu | BACT-PSD |
| MD-0045 | Mattawoman Energy Center | 11/13/2015 | 42 | MMBtu/hr | GCP, Clean fuels | 0.0040 | lb/MMBtu | BACT-PSD |
| | | Nit | rogen Dioxide | | | | | |
| LA-0248 | Direct Reduction Iron Plant | 1/27/2011 | 201 | MMBtu/hr | SCR, LNB | | lb/MMBtu | BACT-PSD |
| LA-0248 | Direct Reduction Iron Plant | 1/27/2011 | 201 | MMBtu/hr | SCR, LNB | 0.0032 | lb/MMBtu | BACT-PSD |
| TX-0731 | Corpus Christi Terminal Condensate Splitter | 4/10/2015 | | | SCR | 0.0060 | lb/MMBtu | BACT-PSD |
| CA-1206 | Stockton Cogen Company | 9/16/2011 | 178 | MMBtu/hr | None | 0.0085 | lb/MMBtu | BACT-PSD |
| AK-0083 | Kenai Nitrogen Operations | 1/6/2015 | 243 | MMBtu/hr | Ultra LNB | 0.0100 | lb/MMBtu | BACT-PSD |
| MD-0046 | Keys Energy Center | 10/31/2014 | 93 | MMBtu/hr | Ultra LNB, GCP, Clean fuels | 0.0100 | lb/MMBtu | BACT-PSD |
| MD-0045 | Mattawoman Energy Center | 11/13/2015 | 42 | MMBtu/hr | Ultra LNB, GCP, Clean fuels | 0.0100 | lb/MMBtu | BACT-PSD |
| TX-0681 | Olefins Plant | 8/8/2014 | | | SCR, LNG, FGR | 0.0100 | lb/MMBtu | BACT-PSD |
| NV-0049 | Harrah's Operating Company, Inc. | 8/20/2009 | 24 | MMBtu/hr | LNB | 0.0108 | lb/MMBtu | BACT-PSD |
| MD-0040 | CPV St Charles | 11/12/2008 | 93 | MMBtu/hr | LNB, FGR | 0.0110 | lb/MMBtu | BACT-PSD |
| TX-0772 | Port of Beaumont Petroleum Transload Terminal (PBPTT) | 11/6/2015 | 95.7 | MMBtu/hr | LNB, FGR | 0.0110 | lb/MMBtu | BACT-PSD |
| IA-0107 | Marshalltown Generating Station | 4/14/2014 | 60.1 | MMBtu/hr | None | 0.0130 | lb/MMBtu | BACT-PSD |
| LA-0305 | Lake Charles Methanol Facility | 6/30/2016 | 225 | MMBtu/hr | SCR | 0.0150 | lb/MMBtu | BACT-PSD |
| WY-0075 | Cheyenne Prairie Generating Station | 7/16/2014 | 25.06 | MMBtu/hr | Ultra LNB, FGR | 0.0175 | lb/MMBtu | BACT-PSD |
| AR-0121 | El Dorado Chemical Company | 11/18/2013 | 240 | MMBtu/hr | LNB, FGR | 0.0180 | lb/MMBtu | BACT-PSD |
| MI-0389 | Karn Weadock Generating Complex | 12/29/2009 | 220 | MMBtu/hr | LNB | 0.0180 | lb/MMBtu | BACT-PSD |
| IN-0263 | Midwest Fertilizer Company LLC | 3/23/2017 | 218.6 | MMBtu/hr | LNB, FGR, GCP | 0.0194 | lb/MMBtu | BACT-PSD |
| IN-0173 | Midwest Fertilizer Corporation | 6/4/2014 | 218.6 | MMBtu/hr | LNB, FGR | 0.0194 | lb/MMBtu | BACT-PSD |
| IN-0180 | Midwest Fertilizer Corporation | 6/4/2014 | 218.6 | MMBtu/hr | LNB, FGR | 0.0194 | lb/MMBtu | BACT-PSD |
| IN-0179 | Ohio Valley Resources, LLC | 9/25/2013 | 218 | MMBtu/hr | Ultra LNB, FGR | 0.0194 | lb/MMBtu | BACT-PSD |
| | La Paloma Energy Center | 2/7/2013 | 150 | MMBtu/hr | LNB | | lb/MMBtu | BACT-PSD |
| WV-0025 | Moundsville Combined Cycle Power Plant | 11/21/2014 | 100 | MMBtu/hr | Ultra LNB, FGR, GCP | 0.0200 | lb/MMBtu | BACT-PSD |
| OH-0352 | Oregon Clean Energy Center | 6/18/2013 | 99 | MMBtu/hr | LNB, FGR | 0.0200 | lb/MMBtu | BACT-PSD |
| NV-0049 | Harrah's Operating Company, Inc. | 8/20/2009 | 16.8 | MMBtu/hr | LNB, FGR | 0.0300 | lb/MMBtu | BACT-PSD |
| NV-0049 | Harrah's Operating Company, Inc. | 8/20/2009 | 31.38 | MMBtu/hr | LNB | 0.0306 | lb/MMBtu | BACT-PSD |
| IN-0158 | St. Joseph Energy Center, LLC | 12/3/2012 | | | LNB, FGR | 0.0320 | lb/MMBtu | BACT-PSD |
| AR-0140 | Big River Steel LLC | 9/18/2013 | | | LNB, Clean Fuels, GCP | 0.0350 | lb/MMBtu | BACT-PSD |
| AR-0140 | Big River Steel LLC | 9/18/2013 | 67 | MMBtu/hr | LNB, Clean Fuels, GCP | 0.0350 | lb/MMBtu | BACT-PSD |

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|---------|---|-------------|------------|----------|-----------------------------|-----------------------|----------|----------|
| AR-0140 | Big River Steel LLC | 9/18/2013 | 51.2 | MMBtu/hr | LNB, GCP, Clean fuels | 0.0350 | lb/MMBtu | BACT-PSD |
| NV-0049 | Harrah's Operating Company, Inc. | 8/20/2009 | 35.4 | MMBtu/hr | LNB | 0.0350 | lb/MMBtu | BACT-PSD |
| AL-0286 | Mount Vernon Mill | 3/25/2010 | 70 | MMBtu/hr | LNB, FGR | 0.0350 | lb/MMBtu | BACT-PSD |
| SC-0112 | Nucor Steel - Berkeley | 5/5/2008 | 50.21 | MMBtu/hr | Ultra LNB | 0.0350 | lb/MMBtu | BACT-PSD |
| MI-0406 | Renaissance Power LLC | 11/1/2013 | 40 | MMBtu/hr | GCP | 0.0350 | lb/MMBtu | BACT-PSD |
| AL-0300 | Thyssenkrupp Stainless USA, LLC | 3/25/2010 | 28.6 | MMBtu/hr | LNB, FGR | 0.0350 | lb/MMBtu | BACT-PSD |
| OR-0050 | Troutdale Energy Center, LLC | 3/5/2014 | 39.8 | MMBtu/hr | LNB, FGR | 0.0350 | lb/MMBtu | BACT-PSD |
| MI-0393 | Ray Compressor Station | 10/14/2010 | 12.25 | MMBtu/hr | LNB | 0.0351 | lb/MMBtu | BACT-PSD |
| NV-0049 | Harrah's Operating Company, Inc. | 8/20/2009 | 14.34 | MMBtu/hr | LNB, FGR | 0.0353 | lb/MMBtu | BACT-PSD |
| SC-0116 | Cytec Carbon Fibers, LLC | 4/30/2008 | 50 | MMBtu/hr | None | 0.0360 | lb/MMBtu | BACT-PSD |
| OK-0137 | Ponca City Refinery | 2/9/2009 | 95 | MMBtu/hr | Ultra LNB | 0.0360 | lb/MMBtu | BACT-PSD |
| TX-0772 | Port of Beaumont Petroleum Transload Terminal (PBPTT) | 11/6/2015 | | MMBtu/hr | LNB | | lb/MMBtu | BACT-PSD |
| TX-0714 | S R Bertron Electric Generating Station | 12/19/2014 | 80 | MMBtu/hr | LNB | 0.0360 | lb/MMBtu | BACT-PSD |
| FL-0335 | Suwannee Mill | 9/5/2012 | | | LNB, FGR | 0.0360 | lb/MMBtu | BACT-PSD |
| AL-0307 | Alloys Plant | 10/9/2015 | 17.5 | MMBtu/hr | LNB, FGR, GCP | 0.0366 | lb/MMBtu | BACT-PSD |
| NV-0049 | Harrah's Operating Company, Inc. | 8/20/2009 | 21 | MMBtu/hr | LNB | 0.0366 | lb/MMBtu | BACT-PSD |
| AL-0307 | Alloys Plant | 10/9/2015 | 24.59 | MMBtu/hr | LNB, FGR, GCP | 0.0366 | lb/MMBtu | BACT-PSD |
| NV-0049 | Harrah's Operating Company, Inc. | 8/20/2009 | 33.48 | MMBtu/hr | LNB | 0.0367 | lb/MMBtu | BACT-PSD |
| MI-0427 | Filer City Station | 11/17/2017 | 182 | MMBtu/hr | LNB, FGR | 0.0400 | lb/MMBtu | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | 1/4/2017 | 182 | MMBtu/hr | LNB, FGR, GCP | 0.0400 | lb/MMBtu | BACT-PSD |
| LA-0295 | Westlake Facility | 7/12/2016 | 63 | MMBtu/hr | GCP, FGR | 0.0437 | lb/MMBtu | BACT-PSD |
| OK-0148 | Buffalo Creek Processing Plant | 9/12/2012 | 11.04 | MMBtu/hr | LNB | 0.0450 | lb/MMBtu | BACT-PSD |
| OH-0323 | Titan Tire Corporation of Bryan | 6/5/2008 | 50.4 | MMBtu/hr | None | 0.0476 | lb/MMBtu | BACT-PSD |
| NV-0049 | Harrah's Operating Company, Inc. | 8/20/2009 | 16.7 | MMBtu/hr | LNB | 0.0490 | lb/MMBtu | BACT-PSD |
| OR-0048 | Carty Plant | 12/29/2010 | 91 | MMBtu/hr | LNB | 0.0495 | lb/MMBtu | BACT-PSD |
| LA-0272 | Ammonia Production Facility | 3/27/2013 | 217.5 | MMBtu/hr | LNG, FGR, GCP | 0.0500 | lb/MMBtu | BACT-PSD |
| MI-0412 | Holland Board of Public Works - East 5th Street | 12/4/2013 | 95 | MMBtu/hr | LNB, FGR, GCP | 0.0500 | lb/MMBtu | BACT-PSD |
| MI-0424 | Holland Board of Public Works - East 5th Street | 12/5/2016 | 83.5 | MMBtu/hr | LNB, FGR, GCP | 0.0500 | lb/MMBtu | BACT-PSD |
| MI-0412 | Holland Board of Public Works - East 5th Street | 12/4/2013 | 55 | MMBtu/hr | LNB, GCP | 0.0500 | lb/MMBtu | BACT-PSD |
| OH-0315 | New Steel International, Inc., Haverhill | 5/6/2008 | 50.4 | MMBtu/hr | LNB | 0.0500 | lb/MMBtu | BACT-PSD |
| FL-0356 | Okeechobee Clean Energy Center | 3/9/2016 | 99.8 | MMBtu/hr | LNB | 0.0500 | lb/MMBtu | BACT-PSD |
| MI-0410 | Thetford Generating Station | 7/25/2013 | 100 | MMBtu/hr | LNB, FGR | 0.0500 | lb/MMBtu | BACT-PSD |
| LA-0314 | Indorama Lake Charles Facility | 8/3/2016 | 229 | MMBtu/hr | Ultra LNB, GCP, Clean fuels | 0.0600 | lb/MMBtu | BACT-PSD |
| | Indorama Lake Charles Facility | 8/3/2016 | 248 | MMBtu/hr | Ultra LNB, GCP, Clean fuels | 0.0600 | lb/MMBtu | BACT-PSD |
| OK-0129 | Chouteau Power Plant | 1/23/2009 | 33.5 | MMBtu/hr | LNB | 0.0700 | lb/MMBtu | BACT-PSD |
| TX-0576 | Pipe Manufacturing Steel Mini Mill | 4/19/2010 | 40 | MMBtu/hr | GCP | 0.1000 | lb/MMBtu | BACT-PSD |
| TX-0772 | Port of Beaumont Petroleum Transload Terminal (PBPTT) | 11/6/2015 | 13.2 | MMBtu/hr | None | 0.1000 | lb/MMBtu | BACT-PSD |
| TX-0732 | Waste Heat Boiler No. 36 | 6/5/2015 | 100 | MMBtu/hr | GCP | 0.1100 | lb/MMBtu | BACT-PSD |

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|---------|---|-------------|---------------|----------|-----------------------------|-----------------------|-----------|----------|
| OH-0310 | American Municipal Power Generating Station | 10/8/2009 | 150 | MMBtu/hr | None | 0.1333 | lb/MMBtu | BACT-PSD |
| OK-0135 | Pryor Plant Chemical | 2/23/2009 | 80 | MMBtu/hr | LNB, GCP | 0.2000 | lb/MMBtu | BACT-PSD |
| AL-0249 | Evonik Degussa Corporation | 1/7/2010 | 212.6 | MMBtu/hr | SNCR | 0.2780 | lb/MMBtu | BACT-PSD |
| SC-0122 | Cytec Carbon Fibers, LLC | 4/30/2008 | 50 | MMBtu/hr | None | 0.3600 | lb/MMBtu | BACT-PSD |
| AK-0083 | Kenai Nitrogen Operations | 1/6/2015 | 50 | MMBtu/hr | SCR | 7.0000 | ppm | BACT-PSD |
| CA-1192 | Avenal Energy Project | 6/21/2011 | 37.4 | MMBtu/hr | Ultra LNB, GCP, Clean fuels | 9.0000 | ppm | BACT-PSD |
| CA-1212 | Palmdale Hybrid Power Project | 10/18/2011 | 40 | MMBtu/hr | None | 9.0000 | ppm | BACT-PSD |
| CA-1212 | Palmdale Hybrid Power Project | 10/18/2011 | 110 | MMBtu/hr | None | 9.0000 | ppm | BACT-PSD |
| TX-0713 | Tenaska Brownsville Generating Station | 4/29/2014 | 90 | MMBtu/hr | Ultra LNB | 9.0000 | ppm | BACT-PSD |
| TX-0712 | Trinidad Generating Facility | 11/20/2014 | | MMBtu/hr | Ultra LNB | 9.0000 | ppm | BACT-PSD |
| CA-1191 | Victorville 2 Hybrid Power Project | 3/11/2010 | 40 | MMBtu/hr | None | 9.0000 | ppm | BACT-PSD |
| CA-1191 | Victorville 2 Hybrid Power Project | 3/11/2010 | 35 | MMBtu/hr | None | 9.0000 | ppm | BACT-PSD |
| | Volkswagen Group of America, Chattanooga Operations | | | | | | | |
| TN-0160 | Volkowagen Group of America, chattanooga operations | 10/10/2008 | | MMBtu/hr | LNB, FGR | 30.0000 | ppm | BACT-PSD |
| | | | iculate Matte | | _ | | • | |
| | Okeechobee Clean Energy Center | 3/9/2016 | | | Clean Fuels | 10.0000 | % opacity | BACT-PSD |
| | Victorville 2 Hybrid Power Project | 3/11/2010 | | · | Clean Fuels | 0.2000 | gr/100 cf | BACT-PSD |
| | Victorville 2 Hybrid Power Project | 3/11/2010 | | | Clean Fuels | | gr/100 cf | BACT-PSD |
| | Avenal Energy Project | 6/21/2011 | | | | | gr/100 cf | BACT-PSD |
| | Suwannee Mill | 9/5/2012 | | MMBtu/hr | GCP | 2.0000 | gr/100 cf | BACT-PSD |
| | Big River Steel LLC | 9/18/2013 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD |
| | Big River Steel LLC | 9/18/2013 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD |
| | Big River Steel LLC | 9/18/2013 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD |
| - | Holland Board of Public Works - East 5th Street | 12/4/2013 | | | GCP | | lb/MMBtu | BACT-PSD |
| | Holland Board of Public Works - East 5th Street | 12/4/2013 | | | GCP | | lb/MMBtu | BACT-PSD |
| | | 12/5/2016 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| | Thetford Generating Station | 7/25/2013 | | MMBtu/hr | GCP, Clean fuels | | lb/MMBtu | BACT-PSD |
| | Midwest Fertilizer Company LLC | 3/23/2017 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| | Midwest Fertilizer Corporation | 6/4/2014 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| | Midwest Fertilizer Corporation | 6/4/2014 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| | Ohio Valley Resources, LLC | 9/25/2013 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| | Middlesex Energy Center, LLC | 7/19/2016 | | | Clean Fuels | | lb/MMBtu | BACT-PSD |
| | Mattawoman Energy Center | 11/13/2015 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD |
| | PSEG Fossil LLC Sewaren Generating Station | 3/10/2016 | | | Clean Fuels | | lb/MMBtu | BACT-PSD |
| - | CPV St Charles | 11/12/2008 | | MMBtu/hr | None | | lb/MMBtu | BACT-PSD |
| | CPV St. Charles | 4/23/2014 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD |
| | Cricket Valley Energy Center | 2/3/2016 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD |
| | Filer City Station | 11/17/2017 | | | GCP | | lb/MMBtu | BACT-PSD |
| | Flopam Inc. | 6/14/2010 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | 1/4/2017 | 182 | MMBtu/hr | GCP | 0.0050 | lb/MMBtu | BACT-PSD |

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре | | |
|---------|---|-------------|------------|----------|------------------|-----------------------|-----------|----------|--|--|
| MI-0406 | Renaissance Power LLC | 11/1/2013 | 40 | MMBtu/hr | GCP | 0.0050 | lb/MMBtu | BACT-PSD | | |
| KS-0029 | The Empire District Electric Company | 7/14/2015 | 18.6 | MMBtu/hr | None | 0.0050 | lb/MMBtu | BACT-PSD | | |
| NY-0104 | CPV Valley Energy Center | 8/1/2013 | 73.5 | MMBtu/hr | Clean Fuels | 0.0063 | lb/MMBtu | BACT-PSD | | |
| NY-0112 | Westrock-Solvay LLC | 11/2/2012 | | | LNB, GCP | 0.0070 | lb/MMBtu | BACT-PSD | | |
| CA-1212 | Palmdale Hybrid Power Project | 10/18/2011 | 110 | MMBtu/hr | Clean Fuels | 0.0073 | lb/MMBtu | BACT-PSD | | |
| AK-0083 | Kenai Nitrogen Operations | 1/6/2015 | 50 | MMBtu/hr | None | 0.0074 | lb/MMBtu | BACT-PSD | | |
| AK-0083 | Kenai Nitrogen Operations | 1/6/2015 | 243 | MMBtu/hr | None | 0.0074 | lb/MMBtu | BACT-PSD | | |
| AL-0249 | Evonik Degussa Corporation | 1/7/2010 | 212.6 | MMBtu/hr | GCP | 0.0074 | lb/MMBtu | BACT-PSD | | |
| MD-0046 | Keys Energy Center | 10/31/2014 | 93 | MMBtu/hr | GCP, Clean fuels | 0.0075 | lb/MMBtu | BACT-PSD | | |
| CA-1212 | Palmdale Hybrid Power Project | 10/18/2011 | | MMBtu/hr | Clean Fuels | 0.0075 | lb/MMBtu | BACT-PSD | | |
| OK-0135 | Pryor Plant Chemical | 2/23/2009 | 80 | MMBtu/hr | None | 0.0075 | lb/MMBtu | BACT-PSD | | |
| IN-0158 | St. Joseph Energy Center, LLC | 12/3/2012 | 80 | MMBtu/hr | GCP, Clean fuels | | lb/MMBtu | BACT-PSD | | |
| | Thyssenkrupp Stainless USA, LLC | 3/25/2010 | 28.6 | MMBtu/hr | None | | lb/MMBtu | BACT-PSD | | |
| | New Steel International, Inc., Haverhill | 5/6/2008 | | MMBtu/hr | Clean Fuels | | lb/MMBtu | BACT-PSD | | |
| IA-0107 | Marshalltown Generating Station | 4/14/2014 | 60.1 | MMBtu/hr | None | 0.0080 | lb/MMBtu | BACT-PSD | | |
| | Cheyenne Prairie Generating Station | 7/16/2014 | | MMBtu/hr | GCP | 0.0175 | lb/MMBtu | BACT-PSD | | |
| MO-0079 | American Energy Producers, Inc. | 1/25/2008 | | MMBtu/hr | None | | lb/MMBtu | BACT-PSD | | |
| MO-0081 | American Energy Producers, Inc. | 1/22/2009 | | MMBtu/hr | None | 0.0236 | lb/MMBtu | BACT-PSD | | |
| | PM10- Filterable | | | | | | | | | |
| | Carty Plant | 12/29/2010 | | MMBtu/hr | Clean Fuels | | lb/MMBtu | BACT-PSD | | |
| | Hess Newark Energy Center | 11/1/2012 | | MMBtu/hr | Clean Fuels | | lb/MMBtu | BACT-PSD | | |
| | CPV St Charles | 11/12/2008 | | | None | | lb/MMBtu | BACT-PSD | | |
| | Highlands Ethanol Facility | 12/10/2009 | | | Fabric Filter* | | lb/MMBtu | BACT-PSD | | |
| | American Municipal Power Generating Station | 10/8/2009 | | | None | | lb/MMBtu | BACT-PSD | | |
| | Evonik Degussa Corporation | 1/7/2010 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD | | |
| | St. Joseph Energy Center, LLC | 12/3/2012 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD | | |
| | Harrah's Operating Company, Inc. | 8/20/2009 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD | | |
| | Nucor Steel - Berkeley | 5/5/2008 | | | GCP | | lb/MMBtu | BACT-PSD | | |
| | Direct Reduction Iron Plant | 1/27/2011 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD | | |
| LA-0248 | Direct Reduction Iron Plant | 1/27/2011 | | MMBtu/hr | GCP | 0.0118 | lb/MMBtu | BACT-PSD | | |
| | | | M10- Total | 1 | | | ı | | | |
| | Avenal Energy Project | 6/21/2011 | | | Clean Fuels | | gr/100 cf | BACT-PSD | | |
| | Suwannee Mill | 9/5/2012 | | , | GCP | | gr/100 cf | BACT-PSD | | |
| | Big River Steel LLC | 9/18/2013 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD | | |
| | Big River Steel LLC | 9/18/2013 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD | | |
| | Big River Steel LLC | 9/18/2013 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD | | |
| | CPV St. Charles | 4/23/2014 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD | | |
| | Flopam Inc. | 6/14/2010 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD | | |
| | PSEG Fossil LLC Sewaren Generating Station | 3/10/2016 | | | Clean Fuels | | lb/MMBtu | BACT-PSD | | |
| MI-0406 | Renaissance Power LLC | 11/1/2013 | 40 | MMBtu/hr | GCP | 0.0050 | lb/MMBtu | BACT-PSD | | |

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Type |
|---------|---|-------------|-------------|----------|------------------|-----------------------|-----------|----------|
| MA-0039 | Salem Harbor Station Redevelopment | 1/30/2014 | | MMBtu/hr | None | 0.0050 | lb/MMBtu | BACT-PSD |
| KS-0029 | The Empire District Electric Company | 7/14/2015 | 18.6 | MMBtu/hr | None | 0.0050 | lb/MMBtu | BACT-PSD |
| NJ-0085 | Middlesex Energy Center, LLC | 7/19/2016 | 97.5 | MMBtu/hr | Clean Fuels | 0.0050 | lb/MMBtu | BACT-PSD |
| OK-0135 | Pryor Plant Chemical | 2/23/2009 | 80 | MMBtu/hr | None | 0.0063 | lb/MMBtu | BACT-PSD |
| MI-0412 | Holland Board of Public Works - East 5th Street | 12/4/2013 | 55 | MMBtu/hr | GCP | 0.0070 | lb/MMBtu | BACT-PSD |
| MI-0412 | Holland Board of Public Works - East 5th Street | 12/4/2013 | 95 | MMBtu/hr | GCP | 0.0070 | lb/MMBtu | BACT-PSD |
| MI-0424 | Holland Board of Public Works - East 5th Street | 12/5/2016 | 83.5 | MMBtu/hr | GCP | 0.0070 | lb/MMBtu | BACT-PSD |
| LA-0314 | Indorama Lake Charles Facility | 8/3/2016 | 229 | MMBtu/hr | GCP, Clean fuels | 0.0070 | lb/MMBtu | BACT-PSD |
| LA-0314 | Indorama Lake Charles Facility | 8/3/2016 | 248 | MMBtu/hr | GCP, Clean fuels | 0.0070 | lb/MMBtu | BACT-PSD |
| MI-0410 | Thetford Generating Station | 7/25/2013 | 100 | MMBtu/hr | GCP, Clean fuels | 0.0070 | lb/MMBtu | BACT-PSD |
| IN-0263 | Midwest Fertilizer Company LLC | 3/23/2017 | 218.6 | MMBtu/hr | GCP | 0.0072 | lb/MMBtu | BACT-PSD |
| IN-0173 | Midwest Fertilizer Corporation | 6/4/2014 | 218.6 | MMBtu/hr | GCP | 0.0072 | lb/MMBtu | BACT-PSD |
| IN-0180 | Midwest Fertilizer Corporation | 6/4/2014 | 218.6 | MMBtu/hr | GCP | 0.0072 | lb/MMBtu | BACT-PSD |
| IN-0179 | Ohio Valley Resources, LLC | 9/25/2013 | 218 | MMBtu/hr | GCP | 0.0072 | lb/MMBtu | BACT-PSD |
| CA-1212 | Palmdale Hybrid Power Project | 10/18/2011 | 110 | MMBtu/hr | Clean Fuels | 0.0073 | lb/MMBtu | BACT-PSD |
| AK-0083 | Kenai Nitrogen Operations | 1/6/2015 | 50 | MMBtu/hr | None | 0.0074 | lb/MMBtu | BACT-PSD |
| AK-0083 | Kenai Nitrogen Operations | 1/6/2015 | 243 | MMBtu/hr | None | | lb/MMBtu | BACT-PSD |
| | Indeck Niles, LLC | 1/4/2017 | | / | GCP | | lb/MMBtu | BACT-PSD |
| MI-0427 | Filer City Station | 11/17/2017 | 182 | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| MD-0046 | Keys Energy Center | 10/31/2014 | | | GCP, Clean fuels | 0.0075 | lb/MMBtu | BACT-PSD |
| MD-0045 | Mattawoman Energy Center | 11/13/2015 | 42 | MMBtu/hr | GCP, Clean fuels | 0.0075 | lb/MMBtu | BACT-PSD |
| CA-1212 | Palmdale Hybrid Power Project | 10/18/2011 | | | Clean Fuels | | lb/MMBtu | BACT-PSD |
| | Pipe Manufacturing Steel Mini Mill | 4/19/2010 | | , | GCP | 0.0075 | lb/MMBtu | BACT-PSD |
| OH-0352 | Oregon Clean Energy Center | 6/18/2013 | 99 | MMBtu/hr | Clean Fuels | 0.0080 | lb/MMBtu | BACT-PSD |
| | Ammonia Production Facility | 3/27/2013 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| OK-0156 | Northstar Agri Ind Enid | 7/31/2013 | 95 | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| MO-0081 | American Energy Producers, Inc. | 1/22/2009 | | MMBtu/hr | None | 0.0164 | lb/MMBtu | BACT-PSD |
| | American Energy Producers, Inc. | 1/25/2008 | | | None | | lb/MMBtu | BACT-PSD |
| MA-0037 | Central Heating Plant: Amherst Campus | 10/29/2008 | | MMBtu/hr | None | 0.0200 | lb/MMBtu | BACT-PSD |
| | | | M2.5- Total | _ | | | | |
| | Renaissance Power LLC | 11/1/2013 | | · · | GCP | | lb/MMBtu | BACT-PSD |
| | Evonik Degussa Corporation | 1/7/2010 | | | GCP | | lb/MMBtu | BACT-PSD |
| | St. Joseph Energy Center, LLC | 12/3/2012 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD |
| | Victorville 2 Hybrid Power Project | 3/11/2010 | | | None | | gr/100 cf | BACT-PSD |
| | Victorville 2 Hybrid Power Project | 3/11/2010 | | | None | | gr/100 cf | BACT-PSD |
| FL-0335 | Suwannee Mill | 9/5/2012 | | | GCP | | gr/100 cf | BACT-PSD |
| | Big River Steel LLC | 9/18/2013 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD |
| | Big River Steel LLC | 9/18/2013 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD |
| | Big River Steel LLC | 9/18/2013 | | | GCP, Clean fuels | | lb/MMBtu | BACT-PSD |
| WV-0025 | Moundsville Combined Cycle Power Plant | 11/21/2014 | 100 | MMBtu/hr | GCP, Clean fuels | 0.0050 | lb/MMBtu | BACT-PSD |

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|---------|---|-------------|---------------|----------|------------------|-----------------------|----------|----------|
| NJ-0084 | PSEG Fossil LLC Sewaren Generating Station | 3/10/2016 | 80 | MMBtu/hr | Clean Fuels | 0.0050 | lb/MMBtu | BACT-PSD |
| MA-0039 | Salem Harbor Station Redevelopment | 1/30/2014 | 80 | MMBtu/hr | None | 0.0050 | lb/MMBtu | BACT-PSD |
| KS-0029 | The Empire District Electric Company | 7/14/2015 | 18.6 | MMBtu/hr | None | 0.0050 | lb/MMBtu | BACT-PSD |
| NJ-0085 | Middlesex Energy Center, LLC | 7/19/2016 | 97.5 | MMBtu/hr | Clean Fuels | 0.0050 | lb/MMBtu | BACT-PSD |
| MI-0412 | Holland Board of Public Works - East 5th Street | 12/4/2013 | 55 | MMBtu/hr | GCP | 0.0070 | lb/MMBtu | BACT-PSD |
| MI-0412 | Holland Board of Public Works - East 5th Street | 12/4/2013 | 95 | MMBtu/hr | GCP | 0.0070 | lb/MMBtu | BACT-PSD |
| MI-0424 | Holland Board of Public Works - East 5th Street | 12/5/2016 | 83.5 | MMBtu/hr | GCP | 0.0070 | lb/MMBtu | BACT-PSD |
| LA-0314 | Indorama Lake Charles Facility | 8/3/2016 | 229 | MMBtu/hr | GCP, Clean fuels | 0.0070 | lb/MMBtu | BACT-PSD |
| LA-0314 | Indorama Lake Charles Facility | 8/3/2016 | 248 | MMBtu/hr | GCP, Clean fuels | 0.0070 | lb/MMBtu | BACT-PSD |
| MI-0410 | Thetford Generating Station | 7/25/2013 | 100 | MMBtu/hr | GCP, Clean fuels | 0.0070 | lb/MMBtu | BACT-PSD |
| IN-0263 | Midwest Fertilizer Company LLC | 3/23/2017 | 218.6 | MMBtu/hr | GCP | 0.0072 | lb/MMBtu | BACT-PSD |
| IN-0179 | Ohio Valley Resources, LLC | 9/25/2013 | 218 | MMBtu/hr | GCP | 0.0072 | lb/MMBtu | BACT-PSD |
| CA-1212 | Palmdale Hybrid Power Project | 10/18/2011 | 110 | MMBtu/hr | Clean Fuels | 0.0073 | lb/MMBtu | BACT-PSD |
| AK-0083 | Kenai Nitrogen Operations | 1/6/2015 | 50 | MMBtu/hr | None | 0.0074 | lb/MMBtu | BACT-PSD |
| AK-0083 | Kenai Nitrogen Operations | 1/6/2015 | 243 | MMBtu/hr | None | 0.0074 | lb/MMBtu | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | 1/4/2017 | 182 | MMBtu/hr | GCP | 0.0075 | lb/MMBtu | BACT-PSD |
| OK-0148 | Buffalo Creek Processing Plant | 9/12/2012 | 11.04 | MMBtu/hr | None | 0.0075 | lb/MMBtu | BACT-PSD |
| MI-0427 | Filer City Station | 11/17/2017 | 182 | MMBtu/hr | GCP | 0.0075 | lb/MMBtu | BACT-PSD |
| MD-0045 | Mattawoman Energy Center | 11/13/2015 | 42 | MMBtu/hr | GCP, Clean fuels | 0.0075 | lb/MMBtu | BACT-PSD |
| CA-1212 | Palmdale Hybrid Power Project | 10/18/2011 | 40 | MMBtu/hr | Clean Fuels | 0.0075 | lb/MMBtu | BACT-PSD |
| LA-0272 | Ammonia Production Facility | 3/27/2013 | 217.5 | MMBtu/hr | GCP | 0.0089 | lb/MMBtu | BACT-PSD |
| OK-0156 | Northstar Agri Ind Enid | 7/31/2013 | 95 | MMBtu/hr | GCP | 0.0126 | lb/MMBtu | BACT-PSD |
| | | | Organic Compo | | | | | |
| TX-0813 | Odessa Petrochemical Plant | 11/22/2016 | 223 | MMBtu/hr | GCP | 0.0005 | lb/MMBtu | BACT-PSD |
| MO-0079 | American Energy Producers, Inc. | 1/25/2008 | 190 | MMBtu/hr | GCP | 0.0010 | lb/MMBtu | BACT-PSD |
| MI-0389 | Karn Weadock Generating Complex | 12/29/2009 | | MMBtu/hr | GCP | 0.0013 | lb/MMBtu | BACT-PSD |
| FL-0318 | Highlands Ethanol Facility | 12/10/2009 | 198 | MMBtu/hr | None | 0.0015 | lb/MMBtu | BACT-PSD |
| WY-0075 | Cheyenne Prairie Generating Station | 7/16/2014 | | MMBtu/hr | GCP | 0.0017 | lb/MMBtu | BACT-PSD |
| SC-0112 | Nucor Steel - Berkeley | 5/5/2008 | 50.21 | MMBtu/hr | GCP, Clean fuels | 0.0026 | lb/MMBtu | BACT-PSD |
| TX-0681 | Olefins Plant | 8/8/2014 | | | GCP | 0.0030 | lb/MMBtu | BACT-PSD |
| FL-0335 | Suwannee Mill | 9/5/2012 | 46 | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| | Westlake Facility | 7/12/2016 | | | Ox Cat, GCP | 0.0033 | lb/MMBtu | BACT-PSD |
| | Perdue Grain And Oilseed, LLC | 7/12/2017 | | | None | | lb/MMBtu | BACT-PSD |
| | El Dorado Chemical Company | 11/18/2013 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| | Indeck Niles, LLC | 1/4/2017 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| MI-0393 | Ray Compressor Station | 10/14/2010 | | MMBtu/hr | None | | lb/MMBtu | BACT-PSD |
| IA-0107 | Marshalltown Generating Station | 4/14/2014 | | MMBtu/hr | None | 0.0050 | lb/MMBtu | BACT-PSD |
| | Renaissance Power LLC | 11/1/2013 | | | GCP | | lb/MMBtu | BACT-PSD |
| IN-0158 | St. Joseph Energy Center, LLC | 12/3/2012 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| IN-0239 | Subaru of Indiana Automotive, Inc. | 2/18/2016 | 38 | MMBtu/hr | None | 0.0050 | lb/MMBtu | BACT-PSD |

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|---------|---|-------------|------------|----------|------------------|-----------------------|----------|----------|
| OR-0050 | Troutdale Energy Center, LLC | 3/5/2014 | 39.8 | MMBtu/hr | LNB, FGR | 0.0050 | lb/MMBtu | BACT-PSD |
| OH-0310 | American Municipal Power Generating Station | 10/8/2009 | 150 | MMBtu/hr | None | 0.0052 | lb/MMBtu | BACT-PSD |
| IN-0263 | Midwest Fertilizer Company LLC | 3/23/2017 | 218.6 | MMBtu/hr | GCP | 0.0052 | lb/MMBtu | BACT-PSD |
| IN-0173 | Midwest Fertilizer Corporation | 6/4/2014 | 218.6 | MMBtu/hr | GCP | 0.0052 | lb/MMBtu | BACT-PSD |
| IN-0180 | Midwest Fertilizer Corporation | 6/4/2014 | 218.6 | MMBtu/hr | GCP | 0.0052 | lb/MMBtu | BACT-PSD |
| IN-0179 | Ohio Valley Resources, LLC | 9/25/2013 | 218 | MMBtu/hr | GCP | 0.0052 | lb/MMBtu | BACT-PSD |
| OH-0323 | Titan Tire Corporation of Bryan | 6/5/2008 | 50.4 | MMBtu/hr | None | 0.0054 | lb/MMBtu | BACT-PSD |
| OH-0350 | Republic Steel | 7/18/2012 | 65 | MMBtu/hr | GCP | 0.0054 | lb/MMBtu | BACT-PSD |
| LA-0272 | Ammonia Production Facility | 3/27/2013 | 217.5 | MMBtu/hr | GCP, FGR | 0.0054 | lb/MMBtu | BACT-PSD |
| AL-0312 | Belk Chip-N-Saw Facility | 5/26/2016 | 60 | MMBtu/hr | GCP | 0.0054 | lb/MMBtu | BACT-PSD |
| AR-0140 | Big River Steel LLC | 9/18/2013 | 24.5 | MMBtu/hr | GCP, Clean fuels | 0.0054 | lb/MMBtu | BACT-PSD |
| AR-0140 | Big River Steel LLC | 9/18/2013 | 51.2 | MMBtu/hr | GCP, Clean fuels | 0.0054 | lb/MMBtu | BACT-PSD |
| OK-0148 | Buffalo Creek Processing Plant | 9/12/2012 | 11.04 | MMBtu/hr | None | 0.0054 | lb/MMBtu | BACT-PSD |
| LA-0314 | Indorama Lake Charles Facility | 8/3/2016 | 229 | MMBtu/hr | GCP | 0.0054 | lb/MMBtu | BACT-PSD |
| LA-0314 | Indorama Lake Charles Facility | 8/3/2016 | 248 | MMBtu/hr | GCP | 0.0054 | lb/MMBtu | BACT-PSD |
| AK-0083 | Kenai Nitrogen Operations | 1/6/2015 | 50 | MMBtu/hr | None | 0.0054 | lb/MMBtu | BACT-PSD |
| | Kenai Nitrogen Operations | 1/6/2015 | 243 | MMBtu/hr | None | 0.0054 | lb/MMBtu | BACT-PSD |
| AL-0282 | Lenzing Fibers, Inc. | 1/22/2014 | 100 | MMBtu/hr | GCP | 0.0054 | lb/MMBtu | BACT-PSD |
| | Pipe Manufacturing Steel Mini Mill | 4/19/2010 | 40 | MMBtu/hr | GCP | 0.0054 | lb/MMBtu | BACT-PSD |
| SC-0160 | US8 Facility | 12/13/2012 | 33.6 | MMBtu/hr | None | 0.0054 | lb/MMBtu | BACT-PSD |
| IA-0096 | Verasun Charles City, LLC | 11/18/2008 | 50 | MMBtu/hr | None | 0.0054 | lb/MMBtu | BACT-PSD |
| MO-0082 | Archer Daniels Midland-Mexico | 10/5/2010 | 85.6 | MMBtu/hr | GCP | 0.0055 | lb/MMBtu | BACT-PSD |
| AL-0286 | Mount Vernon Mill | 3/25/2010 | 70 | MMBtu/hr | None | 0.0055 | lb/MMBtu | BACT-PSD |
| AL-0300 | Thyssenkrupp Stainless USA, LLC | 3/25/2010 | 28.6 | MMBtu/hr | None | 0.0055 | lb/MMBtu | BACT-PSD |
| OH-0315 | New Steel International, Inc., Haverhill | 5/6/2008 | 50.4 | MMBtu/hr | None | 0.0056 | lb/MMBtu | BACT-PSD |
| LA-0248 | Direct Reduction Iron Plant | 1/27/2011 | 201 | MMBtu/hr | GCP | 0.0059 | lb/MMBtu | BACT-PSD |
| AL-0307 | Alloys Plant | 10/9/2015 | 17.5 | MMBtu/hr | GCP | 0.0060 | lb/MMBtu | BACT-PSD |
| AL-0307 | Alloys Plant | 10/9/2015 | 24.59 | MMBtu/hr | GCP | 0.0060 | lb/MMBtu | BACT-PSD |
| WV-0025 | Moundsville Combined Cycle Power Plant | 11/21/2014 | 100 | MMBtu/hr | GCP, Clean fuels | 0.0060 | lb/MMBtu | BACT-PSD |
| OK-0156 | Northstar Agri Ind Enid | 7/31/2013 | 95 | MMBtu/hr | GCP | 0.0060 | lb/MMBtu | BACT-PSD |
| OH-0352 | Oregon Clean Energy Center | 6/18/2013 | 99 | MMBtu/hr | GCP | 0.0060 | lb/MMBtu | BACT-PSD |
| OK-0135 | Pryor Plant Chemical | 2/23/2009 | 80 | MMBtu/hr | None | 0.0063 | lb/MMBtu | BACT-PSD |
| LA-0248 | Direct Reduction Iron Plant | 1/27/2011 | 201 | MMBtu/hr | GCP | 0.0078 | lb/MMBtu | BACT-PSD |
| MI-0412 | Holland Board of Public Works - East 5th Street | 12/4/2013 | 55 | MMBtu/hr | GCP | 0.0080 | lb/MMBtu | BACT-PSD |
| MI-0412 | Holland Board of Public Works - East 5th Street | 12/4/2013 | 95 | MMBtu/hr | GCP | 0.0080 | lb/MMBtu | BACT-PSD |
| MI-0424 | Holland Board of Public Works - East 5th Street | 12/5/2016 | | MMBtu/hr | GCP | 0.0080 | lb/MMBtu | BACT-PSD |
| MI-0410 | Thetford Generating Station | 7/25/2013 | 100 | MMBtu/hr | GCP, Clean fuels | 0.0080 | lb/MMBtu | BACT-PSD |
| | Chouteau Power Plant | 1/23/2009 | 33.5 | MMBtu/hr | GCP | 0.0161 | lb/MMBtu | BACT-PSD |
| MO-0081 | American Energy Producers, Inc. | 1/22/2009 | 95 | MMBtu/hr | None | 0.0164 | lb/MMBtu | BACT-PSD |

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|----------|--------------------------------|-------------|------------|--------------------|----------------------------------|----------------|----------|------|
| | | • | | Nitrogen Dioxide | | | | |
| *AL-0328 | PLANT BARRY | 11/09/2020 | 90.5 | MMBtu/hr | | 0.011 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 88.7 | MMBTU/HR | CBF/GCP/LNB | 0.035 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 0 | | CBF/GCP/LNB | 0.095 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 53.7 | MMBTU/HR | CBF/GCP/LNB | 0.035 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 53.7 | MMBTU/HR | CBF/GCP/LNB | 0.035 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 78.2 | MMBTU/HR | SCR/CBF/GCP/LNB | 0.035 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 85.15 | MMBTU/HR | CBF/GCP/LNB | 0.1 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP/LNB | 0.097 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP/LNB | 0.095 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP/LNB | 0.035 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | SCR/CBF/GCP/LNB | 0.035 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP/LNB | 0.035 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP/LNB | 0.08 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP/LNB | 0.035 | LB/MMBTU | BACT |
| AR-0167 | LION OIL COMPANY | 12/01/2020 | 75 | MMBtu/hr | Ultra-LNB/GCP | 3.5 | LB/HR | BACT |
| AR-0167 | LION OIL COMPANY | 12/01/2020 | 56 | MMBtu/hr | GCP | 2.8 | LB/HR | BACT |
| AR-0167 | LION OIL COMPANY | 12/01/2020 | 70 | MMBtu/hr | | 12.7 | LB/HR | BACT |
| AR-0167 | LION OIL COMPANY | 12/01/2020 | 50 | MMBtu/hr | GCP | 5.3 | LB/HR | BACT |
| AR-0167 | LION OIL COMPANY | 12/01/2020 | 142.2 | | Ultra-LNB/GCP | 6.5 | LB/HR | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 117.9 | MMBtu/hr | CBF/GCP/LNB | 0.1 | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | | MMBtu/hr | CBF/GCP/LNB | | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | | MMBtu/hr | CBF/GCP/LNB | | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 64 | · | CBF/GCP/LNB | | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 0 | , | GCP/Energy efficient burners/CBF | 0.05 | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | 02/14/2019 | 128 | MMBTU/hr | LNB/SCR/SNCR | | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | 02/14/2019 | 50.4 | MMBTU/hr | LNB | | LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | , | LNB | | LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | | LNB | 0.035 | LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | | LNB/SCR/SNCR | 0.0075 | LB/MMBTU | BACT |
| IL-0130 | JACKSON ENERGY CENTER | 12/31/2018 | 96 | mmBtu/hr | Ultra-LNB/FGR/GCP | | LB/MMBTU | LAER |
| KY-0110 | NUCOR STEEL BRANDENBURG | 07/23/2020 | 54 | MMBtu/hr | LNB/GCP | 158 | LB/MMSCF | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | 07/23/2020 | 60 | MMBtu/hr, combined | LNB/GCP | 81.6 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | | MMBtu/hr | LNB/GCP | | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 94 | MMBtu/hr | LNB/GCP | 7.5 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 104.3 | MMBtu/hr | LNB/GCP | | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 65.5 | MMBtu/hr | LNB/GCP | 70 | LB/MMSCF | BACT |
| LA-0364 | FG LA COMPLEX | 01/06/2020 | 0 | , | LNB | | LB/MMBTU | BACT |
| LA-0364 | FG LA COMPLEX | 01/06/2020 | 94 | mm btu/h | SCR/LNB | | LB/H | BACT |
| MI-0441 | LBWLERICKSON STATION | 12/21/2018 | 99 | MMBTU/H | LNB or FGR/GCP | 30 | PPM | BACT |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | | MMBTU/H | GCP/LNB | 0.036 | LB/MMBTU | BACT |
| MI-0447 | LBWLERICKSON STATION | 01/07/2021 | | MMBTU/H | LNB or FGR/GCP | | PPM | BACT |
| OH-0379 | PETMIN USA INCORPORATED | 02/06/2019 | 0 | , | Direct Evacuation Control | | LB/T | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 88 | MMBTU/H | CBF/LNB/GCP | | LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | | MMBTU/H | CBF/LNB/GCP | | LB/H | BACT |
| TX-0851 | RIO BRAVO PIPELINE FACILITY | 12/17/2018 | | MMBTU/HR | LNB/GCP | | LB/MMBTU | BACT |
| TX-0888 | ORANGE POLYETHYLENE PLANT | 04/23/2020 | 0 | | SCR/CEMS | | LB/MMBTU | BACT |
| TX-0888 | ORANGE POLYETHYLENE PLANT | 04/23/2020 | | MMBtu | GCP/LNB | | LB/MMBTU | BACT |
| TX-0888 | ORANGE POLYETHYLENE PLANT | 04/23/2020 | 0 | ** | LNB | | LB/MMBTU | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | 0 | | GCP/LNB | | LB/HR | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | 0 | | GCP/LNB | | LB/HR | BACT |

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|----------|------------------------------------|-------------|------------|---------------------------------------|-------------------------|-----------------------|----------|--------|
| 1,520.15 | Taemey Hame | | | Carbon Monoxide | Control | | 01110 | .,,,,, |
| *AL-0328 | PLANT BARRY | 11/09/2020 | 90.5 | MMBtu/hr | | 0.037 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | | MMBTU/HR | CBF/GCP | | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 53.7 | MMBTU/HR | CBF/GCP | | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | | MMBTU/HR | CBF/GCP | | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | | MMBTU/HR | CBF/GCP | | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | | MMBTU/HR | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0167 | LION OIL COMPANY | 12/01/2020 | 142.2 | MMBtu/hr | GCP | | LB/HR | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | | MMBtu/hr | CBF/GCP | | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | | MMBtu/hr | CBF/GCP | | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | | MMBtu/hr | CBF/GCP | | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | 02/14/2019 | | MMBTU/hr | GCP | | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | 02/14/2019 | | MMBTU/hr | GCP | | LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | · · · · · · · · · · · · · · · · · · · | GCP | | LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | | GCP | 0.084 | LB/MMBTU | BACT |
| IL-0130 | JACKSON ENERGY CENTER | 12/31/2018 | 96 | mmBtu/hr | GCP | | LB/MMBTU | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | 07/23/2020 | 54 | MMBtu/hr | GCP | 84 | LB/MMSCF | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | 07/23/2020 | | MMBtu/hr, combined | GCP | | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 50.4 | MMBtu/hr | GCP | 61 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 94 | MMBtu/hr | GCP | 84 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 104.3 | MMBtu/hr | GCP | 84 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 65.5 | MMBtu/hr | GCP | 84 | LB/MMSCF | BACT |
| LA-0364 | FG LA COMPLEX | 01/06/2020 | 0 | | GCP | 0.037 | LB/MMBTU | BACT |
| LA-0364 | FG LA COMPLEX | 01/06/2020 | 94 | mm btu/h | GCP/OxCat | 26.21 | LB/H | BACT |
| MI-0441 | LBWLERICKSON STATION | 12/21/2018 | 99 | MMBTU/H | GCP | 50 | PPM | BACT |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | 80 | MMBTU/H | GCP | 0.037 | LB/MMBTU | BACT |
| MI-0447 | LBWLERICKSON STATION | 01/07/2021 | 50 | MMBTU/H | GCP | 50 | PPM | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 88 | MMBTU/H | CBF/baffle burners/GCP | 6.16 | LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 112 | MMBTU/H | CBF/baffle burners/GCP | 7.84 | LB/H | BACT |
| SC-0192 | CANFOR SOUTHERN PINE - CONWAY MILL | 05/21/2019 | 0 | | Work Practice Standards | 0.0375 | LB/MMBTU | BACT |
| TX-0851 | RIO BRAVO PIPELINE FACILITY | 12/17/2018 | 71.3 | MMBTU/HR | CBF/GCP | 0.082 | LB/MMBTU | BACT |
| TX-0888 | ORANGE POLYETHYLENE PLANT | 04/23/2020 | 0 | | GCP/proper design | 50 | PPMVD | BACT |
| TX-0888 | ORANGE POLYETHYLENE PLANT | 04/23/2020 | 100 | MMBtu | GCP/proper design | 50 | PPMVD | BACT |
| TX-0888 | ORANGE POLYETHYLENE PLANT | 04/23/2020 | 0 | | CBF/GCP | 0.06 | LB/MMBTU | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | 0 | | CBF/GCP | 58.3 | LB/HR | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | 0 | | GCP | 45.8 | LB/HR | BACT |

| *AL-0328 PLANT BARRY AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL | LC LC LC LC LC LC LC LC LC LC LC LC LC L | 11/09/2020 11/07/2018 11/07/2018 11/07/2018 11/07/2018 11/07/2018 11/07/2018 11/07/2018 11/07/2018 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 | Volatile Organic Compou 90.5 MMBtu/hr 88.7 MMBTU/HR 0 53.7 MMBTU/HR 53.7 MMBTU/HR 78.2 MMBTU/HR 85.15 MMBTU/HR 0 0 0 0 | CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP | 0.0054 0.0054 0.054 0.054 0.0054 0.0054 0.0054 0.0054 0.0054 | LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU | BACT BACT BACT BACT BACT BACT BACT BACT |
|---|--|--|---|---|--|--|---|
| AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL ARK/ AR-0171 NUCOR STEEL ARK/ AR-0172 NUCOR STEEL ARK/ KY-0110 NUCOR STEEL BRAI KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC LC LC LC LC LC LC LC LC LC LC LC LC L | 11/07/2018 11/07/2018 11/07/2018 11/07/2018 11/07/2018 11/07/2018 11/07/2018 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 | 88.7 MMBTU/HR 0 53.7 MMBTU/HR 53.7 MMBTU/HR 78.2 MMBTU/HR 85.15 MMBTU/HR 0 0 0 0 0 0 | CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP | 0.0054 0.0054 0.054 0.054 0.0054 0.0054 0.0054 0.0054 0.0054 | LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU | BACT BACT BACT BACT BACT BACT BACT BACT |
| AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0110 NUCOR STEEL ARK X-0171 NUCOR STEEL ARK X-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC LC LC LC LC LC LC LC LC LC LC LC LC L | 11/07/2018 11/07/2018 11/07/2018 11/07/2018 11/07/2018 11/07/2018 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 | 0 53.7 MMBTU/HR 53.7 MMBTU/HR 78.2 MMBTU/HR 85.15 MMBTU/HR 0 0 0 0 0 0 0 0 0 | CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP | 0.0054 0.0054 0.0054 0.0054 0.0054 0.0054 0.0054 0.0054 | LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU | BACT BACT BACT BACT BACT BACT BACT BACT |
| AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0110 NUCOR STEEL ARKA *AR-0171 NUCOR STEEL ARKA *AR-0172 NUCOR STEEL ARKA KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC LC LC LC LC LC LC LC LC LC LC LC LC | 11/07/2018 11/07/2018 11/07/2018 11/07/2018 11/07/2018 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 | 53.7 MMBTU/HR 53.7 MMBTU/HR 78.2 MMBTU/HR 85.15 MMBTU/HR 0 0 0 0 0 0 0 | CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP | 0.0054 0.054 0.0054 0.0054 0.0054 0.0054 0.0054 0.0054 | LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU | BACT BACT BACT BACT BACT BACT BACT BACT |
| AR-0155 BIG RIVER STEEL LL AR-0155 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL ARK/ AR-0171 NUCOR STEEL ARK/ AR-0172 NUCOR STEEL ARK/ KY-0110 NUCOR STEEL BRAIK KY-0110 NUCOR STEEL BRAIK KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC LC LC LC LC LC LC LC LC LC LC LC | 11/07/2018 11/07/2018 11/07/2018 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 | 53.7 MMBTU/HR 78.2 MMBTU/HR 85.15 MMBTU/HR 0 0 0 0 0 0 0 | CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP | 0.054 0.0054 0.0054 0.0054 0.0054 0.0054 0.0054 | LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU | BACT BACT BACT BACT BACT BACT |
| AR-0155 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL LL AR-0171 NUCOR STEEL ARK/ AR-0171 NUCOR STEEL ARK/ X*AR-0172 NUCOR STEEL ARK/ KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC LC LC LC LC LC LC LC LC LC LC | 11/07/2018 11/07/2018 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 | 78.2 MMBTU/HR 85.15 MMBTU/HR 0 0 0 0 0 0 0 0 0 | CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP | 0.0054 0.0054 0.0054 0.0054 0.0054 0.0054 | LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU | BACT BACT BACT BACT BACT |
| AR-0155 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL ARK/ AR-0171 NUCOR STEEL ARK/ *AR-0172 NUCOR STEEL ARK/ *AR-0172 NUCOR STEEL ARK/ KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC LC LC LC LC LC LC LC LC | 11/07/2018 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 | 85.15 MMBTU/HR 0 0 0 0 0 0 0 0 0 0 | CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP | 0.0054 0.0054 0.0054 0.0054 0.0054 | LB/MMBTU LB/MMBTU LB/MMBTU LB/MMBTU | BACT BACT BACT BACT |
| AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL LL AR-0171 NUCOR STEEL ARK/ *AR-0172 NUCOR STEEL ARK/ *AR-0172 NUCOR STEEL ARK/ KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC LC LC LC LC LC LC LC | 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 | 0 0 0 0 0 | CBF/GCP CBF/GCP CBF/GCP CBF/GCP CBF/GCP | 0.0054 0.0054 0.0054 0.0054 | LB/MMBTU LB/MMBTU LB/MMBTU | BACT BACT BACT |
| AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL ARK AR-0171 NUCOR STEEL ARK AR-0172 NUCOR STEEL ARK KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC LC LC LC LC LC LC | 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 | 0 0 0 0 0 | CBF/GCP CBF/GCP CBF/GCP CBF/GCP | 0.0054 0.0054 0.0054 | LB/MMBTU LB/MMBTU | BACT BACT |
| AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL ARK AR-0171 NUCOR STEEL ARK AR-0172 NUCOR STEEL ARK *AR-0172 NUCOR STEEL ARK KY-0110 NUCOR STEEL BRAI KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC LC LC LC LC LC | 04/05/2019 04/05/2019 04/05/2019 04/05/2019 04/05/2019 | 0 0 0 0 | CBF/GCP CBF/GCP CBF/GCP | 0.0054 0.0054 | LB/MMBTU | BACT |
| AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL ARKA AR-0171 NUCOR STEEL ARKA AR-0172 NUCOR STEEL ARKA *AR-0172 NUCOR STEEL ARKA KY-0110 NUCOR STEEL BRAI KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC LC LC LC LC | 04/05/2019 04/05/2019 04/05/2019 04/05/2019 | 0 0 | CBF/GCP CBF/GCP | 0.0054 | | |
| AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL ARKA AR-0171 NUCOR STEEL ARKA *AR-0172 NUCOR STEEL ARKA *AR-0172 NUCOR STEEL ARKA KY-0110 NUCOR STEEL BRAI KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC LC LC LC LC | 04/05/2019 04/05/2019 04/05/2019 | 0 0 | CBF/GCP | | I B/MMRTU | |
| AR-0159 BIG RIVER STEEL LL AR-0159 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL ARK/ AR-0171 NUCOR STEEL ARK/ *AR-0172 NUCOR STEEL ARK/ *AR-0172 NUCOR STEEL ARK/ KY-0110 NUCOR STEEL BRA/ KY-0110 NUCOR STEEL BRA/ KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC LC LC LC | 04/05/2019 04/05/2019 | 0 | | 0.0054 | 120, | BACT |
| AR-0159 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL ARK/ AR-0171 NUCOR STEEL ARK/ *AR-0172 NUCOR STEEL ARK/ *AR-0172 NUCOR STEEL ARK/ KY-0110 NUCOR STEEL BRAI KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC LC LC | 04/05/2019 | • | | 0.0054 | LB/MMBTU | BACT |
| AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL ARK/ AR-0171 NUCOR STEEL ARK/ *AR-0172 NUCOR STEEL ARK/ *AR-0172 NUCOR STEEL ARK/ KY-0110 NUCOR STEEL BRAI KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC LC | | 0 | CBF/GCP | 0.0054 | LB/MMBTU | BACT |
| AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL ARK AR-0171 NUCOR STEEL ARK *AR-0172 NUCOR STEEL ARK *AR-0172 NUCOR STEEL ARK *KY-0110 NUCOR STEEL BRAI KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC | 03/17/2021 | υĮ | CBF/GCP | 0.0054 | LB/MMBTU | BACT |
| AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL ARK/ AR-0171 NUCOR STEEL ARK/ *AR-0172 NUCOR STEEL ARK/ *AR-0172 NUCOR STEEL ARK/ KY-0110 NUCOR STEEL BRAI KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | | 03/11/2021 | 117.9 MMBtu/hr | CBF/GCP | 0.0054 | LB/MMBTU | BACT |
| AR-0168 BIG RIVER STEEL LL AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL ARKA AR-0171 NUCOR STEEL ARKA *AR-0172 NUCOR STEEL ARKA *AR-0172 NUCOR STEEL ARKA KY-0110 NUCOR STEEL BRAI KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | | 03/17/2021 | 58 MMBtu/hr | CBF/GCP | 0.0054 | LB/MMBTU | BACT |
| AR-0168 BIG RIVER STEEL LL AR-0171 NUCOR STEEL ARKA AR-0171 NUCOR STEEL ARKA *AR-0172 NUCOR STEEL ARKA *AR-0172 NUCOR STEEL ARKA KY-0110 NUCOR STEEL BRAI KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | rC | 03/17/2021 | 66 MMBtu/hr | CBF/GCP | 0.0054 | LB/MMBTU | BACT |
| AR-0171 NUCOR STEEL ARKA AR-0171 NUCOR STEEL ARKA *AR-0172 NUCOR STEEL ARKA *AR-0172 NUCOR STEEL ARKA KY-0110 NUCOR STEEL BRAI KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LC | 03/17/2021 | 64 MMBtu/hr | CBF/GCP | 0.0054 | LB/MMBTU | BACT |
| AR-0171 NUCOR STEEL ARKA *AR-0172 NUCOR STEEL ARKA *AR-0172 NUCOR STEEL ARKA KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | rc | 03/17/2021 | 0 | GCP/Energy efficient burners/CBF | 0.0054 | LB/MMBTU | BACT |
| *AR-0172 NUCOR STEEL ARK/ *AR-0172 NUCOR STEEL ARK/ KY-0110 NUCOR STEEL BRAY KY-0110 NUCOR STEEL BRAY KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | ANSAS | 02/14/2019 | 128 MMBTU/hr | GCP | 0.0055 | LB/MMBTU | BACT |
| *AR-0172 NUCOR STEEL ARK/ KY-0110 NUCOR STEEL BRAY KY-0110 NUCOR STEEL BRAY KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | ANSAS | 02/14/2019 | 50.4 MMBTU/hr | GCP | 0.0026 | LB/HR | BACT |
| KY-0110 NUCOR STEEL BRAI KY-0110 NUCOR STEEL BRAI KY-0115 NUCOR STEEL GALL | ANSAS | 09/01/2021 | 0 | GCP | 0.0055 | LB/MMBTU | BACT |
| KY-0110 NUCOR STEEL BRAY KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | ANSAS | 09/01/2021 | 0 | GCP | 0.0055 | LB/MMBTU | BACT |
| KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | NDENBURG | 07/23/2020 | 54 MMBtu/hr | GCP | 5.5 | LB/MMSCF | BACT |
| KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | NDENBURG | 07/23/2020 | 60 MMBtu/hr, combined | GCP | 5.5 | LB/MMSCF | BACT |
| KY-0115 NUCOR STEEL GALL KY-0115 NUCOR STEEL GALL | LATIN, LLC | 04/19/2021 | 50.4 MMBtu/hr | GCP | 5.5 | LB/MMSCF | BACT |
| KY-0115 NUCOR STEEL GALL | LATIN, LLC | 04/19/2021 | 94 MMBtu/hr | GCP | 5.5 | LB/MMSCF | BACT |
| | LATIN, LLC | 04/19/2021 | 104.3 MMBtu/hr | GCP | 5.5 | LB/MMSCF | BACT |
| LA-0364 FG LA COMPLEX | LATIN, LLC | 04/19/2021 | 65.5 MMBtu/hr | GCP | 5.5 | LB/MMSCF | BACT |
| | | 01/06/2020 | 0 | GCP | 4.02 | LB/H | BACT |
| LA-0364 FG LA COMPLEX | | 01/06/2020 | 94 mm btu/h | OxCat/GCP | 13.37 | LB/H | BACT |
| MI-0441 LBWLERICKSON ST | STATION | 12/21/2018 | 99 MMBTU/H | GCP | 0.5 | LB/H | BACT |
| MI-0442 THOMAS TOWNSH | 1IP ENERGY, LLC | 08/21/2019 | 80 MMBTU/H | GCP | 0.0054 | LB/MMBTU | BACT |
| MI-0447 LBWLERICKSON ST | STATION | 01/07/2021 | 50 MMBTU/H | GCP | 0.3 | LB/H | BACT |
| OH-0381 NORTHSTAR BLUES | SCOPE STEEL, LLC | 09/27/2019 | 88 MMBTU/H | CBF/GCP | 0.48 | LB/H | BACT |
| OH-0381 NORTHSTAR BLUES | SCOPE STEEL, LLC | 09/27/2019 | 112 MMBTU/H | CBF/GCP | 0.62 | LB/H | BACT |
| SC-0192 CANFOR SOUTHER | RN PINE - CONWAY MILL | 05/21/2019 | 0 | Work Practice Standards | 0.0054 | LB/MMBTU | BACT |
| TX-0851 RIO BRAVO PIPELIN | NE EACH ITM | 12/17/2018 | 71.3 MMBTU/HR | CBF/GCP | 0.0054 | LB/MMBTU | BACT |
| TX-0877 SWEENY REFINERY | NE FACILITY | 01/08/2020 | 0 | CBF/GCP | 0.0054 | LB/MMBTU | LAER |
| TX-0888 ORANGE POLYETHY | | 04/23/2020 | 0 | GCP/proper design | 0.0054 | LB/MMBTU | BACT |
| TX-0888 ORANGE POLYETHY | 1 | 04/23/2020 | 100 MMBtu | GCP/proper design | 0.0054 | LB/MMBTU | BACT |
| *WI-0289 GEORGIA-PACIFIC C | Y IYLENE PLANT | 04/01/2019 | 95 mmBTU/hr | GCP | 0.0055 | LB/MMBTU | BACT |

⁽a) OxCat = oxidation catalyst, SCR = selective catalytic reduction, LNB = low-NOx burners, GCP = good combustion practices, CBF = clean burning fuels, SNCR = selective, noncatalytic reduction, CEMS = continuous emission monitoring system

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Type |
|----------|---|-------------|------------|------------------------------------|--|---------------------|-----------------|------|
| KBLC ID | Facility Name | Permit Date | Inrougnput | | Controls | EIIIISSIOII LIIIIIL | Units | Туре |
| | | I | I - | PM ₁₀ (total) | 1 | T | T 6 | |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | | MMBTU/HR | CBF/GCP | | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | | MMBTU/HR | CBF/GCP | | X10^-4 LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | | MMBTU/HR | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | 1 | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | 4 | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | 1 | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | `\ | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | | MMBtu/hr | CBF/GCP | | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | | MMBtu/hr | CBF/GCP | | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | | MMBtu/hr | CBF/GCP | | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | | MMBtu/hr | CBF/GCP | | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 0 | <u> </u> | Mist eliminator/GCP | | GR/DSCF | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | C | | GCP/Energy efficient burners/CBF | | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | 02/14/2019 | | MMBTU/hr | GCP | | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | 02/14/2019 | 50.4 | MMBTU/hr | GCP | | LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | C |) | GCP | | LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | `\ | GCP | | GR/DSCF | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | `\ | Wet Scrubber System with mist eliminator | | LB/MMBTU | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | 07/23/2020 | | MMBtu/hr | GCP | | LB/MMSCF | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | 07/23/2020 | | MMBtu/hr, combined | GCP | | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | | MMBtu/hr | GCP | | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | | MMBtu/hr | GCP | | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | | MMBtu/hr | GCP | | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | | MMBtu/hr | GCP | | LB/MMSCF | BACT |
| LA-0364 | FG LA COMPLEX | 01/06/2020 | 0 | 1 | CBF/GCP | 0.03 | | BACT |
| LA-0364 | FG LA COMPLEX | 01/06/2020 | | mm btu/h | CBF/GCP | | LB/H | BACT |
| MI-0441 | LBWLERICKSON STATION | 12/21/2018 | | MMBTU/H | GCP | | LB/H | BACT |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | | MMBTU/H | CBF/GCP | | LB/MMSCF | BACT |
| MI-0447 | LBWLERICKSON STATION | 01/07/2021 | 50 | MMBTU/H | GCP | | LB/H | BACT |
| OH-0379 | PETMIN USA INCORPORATED | 02/06/2019 | 0 | `\ | Control Efficiency | 0.074 | | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 88 | MMBTU/H | CBF/GCP | 0.88 | LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 112 | MMBTU/H | CBF/GCP | | LB/H | BACT |
| TX-0851 | RIO BRAVO PIPELINE FACILITY | 12/17/2018 | | MMBTU/HR | CBF/GCP | | LB/MMBTU | BACT |
| *VA-0333 | NORFOLK NAVAL SHIPYARD | 12/09/2020 | 76.6 | MMBtu/hr | | 0.0078 | LB | BACT |
| | | | | PM ₁₀ (filterable only) | | | | |
| *AL-0328 | PLANT BARRY | 11/09/2020 | 90.5 | MMBtu/hr | | 0.0075 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 88.7 | MMBTU/HR | CBF/GCP | 9.38 | X10^-4 LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 78.2 | MMBTU/HR | CBF/GCP | 0.0012 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | C |) | CBF/GCP | 0.0075 | LB/MMBTU | BACT |
| TX-0888 | ORANGE POLYETHYLENE PLANT | 04/23/2020 | C |) | CBF/GCP | 0.0075 | LB/MMBTU | BACT |
| TX-0888 | ORANGE POLYETHYLENE PLANT | 04/23/2020 | 100 | MMBtu | CBF/GCP | 0.0075 | LB/MMBTU | BACT |
| TX-0888 | ORANGE POLYETHYLENE PLANT | 04/23/2020 | C |) | CBF/GCP | 0.0075 | LB/MMBTU | BACT |
| | dation catalyst SCR = selective catalytic reduction | | | | | | | |

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|----------|---|--------------------------|-------------|-------------------------------------|---|------------------|---------------------------------|--------------|
| ROLC ID | racinty rearie | Terrinic Date | Illioughput | PM _{2.5} (total) | Controls | Liniosion Liniic | Onics | Турс |
| AD 0455 | DIC DIVED CTEEL II C | 44 /07 /2040 | 00.7 | | CBF/GCP | 0.24 | NACA ALD AAAADTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC BIG RIVER STEEL LLC | 11/07/2018 11/07/2018 | | MMBTU/HR MMBTU/HR | CBF/GCP | | 3 X10^-4 LB/MMBTU 9 LB/MMBTU | BACT |
| AR-0155 | | 11/07/2018 | | · ' | | | | |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | | MMBTU/HR MMBTU/HR | CBF/GCP | | X10^-4 LB/MMBTU | BACT BACT |
| AR-0155 | BIG RIVER STEEL LLC | | | | • | | | |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 85.15 | MMBTU/HR | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | ŭ | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | | MMBtu/hr | CBF/GCP | | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | | MMBtu/hr | CBF/GCP | | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | | MMBtu/hr | CBF/GCP | | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | | MMBtu/hr | CBF/GCP | | B LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 0 | | Mist eliminator/GCP | | GR/DSCF | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 0 | | GCP/Energy efficient burners/CBF | | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | 02/14/2019 | _ | MMBTU/hr | GCP | | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | 02/14/2019 | | MMBTU/hr | GCP | | LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | | GCP | | LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | | GCP | | GR/DSCF | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | | Wet Scrubber System with mist eliminator | | GR/DSCF | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | 07/23/2020 | | MMBtu/hr | GCP | 7.6 | LB/MMSCF | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | 07/23/2020 | 60 | MMBtu/hr, combined | GCP | 7.6 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 50.4 | MMBtu/hr | GCP | 7.6 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 94 | MMBtu/hr | GCP | 7.6 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 104.3 | MMBtu/hr | GCP | 7.6 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 65.5 | MMBtu/hr | GCP | 7.6 | LB/MMSCF | BACT |
| LA-0364 | FG LA COMPLEX | 01/06/2020 | 0 | | CBF/GCP | | B LB/H | BACT |
| LA-0364 | FG LA COMPLEX | 01/06/2020 | 94 | mm btu/h | CBF/GCP | 0.63 | L LB/H | BACT |
| MI-0441 | LBWLERICKSON STATION | 12/21/2018 | 99 | MMBTU/H | GCP | 0.74 | LB/H | BACT |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | 80 | MMBTU/H | CBF/GCP | 7.6 | LB/MMSCF | BACT |
| MI-0447 | LBWLERICKSON STATION | 01/07/2021 | 50 | MMBTU/H | GCP | 0.4 | LB/H | BACT |
| OH-0379 | PETMIN USA INCORPORATED | 02/06/2019 | 0 | | Control Efficiency | 0.0063 | L LB/T | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 88 | MMBTU/H | CBF/GCP | 0.88 | B LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 112 | MMBTU/H | CBF/GCP | 1.12 | LB/H | BACT |
| TX-0851 | RIO BRAVO PIPELINE FACILITY | 12/17/2018 | 71.3 | MMBTU/HR | CBF/GCP | 0.0075 | LB/MMBTU | BACT |
| *VA-0333 | NORFOLK NAVAL SHIPYARD | 12/09/2020 | 76.6 | MMBtu/hr | | 0.0078 | 3 LB | BACT |
| | • | , <i>, ,</i> , | | PM _{2.5} (filterable only) | | | • | |
| *AL-0328 | PLANT BARRY | 11/09/2020 | 90.5 | MMBtu/hr | | 0.007 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 0 | , | CBF/GCP | | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| TX-0888 | ORANGE POLYETHYLENE PLANT | 04/23/2020 | 0 | | CBF/GCP | | LB/MMBTU | BACT |
| TX-0888 | ORANGE POLYETHYLENE PLANT | 04/23/2020 | 100 | MMBtu | CBF/GCP | | LB/MMBTU | BACT |
| TX-0888 | ORANGE POLYETHYLENE PLANT | 04/23/2020 | 100 | <u> </u> | CBF/GCP | | LB/MMBTU | BACT |
| | | ' ' | · | | hurning fuels SNCR = selective noncatalytic reduction | | | |

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|----------|--------------------------------|-------------|------------|-------------------------------------|---|----------------|-------------|------|
| | | | | Greenhouse Gases - CO ₂ | | | | |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 88.7 | MMBTU/HR | GCP/Minimum Boiler Efficiency | 117 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 0 | | CBF/GCP | 117 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 53.7 | MMBTU/HR | GCP/Minimum Boiler Efficiency | 117 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 53.7 | MMBTU/HR | GCP/Minimum Boiler Efficiency | 117 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 78.2 | MMBTU/HR | GCP | 117 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 85.15 | MMBTU/HR | GCP | 117 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | GCP | 117 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | GCP/Minimum Boiler Efficiency | 117 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | GCP | 117 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | GCP/Minimum Boiler Efficiency | 117 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | GCP | 117 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | GCP/Minimum Boiler Efficiency | 117 | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 117.9 | MMBtu/hr | GCP | 117 | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 66 | MMBtu/hr | GCP | 117 | LB/MMBTU | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 64 | MMBtu/hr | GCP | 117 | LB/MMBTU | BACT |
| | | | Greer | house Gases - CO ₂ equiv | alents | | | |
| *AL-0328 | PLANT BARRY | 11/09/2020 | 90.5 | MMBtu/hr | | 46416 | TPY | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | GCP | 117 | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | 02/14/2019 | 128 | MMBTU/hr | GCP | 121 | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | 02/14/2019 | 50.4 | MMBTU/hr | GCP | 121 | LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | | GCP | 121 | LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | | GCP | 121 | LB/MMBTU | BACT |
| IL-0130 | JACKSON ENERGY CENTER | 12/31/2018 | 96 | mmBtu/hr | GCP | 11250 | TONS/YEAR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | 07/23/2020 | 54 | MMBtu/hr | GCP | 27991 | TON/YR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | 07/23/2020 | 60 | MMBtu/hr, combined | GCP | 31101 | TON/YR | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 50.4 | MMBtu/hr | GCP | 26125 | TONS/YR | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 94 | MMBtu/hr | GCP | 48725 | TONS/YR | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 104.3 | MMBtu/hr | GCP | 54065 | TONS/YR | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 65.5 | MMBtu/hr | GCP | 33952 | TONS/YR | BACT |
| LA-0364 | FG LA COMPLEX | 01/06/2020 | 0 | | GCP | 5858 | TONS/YR | BACT |
| LA-0364 | FG LA COMPLEX | 01/06/2020 | 94 | mm btu/h | CBF/energy-efficient design options/GCP | 455475 | T/YR | BACT |
| MI-0441 | LBWLERICKSON STATION | 12/21/2018 | 99 | MMBTU/H | CBF/GCP/energy efficiency measures | 50776 | T/YR | BACT |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | 80 | MMBTU/H | Energy efficiency | 41031 | | BACT |
| MI-0447 | LBWLERICKSON STATION | 01/07/2021 | 50 | MMBTU/H | CBF/GCP/energy efficiency measures | 25644 | T/YR | BACT |
| OH-0379 | PETMIN USA INCORPORATED | 02/06/2019 | 0 | | GCP | 186.41 | | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | | MMBTU/H | CBF/energy efficient design | 10283.06 | , | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 112 | MMBTU/H | CBF/energy efficient design | 13087.2 | LB/H | BACT |
| *VA-0333 | NORFOLK NAVAL SHIPYARD | 12/09/2020 | 76.6 | MMBtu/hr | | 117.1 | LB | BACT |
| | | | | Sulfuric Acid Mist | | | | |
| IL-0130 | JACKSON ENERGY CENTER | 12/31/2018 | 96 | mmBtu/hr | GCP | 0.1 | POUNDS/HOUR | BACT |

⁽a) OxCat = oxidation catalyst, SCR = selective catalytic reduction, LNB = low-NOx burners, GCP = good combustion practices, CBF = clean burning fuels, SNCR = selective, noncatalytic reduction, CEMS = continuous emission monitoring system

| RBLC ID | Facility Name | Permit Date | Throughput | Units | Controls | Emission Limit Uni | its Type |
|----------|----------------------------|-------------|------------|----------|--|--------------------|----------|
| | | | | Opacity | | | |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 88.7 | MMBTU/HR | CBF/GCP | 5 % | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 0 | | CBF/GCP | 5 % | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 53.7 | MMBTU/HR | CBF/GCP | 5 % | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 53.7 | MMBTU/HR | CBF/GCP | 5 % | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 78.2 | MMBTU/HR | CBF/GCP | 5 % | BACT |
| AR-0155 | BIG RIVER STEEL LLC | 11/07/2018 | 85.15 | MMBTU/HR | CBF/GCP | 5 % | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | 5 % | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | 5 % | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | 5 % | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | 5 % | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | 5 % | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | 5 % | BACT |
| AR-0159 | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | CBF/GCP | 5 % | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 117.9 | MMBtu/hr | CBF/GCP | 5 % | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 58 | MMBtu/hr | CBF/GCP | 5 % | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 66 | MMBtu/hr | CBF/GCP | 5 % | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 64 | MMBtu/hr | CBF/GCP | 5 % | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 0 | | Mist eliminator/GCP | 5 % | BACT |
| AR-0168 | BIG RIVER STEEL LLC | 03/17/2021 | 0 | | GCP/Energy efficient burners/CBF | 5 % | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | 02/14/2019 | 128 | MMBTU/hr | GCP | 5 % | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | 02/14/2019 | 50.4 | MMBTU/hr | GCP | 5 % | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | | GCP | 5 % | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | | GCP | 5 % | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | 09/01/2021 | 0 | | Wet Scrubber System with mist eliminator | 10 % | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | 0 | | | 15 % | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | 0 | | | 15 % | BACT |

⁽a) OxCat = oxidation catalyst, SCR = selective catalytic reduction, LNB = low-NOx burners, GCP = good combustion practices, CBF = clean burning fuels, SNCR = selective, noncatalytic reduction, CEMS = continuous emission monitoring system

Table D-3 Removed Cooling Tower removed from Application

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|---------|--|-----------------------------|-------------|------------|----------|------------------|-----------------------|----------|----------|
| | <u>.</u> | Carbo | n Monoxide | | • | 1 | | • | |
| OK-0168 | Seminole Generating Station | O G AND E | 5/5/2015 | 40.4 | MMBtu/hr | GCP | 0.0075 | lb/MMBtu | BACT-PSD |
| | | | | | | | | | |
| IA-0106 | CF Industries Nitrogen, LLC - Port Neal Nitrogen Complex | CF INDUSTRIES NITROGEN, LLC | 7/12/2013 | 58.8 | MMBtu/hr | GCP, clean fuels | 0.0194 | lb/MMBtu | BACT-PSD |
| | | MIDWEST FERTILIZER | | | | | | | |
| IN-0263 | Midwest Fertilizer Company LLC | COMPANY LLC | 3/23/2017 | 70 | MMBtu/hr | GCP | 0.0365 | lb/MMBtu | BACT-PSD |
| | | | | | | | | | |
| IN-0285 | Whiting Clean Energy, Inc. | WHITING CLEAN ENERGY, INC. | 8/2/2017 | 0 | | None | 0.0380 | lb/MMBtu | BACT-PSD |
| | | INTERSTATE POWER AND | | | | | | | |
| IA-0107 | Marshalltown Generating Station | LIGHT | 4/14/2014 | 13.32 | MMBtu/hr | None | 0.0410 | lb/MMBtu | BACT-PSD |
| | | DYNO NOBEL LOUISIANA | | | | | | | |
| LA-0272 | Ammonia Production Facility | AMMONIA, LLC | 3/27/2013 | 59.4 | MMBtu/hr | GCP | 0.0500 | lb/MMBtu | BACT-PSD |
| | | LAKE CHARLES | | | | | | | |
| LA-0231 | Lake Charles Gasification Facility | COGENERATION, LLC | 6/22/2009 | 35 | MMBtu/hr | GCP | 0.0560 | lb/MMBtu | BACT-PSD |
| SC-0114 | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | 20.89 | MMBtu/hr | None | 0.0799 | lb/MMBtu | BACT-PSD |
| | | COMPETITIVE POWER | | | | | | | |
| | | VENTURES, INC./CPV | | | | | | | |
| MD-0040 | CPV St Charles | MARYLAND, LLC | 11/12/2008 | 1.7 | MMBtu/hr | None | 0.0800 | lb/MMBtu | BACT-PSD |
| MS-0092 | Emberclear GTL MS | EMBERCLEAR GTL MS LLC | 5/8/2014 | 12 | MMBtu/hr | None | 0.0800 | lb/MMBtu | BACT-PSD |
| MS-0092 | Emberclear GTL MS | EMBERCLEAR GTL MS LLC | 5/8/2014 | 13 | MMBtu/hr | None | 0.0800 | lb/MMBtu | BACT-PSD |
| SC-0114 | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | 75 | MMBtu/hr | GCP | 0.0800 | lb/MMBtu | BACT-PSD |
| MI-0421 | Grayling Particleboard | ARAUCO NORTH AMERICA | 8/26/2016 | 34 | MMBtu/hr | GCP | 0.0820 | lb/MMBtu | BACT-PSD |
| MI-0425 | Grayling Particleboard | ARAUCO NORTH AMERICA | 5/9/2017 | 38 | MMBtu/hr | GCP | 0.0820 | lb/MMBtu | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | 27 | MMBtu/hr | GCP | 0.0822 | lb/MMBtu | BACT-PSD |
| | | | | | | | | | |
| LA-0311 | Donaldsonville Nitrogen Complex | CF INDUSTRIES NITROGEN, LLC | 7/15/2013 | 94.5 | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| OK-0153 | Rose Valley Plant | SEMGAS LP | 3/1/2013 | 17.4 | MMBtu/hr | GCP | 0.0824 | lb/MMBtu | BACT-PSD |
| OK-0153 | Rose Valley Plant | SEMGAS LP | 3/1/2013 | 5.61 | MMBtu/hr | GCP | 0.0824 | lb/MMBtu | BACT-PSD |
| | | LAKE CHARLES | | | | | | | |
| LA-0231 | Lake Charles Gasification Facility | COGENERATION, LLC | 6/22/2009 | 56.9 | MMBtu/hr | GCP | 0.0824 | lb/MMBtu | BACT-PSD |
| | | LAKE CHARLES | | | | | | | |
| LA-0231 | Lake Charles Gasification Facility | COGENERATION, LLC | 6/22/2009 | 34.2 | MMBtu/hr | GCP | 0.0825 | lb/MMBtu | BACT-PSD |
| | | PRYOR PLANT CHEMICAL | | | | | | | |
| OK-0134 | Pryor Plant Chemical | COMPANY | 2/23/2009 | 20 | MMBtu/hr | GCP | 0.0825 | lb/MMBtu | BACT-PSD |
| | | PRYOR PLANT CHEMICAL | | | | | | | |
| OK-0134 | Pryor Plant Chemical | COMPANY | 2/23/2009 | 20 | MMBtu/hr | GCP | 0.0825 | lb/MMBtu | BACT-PSD |
| | | PRYOR PLANT CHEMICAL | | | | | | | |
| OK-0135 | Pryor Plant Chemical | COMPANY | 2/23/2009 | 20 | MMBtu/hr | GCP | 0.0825 | lb/MMBtu | BACT-PSD |
| | | COMMERCIAL METALS | | | | | | | |
| OK-0173 | CMC Steel Oklahoma | COMPANY | 1/19/2016 | 0 | | Clean fuels | 0.0840 | lb/MMBtu | BACT-PSD |
| SC-0112 | Nucor Steel - Berkeley | NUCOR STEEL | 5/5/2008 | 58 | MMBtu/hr | GCP, clean fuels | 0.0840 | lb/MMBtu | BACT-PSD |
| | | HOLLAND BOARD OF PUBLIC | | | <u> </u> | | | | |
| MI-0412 | Holland Board Of Public Works - East 5th Street | WORKS | 12/4/2013 | 3.7 | MMBtu/hr | GCP | 0.1108 | lb/MMBtu | BACT-PSD |
| | | HOLLAND BOARD OF PUBLIC | | | | | | | |
| MI-0424 | Holland Board Of Public Works - East 5th Street | WORKS | 12/5/2016 | 3.7 | MMBtu/hr | GCP | 0.1108 | lb/MMBtu | BACT-PSD |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|--------------------|--|--|-----------------------|-------------|----------------------|----------------------|---------------------|----------------------|----------------------|
| NOLC ID | rucinty Hume | | ases - Carbon Di | | Onits | Controls | LIIII33IOII LIIIIIC | Onics | Туре |
| | | Greenilouse G | ases - Carbon D | Oxide | | | | l | 1 |
| LA-0311 | Donaldsonville Nitrogen Complex | CF INDUSTRIES NITROGEN, LLC | 7/15/2013 | 94.5 | MMBtu/hr | GCP, clean fuels | 117 | lb/MMBtu | BACT-PSD |
| | | MIDWEST FERTILIZER | | | | | | | |
| IN-0263 | Midwest Fertilizer Company LLC | COMPANY LLC | 3/23/2017 | 70 | MMBtu/hr | GCP | 117 | lb/MMBtu | BACT-PSD |
| IA-0106 | CF Industries Nitrogen, LLC - Port Neal Nitrogen Complex | CF INDUSTRIES NITROGEN, LLC | 7/12/2013 | 58.8 | MMBtu/hr | GCP, clean fuels | 117 | lb/MMBtu | BACT-PSD |
| | | Greenhouse Gases - | Carbon Dioxide | Equivalents | | | | | |
| | | | | | | | | | |
| LA-0311 | Donaldsonville Nitrogen Complex | CF INDUSTRIES NITROGEN, LLC | 7/15/2013 | 94.5 | MMBtu/hr | GCP, clean fuels | 117 | lb/MMBtu | BACT-PSD |
| | | COMMERCIAL METALS | | | | | | | |
| OK-0173 | CMC Steel Oklahoma | COMPANY | 1/19/2016 | 0 | | Clean fuels | 120 | lb/MMBtu | BACT-PSD |
| IA-0106 | CF Industries Nitrogen, LLC - Port Neal Nitrogen Complex | CF INDUSTRIES NITROGEN, LLC | 7/12/2013 | 58.8 | MMBtu/hr | GCP, clean fuels | 345 | tpy | BACT-PSD |
| | | DYNO NOBEL LOUISIANA | | | | | | | |
| LA-0272 | Ammonia Production Facility | AMMONIA, LLC | 3/27/2013 | 59.4 | MMBtu/hr | GCP | 1,738 | tpy | BACT-PSD |
| | _ | HOLLAND BOARD OF PUBLIC | | | | | | | |
| MI-0412 | Holland Board Of Public Works - East 5th Street | WORKS | 12/4/2013 | 3.7 | MMBtu/hr | GCP | 1,934 | tpy | BACT-PSD |
| | III. III. I B I Of B. I P. W. I | HOLLAND BOARD OF PUBLIC | 42/5/2046 | 2 7 | AAAAD: // | 665 | 4.024 | | DA CT DCD |
| MI-0424 | Holland Board Of Public Works - East 5th Street | WORKS | 12/5/2016 | 3./ | MMBtu/hr | GCP | 1,934 | тру | BACT-PSD |
| IA-0107 | Marchalltown Congrating Station | INTERSTATE POWER AND LIGHT | 4/14/2014 | 12 22 | MMBtu/hr | None | 6,860 | tou | BACT-PSD |
| IA-0107 | Marshalltown Generating Station | INTERSTATE POWER AND | 4/14/2014 | 15.52 | IVIIVIBLU/III | None | 0,800 | гру | BACI-P3D |
| IA-0107 | Marshalltown Generating Station | LIGHT | 4/14/2014 | 13 32 | MMBtu/hr | None | 6,860 | tny | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | | MMBtu/hr | GCP, clean fuels | 13,848 | | BACT-PSD |
| MI-0421 | Grayling Particleboard | ARAUCO NORTH AMERICA | 8/26/2016 | | MMBtu/hr | GCP, clean fuels | 17,438 | tpy | BACT-PSD |
| MI-0425 | Grayling Particleboard | ARAUCO NORTH AMERICA | 5/9/2017 | | MMBtu/hr | GCP, clean fuels | 19,490 | | BACT-PSD |
| | . , , , | TINKER AIR FORCE BASE | 5/5/252 | | | | | -1-7 | |
| OK-0164 | Midwest City Air Depot | LOGISTICS CENTER | 1/8/2015 | 0 | MMBtu/hr | GCP, clean fuels | 153,716 | tpy | BACT-PSD |
| | , , | Nitro | gen Oxides | | · · · · · · | • | | | ' |
| | | INTERSTATE POWER AND | | | | | | | |
| IA-0107 | Marshalltown Generating Station | LIGHT | 4/14/2014 | 13.32 | MMBtu/hr | None | 0.0130 | lb/MMBtu | BACT-PSD |
| | | CHUGACH ELECTRIC | | | | | | | |
| AK-0071 | International Station Power Plant | ASSOCIATION, INC. | 12/20/2010 | 12.5 | MMBtu/hr | LNB, FGR | 0.0305 | lb/MMBtu | BACT-PSD |
| OK-0153 | Rose Valley Plant | SEMGAS LP | 3/1/2013 | | MMBtu/hr | LNB | | lb/MMBtu | BACT-PSD |
| OK-0153 | Rose Valley Plant | SEMGAS LP | 3/1/2013 | 17.4 | MMBtu/hr | LNB | 0.0450 | lb/MMBtu | BACT-PSD |
| SC-0114 | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | 75 | MMBtu/hr | LNB | 0.0476 | lb/MMBtu | BACT-PSD |
| | | PRYOR PLANT CHEMICAL | | | | | | | |
| OK-0134 | Pryor Plant Chemical | COMPANY | 2/23/2009 | 20 | MMBtu/hr | LNB, GCP | 0.0490 | lb/MMBtu | BACT-PSD |
| | | PRYOR PLANT CHEMICAL | | | | | | l | |
| OK-0135 | Pryor Plant Chemical | COMPANY | 2/23/2009 | 20 | MMBtu/hr | LNB, GCP | 0.0490 | lb/MMBtu | BACT-PSD |
| OB 0040 | Carty Plant | DODTI AND CENTRAL FLECTRIC | 12/20/2010 | 24 | NANAD+ /l | LND | 0.0405 | Ib /NANAD±: | DACT DCD |
| OR-0048 | Carty Plant | PORTLAND GENERAL ELECTRIC ARAUCO NORTH AMERICA | 12/29/2010 | | MMBtu/hr MMBtu/hr | LNB | | lb/MMBtu | BACT-PSD |
| MI-0425 MI-0421 | Grayling Particleboard Grayling Particleboard | ARAUCO NORTH AMERICA | 5/9/2017 8/26/2016 | | MMBtu/hr | LNB, GCP LNB, GCP | 0.0500 0.0500 | lb/MMBtu lb/MMBtu | BACT-PSD BACT-PSD |
| 1711-0421 | Graying Farticesoard | ANAUCU NUNTITI AIVIENICA | 0/20/2010 | 34 | iviivibtu/III | LIND, GCP | 0.0300 | ID/ IVIIVIDLU | DAC1-P3D |
| IN-0285 | Whiting Clean Energy, Inc. | WHITING CLEAN ENERGY, INC. | 8/2/2017 | 0 | | None | 0.0500 | lb/MMBtu | BACT-PSD |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|-----------|--|-----------------------------|--------------|------------|----------------|------------------|-----------------------|---------------|----------------------|
| | | | | | | | | | |
| LA-0244 | Lake Charles Chemical Complex - Lab Unit | SASOL NORTH AMERICA, INC. | 11/29/2010 | | MMBtu/hr | LNB | 0.0819 | lb/MMBtu | BACT-PSD |
| SC-0114 | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | 20.89 | MMBtu/hr | None | 0.0953 | lb/MMBtu | BACT-PSD |
| | | LAKE CHARLES | | | | | | | |
| LA-0231 | Lake Charles Gasification Facility | COGENERATION, LLC | 6/22/2009 | 34.2 | MMBtu/hr | GCP | 0.0980 | lb/MMBtu | BACT-PSD |
| | | LAKE CHARLES | | | | | | | |
| LA-0231 | Lake Charles Gasification Facility | COGENERATION, LLC | 6/22/2009 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | 27 | MMBtu/hr | GCP | 0.0981 | lb/MMBtu | BACT-PSD |
| | | COMMERCIAL METALS | | | | | | | |
| OK-0173 | CMC Steel Oklahoma | COMPANY | 1/19/2016 | 0 | | Clean fuels | 0.1000 | lb/MMBtu | BACT-PSD |
| | | COMPETITIVE POWER | | | | | | | |
| | | VENTURES, INC./CPV | | | | | | | |
| | CPV St Charles | MARYLAND, LLC | 11/12/2008 | | MMBtu/hr | None | | lb/MMBtu | BACT-PSD |
| SC-0112 | Nucor Steel - Berkeley | NUCOR STEEL | 5/5/2008 | | MMBtu/hr | LNB | 0.1000 | lb/MMBtu | BACT-PSD |
| FL-0356 | Okeechobee Clean Energy Center | FLORIDA POWER & LIGHT | 3/9/2016 | 10 | MMBtu/hr | GCP | 0.1000 | lb/MMBtu | BACT-PSD |
| | | LAKE CHARLES | | | | | | | |
| LA-0231 | Lake Charles Gasification Facility | COGENERATION, LLC | 6/22/2009 | 35 | MMBtu/hr | GCP | 0.1100 | lb/MMBtu | BACT-PSD |
| | | | | | | | | | |
| LA-0244 | Lake Charles Chemical Complex - Lab Unit | SASOL NORTH AMERICA, INC. | 11/29/2010 | 21 | MMBtu/hr | LNB | 0.1290 | lb/MMBtu | BACT-PSD |
| | | ASSOCIATED ELECTRIC | . / / | | | | | | |
| OK-0129 | Chouteau Power Plant | COOPERATIVE INC | 1/23/2009 | 18.8 | MMBtu/hr | None | 0.1436 | lb/MMBtu | BACT-PSD |
| | | HOLLAND BOARD OF PUBLIC | | | | | | | |
| MI-0424 | Holland Board Of Public Works - East 5th Street | WORKS | 12/5/2016 | 3.7 | MMBtu/hr | GCP | 0.1486 | lb/MMBtu | BACT-PSD |
| | | HOLLAND BOARD OF PUBLIC | | | | | | | |
| MI-0412 | Holland Board Of Public Works - East 5th Street | WORKS | 12/4/2013 | 3./ | MMBtu/hr | GCP | 0.1486 | lb/MMBtu | BACT-PSD |
| | Miles I Selling Consequent | MIDWEST FERTILIZER | 0/00/0047 | | | 000 | 2 4 2 2 2 | / | |
| IN-0263 | Midwest Fertilizer Company LLC | COMPANY LLC | 3/23/2017 | /0 | MMBtu/hr | GCP | 0.1802 | lb/MMBtu | BACT-PSD |
| | A to B Lotte . For the | DYNO NOBEL LOUISIANA | 2/27/2042 | 50.4 | 1 4 1 4 D 1 /1 | 665 | 0.2466 | U. /a.a.a.a. | DACT DCD |
| LA-0272 | Ammonia Production Facility | AMMONIA, LLC | 3/27/2013 | 59.4 | MMBtu/hr | GCP | 0.2466 | lb/MMBtu | BACT-PSD |
| | | MIDWEST FERTILIZER | ulate Matter | | I | I | | l | |
| IN-0263 | Midwest Fertilizer Company LLC | COMPANY LLC | 3/23/2017 | 70 | MMBtu/hr | GCP | 0.0019 | lb/MMBtu | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | | MMBtu/hr | GCP | 0.0019 | lb/MMBtu | BACT-PSD BACT-PSD |
| 1011-0423 | illueck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | 21 | IVIIVIBLU/III | GCP | 0.0020 | ID/IVIIVIBLU | BACI-P3D |
| IA-0106 | CF Industries Nitrogen, LLC - Port Neal Nitrogen Complex | CF INDUSTRIES NITROGEN, LLC | 7/12/2013 | E0 0 | MMBtu/hr | GCP, clean fuels | 0.0024 | lb/MMBtu | BACT-PSD |
| IA-0106 | er industries Nitrogen, LLC - Fort Near Nitrogen Complex | COMPETITIVE POWER | 7/12/2013 | 36.6 | IVIIVIBLU/III | GCP, Clean rueis | 0.0024 | ID/IVIIVIBLU | BACT-P3D |
| | | VENTURES, INC./CPV | | | | | | | |
| MD 0040 | CPV St Charles | MARYLAND, LLC | 11/12/2008 | 1 7 | MMBtu/hr | None | 0.0070 | lb/MMBtu | BACT-PSD |
| 1010-0040 | or v st chanes | HOLLAND BOARD OF PUBLIC | 11/12/2008 | 1.7 | IVIIVIBLU/III | INUITE | 0.0070 | io, iviivibtu | DVC1-L2D |
| MI-0424 | Holland Board Of Public Works - East 5th Street | WORKS | 12/5/2016 | 2 7 | MMBtu/hr | GCP | 0.0070 | lb/MMBtu | BACT-PSD |
| 1911-0424 | THORATA BOOK OF THOME WORKS - LOST STILL STREET | HOLLAND BOARD OF PUBLIC | 12/3/2010 | 3.7 | IVIIVIDEU/III | Julia | 0.0070 | io, iviivibtu | DACI-F3D |
| MI-0412 | Holland Board Of Public Works - East 5th Street | WORKS | 12/4/2013 | 27 | MMBtu/hr | GCP | 0 0070 | lb/MMBtu | BACT-PSD |
| SC-0114 | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | | MMBtu/hr | None | 0.0070 | lb/MMBtu | BACT-PSD BACT-PSD |
| SC-0114 | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | | MMBtu/hr | None | 0.0072 | lb/MMBtu | BACT-PSD |
| 30-0114 | or Alleridate El | CHUGACH ELECTRIC | 11/23/2008 | /3 | IVIIVIDEA/III | INOTIC | 0.0072 | io, iviivibtu | DACI-F 3D |
| AK-0071 | International Station Power Plant | ASSOCIATION, INC. | 12/20/2010 | 12 5 | MMBtu/hr | GCP | 0.0072 | lb/MMBtu | BACT-PSD |
| MI-0421 | Grayling Particleboard | ARAUCO NORTH AMERICA | 8/26/2016 | | MMBtu/hr | GCP | 0.0072 | lb/MMBtu | BACT-PSD |
| MI-0421 | Grayling Particleboard | ARAUCO NORTH AMERICA | 5/9/2017 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD BACT-PSD |
| 1411 0423 | oraying randicioudia | AND TO NOT THE ANIETICA | 3/3/2017 | 36 | iviivibtu/iii | 301 | 0.0073 | ואוועוועוועו | BACT 13D |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|---------|--|-----------------------------|-------------|------------|----------|------------------|-----------------------|----------|----------|
| | | PRYOR PLANT CHEMICAL | | | | | | | |
| OK-0135 | Pryor Plant Chemical | COMPANY | 2/23/2009 | 20 | MMBtu/hr | None | 0.0075 | lb/MMBtu | BACT-PSD |
| | | INTERSTATE POWER AND | | | | | | | |
| IA-0107 | Marshalltown Generating Station | LIGHT | 4/14/2014 | 13.32 | MMBtu/hr | None | 0.0080 | lb/MMBtu | BACT-PSD |
| | | | PM10 | | | | | | |
| | | | | | | | | | |
| OR-0048 | Carty Plant | PORTLAND GENERAL ELECTRIC | 12/29/2010 | 91 | MMBtu/hr | Clean fuels | 0.0024 | lb/MMBtu | BACT-PSD |
| | | COMPETITIVE POWER | | | | | | | |
| | | VENTURES, INC./CPV | | | | | | | |
| | CPV St Charles | MARYLAND, LLC | 11/12/2008 | | MMBtu/hr | None | | lb/MMBtu | BACT-PSD |
| | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | | MMBtu/hr | None | | lb/MMBtu | BACT-PSD |
| | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | | MMBtu/hr | None | | lb/MMBtu | BACT-PSD |
| SC-0112 | Nucor Steel - Berkeley | NUCOR STEEL | 5/5/2008 | | MMBtu/hr | GCP, clean fuels | | lb/MMBtu | BACT-PSD |
| MI-0421 | Grayling Particleboard | ARAUCO NORTH AMERICA | 8/26/2016 | 34 | MMBtu/hr | GCP | 0.0005 | lb/MMBtu | BACT-PSD |
| MI-0425 | Grayling Particleboard | ARAUCO NORTH AMERICA | 5/9/2017 | 38 | MMBtu/hr | GCP | 0.0005 | lb/MMBtu | BACT-PSD |
| | | LAKE CHARLES | | | | | | | |
| LA-0231 | Lake Charles Gasification Facility | COGENERATION, LLC | 6/22/2009 | 35 | MMBtu/hr | GCP | 0.0009 | lb/MMBtu | BACT-PSD |
| | | | | | | | | | |
| IA-0106 | CF Industries Nitrogen, LLC - Port Neal Nitrogen Complex | CF INDUSTRIES NITROGEN, LLC | 7/12/2013 | 58.8 | MMBtu/hr | GCP, clean fuels | 0.0024 | lb/MMBtu | BACT-PSD |
| | | CHUGACH ELECTRIC | | | | | | | |
| AK-0071 | International Station Power Plant | ASSOCIATION, INC. | 12/20/2010 | 12.5 | MMBtu/hr | GCP | 0.0072 | lb/MMBtu | BACT-PSD |
| | | LAKE CHARLES | | | | | | | |
| LA-0231 | Lake Charles Gasification Facility | COGENERATION, LLC | 6/22/2009 | 34.2 | MMBtu/hr | GCP | 0.0073 | lb/MMBtu | BACT-PSD |
| | | LAKE CHARLES | | | | | | | |
| LA-0231 | Lake Charles Gasification Facility | COGENERATION, LLC | 6/22/2009 | 56.9 | MMBtu/hr | GCP | 0.0074 | lb/MMBtu | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | 27 | MMBtu/hr | GCP | 0.0074 | lb/MMBtu | BACT-PSD |
| | | MIDWEST FERTILIZER | | | | | | | |
| IN-0263 | Midwest Fertilizer Company LLC | COMPANY LLC | 3/23/2017 | 70 | MMBtu/hr | GCP | 0.0075 | lb/MMBtu | BACT-PSD |
| | | HOLLAND BOARD OF PUBLIC | | | | | | | |
| MI-0412 | Holland Board Of Public Works - East 5th Street | WORKS | 12/4/2013 | 3.7 | MMBtu/hr | GCP | 0.0075 | lb/MMBtu | BACT-PSD |
| | | HOLLAND BOARD OF PUBLIC | | | | | | | |
| MI-0424 | Holland Board Of Public Works - East 5th Street | WORKS | 12/5/2016 | 3.7 | MMBtu/hr | GCP | 0.0075 | lb/MMBtu | BACT-PSD |
| | | PRYOR PLANT CHEMICAL | | | | | | | |
| OK-0134 | Pryor Plant Chemical | COMPANY | 2/23/2009 | 20 | MMBtu/hr | Clean fuels | 0.0075 | lb/MMBtu | BACT-PSD |
| | | PRYOR PLANT CHEMICAL | | | | | | | |
| OK-0135 | Pryor Plant Chemical | COMPANY | 2/23/2009 | 20 | MMBtu/hr | None | 0.0075 | lb/MMBtu | BACT-PSD |
| | | COMMERCIAL METALS | | | | | | | |
| OK-0173 | CMC Steel Oklahoma | COMPANY | 1/19/2016 | 0 | | Clean fuels | 0.0076 | lb/MMBtu | BACT-PSD |
| | | DYNO NOBEL LOUISIANA | | | | | | | |
| LA-0272 | Ammonia Production Facility | AMMONIA, LLC | 3/27/2013 | 59.4 | MMBtu/hr | GCP | 0.0089 | lb/MMBtu | BACT-PSD |
| | | | | | | | | | |
| LA-0244 | Lake Charles Chemical Complex - Lab Unit | SASOL NORTH AMERICA, INC. | 11/29/2010 | 87.3 | MMBtu/hr | None | 0.0099 | lb/MMBtu | BACT-PSD |
| | | | | | | | | | |
| LA-0244 | Lake Charles Chemical Complex - Lab Unit | SASOL NORTH AMERICA, INC. | 11/29/2010 | 21 | MMBtu/hr | None | 0.0100 | lb/MMBtu | BACT-PSD |
| | | | PM2.5 | | | | | | |
| MI-0421 | Grayling Particleboard | ARAUCO NORTH AMERICA | 8/26/2016 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| MI-0425 | Grayling Particleboard | ARAUCO NORTH AMERICA | 5/9/2017 | 38 | MMBtu/hr | GCP | 0.0004 | lb/MMBtu | BACT-PSD |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | Emission Limit | Units | Туре |
|--------------------|--|-----------------------------|-----------------------|------------|----------------------|---------------------------|-----------------------|----------------------|----------------------|
| | | | | | | | | | |
| IA-0106 | CF Industries Nitrogen, LLC - Port Neal Nitrogen Complex | CF INDUSTRIES NITROGEN, LLC | 7/12/2013 | 58.8 | MMBtu/hr | GCP, clean fuels | 0.0024 | lb/MMBtu | BACT-PSD |
| | | CHUGACH ELECTRIC | | | | | | | |
| AK-0071 | International Station Power Plant | ASSOCIATION, INC. | 12/20/2010 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | 27 | MMBtu/hr | GCP | 0.0074 | lb/MMBtu | BACT-PSD |
| | | MIDWEST FERTILIZER | | | | | | | |
| IN-0263 | Midwest Fertilizer Company LLC | COMPANY LLC | 3/23/2017 | 70 | MMBtu/hr | GCP | 0.0075 | lb/MMBtu | BACT-PSD |
| | | HOLLAND BOARD OF PUBLIC | | | | | | | |
| MI-0412 | Holland Board Of Public Works - East 5th Street | WORKS | 12/4/2013 | 3.7 | MMBtu/hr | GCP | 0.0075 | lb/MMBtu | BACT-PSD |
| | | HOLLAND BOARD OF PUBLIC | | | | | | | |
| MI-0424 | Holland Board Of Public Works - East 5th Street | WORKS | 12/5/2016 | 3.7 | MMBtu/hr | GCP | 0.0075 | lb/MMBtu | BACT-PSD |
| | | COMMERCIAL METALS | | | | | | | |
| OK-0173 | CMC Steel Oklahoma | COMPANY | 1/19/2016 | 0 | | Clean fuels | 0.0076 | lb/MMBtu | BACT-PSD |
| | | DYNO NOBEL LOUISIANA | | | | | | | |
| LA-0272 | Ammonia Production Facility | AMMONIA, LLC | 3/27/2013 | 59.4 | MMBtu/hr | GCP | 0.0089 | lb/MMBtu | BACT-PSD |
| | · | Volatile Or | ganic Compoun | ds | • | | | <u> </u> | , |
| | | | · | | | | | | |
| IA-0106 | CF Industries Nitrogen, LLC - Port Neal Nitrogen Complex | CF INDUSTRIES NITROGEN, LLC | 7/12/2013 | 58.8 | MMBtu/hr | GCP, clean fuels | 0.0014 | lb/MMBtu | BACT-PSD |
| | 5 , | SEMINOLE ELECTRIC | , , , | | | , , , , , , , , , , , , , | | ., | |
| FL-0364 | Seminole Generating Station | COOPERATIVE, INC. | 3/21/2018 | 9.9 | MMBtu/hr | None | 0.0050 | lb/MMBtu | BACT-PSD |
| SC-0114 | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| SC-0114 | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | | MMBtu/hr | None | | lb/MMBtu | BACT-PSD |
| | 2 | ASSOCIATED ELECTRIC | ==,==,==== | | | | | , | |
| OK-0129 | Chouteau Power Plant | COOPERATIVE INC | 1/23/2009 | 18.8 | MMBtu/hr | None | 0.0053 | lb/MMBtu | BACT-PSD |
| | Grayling Particleboard | ARAUCO NORTH AMERICA | 8/26/2016 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| MI-0425 | Grayling Particleboard | ARAUCO NORTH AMERICA | 5/9/2017 | | MMBtu/hr | GCP | | lb/MMBtu | BACT-PSD |
| 1411 0423 | oraying randeboara | MIDWEST FERTILIZER | 3/3/2017 | 30 | IVIIVIBCU/III | GCI | 0.0054 | ib/ iviivibtu | BACT 13B |
| IN-0263 | Midwest Fertilizer Company LLC | COMPANY LLC | 3/23/2017 | 70 | MMBtu/hr | GCP | 0.0054 | lb/MMBtu | BACT-PSD |
| 114 0203 | what i cramzer company the | COMMERCIAL METALS | 3/23/2017 | 70 | iviivibta/iii | GCI | 0.0034 | Ib/ WIIVIBCO | BACTISB |
| OK-0173 | CMC Steel Oklahoma | COMPANY | 1/19/2016 | 0 | | Clean fuels | 0.0055 | lb/MMBtu | BACT-PSD |
| SC-0112 | Nucor Steel - Berkeley | NUCOR STEEL | 5/5/2008 | 50 | MMBtu/hr | GCP, clean fuels | | lb/MMBtu | BACT-PSD |
| 30-0112 | Tracol Steel - Delikeley | PRYOR PLANT CHEMICAL | 3/3/2006 | 30 | iviivibtu/iii | GCF, Clean ruels | 0.0033 | io, iviivibtu | שאכו-ו אט |
| OK-0134 | Pryor Plant Chemical | COMPANY | 2/23/2009 | 20 | MMBtu/hr | GCP | 0.0055 | lb/MMBtu | BACT-PSD |
| UK-0154 | Fryor Flant Chemical | PRYOR PLANT CHEMICAL | 2/23/2009 | 20 | IVIIVIDLU/III | GCF | 0.0055 | ID/IVIIVIDLU | BACI-POU |
| OK 0135 | Pryor Plant Chemical | COMPANY | 2/22/2000 | 30 | NANAD+/b~ | None | 0.0055 | Ib/NANAD+ | DACT DCD |
| OK-0135 MI-0423 | , | INDECK NILES, LLC | 2/23/2009 1/4/2017 | | MMBtu/hr MMBtu/hr | None GCP | | lb/MMBtu lb/MMBtu | BACT-PSD BACT-PSD |
| IVII-U4Z3 | Indeck Niles, LLC | DYNO NOBEL LOUISIANA | 1/4/201/ | 27 | iviiviBtu/iif | GCP | 0.0056 | ID/IVIIVIBLU | DACI-PSU |
| 14 0272 | Ammonio Droduction Facility | | 2/27/2012 | FO 4 | N 4 N 4 D + / b :- | | 0.0004 | | DACT DCD |
| LA-0272 | Ammonia Production Facility | AMMONIA, LLC | 3/27/2013 | 59.4 | MMBtu/hr | | 0.0064 | lb/MMBtu | BACT-PSD |
| | Halland Broad Of B. H. Wallan Fran Fill Co. | HOLLAND BOARD OF PUBLIC | 42/4/2012 | <u> </u> | | 665 | 0.0001 | | DA CT DCD |
| MI-0412 | Holland Board Of Public Works - East 5th Street | WORKS | 12/4/2013 | 3.7 | MMBtu/hr | GCP | 0.0081 | lb/MMBtu | BACT-PSD |
| | | HOLLAND BOARD OF PUBLIC | | _ | l | | | | |
| MI-0424 | Holland Board Of Public Works - East 5th Street | WORKS | 12/5/2016 | 3.7 | MMBtu/hr | GCP | 0.0081 | lb/MMBtu | BACT-PSD |
| | | TINKER AIR FORCE BASE | | | 1 | | | | |
| OK-0164 | Midwest City Air Depot | LOGISTICS CENTER | 1/8/2015 | 0 | MMBtu/hr | GCP, clean fuels | 7.1 | tpy | BACT-PSD |

| | | | | | | | Emission | | |
|----------|----------------------------------|--|-------------|-------------------|--------------------|-----------------------|----------|------------|------|
| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls ^A | Limit | Units | Туре |
| | | | Nitro | gen Oxides | | | | | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 32 | MMBtu/hr | LNB/GCP | 0.030 | LB/MMBTU | BACT |
| *AL-0329 | COLBERT COMBUSTION TURBINE PLANT | TENNESSEE VALLEY AUTHORITY | 09/21/2021 | 10 | MMBtu/hr | | 0.01 | 1 LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | 0 | | LNB/CBF/GCP | 0.09 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | 53.7 | MMBTU/HR | LNB/CBF/GCP | 0.03 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | 53.7 | MMBTU/HR | LNB/CBF/GCP | 0.03 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | LNB/CBF/GCP | 0.09 | 7 LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | LNB/CBF/GCP | 0.09 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | LNB/CBF/GCP | 0.03 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | SCR/LNB/CBF/GCP | 0.03 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | LNB/CBF/GCP | 0.03 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | LNB/CBF/GCP | 0.08 | B LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | LNB/CBF/GCP | 0.03 | LB/MMBTU | BACT |
| AR-0167 | LION OIL COMPANY | DELEK US | 12/01/2020 | 40 | MMBtu/hr | Ultra-LNB/GCP | 1.9 | B/HR | BACT |
| AR-0167 | LION OIL COMPANY | DELEK US | 12/01/2020 | 50 | MMBtu/hr | GCP | 5.3 | B LB/HR | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 0 | | LNB | 0.06 | B LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 3 | MMBTU/hr each | LNB | 0.: | 1 LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 50.4 | MMBTU/hr | LNB | 0.03 | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 15 | MMBTU/hr each | LNB | 0.: | 1 LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 09/01/2021 | 0 | | LNB | 0.03 | LB/MMBTU | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 40 | MMBtu/hr, combined | LNB/GCP | 70 | LB/MMSCF | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 22 | MMBtu/hr, combined | LNB/GCP | 50 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 40 | MMBtu/hr, total | GCP | 100 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 50.4 | MMBtu/hr | LNB/GCP | 3! | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 18 | MMBtu/hr, each | LNB/GCP | 50 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 23 | MMBtu/hr | LNB/GCP | 50 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 14.5 | MMBtu/hr, each | LNB/GCP | 50 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 3 | MMBtu/hr | LNB/GCP | 7(| LB/MMSCF | BACT |
| LA-0364 | FG LA COMPLEX | FG LA LLC | 01/06/2020 | 0 | | LNB | 0.0 | LB/MMBTU | BACT |
| LA-0377 | TOKAI ADDIS FACILITY | TOKAI CARBON CB LTD. | 05/27/2020 | 12 | MW | LNB/GCP | 0.0 | B LB/MMBTU | BACT |
| LA-0377 | TOKAI ADDIS FACILITY | TOKAI CARBON CB LTD. | 05/27/2020 | 5.88 | MM scf/h | LNB/FGR/GCP | 300 | PPM | BACT |
| MI-0440 | MICHIGAN STATE UNIVERSITY | MICHIGAN STATE UNIVERSITY | 05/22/2019 | 25 | MMBTU/H | LNB/GCP | 0.0 | LB/MMBTU | BACT |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | 7 | MMBTU/H | LNB/GCP | 0.030 | LB/MMBTU | BACT |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 27 | MMBTU/H | GCP | 1.33 | LB/H | BACT |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 50 | MMBTU/H | LNB/FGR/GCP | 30 | PPM | BACT |
| OH-0379 | PETMIN USA INCORPORATED | PETMIN USA INCORPORATED | 02/06/2019 | 15.17 | MMBTU/H | LNB/CBF/GCP | 0.634 | 4 LB/H | BACT |
| OH-0379 | PETMIN USA INCORPORATED | PETMIN USA INCORPORATED | 02/06/2019 | 15 | MMBTU/H | GCP/CBF | 2.12 | LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 1.2 | MMBTU/H | GCP/CBF | 0.12 | LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 16 | MMBTU/H | GCP/CBF | 1.0 | 5 LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 9.5 mmbtu/hr GCP/ | | GCP/CBF | 0.9 | 5 LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | | | LNB/CBF/GCP | 2.: | 1 LB/H | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | | | LNB/GCP | 43.8 | B LB/HR | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | 0 | | LNB/GCP | 68.8 | | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | 1.5 | mmBTU/hr | GCP | 0.: | 1 LB/MMBTU | BACT |

| | | | | | | | Emission | |
|---------------------|--|---|--------------------------|-----------------|----------------------------|-------------------------|------------------------------------|--------------|
| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls ^A | Limit Units | Туре |
| | | | | n Monoxide | | | | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | | MMBtu/hr | GCP/CBF | 0.087 LB/MMBTU | BACT |
| *AL-0329 AR-0155 | COLBERT COMBUSTION TURBINE PLANT BIG RIVER STEEL LLC | TENNESSEE VALLEY AUTHORITY BIG RIVER STEEL LLC | 09/21/2021 11/07/2018 | 10 | MMBtu/hr | GCP/CBF | 0.08 LB/MMBTU 0.0824 LB/MMBTU | BACT BACT |
| AR-0155 AR-0155 | BIG RIVER STEEL LLC BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | | MMBTU/HR | GCP/CBF GCP/CBF | 0.0824 LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | | MMBTU/HR | GCP/CBF | 0.0824 LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 33.7 |) | GCP/CBF | 0.0824 LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| | GCP/CBF | 0.0824 LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (|) | GCP/CBF | 0.0824 LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| | GCP/CBF | 0.0824 LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| | GCP/CBF | 0.0824 LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | C | 1 | GCP/CBF | 0.0824 LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | | | GCP/CBF | 0.0824 LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | (| A AA ADTII //b b | GCP | 0.084 LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | | MMBTU/hr each | GCP | 0.084 LB/MMBTU 0.075 LB/MMBTU | BACT BACT |
| AR-0171 AR-0171 | NUCOR STEEL ARKANSAS NUCOR STEEL ARKANSAS | NUCOR CORPORATION NUCOR CORPORATION | 02/14/2019 02/14/2019 | | MMBTU/hr MMBTU/hr each | GCP GCP | 0.075 LB/MMBTU 0.084 LB/MMBTU | BACT |
| *AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION NUCOR CORPORATION | 09/01/2021 | 13 | IVIIVIBTO/III eacii | GCP | 0.084 LB/MMBTU | BACT |
| IL-0130 | JACKSON ENERGY CENTER | JACKSON GENERATION, LLC | 12/31/2018 | 13 | mmBtu/hour | GCP | 0.08 LB/MMBTU | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | | MMBtu/hr, combined | GCP | 84 LB/MMSCF | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | | MMBtu/hr, combined | GCP | 84 LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | | MMBtu/hr, total | GCP | 84 LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 50.4 | MMBtu/hr | GCP | 61 LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 18 | MMBtu/hr, each | GCP | 84 LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 23 | MMBtu/hr | GCP | 84 LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | | MMBtu/hr, each | GCP | 84 LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 13 | MMBtu/hr | GCP | 84 LB/MMSCF | BACT |
| LA-0364 | FG LA COMPLEX | FG LA LLC | 01/06/2020 | (| | GCP | 0.037 LB/MMBTU | BACT |
| MI-0440 | MICHIGAN STATE UNIVERSITY | MICHIGAN STATE UNIVERSITY | 05/22/2019 | | MMBTU/H | GCP | 0.08 LB/MMBTU | BACT |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | | MMBTU/H | GCP | 0.037 LB/MMBTU | BACT |
| *MI-0445 MI-0447 | INDECK NILES, LLC LBWLERICKSON STATION | INDECK NILES, LLC LANSING BOARD OF WATER AND LIGHT | 11/26/2019 | | MMBTU/H MMBTU/H | GCP GCP | 1.11 LB/H 50 PPM | BACT BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 01/07/2021 09/27/2019 | | MMBTU/H | GCP/CBF | 0.02 LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | | MMBTU/H | GCP/CBF | 0.32 LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | | mmbtu/hr | GCP/CBF | 0.19 LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | | MMBTU/H | CBF/baffle burners/GCP | 2.1 LB/H | BACT |
| SC-0192 | CANFOR SOUTHERN PINE - CONWAY MILL | CANFOR SOUTHERN PINE | 05/21/2019 | (|) | Work Practice Standards | 0.0375 LB/MMBTU | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | (| | GCP | 58.3 LB/HR | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | (| | GCP | 45.8 LB/HR | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | | mmBTU/hr | GCP | 0.082 LB/MMBTU | BACT |
| | | | | ganic Compounds | | | | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 32 | MMBtu/hr | GCP/CBF | 0.0057 LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | (| | GCP/CBF | 0.0054 LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | | MMBTU/HR | GCP/CBF GCP/CBF | 0.0054 LB/MMBTU | BACT |
| AR-0155 AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | 53.7 | MMBTU/HR | GCP/CBF GCP/CBF | 0.054 LB/MMBTU 0.0054 LB/MMBTU | BACT BACT |
| AR-0159 AR-0159 | BIG RIVER STEEL LLC BIG RIVER STEEL LLC | BIG RIVER STEEL LLC BIG RIVER STEEL LLC | 04/05/2019 04/05/2019 | (| | GCP/CBF GCP/CBF | 0.0054 LB/MMBTU 0.0054 LB/MMBTU | BACT |
| AR-0159 AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| | GCP/CBF GCP/CBF | 0.0054 LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| | GCP/CBF GCP/CBF | 0.0054 LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| | GCP/CBF | 0.0054 LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | | | GCP/CBF | 0.0054 LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| i | GCP/CBF | 0.0054 LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | (| | GCP | 0.0076 LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | | MMBTU/hr each | GCP | 0.0076 LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | | MMBTU/hr | GCP | 0.0026 LB/HR | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 15 | MMBTU/hr each | GCP | 0.0055 LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 09/01/2021 | (| | GCP | 0.0055 LB/MMBTU | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | | MMBtu/hr, combined | GCP | 5.5 LB/MMSCF | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | | MMBtu/hr, combined | GCP | 5.5 LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | | MMBtu/hr, total | GCP GCP | 5.5 LB/MMSCF | BACT |
| KY-0115 KY-0115 | NUCOR STEEL GALLATIN, LLC NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC NUCOR STEEL GALLATIN, LLC | 04/19/2021 04/19/2021 | | MMBtu/hr MMBtu/hr, each | GCP | 5.5 LB/MMSCF 5.5 LB/MMSCF | BACT BACT |
| KY-0115 KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | | MMBtu/hr | GCP | 5.5 LB/MMSCF 5.5 LB/MMSCF | BACT |
| K1-0113 | INOCON STEEL GALLATIN, ELC | MOCON STELL GALLATIN, LLC | 04/13/2021 | ZS | TIVIIVIDEU/III | 901 | J.J LD/IVIIVIJCF | DACI |

| | | | | | | | Emission | | |
|----------|---|---|-------------------|--------------------|--------------------|------------------------------------|----------|------------|------|
| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls ^A | Limit | Units | Туре |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 14.5 | MMBtu/hr, each | GCP | 5.5 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 3 | MMBtu/hr | GCP | 5.5 | LB/MMSCF | BACT |
| LA-0364 | FG LA COMPLEX | FG LA LLC | 01/06/2020 | (|) | GCP | 4.02 | LB/H | BACT |
| MI-0440 | MICHIGAN STATE UNIVERSITY | MICHIGAN STATE UNIVERSITY | 05/22/2019 | 25 | MMBTU/H | GCP | 0.005 | LB/MMBTU | BACT |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | 7 | MMBTU/H | GCP | 0.025 | LB/MMBTU | BACT |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 27 | MMBTU/H | GCP | 0.07 | 7 LB/H | BACT |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 50 | MMBTU/H | GCP | 0.3 | B LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 1.2 | MMBTU/H | GCP/CBF | 0.01 | L LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 16 | MMBTU/H | GCP/CBF | 0.09 | LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 9.5 | mmbtu/hr | GCP/CBF | 0.05 | LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 30 | MMBTU/H | GCP/CBF | 0.17 | 7 LB/H | BACT |
| SC-0192 | CANFOR SOUTHERN PINE - CONWAY MILL | CANFOR SOUTHERN PINE | 05/21/2019 | (| | Work Practice Standards | 0.0054 | LB/MMBTU | BACT |
| *WI-0292 | GREEN BAY PACKAGING INC. â€"MILL DIVISION | GREEN BAY PACKAGING INC. â€"MILL DIVISION | 04/01/2019 | 20 | mmBTU/hr | LNB/GCP | 0.0055 | LB/MMBTU | BACT |
| | | Gre | eenhouse Gases -0 | Carbon Dioxide Equ | uivalents | | | | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 32 | MMBtu/hr | GCP/CBF | 117.1 | LB/MMBTU | BACT |
| *AL-0329 | COLBERT COMBUSTION TURBINE PLANT | TENNESSEE VALLEY AUTHORITY | 09/21/2021 | 10 | MMBtu/hr | | 117.1 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| , | GCP | | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | (|) | GCP | 12: | L LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 3 | MMBTU/hr each | GCP | 123 | L LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 50.4 | MMBTU/hr | GCP | | L LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 15 | MMBTU/hr each | GCP | 123 | LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 09/01/2021 | (| | GCP | 12: | L LB/MMBTU | BACT |
| IL-0130 | JACKSON ENERGY CENTER | JACKSON GENERATION, LLC | 12/31/2018 | 13 | mmBtu/hour | GCP | 6700 | TONS/YEAR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 40 | MMBtu/hr, combined | GCP | 20734 | TON/YR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 22 | MMBtu/hr, combined | GCP | 11404 | TON/YR | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 40 | MMBtu/hr, total | GCP | 20734 | TONS/YR | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 50.4 | MMBtu/hr | GCP | 26125 | TONS/YR | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 18 | MMBtu/hr, each | GCP | 12675 | TONS/YR | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 23 | MMBtu/hr | GCP | 11922 | TONS/YR | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 14.5 | MMBtu/hr, each | GCP | 15032 | TONS/YR | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 3 | MMBtu/hr | GCP | 30 | TONS/YR | BACT |
| LA-0364 | FG LA COMPLEX | FG LA LLC | 01/06/2020 | (| | CBF/energy efficient design/GCP | 5858 | TONS/YR | BACT |
| MI-0440 | MICHIGAN STATE UNIVERSITY | MICHIGAN STATE UNIVERSITY | 05/22/2019 | 25 | MMBTU/H | GCP/CBF | 12822 | T/YR | BACT |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | 7 | MMBTU/H | Energy Efficiency | 3590 | T/YR | BACT |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 27 | MMBTU/H | Energy Efficiency Measures/CBF | 13848 | T/YR | BACT |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 50 | MMBTU/H | Energy Efficiency Measures/CBF/GCP | 25644 | 1 T/YR | BACT |
| OH-0379 | PETMIN USA INCORPORATED | PETMIN USA INCORPORATED | 02/06/2019 | 15.17 | MMBTU/H | GCP/CBF | 1784 | LB/H | BACT |
| OH-0379 | PETMIN USA INCORPORATED | PETMIN USA INCORPORATED | 02/06/2019 | 15 | MMBTU/H | GCP/CBF | 1764 | 1 LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 1.2 | MMBTU/H | CBF/Energy Efficient Design | 140.22 | LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 16 | MMBTU/H | CBF/Energy Efficient Design | 1869.65 | LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 9.5 | mmbtu/hr | CBF/Energy Efficient Design | 1110.1 | L LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 30 | MMBTU/H | CBF/Energy Efficient Design | 3505.59 | LB/H | BACT |

| | | | | | | | Emission | | |
|----------|----------------------------------|--|----------------------|-------------------------|--------------------|--|----------|-----------------|------|
| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls ^A | Limit | Units | Туре |
| | | | PIV | l ₁₀ (total) | | | | | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 32 | MMBtu/hr | GCP/CBF | 0.0079 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | (| ĺ | GCP/CBF | 0.0075 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | 53.7 | MMBTU/HR | GCP/CBF | 0.0019 | LB/MMBTU | BACT |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | 53.7 | MMBTU/HR | GCP/CBF | 6.8 | X10^-4 LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| | GCP/CBF | 0.0075 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| | GCP/CBF | 0.0019 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| | GCP/CBF | 0.0012 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| i | GCP/CBF | 0.0019 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| | GCP/CBF | 0.0075 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| | GCP/CBF | 0.0007 | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | (| | GCP | 0.0076 | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 3 | MMBTU/hr each | GCP | 0.0076 | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 50.4 | MMBTU/hr | GCP | 0.0076 | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 15 | MMBTU/hr each | GCP | 0.0076 | LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 09/01/2021 | (| | GCP | 0.0076 | GR/DSCF | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 09/01/2021 | (| | Wet Scrubber System with mist eliminator | 0.0013 | LB/MMBTU | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 40 | MMBtu/hr, combined | GCP | 7.6 | LB/MMSCF | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 22 | MMBtu/hr, combined | GCP | 7.6 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 40 | MMBtu/hr, total | GCP | 7.6 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 50.4 | MMBtu/hr | GCP | 7.6 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 18 | MMBtu/hr, each | GCP | 7.6 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 23 | MMBtu/hr | GCP | 7.6 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 14.5 | MMBtu/hr, each | GCP | 7.6 | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 3 | MMBtu/hr | GCP | 7.6 | LB/MMSCF | BACT |
| LA-0364 | FG LA COMPLEX | FG LA LLC | 01/06/2020 | (| | GCP/CBF | 0.03 | LB/H | BACT |
| MI-0440 | MICHIGAN STATE UNIVERSITY | MICHIGAN STATE UNIVERSITY | 05/22/2019 | 25 | MMBTU/H | GCP | 0.008 | LB/MMBTU | BACT |
| MI-0442 | THOMAS TOWNSHIP ENERGY, LLC | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | 7 | MMBTU/H | GCP/CBF | 7.6 | LB/MMSCF | BACT |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 27 | MMBTU/H | GCP | 0.1 | LB/H | BACT |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 50 | MMBTU/H | GCP | 0.74 | LB/H | BACT |
| OH-0379 | PETMIN USA INCORPORATED | PETMIN USA INCORPORATED | 02/06/2019 | 15.17 | MMBTU/H | GCP/CBF | 0.113 | LB/H | BACT |
| OH-0379 | PETMIN USA INCORPORATED | PETMIN USA INCORPORATED | 02/06/2019 | 15 | MMBTU/H | GCP/CBF | 0.112 | LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 1.2 | MMBTU/H | GCP/CBF | 0.004 | LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 16 | MMBTU/H | GCP/CBF | 0.05 | LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 9.5 | mmbtu/hr | GCP/CBF | 0.03 | LB/H | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | 30 | MMBTU/H | GCP/CBF | 0.3 | LB/H | BACT |
| | | | PM ₁₀ (fi | ilterable only) | | | | | |
| *AL-0329 | COLBERT COMBUSTION TURBINE PLANT | TENNESSEE VALLEY AUTHORITY | 09/21/2021 | | MMBtu/hr | | 0.008 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | (| , | GCP/CBF | | LB/MMBTU | BACT |

| DDI C ID | Facility Manager | G | Daniel Data | Thursday | 11-2- | Countrie! A | Emission | Harte | Ŧ |
|--------------------|--|--|--------------------------|------------------------|--------------------------|--|----------|--------------------------|--------------|
| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls ^A | Limit | Units | Туре |
| **** | To a company and a same | | | _{2.5} (total) | Is as any # | Toon tone | 0.007 | ali a /a aa aa w | In a corr |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | | MMBtu/hr | GCP/CBF | 0.007 | <u> </u> | BACT |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | | MMBTU/HR | GCP/CBF | 0.001 | | BACT |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | 53. | MMBTU/HR | GCP/CBF | 6.0 | , , | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | |) | GCP/CBF | 0.007 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | |) | GCP/CBF | 0.001 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | |) | GCP/CBF | 0.001 | <u> </u> | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | | , | GCP/CBF | 0.001 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | |) | GCP/CBF | 0.007 | LB/MMBTU | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | |) | GCP/CBF | 0.000 | 7 LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | |) AAAADTII/b | GCP | 0.007 | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | | MMBTU/hr each | GCP | 0.007 | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | | MMBTU/hr | GCP | 0.007 | LB/MMBTU | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 13 | MMBTU/hr each | GCP | 0.007 | LB/MMBTU | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 09/01/2021 | |) | GCP | 0.007 | GR/DSCF | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 09/01/2021 | (| AAAADa. /b.s. saasbissad | Wet Scrubber System with mist eliminator | 0.001 | GR/DSCF | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | | MMBtu/hr, combined | GCP | 7.0 | <u> </u> | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | | MMBtu/hr, combined | GCP | | LB/MMSCF | BACT |
| KY-0115 KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | | MMBtu/hr, total | GCP GCP | | LB/MMSCF | BACT BACT |
| | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | | MMBtu/hr | | | LB/MMSCF | |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | | MMBtu/hr, each | GCP | _ | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | | MMBtu/hr | GCP | | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 14.: | MMBtu/hr, each | GCP | | LB/MMSCF | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | | MMBtu/hr | GCP | | 5 LB/MMSCF 3 LB/H | BACT BACT |
| LA-0364 MI-0440 | FG LA COMPLEX MICHIGAN STATE UNIVERSITY | FG LA LLC MICHIGAN STATE UNIVERSITY | 01/06/2020 05/22/2019 | | MMBTU/H | GCP/CBF GCP | 0.00 | | BACT |
| MI-0440 | THOMAS TOWNSHIP ENERGY, LLC | THOMAS TOWNSHIP ENERGY, LLC | 08/21/2019 | | MMBTU/H | GCP/CBF | | 5 LB/MMSCF | BACT |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | | MMBTU/H | GCP GCP | | 1 LB/H | BACT |
| MI-0445 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | | MMBTU/H | GCP | | LB/H | BACT |
| OH-0379 | PETMIN USA INCORPORATED | PETMIN USA INCORPORATED | 02/06/2019 | | MMBTU/H | GCP/CBF | | B LB/H | BACT |
| OH-0379 | PETMIN USA INCORPORATED PETMIN USA INCORPORATED | PETMIN USA INCORPORATED PETMIN USA INCORPORATED | 02/06/2019 | | MMBTU/H | GCP/CBF GCP/CBF | | 2 LB/H | BACT |
| OH-0379 OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | | MMBTU/H | GCP/CBF GCP/CBF | 0.00 | <u> </u> | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | | MMBTU/H | GCP/CBF GCP/CBF | 0.00 | <u> </u> | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | | mmbtu/hr | GCP/CBF | 0.0 | | BACT |
| OH-0381 | NORTHSTAR BLUESCOPE STEEL, LLC | NORTHSTAR BLUESCOPE STEEL, LLC | 09/27/2019 | | MMBTU/H | GCP/CBF | | B LB/H | BACT |
| 011-0381 | NORTHSTAR BEOESCOPE STEEL, ELC | NONTHSTAN BEDESCOPE STEEL, EEC | | ilterable only) | JIVIIVID I O/III | ОСЕУСЫ | | эјсолі | IBACI |
| *AL-0329 | COLBERT COMBUSTION TURBINE PLANT | TENNESSEE VALLEY AUTHORITY | 09/21/2021 | | MMBtu/hr | T | 0.00 | В LB/ММВТИ | BACT |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | | 10 |) IVIIVIBLU/III | GCP/CBF | 0.007 | <u> </u> | BACT |
| AR-0155 AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 04/05/2019 | |) | GCP/CBF GCP/CBF | 0.007 | | BACT |
| AK-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | | casa Carban Dian | / | GCP/CBF | 0.007 | D LB/IVIIVIB I U | BACI |
| AD 0155 | DIC DIVED STEEL LLC | DIC DIVED STEEL LIC | | ases -Carbon Diox | de N | GCP/CBF | 111 | ZILD /NANADTLI | BACT |
| AR-0155 AR-0155 | BIG RIVER STEEL LLC BIG RIVER STEEL LLC | BIG RIVER STEEL LLC BIG RIVER STEEL LLC | 11/07/2018 11/07/2018 | F2 - | MMBTU/HR | GCP/Boiler Efficiency | | 7 LB/MMBTU 7 LB/MMBTU | BACT |
| AR-0155 AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | | · | GCP/Boiler Efficiency | | 7 LB/MMBTU | BACT |
| AR-0155 AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 53.7 MMBTU/HR | | GCP/Boller Efficiency | | 7 LB/MMBTU | BACT |
| AR-0159 AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | | | GCP/Boiler Efficiency | | 7 LB/MMBTU | BACT |
| AR-0159 AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | | | GCP/Boller Efficiency | | 7 LB/MMBTU | BACT |
| AR-0159 AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | | | GCP/Boiler Efficiency | _ | 7 LB/MMBTU | BACT |
| AR-0159 AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | | | GCP/Boller Efficiency | | 7 LB/MMBTU | BACT |
| AR-0159 AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | | | GCP/Boiler Efficiency | | 7 LB/MMBTU | BACT |
| VIV-0133 | DIG NIVEN STEEL LLC | DIO MYEN STEEL LLC | | ic Acid Mist | <u>'I</u> | OCF/Boilet Efficiency | 1 11 | LD/ MINIDIO | IDACI |
| IL-0130 | JACKSON ENERGY CENTER | JACKSON GENERATION, LLC | 12/31/2018 | | mmBtu/hour | GCP | 0.01 | 4 POUNDS/HOUR | BACT |
| | | 3F = clean burning fuels, FGR = flue gas recirculation | 12/31/2010 | 1. | Sta/noui | | 5.01 | 551105/11001 | DACI |

| | | | | | | | Emission | | |
|----------|----------------------------|----------------------------|-------------|------------|---------------|--|----------|-------|------|
| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls ^A | Limit | Units | Type |
| | | | (| Opacity | | | | | |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | 0 | | GCP/CBF | 5 | % | BACT |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | 53.7 | MMBTU/HR | GCP/CBF | 5 | % | BACT |
| AR-0155 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 11/07/2018 | 53.7 | MMBTU/HR | GCP/CBF | 5 | % | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | GCP/CBF | 5 | % | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | GCP/CBF | 5 | % | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | GCP/CBF | 5 | % | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | GCP/CBF | 5 | % | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | GCP/CBF | 5 | % | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | GCP/CBF | 5 | % | BACT |
| AR-0159 | BIG RIVER STEEL LLC | BIG RIVER STEEL LLC | 04/05/2019 | 0 | | GCP/CBF | 5 | % | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 0 | | GCP | 5 | % | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 3 | MMBTU/hr each | GCP | 5 | % | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 50.4 | MMBTU/hr | GCP | 5 | % | BACT |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 15 | MMBTU/hr each | GCP | 5 | % | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 09/01/2021 | 0 | | GCP | 5 | % | BACT |
| *AR-0172 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 09/01/2021 | 0 | | Wet Scrubber System with mist eliminator | 10 | % | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | 0 | | GCP/LNB | 15 | % | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | 0 | | GCP/LNB | 15 | % | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | 1.5 | mmBTU/hr | GCP | 10 | % | BACT |

⁽a) GCP = good combustion practices, LNB = low-NOx burners, CBF = clean burning fuels, FGR = flue gas recirculation

Emergency Generator Table D-5 - RBLC Results for Emergency-Fire-Pump

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|---------|---|----------------------------------|---------------|------------|-------|-----------------|---------------|---------|--------------------|
| | | | Carbon Mon | | | | | | • |
| | | WESTERN FARMERS ELECTRIC | | | | | | | |
| OK-0154 | Mooreland Generating Sta | COOPERATIVE | 7/2/2013 | 1,341 | HP | GCP | 0.00 | g/hp-hr | BACT-PSD |
| | | | | | | | | | |
| TX-0728 | Peony Chemical Manufacturing Facility | BASF | 4/1/2015 | 1,500 | HP | NSPS Compliance | 0.01 | g/hp-hr | Other Case-by-Case |
| | | | | | | | | | |
| PA-0278 | Moxie Liberty LLC/Asylum Power Pl T | MOXIE ENERGY LLC | 10/10/2012 | | | None | 0.13 | g/hp-hr | Other Case-by-Case |
| | | | | | | | | | |
| LA-0231 | Lake Charles Gasification Facility | LAKE CHARLES COGENERATION, LLC | 6/22/2009 | 1,341 | HP | NSPS Compliance | 0.21 | g/hp-hr | BACT-PSD |
| | | 99 CIVIL ENGINEER SQUADRON OF | | | | | | | |
| NV-0047 | Nellis Air Force Base | USAF | 2/26/2008 | 1,350 | hP | Turbocharger | 0.22 | g/hp-hr | Other Case-by-Case |
| | | WOLVERINE POWER SUPPLY | | | | | | | |
| MI-0402 | Sumpter Power Plant | COOPERATIVE INC. | 11/17/2011 | 732 | HP | GCP | | g/hp-hr | BACT-PSD |
| NY-0104 | CPV Valley Energy Center | CPV VALLEY LLC | 8/1/2013 | | | GCP | | g/hp-hr | BACT-PSD |
| NV-0050 | MGM Mirage | MGM MIRAGE | 11/30/2009 | 2,206 | HP | Turbocharger | 0.82 | g/hp-hr | LAER |
| SC-0115 | GP Clarendon LP | GP CLARENDON LP | 2/10/2009 | 1,400 | HP | GCP | 0.98 | g/hp-hr | BACT-PSD |
| SC-0114 | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | | HP | None | 0.98 | g/hp-hr | BACT-PSD |
| PA-0291 | Hickory Run Energy Station | HICKORY RUN ENERGY LLC | 4/23/2013 | 1,135 | hP | None | 2.31 | g/hp-hr | Other Case-by-Case |
| | | | | | | | | | |
| NV-0049 | Harrah's Operating Company, Inc. | HARRAH'S OPERATING COMPANY, INC. | 8/20/2009 | 1,232 | | Turbocharger | | g/hp-hr | Other Case-by-Case |
| AL-0301 | Nucor Steel Tuscaloosa, Inc. | NUCOR STEEL TUSCALOOSA, INC. | 7/22/2014 | 800 | HP | None | 2.49 | g/hp-hr | BACT-PSD |
| | | MID AMERICAN STEEL AND WIRE | | | | | | | |
| OK-0128 | Mid American Steel Rolling Mill | COMPANY | 9/8/2008 | 1,200 | HP | None | 2.49 | g/hp-hr | BACT-PSD |
| | Energy Answers Arecibo Puerto Rico | | | | | | | | |
| PR-0009 | Renewable Energy Project | ENERGY ANSWERS ARECIBO, LLC | 4/10/2014 | | hP | None | 2.60 | Or I | BACT-PSD |
| MI-0406 | Renaissance Power LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | 1,000 | | GCP | 2.60 | g/hp-hr | BACT-PSD |
| LA-0313 | St. Charles Power Station | ENTERGY LOUISIANA, LLC | 8/31/2016 | 2,584 | | NSPS Compliance | | g/hp-hr | BACT-PSD |
| IN-0158 | St. Joseph Energy Center, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | | HP | GCP | 2.60 | g/hp-hr | BACT-PSD |
| IN-0158 | St. Joseph Energy Center, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 2,012 | HP | GCP | 2.60 | g/hp-hr | BACT-PSD |
| | Endicott Production Facility, Liberty | BRITISH PETROLEUM EXPLORATION | | | | | | | |
| AK-0066 | Development Project | ALASKA (BPXA) | 6/15/2009 | 1,041 | | GCP | 2.60 | g/hp-hr | BACT-PSD |
| MD-0044 | Cove Point LNG Terminal | DOMINION COVE POINT LNG, LP | 6/9/2014 | 1,550 | HP | GCP | 2.60 | g/hp-hr | BACT-PSD |
| | Ni sa saila Bai at Flantais Canadati a Blanta | ENTER CY LOUISIANIA LL C | 0/46/2044 | 4 050 | | 000 01 5 1 | 2.50 | , , | DA OT DOD |
| LA-0254 | Ninemile Point Electric Generating Plant | | 8/16/2011 | 1,250 | | GCP, Clean Fuel | | U. 1 | BACT-PSD |
| CA-1191 | Victorville 2 Hybrid Power Project | CITY OF VICTORVILLE | 3/11/2010 | , | kW | None | 2.60 | g/hp-hr | BACT-PSD |
| CA-1212 | Palmdale Hybrid Power Project | CITY OF PALMDALE | 10/18/2011 | 2,683 | HP | None | 2.60 | g/hp-hr | BACT-PSD |
| | Moundsville Combined Cycle Power | | 44 /24 /224 4 | 2.016 | | | 2.50 | , , | DAGT DOD |
| WV-0025 | Plant | MOUNDSVILLE POWER, LLC | 11/21/2014 | 2,016 | HP | None | 2.60 | g/hp-hr | BACT-PSD |
| | | FOOTPRINT POWER SALEM HARBOR | 1 /20 /201 1 | 750 | | | 2.50 | /, , | |
| | Salem Harbor Station Redevelopment | DEVELOPMENT LP | 1/30/2014 | 750 | | None | | g/hp-hr | Other Case-by-Case |
| AK-0082 | Point Thomson Production Facility | EXXON MOBIL CORPORATION | 1/23/2015 | | HP | None | 2.60 | g/hp-hr | BACT-PSD |
| LA-0288 | Lake Charles Chemical Complex | SASOL CHEMICALS (USA) LLC | 5/23/2014 | 2,682 | HP | GCP | 2.61 | g/hp-hr | BACT-PSD |
| | Lake Charles Chemical Complex LDPE | | | | | | | , . | |
| LA-0296 | Unit | SASOL CHEMICALS (USA) LLC | 5/23/2014 | 2,682 | HP | GCP | 2.61 | g/hp-hr | BACT-PSD |
| | | | 614/554 | | | 0.00 | | , . | D 4 CT DCD |
| IN-0173 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | 3,600 | HP | GCP | 2.61 | g/hp-hr | BACT-PSD |

Emergency Generator Table D-5 - RBLC Results for Emergency-Fire Pump

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|---------|--|----------------------------------|--------------------|----------------|--------|-----------------|---------------|----------|----------|
| IN-0179 | Ohio Valley Resources, LLC | OHIO VALLEY RESOURCES, LLC | 9/25/2013 | 4,690 | HP | GCP | 2.61 | g/hp-hr | BACT-PSD |
| | | | | • | | | | | |
| IN-0180 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | 3,600 | HP | GCP | 2.61 | g/hp-hr | BACT-PSD |
| | | | | • | | | | | |
| IN-0263 | Midwest Fertilizer Company LLC | MIDWEST FERTILIZER COMPANY LLC | 3/23/2017 | 3,600 | HP | GCP | 2.61 | g/hp-hr | BACT-PSD |
| OH-0352 | Oregon Clean Energy Center | ARCADIS, US, INC. | 6/18/2013 | 2,250 | kW | NSPS Compliance | 3.50 | g/hp-hr | BACT-PSD |
| | Shady Hills Generating Station | SHADY HILLS POWER COMPANY | 1/12/2009 | 2,500 | | NSPS Compliance | | g/hp-hr | BACT-PSD |
| | - | ASSOCIATED ELECTRIC COOPERATIVE | | | | | | | |
| OK-0129 | Chouteau Power Plant | INC | 1/23/2009 | 2,200 | HP | None | 3.50 | g/kW-hr | BACT-PSD |
| MI-0421 | Grayling Particleboard | ARAUCO NORTH AMERICA | 8/26/2016 | 1,600 | kW | GCP | 3.50 | g/kW-hr | BACT-PSD |
| MI-0425 | Grayling Particleboard | ARAUCO NORTH AMERICA | 5/9/2017 | 1,500 | kW | GCP | 3.50 | g/kW-hr | BACT-PSD |
| MI-0425 | Grayling Particleboard | ARAUCO NORTH AMERICA | 5/9/2017 | 1,500 | kW | GCP | 3.50 | g/kW-hr | BACT-PSD |
| LA-0251 | Flopam Inc. Facility | FLOPAM INC. | 4/26/2011 | 1,175 | hP | None | 3.50 | g/kW-hr | BACT-PSD |
| | | | | | | | | | |
| IA-0095 | Tate & Lyle Ingredients Americas, Inc. | | 9/19/2008 | 700 | kW | None | 3.50 | g/kW-hr | BACT-PSD |
| OH-0317 | Ohio River Clean Fuels, LLC | OHIO RIVER CLEAN FUELS, LLC | 11/20/2008 | 2,922 | НР | GCP | 3.50 | g/kW-hr | BACT-PSD |
| IA-0105 | Iowa Fertilizer Company | IOWA FERTILIZER COMPANY | 10/26/2012 | | kW | GCP | 3.50 | g/kW-hr | BACT-PSD |
| | CF Industries Nitrogen, LLC - Port Neal | | | • | | | | | |
| IA-0106 | Nitrogen Complex | CF INDUSTRIES NITROGEN, LLC | 7/12/2013 | | | GCP | 3.50 | g/kW-hr | BACT-PSD |
| MI-0389 | Karn Weadock Generating Complex | CONSUMERS ENERGY | 12/29/2009 | 2,000 | kW | GCP, Clean Fuel | | g/kW-hr | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | 2,922 | hP | GCP | 3.50 | g/kW-hr | BACT-PSD |
| | Highlands Biorefinery And Cogeneration | | | | | | | | |
| FL-0332 | 1 - | HIGHLANDS ENVIROFUELS (HEF), LLC | 9/23/2011 | 2,682 | hP | NSPS Compliance | 3.50 | g/kW-hr | BACT-PSD |
| ID-0018 | Langley Gulch Power Plant | IDAHO POWER COMPANY | 6/25/2010 | 750 | kW | GCP | | g/kW-hr | BACT-PSD |
| IL-0114 | Cronus Chemicals, LLC | CRONUS CHEMICALS, LLC | 9/5/2014 | 3,755 | НР | NSPS Compliance | 3.50 | g/kW-hr | BACT-PSD |
| AK-0076 | Point Thomson Production Facility | EXXON MOBIL CORPORATION | 8/20/2012 | 1,750 | | None | | g/kW-hr | BACT-PSD |
| | Sweet Sorghum-To-Ethanol Advanced | SOUTHEAST RENEWABLE FUELS (SRF), | | • | | | | | |
| FL-0322 | Biorefinery | LLC | 12/23/2010 | 2,000 | kW | None | 3.50 | g/kW-hr | BACT-PSD |
| FL-0356 | Okeechobee Clean Energy Center | FLORIDA POWER & LIGHT | 3/9/2016 | 3,300 | | GCP | | g/kW-hr | BACT-PSD |
| | | DYNO NOBEL LOUISIANA AMMONIA, | | • | | | | | |
| LA-0272 | Ammonia Production Facility | LLC | 3/27/2013 | 1,200 | HP | GCP | 3.50 | g/kW-hr | BACT-PSD |
| SC-0113 | Pyramax Ceramics, LLC | PYRAMAX CERAMICS, LLC | 2/8/2012 | 757 | HP | NSPS Compliance | 3.50 | g/kW-hr | BACT-PSD |
| FL-0346 | Lauderdale Plant | FLORIDA POWER & LIGHT | 4/22/2014 | 3,100 | kW | GCP | 3.50 | g/kW-hr | BACT-PSD |
| LA-0204 | Plaquemine PVC Plant | SHINTECH LOUISIANA LLC | 2/27/2009 | 1,389 | НР | GCP | 0.85 | lb/MMBtu | BACT-PSD |
| | | Greenho | ouse Gases - C | Carbon Dioxide | | | 1 | | • |
| | | | | | | | | | |
| IN-0173 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | 3,600 | HP | GCP | 526.39 | g/hp-hr | BACT-PSD |
| IN-0179 | Ohio Valley Resources, LLC | OHIO VALLEY RESOURCES, LLC | 9/25/2013 | 4,690 | | GCP | | g/hp-hr | BACT-PSD |
| | | | | | | | | | |
| IN-0180 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | 3,600 | HP | GCP | 526.39 | g/hp-hr | BACT-PSD |
| IA-0105 | lowa Fertilizer Company | IOWA FERTILIZER COMPANY | 10/26/2012 | 2,000 | kW | GCP | 1.55 | g/kW-hr | BACT-PSD |
| | CF Industries Nitrogen, LLC - Port Neal | | | - | | | | | |
| IA-0106 | Nitrogen Complex | CF INDUSTRIES NITROGEN, LLC | 7/12/2013 | | | GCP | 703.07 | g/kW-hr | BACT-PSD |
| | - | • | | | | | | | |
| LA-0254 | Ninemile Point Electric Generating Plant | ENTERGY LOUISIANA LLC | 8/16/2011 | 1,250 | HP | GCP | 163.00 | lb/MMBtu | BACT-PSD |
| | | Greenhouse G | ases - Carbon | Dioxide Equiv | alents | | • | | • |

Emergency Generator Table D-5 - RBLC Results for Emergency-Fire-Pump

| N | Sumpter Power Plant | WOLVERINE POWER SUPPLY | | <u> </u> | | | | | • |
|------------|--|---------------------------------|------------------------|----------------|--------------|-------------------|----------|--------------------|--------------------------------|
| N | | | | | | | | | |
| N | | COOPERATIVE INC. | 11/17/2011 | 732 | HP | GCP | 444.05 | g/hp-hr | BACT-PSD |
| | Moundsville Combined Cycle Power | | | | | | | <u> </u> | |
| | • | MOUNDSVILLE POWER, LLC | 11/21/2014 | 2,016 | НР | None | 543.67 | g/hp-hr | BACT-PSD |
| | | FOOTPRINT POWER SALEM HARBOR | | | | | | 6/ ·· F ··· | |
| MA-0039 S | Salem Harbor Station Redevelopment | DEVELOPMENT LP | 1/30/2014 | 750 | kW | None | 162.85 | lh/MMRtu | BACT-PSD |
| 1417 0033 | Salem Harbor Station Redevelopment | DEVELOT MENT E | Sulfuric Acid | | 11.00 | i tone | 102.03 | 110/ IVIIVIDEA | Brief 100 |
| Т | | FOOTPRINT POWER SALEM HARBOR | | | | I | | | |
| MA-0039 S | Salem Harbor Station Redevelopment | DEVELOPMENT LP | 1/30/2014 | 750 | k\\\ | None | 5 AAE-0A | g/kW-hr | BACT-PSD |
| WIA-0033 3 | Salem Harbor Station Redevelopment | DEVELOTIVIENT ET | 1/30/2014 | 730 | KVV | None | J.44L-04 | g/KVV-III | DACI-13D |
| NY-0101 C | Cornell Combined Heat & Power Project | CORNELL UNIVERSITY | 3/12/2008 | 1,000 | ۲ /۸/ | Clean fuels | 9.07F-04 | g/kW-hr | BACT-PSD |
| | CPV Valley Energy Center | CPV VALLEY LLC | 8/1/2013 | , | KVV | Clean fuels | | · · | BACT-PSD |
| 111-0104 | Cr v valley Ellergy Celiter | CFV VALLET ELC | Nitrogen O | | | Clean rueis | 3.001-03 | ID/IVIIVIBLU | BACIFOD |
| | | I | Niti ogen O | kiues | | | T | | |
| TX-0728 P | Peony Chemical Manufacturing Facility | BASF | 4/1/2015 | 1,500 | нр | NSPS Compliance | 0.02 | g/hp-hr | LAER |
| | Energy Answers Arecibo Puerto Rico | DAGI | 4/1/2013 | 1,300 | | 1431 3 Compliance | 0.02 | g/ IIP-III | LALIN |
| | 0, | ENERGY ANSWERS ARECIBO, LLC | 4/10/2014 | 670 | hD | None | 2 05 | g/hp-hr | BACT-PSD |
| | Pacific Bell | PACIFIC BELL | | | | NSPS Compliance | | g/hp-hr | |
| | GP CLARENDON LP | GP CLARENDON LP | 12/5/2011 2/10/2009 | 3,634 1,400 | | GCP | | g/hp-hr | Other Case-by-Case BACT-PSD |
| | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | 1,400 | | None | | g/np-nr g/hp-hr | BACT-PSD |
| 3C-0114 C | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | 1,400 | пР | None | 3.70 | g/np-nr | BACT-P3D |
| 64 4220 (| Can Diago International Aireant | CAN DIECO INTERNATIONAL AIRPORT | 40/2/2044 | 4 004 | | NICRC Consultance | 2.00 | - /h - h - | Other Core by Core |
| | | SAN DIEGO INTERNATIONAL AIRPORT | 10/3/2011 | 1,881 | | NSPS Compliance | | g/hp-hr | Other Case-by-Case |
| PA-0291 H | Hickory Run Energy Station | HICKORY RUN ENERGY LLC | 4/23/2013 | 1,135 | hP | None | 3.95 | g/hp-hr | Other Case-by-Case |
| | | CITY OF SAN DIEGO PUD (PUMP | - /2 /22 / 2 | | | | | , . | |
| CA-1219 C | City Of San Diego PUD (Pump Station 1) | STATION 1) | 7/9/2012 | 2,722 | НР | NSPS Compliance | 4.00 | g/hp-hr | Other Case-by-Case |
| | | | 2 /22 /224 7 | 2.500 | | | | , , | D 4 CT DCD |
| IN-0263 N | Midwest Fertilizer Company LLC | MIDWEST FERTILIZER COMPANY LLC | 3/23/2017 | 3,600 | нР | GCP | 4.42 | g/hp-hr | BACT-PSD |
| | | | | | | | | , . | |
| | Midwest Fertilizer Corporation | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | 3,600 | | GCP | | g/hp-hr | BACT-PSD |
| IN-0179 C | Ohio Valley Resources, LLC | OHIO VALLEY RESOURCES, LLC | 9/25/2013 | 4,690 | HP | GCP | 4.46 | g/hp-hr | BACT-PSD |
| | | | _ , , , | | | | | | |
| | • | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | 3,600 | | GCP | | g/hp-hr | BACT-PSD |
| | Victorville 2 Hybrid Power Project | CITY OF VICTORVILLE | 3/11/2010 | 2,000 | | None | _ | g/hp-hr | BACT-PSD |
| | Lake Charles Chemical Complex | SASOL CHEMICALS (USA) LLC | 5/23/2014 | 2,682 | HP | GCP | 4.63 | g/hp-hr | BACT-PSD |
| | Lake Charles Chemical Complex LDPE | | | | | | | | |
| | | SASOL CHEMICALS (USA) LLC | 5/23/2014 | 2,682 | HP | GCP | 4.63 | g/hp-hr | BACT-PSD |
| | Endicott Production Facility, Liberty | BRITISH PETROLEUM EXPLORATION | | | | | | | |
| | | ALASKA (BPXA) | 6/15/2009 | 1,041 | | GCP | | g/hp-hr | BACT-PSD |
| WV-0027 II | Inwood | KNAUF INSULATION INC. | 9/15/2017 | 900 | HP | GCP, Clean Fuel | 4.77 | g/hp-hr | BACT-PSD |
| | | LOUISIANA ENERGY AND POWER | | | | | | | |
| | Morgan City Power Plant | AUTHORITY (LEPA) | 9/26/2013 | 2,000 | | GCP | | g/hp-hr | BACT-PSD |
| | Renaissance Power LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | 1,000 | | GCP | | g/hp-hr | BACT-PSD |
| LA-0313 S | St. Charles Power Station | ENTERGY LOUISIANA, LLC | 8/31/2016 | 2,584 | HP | NSPS Compliance | 4.80 | g/hp-hr | BACT-PSD |
| | | | | | | | | | |
| LA-0292 F | Holbrook Compressor Station | CAMERON INTERSTATE PIPELINE LLC | 1/22/2016 | | | GCP, Clean Fuel | | g/hp-hr | BACT-PSD |
| IN-0158 S | St. Joseph Energy Center, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 1,006 | HP | GCP | 4.80 | g/hp-hr | BACT-PSD |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|----------|--|----------------------------------|--------------|------------|-------|-----------------|---------------|------------|--------------------|
| IN-0158 | St. Joseph Energy Center, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 2,012 | HP | GCP | 4.80 | g/hp-hr | BACT-PSD |
| MD-0044 | Cove Point LNG Terminal | DOMINION COVE POINT LNG, LP | 6/9/2014 | 1,550 | HP | GCP | 4.80 | g/hp-hr | LAER |
| | | CONSTELLATION POWER SOURCE | | | | | | | |
| MD-0043 | Perryman Generating Station | GENERATION, INC. | 7/1/2014 | 1,300 | HP | GCP | 4.80 | g/hp-hr | LAER |
| CA-1212 | Palmdale Hybrid Power Project | CITY OF PALMDALE | 10/18/2011 | 2,683 | HP | None | 4.80 | g/hp-hr | BACT-PSD |
| | Moundsville Combined Cycle Power | | | | | | | | |
| WV-0025 | Plant | MOUNDSVILLE POWER, LLC | 11/21/2014 | 2,016 | HP | None | 4.80 | g/hp-hr | BACT-PSD |
| | | FOOTPRINT POWER SALEM HARBOR | | | | | | | |
| MA-0039 | Salem Harbor Station Redevelopment | DEVELOPMENT LP | 1/30/2014 | 750 | kW | None | 4.80 | g/hp-hr | LAER |
| AK-0082 | Point Thomson Production Facility | EXXON MOBIL CORPORATION | 1/23/2015 | 2,695 | HP | None | 4.80 | g/hp-hr | BACT-PSD |
| | | WOLVERINE POWER SUPPLY | | | | | | | |
| MI-0402 | Sumpter Power Plant | COOPERATIVE INC. | 11/17/2011 | 732 | HP | GCP | 4.85 | g/hp-hr | BACT-PSD |
| | | | | | | | | | |
| PA-0278 | Moxie Liberty LLC/Asylum Power Pl T | MOXIE ENERGY LLC | 10/10/2012 | | | None | 4.93 | g/hp-hr | Other Case-by-Case |
| | Blue Plains Advanced Wastewater | DISTRICT OF COLUMBIA WATER AND | | | | | | | |
| DC-0009 | Treatment Plant | SEWER AUTHORITY | 3/15/2012 | 2,682 | HP | None | 5.39 | g/hp-hr | LAER |
| OH-0352 | Oregon Clean Energy Center | ARCADIS, US, INC. | 6/18/2013 | 2,250 | kW | NSPS Compliance | | g/hp-hr | BACT-PSD |
| | | | | | | - | | | |
| LA-0231 | Lake Charles Gasification Facility | LAKE CHARLES COGENERATION, LLC | 6/22/2009 | 1,341 | HP | NSPS Compliance | 5.78 | g/hp-hr | BACT-PSD |
| | · | MID AMERICAN STEEL AND WIRE | | • | | · | | | |
| OK-0128 | Mid American Steel Rolling Mill | COMPANY | 9/8/2008 | 1,200 | HP | None | 5.90 | g/hp-hr | BACT-PSD |
| NV-0050 | MGM Mirage | MGM MIRAGE | 11/30/2009 | 2,206 | | Turbocharger | 5.94 | | Other Case-by-Case |
| MD-0037 | Medimmune Frederick Campus | MEDIMMUNE, INC. | 1/28/2008 | 2,500 | | None | 6.06 | g/hp-hr | LAER |
| AL-0301 | Nucor Steel Tuscaloosa, Inc. | NUCOR STEEL TUSCALOOSA, INC. | 7/22/2014 | 800 | | None | | g/hp-hr | BACT-PSD |
| FL-0310 | Shady Hills Generating Station | SHADY HILLS POWER COMPANY | 1/12/2009 | 2,500 | | NSPS Compliance | | g/hp-hr | BACT-PSD |
| | , , | 99 CIVIL ENGINEER SQUADRON OF | | , | | · | | J. 1 | |
| NV-0047 | Nellis Air Force Base | USAF | 2/26/2008 | 1,350 | hP | Turbocharger | 7.58 | g/hp-hr | BACT-PSD |
| | | | | • | | 9 | | | |
| NV-0049 | Harrah's Operating Company, Inc. | HARRAH'S OPERATING COMPANY, INC. | 8/20/2009 | 1,232 | HP | Turbocharger | 10.89 | g/hp-hr | BACT-PSD |
| NJ-0073 | Trigen | TRIGEN - TRENTON ENERGY CORP | 3/8/2008 | , | | None | | g/hp-hr | RACT |
| IL-0114 | Cronus Chemicals, LLC | CRONUS CHEMICALS, LLC | 9/5/2014 | 3,755 | HP | NSPS Compliance | | g/kW-hr | BACT-PSD |
| MI-0425 | Grayling Particleboard | ARAUCO NORTH AMERICA | 5/9/2017 | 1,500 | | GCP | | g/kW-hr | BACT-PSD |
| SC-0113 | Pyramax Ceramics, LLC | PYRAMAX CERAMICS, LLC | 2/8/2012 | 757 | HP | NSPS Compliance | 4.00 | g/kW-hr | BACT-PSD |
| | | WESTERN FARMERS ELECTRIC | | | | · | | | |
| OK-0154 | Mooreland Generating Sta | COOPERATIVE | 7/2/2013 | 1,341 | HP | GCP | 4.99 | g/kW-hr | BACT-PSD |
| | | GENERAL MOTORS TECHNICAL CENTER- | | , | | | | J. | |
| MI-0394 | Warren Technical Center | WARREN | 2/29/2012 | 3,010 | kW | GCP, ITR | 5.98 | g/kW-hr | BACT-PSD |
| | | GENERAL MOTORS TECHNICAL CENTER- | | , | | | | J. | |
| MI-0395 | Warren Technical Center | -WARREN | 7/13/2012 | 3,010 | kW | GCP, ITR | 5.98 | g/kW-hr | BACT-PSD |
| IA-0105 | Iowa Fertilizer Company | IOWA FERTILIZER COMPANY | 10/26/2012 | 2,000 | | GCP | | g/kW-hr | BACT-PSD |
| 1-11 | | | -, -, | _, | | | 1.50 | | |
| IA-0095 | Tate & Lyle Ingredients Americas, Inc. | | 9/19/2008 | 700 | kW | None | 6.20 | g/kW-hr | BACT-PSD |
| | , 0 22 22 22,000 | ASSOCIATED ELECTRIC COOPERATIVE | 2, 2,230 | | | - | 1.20 | | |
| OK-0129 | Chouteau Power Plant | INC | 1/23/2009 | 2,200 | HP | None | 6.40 | g/kW-hr | BACT-PSD |
| LA-0251 | Flopam Inc. Facility | FLOPAM INC. | 4/26/2011 | 1,175 | | None | | g/kW-hr | LAER |
| | Ohio River Clean Fuels, LLC | OHIO RIVER CLEAN FUELS, LLC | 11/20/2008 | | | GCP | | g/kW-hr | BACT-PSD |
| 5.1 0517 | OO MITCH CICATI I ACID, ELC | | -1, 20, 2000 | 2,322 | | 1~~. | 0.40 | 0/ 1/4 111 | 2.101 1 35 |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|---------|--|----------------------------------|--------------------|------------|-------|-----------------|---------------|------------|--------------------|
| AK-0073 | International Station Power Plant | CHUGACH ELECTRIC ASSOCIATION | 12/20/2010 | 1,500 | kW | GCP | 6.40 | g/kW-hr | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | 2,922 | hP | GCP | 6.40 | g/kW-hr | BACT-PSD |
| | Highlands Biorefinery And Cogeneration | | | | | | | | |
| FL-0332 | Plant | HIGHLANDS ENVIROFUELS (HEF), LLC | 9/23/2011 | 2,682 | hP | NSPS Compliance | 6.40 | g/kW-hr | BACT-PSD |
| ID-0018 | Langley Gulch Power Plant | IDAHO POWER COMPANY | 6/25/2010 | 750 | kW | GCP | 6.40 | g/kW-hr | BACT-PSD |
| AK-0076 | Point Thomson Production Facility | EXXON MOBIL CORPORATION | 8/20/2012 | 1,750 | kW | None | 6.40 | g/kW-hr | BACT-PSD |
| | Sweet Sorghum-To-Ethanol Advanced | SOUTHEAST RENEWABLE FUELS (SRF), | | | | | | | |
| FL-0322 | Biorefinery | LLC | 12/23/2010 | 2,000 | kW | None | 6.40 | g/kW-hr | BACT-PSD |
| | | BENTELER STEEL / TUBE | | | | | | | |
| LA-0309 | Benteler Steel Tube Facility | MANUFACTURING CORPORATION | 6/4/2015 | 2,922 | HP | NSPS Compliance | 6.40 | g/kW-hr | BACT-PSD |
| | | DYNO NOBEL LOUISIANA AMMONIA, | | | | | | | |
| LA-0272 | Ammonia Production Facility | LLC | 3/27/2013 | 1,200 | | GCP | 6.40 | g/kW-hr | BACT-PSD |
| MI-0421 | Grayling Particleboard | ARAUCO NORTH AMERICA | 8/26/2016 | 1,600 | kW | GCP | 6.41 | g/kW-hr | BACT-PSD |
| MI-0425 | Grayling Particleboard | ARAUCO NORTH AMERICA | 5/9/2017 | 1,500 | kW | GCP | 6.41 | g/kW-hr | BACT-PSD |
| | | GENERAL MOTORS TECHNICAL CENTER- | | | | | | | |
| MI-0394 | Warren Technical Center | WARREN | 2/29/2012 | 2,280 | kW | GCP, ITR | 6.93 | g/kW-hr | BACT-PSD |
| | | GENERAL MOTORS TECHNICAL CENTER- | | | | | | | |
| MI-0395 | Warren Technical Center | -WARREN | 7/13/2012 | 2,500 | kW | GCP, ITR | 7.13 | g/kW-hr | BACT-PSD |
| | | GENERAL MOTORS TECHNICAL CENTER | | | | | | | |
| MI-0418 | Warren Technical Center | - WARREN | 1/14/2015 | 2,710 | kW | GCP, ITR | 7.13 | g/kW-hr | BACT-PSD |
| | | GENERAL MOTORS TECHNICAL CENTER | | | | | | | |
| MI-0418 | Warren Technical Center | - WARREN | 1/14/2015 | 3,490 | kW | GCP, ITR | 8.00 | g/kW-hr | BACT-PSD |
| AK-0072 | Dutch Harbor Power Plant | CITY OF UNALASKA | 7/14/2011 | 4,400 | kW | GCP | 9.80 | g/kW-hr | BACT-PSD |
| NH-0015 | Concord Steam Corporation | CONCORD STEAM CORPORATION | 2/27/2009 | | | None | | lb/MMBtu | |
| NH-0015 | Concord Steam Corporation | CONCORD STEAM CORPORATION | 2/27/2009 | | | None | 1.98 | lb/MMBtu | LAER |
| LA-0204 | Plaquemine PVC Plant | SHINTECH LOUISIANA LLC | 2/27/2009 | 1,389 | HP | GCP | 3.20 | lb/MMBtu | BACT-PSD |
| | | | PM10 - filte | rable | | | | | |
| | | | | | | | | | |
| | Peony Chemical Manufacturing Facility | BASF | 4/1/2015 | 1,500 | | NSPS Compliance | | g/hp-hr | Other Case-by-Case |
| | MGM Mirage | MGM MIRAGE | 11/30/2009 | 2,206 | | Turbocharger | | g/hp-hr | Other Case-by-Case |
| | GP Clarendon LP | GP CLARENDON LP | 2/10/2009 | 1,400 | | GCP | _ | g/hp-hr | BACT-PSD |
| SC-0114 | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | 1,400 | HP | None | 0.06 | g/hp-hr | BACT-PSD |
| | | 99 CIVIL ENGINEER SQUADRON OF | | | | | | | |
| NV-0047 | Nellis Air Force Base | USAF | 2/26/2008 | 1,350 | | Turbocharger | | g/hp-hr | Other Case-by-Case |
| | St. Joseph Energy Center, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 1,006 | | GCP | | g/hp-hr | BACT-PSD |
| | St. Joseph Energy Center, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 2,012 | | GCP | | g/hp-hr | BACT-PSD |
| AK-0082 | Point Thomson Production Facility | EXXON MOBIL CORPORATION | 1/23/2015 | 2,695 | | None | | g/hp-hr | BACT-PSD |
| LA-0313 | St. Charles Power Station | ENTERGY LOUISIANA, LLC | 8/31/2016 | 2,584 | HP | GCP | 0.15 | g/hp-hr | BACT-PSD |
| | | | - 4 4 | | | | | <i>"</i> | |
| NV-0049 | Harrah's Operating Company, Inc. | HARRAH'S OPERATING COMPANY, INC. | 8/20/2009 | 1,232 | HP | Turbocharger | 0.32 | g/hp-hr | Other Case-by-Case |
| | Take 0 to be because it is a second | | 0/40/225 | | | | | // / / / / | D 4 CT DCD |
| IA-0095 | Tate & Lyle Ingredients Americas, Inc. | 0.110 0.115 0.544 5.1516 1.16 | 9/19/2008 | 700 | | None | | g/kW-hr | BACT-PSD |
| OH-0317 | Ohio River Clean Fuels, LLC | OHIO RIVER CLEAN FUELS, LLC | 11/20/2008 | 2,922 | | GCP | | g/kW-hr | BACT-PSD |
| LA-0251 | Flopam Inc. Facility | FLOPAM INC. | 4/26/2011 | 1,175 | nP | None | 0.20 | g/kW-hr | BACT-PSD |
| 14 6366 | AAaaaa Cila Baaaa Si | LOUISIANA ENERGY AND POWER | 0/20/2015 | 2 222 | 1.14 | CCD | 0.5. | -/13441 | DACT DCD |
| LA-0308 | Morgan City Power Plant | AUTHORITY (LEPA) | 9/26/2013 | 2,000 | κW | GCP | 0.24 | g/kW-hr | BACT-PSD |

Emergency Generator Table D-5 - RBLC Results for Emergency-Fire-Pump

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|---------|--|---------------------------------|-------------|------------|----------|-----------------|---------------|---------|--------------------|
| | | | PM10 - to | tal | | | <u> </u> | | |
| | | | | | | | | | |
| PA-0278 | Moxie Liberty LLC/Asylum Power Pl T | MOXIE ENERGY LLC | 10/10/2012 | | | None | 0.02 | g/hp-hr | Other Case-by-Case |
| | | | | | | | | | , |
| LA-0231 | Lake Charles Gasification Facility | LAKE CHARLES COGENERATION, LLC | 6/22/2009 | 1,341 | HP | NSPS Compliance | 0.02 | g/hp-hr | BACT-PSD |
| AK-0073 | International Station Power Plant | CHUGACH ELECTRIC ASSOCIATION | 12/20/2010 | 1,500 | kW | Turbo Charging | 0.03 | g/hp-hr | BACT-PSD |
| LA-0288 | Lake Charles Chemical Complex | SASOL CHEMICALS (USA) LLC | 5/23/2014 | 2,682 | HP | GCP | 0.15 | g/hp-hr | BACT-PSD |
| | Lake Charles Chemical Complex LDPE | | | | | | | | |
| LA-0296 | Unit | SASOL CHEMICALS (USA) LLC | 5/23/2014 | 2,682 | HP | GCP | 0.15 | g/hp-hr | BACT-PSD |
| | | | | | | | | | |
| IN-0173 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | 3,600 | HP | GCP | 0.15 | g/hp-hr | BACT-PSD |
| IN-0179 | Ohio Valley Resources, LLC | OHIO VALLEY RESOURCES, LLC | 9/25/2013 | 4,690 | HP | GCP | 0.15 | g/hp-hr | BACT-PSD |
| | | | | | | | | | |
| IN-0180 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | 3,600 | HP | GCP | 0.15 | g/hp-hr | BACT-PSD |
| MI-0406 | Renaissance Power LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | 1,000 | kW | GCP | 0.15 | g/hp-hr | BACT-PSD |
| | Energy Answers Arecibo Puerto Rico | | | | | | | | |
| PR-0009 | Renewable Energy Project | ENERGY ANSWERS ARECIBO, LLC | 4/10/2014 | 670 | hP | None | 0.15 | g/hp-hr | BACT-PSD |
| | | | | | | | | | |
| LA-0254 | Ninemile Point Electric Generating Plant | ENTERGY LOUISIANA LLC | 8/16/2011 | 1,250 | HP | GCP, Clean Fuel | 0.15 | g/hp-hr | BACT-PSD |
| CA-1212 | Palmdale Hybrid Power Project | CITY OF PALMDALE | 10/18/2011 | 2,683 | HP | Clean fuels | | g/hp-hr | BACT-PSD |
| | | | | | | | | | |
| IN-0263 | Midwest Fertilizer Company LLC | MIDWEST FERTILIZER COMPANY LLC | 3/23/2017 | 3,600 | HP | GCP | 0.15 | g/hp-hr | BACT-PSD |
| | | FOOTPRINT POWER SALEM HARBOR | | • | | | | | |
| MA-0039 | Salem Harbor Station Redevelopment | DEVELOPMENT LP | 1/30/2014 | 750 | kW | None | 0.15 | g/hp-hr | BACT-PSD |
| MD-0044 | Cove Point LNG Terminal | DOMINION COVE POINT LNG, LP | 6/9/2014 | 1,550 | HP | GCP, Clean Fuel | 0.17 | g/hp-hr | BACT-PSD |
| | | CONSTELLATION POWER SOURCE | | | | | | | |
| MD-0043 | Perryman Generating Station | GENERATION, INC. | 7/1/2014 | 1,300 | HP | GCP | 0.17 | g/hp-hr | BACT-PSD |
| OH-0352 | Oregon Clean Energy Center | ARCADIS, US, INC. | 6/18/2013 | 2,250 | kW | NSPS Compliance | 0.20 | g/hp-hr | BACT-PSD |
| | | WOLVERINE POWER SUPPLY | | | | | | | |
| MI-0400 | Wolverine Power | COOPERATIVE, INC. | 6/29/2011 | 4,000 | HP | None | 0.20 | g/hp-hr | BACT-PSD |
| WV-0027 | Inwood | KNAUF INSULATION INC. | 9/15/2017 | 900 | HP | Clean fuels | 0.20 | g/hp-hr | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | 2,922 | hP | GCP | 0.25 | g/hp-hr | BACT-PSD |
| | | MID AMERICAN STEEL AND WIRE | | | | | | | |
| OK-0128 | Mid American Steel Rolling Mill | COMPANY | 9/8/2008 | 1,200 | HP | None | 0.32 | g/hp-hr | BACT-PSD |
| FL-0310 | Shady Hills Generating Station | SHADY HILLS POWER COMPANY | 1/12/2009 | 2,500 | kW | GCP, Clean Fuel | 0.40 | g/hp-hr | BACT-PSD |
| FL-0310 | Shady Hills Generating Station | SHADY HILLS POWER COMPANY | 1/12/2009 | 2,500 | kW | Clean fuels | 0.40 | g/hp-hr | BACT-PSD |
| AR-0140 | Big River Steel LLC | BIG RIVER STEEL LLC | 9/18/2013 | 1,500 | kW | GCP | 0.04 | g/kW-hr | BACT-PSD |
| MI-0425 | Grayling Particleboard | ARAUCO NORTH AMERICA | 5/9/2017 | 1,500 | kW | GCP | 0.07 | g/kW-hr | BACT-PSD |
| IL-0114 | Cronus Chemicals, LLC | CRONUS CHEMICALS, LLC | 9/5/2014 | 3,755 | HP | NSPS Compliance | 0.10 | g/kW-hr | BACT-PSD |
| MI-0425 | Grayling Particleboard | ARAUCO NORTH AMERICA | 5/9/2017 | 1,500 | kW | GCP | 0.20 | g/kW-hr | BACT-PSD |
| | | ASSOCIATED ELECTRIC COOPERATIVE | | | | | | | |
| OK-0129 | Chouteau Power Plant | INC | 1/23/2009 | 2,200 | HP | None | | g/kW-hr | BACT-PSD |
| IA-0105 | Iowa Fertilizer Company | IOWA FERTILIZER COMPANY | 10/26/2012 | 2,000 | kW | GCP | 0.20 | g/kW-hr | BACT-PSD |
| | CF Industries Nitrogen, LLC - Port Neal | | | | | | | | |
| IA-0106 | Nitrogen Complex | CF INDUSTRIES NITROGEN, LLC | 7/12/2013 | | <u> </u> | GCP | 0.20 | g/kW-hr | BACT-PSD |

Emergency Generator Table D-5 - RBLC Results for Emergency-Fire-Pump

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|---------|--|---------------------------------|--------------------|------------|-------|--------------------------------|---------------|-----------|--------------------|
| | | BENTELER STEEL / TUBE | | | | | | | |
| LA-0309 | Benteler Steel Tube Facility | MANUFACTURING CORPORATION | 6/4/2015 | 2,922 | HP | NSPS Compliance | 0.20 | g/kW-hr | BACT-PSD |
| | | DYNO NOBEL LOUISIANA AMMONIA, | | | | | | | |
| LA-0272 | Ammonia Production Facility | LLC | 3/27/2013 | 1,200 | HP | GCP | 0.20 | g/kW-hr | BACT-PSD |
| MI-0421 | Grayling Particleboard | ARAUCO NORTH AMERICA | 8/26/2016 | 1,600 | kW | GCP | 0.40 | g/kW-hr | BACT-PSD |
| MI-0389 | Karn Weadock Generating Complex | CONSUMERS ENERGY | 12/29/2009 | 2,000 | kW | GCP, Clean Fuel | 0.06 | lb/MMBtu | BACT-PSD |
| | | WOLVERINE POWER SUPPLY | | | | | | | |
| MI-0402 | Sumpter Power Plant | COOPERATIVE INC. | 11/17/2011 | 732 | | GCP | 0.06 | lb/MMBtu | BACT-PSD |
| LA-0204 | Plaquemine PVC Plant | SHINTECH LOUISIANA LLC | 2/27/2009 | 1,389 | HP | GCP | 0.10 | lb/MMBtu | BACT-PSD |
| IN-0166 | Indiana Gasification, LLC | INDIANA GASIFICATION, LLC | 6/27/2012 | 1,341 | HP | Clean fuels | 15.00 | ppm Sulfu | r BACT-PSD |
| | | | PM2.5 - filte | rable | | 1 | _ | _ | 1 |
| | | | | | | | | | |
| TX-0728 | Peony Chemical Manufacturing Facility | BASF | 4/1/2015 | 1,500 | | NSPS Compliance | | g/hp-hr | Other Case-by-Case |
| IN-0158 | St. Joseph Energy Center, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 1,006 | | GCP | | g/hp-hr | BACT-PSD |
| IN-0158 | St. Joseph Energy Center, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 2,012 | HP | GCP | 0.15 | g/hp-hr | BACT-PSD |
| | Moundsville Combined Cycle Power | | | | | | | | |
| WV-0025 | Plant | MOUNDSVILLE POWER, LLC | 11/21/2014 | 2,016 | | None | | g/hp-hr | BACT-PSD |
| AK-0082 | Point Thomson Production Facility | EXXON MOBIL CORPORATION | 1/23/2015 | 2,695 | | None | | g/hp-hr | BACT-PSD |
| LA-0313 | St. Charles Power Station | ENTERGY LOUISIANA, LLC | 8/31/2016 | 2,584 | HP | GCP | 0.15 | g/hp-hr | BACT-PSD |
| | | DYNO NOBEL LOUISIANA AMMONIA, | | | | | | | |
| LA-0272 | Ammonia Production Facility | LLC | 3/27/2013 | 1,200 | HP | GCP | 0.20 | g/kW-hr | BACT-PSD |
| | | LOUISIANA ENERGY AND POWER | | | | | | | |
| LA-0308 | Morgan City Power Plant | AUTHORITY (LEPA) | 9/26/2013 | 2,000 | | GCP | | g/kW-hr | BACT-PSD |
| AK-0072 | Dutch Harbor Power Plant | CITY OF UNALASKA | 7/14/2011 | 4,400 | kW | Positive Crankcase Ventilation | 0.50 | g/kW-hr | BACT-PSD |
| | ı | I | PM2.5 - to | otal | ı | | | 1 | 1 |
| PA-0278 | Moxie Liberty LLC/Asylum Power Pl T | MOXIE ENERGY LLC | 10/10/2012 | | | None | 0.02 | g/hp-hr | Other Case-by-Case |
| LA-0288 | Lake Charles Chemical Complex | SASOL CHEMICALS (USA) LLC | 5/23/2014 | 2,682 | НР | GCP | | g/hp-hr | BACT-PSD |
| 27.0200 | Lake Charles Chemical Complex LDPE | | 3/23/201 | 2,002 | | | 0.13 | 6/ | 57.67.755 |
| LA-0296 | Unit | SASOL CHEMICALS (USA) LLC | 5/23/2014 | 2,682 | НР | GCP | 0.15 | g/hp-hr | BACT-PSD |
| | | WESTERN FARMERS ELECTRIC | 0, 20, 202 | | | | 5.25 | 6/ 11/ | |
| OK-0154 | Mooreland Generating Sta | COOPERATIVE | 7/2/2013 | 1,341 | HP | GCP | 0.15 | g/hp-hr | BACT-PSD |
| | | | | , | | | | J. 1 | |
| IN-0173 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | 3,600 | HP | GCP | 0.15 | g/hp-hr | BACT-PSD |
| | | | | | | | | | |
| IN-0180 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | 3,600 | HP | GCP | 0.15 | g/hp-hr | BACT-PSD |
| MI-0406 | Renaissance Power LLC | LS POWER DEVELOPMENT LLC | 11/1/2013 | 1,000 | kW | GCP | | g/hp-hr | BACT-PSD |
| | Energy Answers Arecibo Puerto Rico | | | | | | | | |
| PR-0009 | Renewable Energy Project | ENERGY ANSWERS ARECIBO, LLC | 4/10/2014 | 670 | hP | None | 0.15 | g/hp-hr | BACT-PSD |
| | | | | | | | | | |
| LA-0292 | Holbrook Compressor Station | CAMERON INTERSTATE PIPELINE LLC | 1/22/2016 | 1,341 | HP | GCP, Clean Fuel | 0.15 | g/hp-hr | BACT-PSD |
| | | | | | | | | | |
| LA-0254 | Ninemile Point Electric Generating Plant | ENTERGY LOUISIANA LLC | 8/16/2011 | 1,250 | HP | GCP, Clean Fuel | 0.15 | g/hp-hr | BACT-PSD |
| CA-1191 | Victorville 2 Hybrid Power Project | CITY OF VICTORVILLE | 3/11/2010 | 2,000 | kW | Clean fuels | 0.15 | g/hp-hr | BACT-PSD |
| CA-1212 | Palmdale Hybrid Power Project | CITY OF PALMDALE | 10/18/2011 | 2,683 | HP | Clean fuels | 0.15 | g/hp-hr | BACT-PSD |

Emergency Generator Table D-5 - RBLC Results for Emergency-Fire Pump

| IN-0263 Midwest Fertilizer Company LLC | ontrols EmissionLimit | Units | Type |
|--|--|--------------------|----------------------|
| MA-0039 Salem Harbor Station Redevelopment DEVELOPMENT LP 1/30/2014 750 kW None | STATE OF STA | Omics | 1,460 |
| MA-0039 Salem Harbor Station Redevelopment DEVELOPMENT LP 1/30/2014 750 kW None | 0.15 | g/hp-hr | BACT-PSD |
| MI-0404 | | 0, 1 | |
| MI-0400 Wolverine Power | 0.15 | g/hp-hr | BACT-PSD |
| MI-0400 Molverine Power COOPERATIVE, INC. 6/29/2011 4,000 HP None MI-0423 Indeck Niles, LLC INDECK NILES, LLC 1/4/2017 2,922 hP GCP | | g/hp-hr | BACT-PSD |
| MI-0423 Indeck Niles, LLC INDECK NILES, LLC 1/4/2017 2,922 hP GCP IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP AR-0140 Big River Steel LLC Big River Steel LLC Big River Steel LLC 9/18/2013 1,500 kW GCP II-0114 Cronus Chemicals, LLC CRONUS CHEMICALS, LLC 9/5/2017 1,500 kW GCP II-0114 Cronus Chemicals, LLC CRONUS CHEMICALS, LLC 9/5/2014 3,755 HP NSPS Complia AR-0203 Point Thomson Production Facility EXXONMOBIL CORPORATION 6/12/2013 610 HP GCP MI-0425 Grayling Particleboard ARAUCO NORTH AMERICA 5/9/2017 1,500 kW GCP II-0105 lowa Fertilizer Company IOWA FERTILIZER COMPANY 10/26/2012 2,000 kW GCP II-0105 lowa Fertilizer Company IOWA FERTILIZER COMPANY 10/26/2012 2,000 kW GCP GCP II-0105 II-0106 Mitrogen Complex EXXON MOBIL CORPORATION 8/20/2012 1,750 kW None II-0406 II-0 | | - | |
| IN-0179 Ohio Valley Resources, LLC | 0.20 | g/hp-hr | BACT-PSD |
| AR-0140 Big River Steel LLC | 0.25 | g/hp-hr | BACT-PSD |
| MI-0425 Grayling Particleboard ARAUCO NORTH AMERICA 5/9/2017 1,500 kW GCP | 68.04 | g/hp-hr | BACT-PSD |
| IL-0114 Cronus Chemicals, LLC | 0.04 | g/kW-hr | BACT-PSD |
| AK-0081 Point Thomson Production Facility EXXONMOBIL CORPORATION 6/12/2013 610 HP GCP | 0.07 | g/kW-hr | BACT-PSD |
| MI-0425 Grayling Particleboard ARAUCO NORTH AMERICA 5/9/2017 1,500 kW GCP IA-0105 Iowa Fertilizer Company IOWA FERTILIZER COMPANY 10/26/2012 2,000 kW GCP CF Industries Nitrogen, LLC - Port Neal IA-0106 Nitrogen Complex CF INDUSTRIES NITROGEN, LLC 7/12/2013 GCP AK-0076 Point Thomson Production Facility EXXON MOBIL CORPORATION 8/20/2012 1,750 kW None BENTELER STEEL / TUBE BENTELER STEEL / TUBE MANUFACTURING CORPORATION 6/4/2015 2,922 HP NSPS Complia MI-0421 Grayling Particleboard ARAUCO NORTH AMERICA 8/26/2016 1,600 kW GCP MI-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0166 Indiana Gasification, LLC INDIANA GASIFICATION, LLC 6/27/2012 1,341 HP Clean fuels NY-0104 CPV Valley Energy Center CPV VALLEY LLC 8/1/2013 Clean fuels TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Complia MI-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP MI-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP MI-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP MI-0403 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0173 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0180 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP | | g/kW-hr | BACT-PSD |
| IA-0105 lowa Fertilizer Company CF Industries Nitrogen, LLC - Port Neal IA-0106 Nitrogen Complex AK-0076 Point Thomson Production Facility EXXON MOBIL CORPORATION BENTELER STEEL / TUBE LA-0309 Benteler Steel Tube Facility MANUFACTURING CORPORATION MI-0421 Grayling Particleboard ARAUCO NORTH AMERICA WOLVERINE POWER SUPPLY IN-0166 Indiana Gasification, LLC INDIANA GASIFICATION, LLC EXXON MOBIL CORPORATION MI-0402 Sumpter Power Plant COOPERATIVE INC. TX-0728 Peony Chemical Manufacturing Facility MI-0402 Sumpter Power Plant COOPERATIVE INC. MI-0402 Sumpter Power Plant COOPERATIVE INC. TX-0728 Peony Chemical Manufacturing Facility MI-0402 Sumpter Power Plant COOPERATIVE INC. MI-0402 Sumpter Power Plant COOPERATIVE INC. TX-0728 Peony Chemical Manufacturing Facility MI-0402 Sumpter Power Plant COOPERATIVE INC. MI-0403 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION MIDWEST | 0.15 | g/kW-hr | Other Case-by-Case |
| IA-0106 Nitrogen Complex CF INDUSTRIES NITROGEN, LLC 7/12/2013 GCP | 0.20 | g/kW-hr | BACT-PSD |
| IA-0106 Nitrogen Complex | 0.20 | g/kW-hr | BACT-PSD |
| AK-0076 Point Thomson Production Facility EXXON MOBIL CORPORATION 8/20/2012 1,750 kW None BENTELER STEEL / TUBE | | | |
| BENTELER STEEL / TUBE ANANUFACTURING CORPORATION BENTELER STEEL / TUBE ANANUFACTURING CORPORATION BENTELER STEEL / TUBE ANANUFACTURING CORPORATION BENTELER STEEL / TUBE ANANUFACTURING CORPORATION BENTELER STEEL / TUBE ANANUFACTURING CORPORATION BASIC CORPORATION B | 0.20 | g/kW-hr | BACT-PSD |
| LA-0309 Benteler Steel Tube Facility MANUFACTURING CORPORATION 6/4/2015 2,922 HP NSPS Complia MI-0421 Grayling Particleboard ARAUCO NORTH AMERICA 8/26/2016 1,600 kW GCP MI-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0166 Indiana Gasification, LLC INDIANA GASIFICATION, LLC 6/27/2012 1,341 HP Clean fuels NY-0104 CPV Valley Energy Center CPV VALLEY LLC 8/12013 Clean fuels TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Complia MI-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP MI-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0173 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | 0.20 | g/kW-hr | BACT-PSD |
| MI-0421 Grayling Particleboard ARAUCO NORTH AMERICA 8/26/2016 1,600 kW GCP WOLVERINE POWER SUPPLY OOOPERATIVE INC. 11/17/2011 732 HP GCP IN-0166 Indiana Gasification, LLC INDIANA GASIFICATION, LLC 6/27/2012 1,341 HP Clean fuels PM - filterable NY-0104 CPV Valley Energy Center CPV VALLEY LLC 8/1/2013 Clean fuels TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Complia WOLVERINE POWER SUPPLY MI-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0173 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | | | |
| MI-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0166 Indiana Gasification, LLC INDIANA GASIFICATION, LLC 6/27/2012 1,341 HP Clean fuels PM - filterable NY-0104 CPV Valley Energy Center CPV VALLEY LLC 8/1/2013 Clean fuels TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Complia WOLVERINE POWER SUPPLY COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0173 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | iance 0.20 | g/kW-hr | BACT-PSD |
| MI-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0166 Indiana Gasification, LLC INDIANA GASIFICATION, LLC 6/27/2012 1,341 HP Clean fuels PM - filterable NY-0104 CPV Valley Energy Center CPV VALLEY LLC 8/1/2013 Clean fuels TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Complia WOLVERINE POWER SUPPLY MI-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0173 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | 0.40 | g/kW-hr | BACT-PSD |
| IN-0166 Indiana Gasification, LLC INDIANA GASIFICATION, LLC 6/27/2012 1,341 HP Clean fuels PM - filterable NY-0104 CPV Valley Energy Center CPV VALLEY LLC 8/1/2013 Clean fuels TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Complia WOLVERINE POWER SUPPLY MI-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0173 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | | | |
| NY-0104 CPV Valley Energy Center CPV VALLEY LLC 8/1/2013 Clean fuels TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Complia WOLVERINE POWER SUPPLY 11/17/2011 732 HP GCP IN-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0173 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | | lb/MMBtu | |
| NY-0104 CPV Valley Energy Center CPV VALLEY LLC 8/1/2013 Clean fuels TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Complia WOLVERINE POWER SUPPLY MI-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0173 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | 15.00 | ppm Sulfur | BACT-PSD |
| TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Complia WOLVERINE POWER SUPPLY COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0173 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | | 1 | 1 |
| WOLVERINE POWER SUPPLY COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0173 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | 0.03 | g/hp-hr | BACT-PSD |
| WOLVERINE POWER SUPPLY COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0173 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | | | |
| MI-0402 Sumpter Power Plant COOPERATIVE INC. 11/17/2011 732 HP GCP IN-0173 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | iance 0.05 | g/hp-hr | Other Case-by-Case |
| IN-0173 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | | , . | |
| IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | 0.05 | g/hp-hr | BACT-PSD |
| IN-0179 Ohio Valley Resources, LLC OHIO VALLEY RESOURCES, LLC 9/25/2013 4,690 HP GCP IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | 0.45 | , , | 2407.000 |
| IN-0180 Midwest Fertilizer Corporation MIDWEST FERTILIZER CORPORATION 6/4/2014 3,600 HP GCP MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | | g/hp-hr | BACT-PSD |
| MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | 0.15 | g/hp-hr | BACT-PSD |
| MI-0406 Renaissance Power LLC LS POWER DEVELOPMENT LLC 11/1/2013 1,000 kW GCP Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | 0.15 | -/hh | DACT DCD |
| Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | | g/hp-hr g/hp-hr | BACT-PSD BACT-PSD |
| PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | 0.15 | g/np-nr | BACI-PSD |
| IN-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 1,006 HP GCP | 0.15 | g/hp-hr | BACT-PSD |
| | | g/hp-hr | BACT-PSD |
| N-0158 St. Joseph Energy Center, LLC ST. JOSEPH ENERGY CENTER, LLC 12/3/2012 2,012 HP GCP | | g/hp-hr | BACT-PSD |
| MD-0044 Cove Point LNG Terminal DOMINION COVE POINT LNG, LP 6/9/2014 1,550 HP GCP, Clean Fu | | g/hp-hr | BACT-PSD |
| WOLVERINE POWER SUPPLY | 0.15 | P/ 11h,111 | DACI-13D |
| MI-0400 Wolverine Power COOPERATIVE, INC. 6/29/2011 4,000 HP None | 0.15 | g/hp-hr | BACT-PSD |
| AL-0301 Nucor Steel Tuscaloosa, Inc. NUCOR STEEL TUSCALOOSA, INC. 7/22/2014 800 HP None | | g/hp-hr | BACT-PSD |
| AR-0140 Big River Steel LLC BIG RIVER STEEL LLC 9/18/2013 1,500 kW GCP | | g/kW-hr | BACT-PSD |
| IL-0114 Cronus Chemicals, LLC CRONUS CHEMICALS, LLC 9/5/2014 3,755 HP NSPS Complia | | g/kW-hr | BACT-PSD |

Emergency Generator Table D-5 - RBLC Results for Emergency Fire Pump

| Tate & Lyle Ingredients Americas, Inc. | RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|--|----------|---------------------------------------|----------------------------------|----------------|------------|-------|---------------------------------------|---------------|--------------|--------------------|
| DAD-10 Langley Gulch Power Plant DAH-0 POWER COMPANY 672/2010 750 kW GCP 0.20 87kW-hr BACT-PSD | | | | 0 /40 /0000 | 700 | | | | (1.5.4.1 | D 4 07 D 0 |
| MI-MAZI Grayling Particleboard ARAUCO NORTH AMERICA S7/6/2017 1.500 kW GCP 0.20 g/kW-hr BACT-PSD | | , <u> </u> | IDALIO DOMED COMPANY | | | | | | 0. | |
| MI-0425 GrayIling Particleboard ARAUCO NORTH AMERICA 5/9/2017 1.500 kW GCP 0.20 g/kW-hr BACT-PSD | | | | | | | | | 0. | |
| Mi-0425 Grayling Particleboard | | | | | | | I . | | | |
| Mi-10423 Indeck Niles, LIC INDECK NILES, LIC INDECK NILES, LIC INDIANA GASIFICATION, LIC 6/27/2012 1,341 HP Clean fuels 15.00 ppm Sufur BACT-PSD | | | | | | | | | | |
| NO 1956 Indiana Gasification, LLC NO IANA GASIFICATION, LLC 6/27/2012 1,341 HP Glean fuels 15.00 ppm Sulfur BACT-PSD | | | | | | | | | | |
| PM - total | | | | | | | I . | | | |
| SC-0115 GP Clarendon IP | IN-0166 | Indiana Gasification, LLC | INDIANA GASIFICATION, LLC | | | HP | Clean fuels | 15.00 | ppm Sulfur | BACT-PSD |
| SC-0114 GP Allendale LP | | 1 | | | | | | T | | T |
| CA-1191 Victorville 2 Hybrid Power Project CITY OF VICTORVILE 3/11/2010 2,000 kW Clean fuels 0.15 g/hp-hr BACT-PSD | | I . | | | | | | | | |
| CA-1212 Palmdale Hybrid Power Project CITY OF PALMDALE 10/18/2011 2,683 HP Clean fuels 0.15 g/hp-hr BACT-PSD | | | | | | | | | | |
| N-0263 Midwest Fertilizer Company LLC MIDWEST FERTILIZER COMPANY LLC 3/23/2017 3,600 HP GCP 0.15 g/hp-hr BACT-PSD | CA-1191 | | | | | | Clean fuels | | | |
| IA-0105 Iowa Fertilizer Company IOWA FERTILIZER COMPANY 10/26/2012 2,000 kW GCP 0.20 g/kW-hr BACT-PSD IA-0106 Infustries Nitrogen, LLC - Port Neal CF INDUSTRIES NITROGEN, LLC 7/12/2013 GCP 0.20 g/kW-hr BACT-PSD IA-0108 Mirogen Complex CF INDUSTRIES NITROGEN, LLC 7/12/2013 GCP 0.20 g/kW-hr BACT-PSD IA-0108 Mirogen Complex CF INDUSTRIES NITROGEN, LLC 7/12/2013 GCP 0.20 g/kW-hr BACT-PSD IA-0108 Mirogen Complex CONSUMERS ENERGY 12/29/2009 2,000 kW GCP, Clean Fuel 0.20 g/kW-hr BACT-PSD IA-0108 Mirogen Complex HighLands Biorefinery And Cogeneration HIGHLANDS ENVIROFUELS (HEF), LLC 9/23/2011 2,682 hp NSPS Compliance 0.20 g/kW-hr BACT-PSD IA-0228 Biorefinery LLC L1/23/2010 2,000 kW None 0.20 g/kW-hr BACT-PSD IA-0326 Biorefinery LLC L1/23/2010 3,300 kW GCP 0.20 g/kW-hr BACT-PSD IA-0346 Lauderdale Plant FLORIDA POWER & LIGHT 4/22/2014 3,100 kW GCP 0.20 g/kW-hr BACT-PSD IA-0278 Moxie Liberty LLC/Asylum Power PIT MOXIE ENERGY LLC 10/10/2012 None 0.01 g/hp-hr BACT-PSD IA-0278 MGM ELIBERTY MGM MIRAGE 11/30/2009 2,206 HP Turbocharger 0.11 g/hp-hr BACT-PSD IA-0286 Lake Charles Chemical Complex LDPE LA-0296 Unit SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP NSPS Compliance 0.14 g/hp-hr BACT-PSD IA-0288 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP SCP 0.14 g/hp-hr BACT-PSD IA-0288 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP NSPS Compliance 0.14 g/hp-hr BACT-PSD IA-0288 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP NSPS Compliance 0.14 g/hp-hr BACT-PSD IA-0288 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP NSPS Compliance 0.14 g/hp-hr BACT-PSD IA-0288 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP | CA-1212 | Palmdale Hybrid Power Project | CITY OF PALMDALE | 10/18/2011 | 2,683 | HP | Clean fuels | 0.15 | g/hp-hr | BACT-PSD |
| IA-0105 Iowa Fertilizer Company IOWA FERTILIZER COMPANY 10/26/2012 2,000 kW GCP 0.20 g/kW-hr BACT-PSD IA-0106 Introgen Complex CF INDUSTRIES NITROGEN, LLC 7/12/2013 GCP 0.20 g/kW-hr BACT-PSD IA-0108 Karn Weadock Generating Complex CONSUMERS ENERGY 12/29/2009 2,000 kW GCP, Clean Fuel 0.20 g/kW-hr BACT-PSD IA-0108 Karn Weadock Generating Complex Highlands Biorefinery And Cogeneration HIGHLANDS ENVIROFUELS (HEF), LLC 9/23/2011 2,682 hP NSPS Compliance 0.20 g/kW-hr BACT-PSD IA-0228 Biorefinery HIGHLANDS ENVIROFUELS (HEF), LLC 12/23/2010 2,000 kW None 0.20 g/kW-hr BACT-PSD IA-0328 Sweet Sorghum-To-Ethanol Advanced SOUTHEAST RENEWABLE FUELS (SRF), LLC 12/23/2010 2,000 kW None 0.20 g/kW-hr BACT-PSD IA-0326 College Clean Energy Center FLORIDA POWER & LIGHT 3/9/2016 3,300 kW Clean fuels 0.20 g/kW-hr BACT-PSD IA-0326 Lauderdale Plant FLORIDA POWER & LIGHT 4/22/2014 3,100 kW GCP 0.20 g/kW-hr BACT-PSD IA-0326 College Clean Energy Center FLORIDA POWER & LIGHT 4/22/2014 3,100 kW GCP 0.20 g/kW-hr BACT-PSD IA-0326 College Clean Fuely Center FLORIDA POWER & LIGHT 4/22/2014 3,100 kW GCP 0.20 g/kW-hr BACT-PSD IA-0326 College Clean Fuely Center FLORIDA POWER & LIGHT 4/22/2014 3,100 kW GCP 0.20 g/kW-hr BACT-PSD IA-0327 Moxile Liberty LLC/Asylum Power PIT MOXIE ENERGY LLC 10/10/2012 None 0.01 g/hp-hr BACT-PSD IA-0228 College Clean Fuely Center FLORIDA POWER & LIGHT 4/22/2014 1/2008 1/400 HP None 0.01 g/hp-hr BACT-PSD IA-0228 College Clean Fuely Center FLORIDA POWER & IN-02014 1/2008 1/400 HP None 0.10 g/hp-hr BACT-PSD IA-0228 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP NSPS Compliance 0.14 g/hp-hr BACT-PSD IA-0228 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP GCP 0.14 g/hp-hr BACT-PSD IA-0 | IN-0263 | Midwest Fertilizer Company LLC | MIDWEST FERTILIZER COMPANY LLC | 3/23/2017 | 3,600 | НР | GCP | 0.15 | g/hp-hr | BACT-PSD |
| CF Industries Nitrogen, LLC - Port Neal Nitrogen, Complex CF INDUSTRIES NITROGEN, LLC 7/12/2013 GCP 0.20 g/kW-hr BACT-PSD | IA-0105 | | IOWA FERTILIZER COMPANY | | 2,000 | kW | GCP | | | BACT-PSD |
| IA-0106 Nitrogen Complex | | | | | , | | | | Ç. | |
| MI-0389 Karn Weadock Generating Complex CONSUMERS ENERGY 12/29/2009 2,000 kW GCP, Clean Fuel 0.20 g/kW-hr BACT-PSD | IA-0106 | _ | CF INDUSTRIES NITROGEN, LLC | 7/12/2013 | | | GCP | 0.20 | g/kW-hr | BACT-PSD |
| Highlands Biorefinery And Cogeneration HighLaNDS ENVIROFUELS (HEF), LLC 9/23/2011 2,682 hP NSPS Compliance 0.20 g/kW-hr BACT-PSD | | | <u> </u> | | 2.000 | kW | | | | |
| FL-0332 Plant | | _ : | | | =,000 | | | 0.20 | G/ · · · · · | |
| Sweet Sorghum-To-Ethanol Advanced SOUTHEAST RENEWABLE FUELS (SRF), 12/23/2010 2,000 kW None 0.20 g/kW-hr BACT-PSD | FI-0332 | | HIGHLANDS ENVIROPUELS (HEF), LLC | 9/23/2011 | 2.682 | hP | NSPS Compliance | 0.20 | g/kW-hr | BACT-PSD |
| FL-0322 Biorefinery | | | , , , | 0, 20, 2022 | _, | | | 0.20 | G/ · · · · · | |
| FL-0356 Okeechobee Clean Energy Center FLORIDA POWER & LIGHT 3/9/2016 3,300 kW Clean fuels 0.20 g/kW-hr BACT-PSD | FI-0322 | _ | ` ' | 12/23/2010 | 2 000 | kW | None | 0.20 | g/k\M-hr | BACT-PSD |
| FLO346 Lauderdale Plant | | | | | | | I . | | Ď | |
| PA-0278 Moxie Liberty LLC/Asylum Power PI T MOXIE ENERGY LLC 10/10/2012 None 0.01 g/hp-hr Other Case-by-Case | | | | | | | | | O, | |
| PA-0278 Moxie Liberty LLC/Asylum Power Pl T MOXIE ENERGY LLC 10/10/2012 None 0.01 g/hp-hr Other Case-by-Case SC-0115 GP Clarendon LP GP CLARENDON LP 2/10/2009 1,400 HP GCP 0.10 g/hp-hr BACT-PSD SC-0114 GP Allendale LP GP ALLENDALE LP 11/25/2008 1,400 HP None 0.10 g/hp-hr BACT-PSD NV-0050 MGM Mirage MGM MIRAGE 11/30/2009 2,206 HP Turbocharger 0.14 g/hp-hr Other Case-by-Case LA-0296 Unit SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP NSPS Compliance 0.14 g/hp-hr BACT-PSD LA-0288 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP GCP 0.14 g/hp-hr BACT-PSD PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None 0.15 g/hp-hr BACT-PSD NV-0047 Nellis Air Force Base USAF 2/26/2008 1,350 hP Turbocharger 0.20 g/hp-hr Other Case-by-Case | 12 0340 | Ladderdale Flatte | | | | N V V | Julia | 0.20 | 6/ KVV 111 | BACTISE |
| SC-0115 GP Clarendon LP GP CLARENDON LP 2/10/2009 1,400 HP GCP 0.10 g/hp-hr BACT-PSD SC-0114 GP Allendale LP GP ALLENDALE LP 11/25/2008 1,400 HP None 0.10 g/hp-hr BACT-PSD NV-0050 MGM Mirage MGM MIRAGE 11/30/2009 2,206 HP Turbocharger 0.14 g/hp-hr Other Case-by-Case LA-0296 Unit SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP NSPS Compliance 0.14 g/hp-hr BACT-PSD LA-0288 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP GCP 0.14 g/hp-hr BACT-PSD Energy Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo | | | | line Organic C | ompounds | l | | | | |
| SC-0115 GP Clarendon LP GP CLARENDON LP 2/10/2009 1,400 HP GCP 0.10 g/hp-hr BACT-PSD SC-0114 GP Allendale LP GP ALLENDALE LP 11/25/2008 1,400 HP None 0.10 g/hp-hr BACT-PSD NV-0050 MGM Mirage MGM MIRAGE 11/30/2009 2,206 HP Turbocharger 0.14 g/hp-hr Other Case-by-Case LA-0296 Unit SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP NSPS Compliance 0.14 g/hp-hr BACT-PSD LA-0288 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP GCP 0.14 g/hp-hr BACT-PSD Energy Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo Puerto Rico Foreign Answers Arecibo | PA-0278 | Moxie Liberty LLC/Asylum Power Pl T | MOXIE ENERGY LLC | 10/10/2012 | | | None | 0.01 | g/hp-hr | Other Case-by-Case |
| SC-0114 GP Allendale LP GP ALLENDALE LP 11/25/2008 1,400 HP None 0.10 g/hp-hr BACT-PSD NV-0050 MGM Mirage MGM MIRAGE 11/30/2009 2,206 HP Turbocharger 0.14 g/hp-hr Other Case-by-Case Lake Charles Chemical Complex LDPE LA-0296 Unit SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP NSPS Compliance 0.14 g/hp-hr BACT-PSD LA-0288 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP GCP 0.14 g/hp-hr BACT-PSD Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None 0.15 g/hp-hr BACT-PSD 99 CIVIL ENGINEER SQUADRON OF USAF 2/26/2008 1,350 hP Turbocharger 0.20 g/hp-hr Other Case-by-Case TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Compliance 0.21 g/hp-hr Other Case-by-Case | SC-0115 | GP Clarendon LP | GP CLARENDON LP | 2/10/2009 | 1,400 | HP | GCP | | | BACT-PSD |
| NV-0050 MGM Mirage MGM MIRAGE 11/30/2009 2,206 HP Turbocharger 0.14 g/hp-hr Other Case-by-Case Lake Charles Chemical Complex LDPE LA-0296 Unit SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP NSPS Compliance 0.14 g/hp-hr BACT-PSD LA-0288 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP GCP 0.14 g/hp-hr BACT-PSD Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None 0.15 g/hp-hr BACT-PSD NV-0047 Nellis Air Force Base USAF 2/26/2008 1,350 hP Turbocharger 0.20 g/hp-hr Other Case-by-Case TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Compliance 0.21 g/hp-hr Other Case-by-Case | SC-0114 | GP Allendale LP | GP ALLENDALE LP | 11/25/2008 | 1,400 | НР | | | | BACT-PSD |
| Lake Charles Chemical Complex LDPE LA-0296 Unit SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP NSPS Compliance 0.14 g/hp-hr BACT-PSD LA-0288 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP GCP 0.14 g/hp-hr BACT-PSD Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None 0.15 g/hp-hr BACT-PSD NV-0047 Nellis Air Force Base USAF 2/26/2008 1,350 hP Turbocharger 0.20 g/hp-hr Other Case-by-Case TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Compliance 0.21 g/hp-hr Other Case-by-Case | - | | | | | | | | | |
| LA-0296 Unit SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP NSPS Compliance 0.14 g/hp-hr BACT-PSD LA-0288 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP GCP 0.14 g/hp-hr BACT-PSD Energy Answers Arecibo Puerto Rico Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None 0.15 g/hp-hr BACT-PSD NV-0047 Nellis Air Force Base USAF 2/26/2008 1,350 hP Turbocharger 0.20 g/hp-hr Other Case-by-Case TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Compliance 0.21 g/hp-hr Other Case-by-Case | | _ | | , , | , | | | | O/ 1 | |
| LA-0288 Lake Charles Chemical Complex SASOL CHEMICALS (USA) LLC 5/23/2014 2,682 HP GCP 0.14 g/hp-hr BACT-PSD Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None 0.15 g/hp-hr BACT-PSD 99 CIVIL ENGINEER SQUADRON OF USAF 2/26/2008 1,350 hP Turbocharger 0.20 g/hp-hr Other Case-by-Case TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Compliance 0.21 g/hp-hr Other Case-by-Case | LA-0296 | - | SASOL CHEMICALS (USA) LLC | 5/23/2014 | 2.682 | НР | NSPS Compliance | 0.14 | g/hn-hr | BACT-PSD |
| Energy Answers Arecibo Puerto Rico PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None 0.15 g/hp-hr BACT-PSD 99 CIVIL ENGINEER SQUADRON OF VSAF 1,350 hP Turbocharger 0.20 g/hp-hr Other Case-by-Case TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Compliance 0.21 g/hp-hr Other Case-by-Case | - | | | | | | · · · · · · · · · · · · · · · · · · · | | | |
| PR-0009 Renewable Energy Project ENERGY ANSWERS ARECIBO, LLC 4/10/2014 670 hP None 0.15 g/hp-hr BACT-PSD 99 CIVIL ENGINEER SQUADRON OF USAF 2/26/2008 1,350 hP Turbocharger 0.20 g/hp-hr Other Case-by-Case TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Compliance 0.21 g/hp-hr Other Case-by-Case | 271 0200 | <u>.</u> | 57.502 67.27.000 (667.1) 226 | 3/23/2011 | 2,002 | | 00. | 0.11 | 6/ 11P 111 | DACT 13D |
| NV-0047 Nellis Air Force Base USAF 2/26/2008 1,350 hP Turbocharger 0.20 g/hp-hr Other Case-by-Case TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Compliance 0.21 g/hp-hr Other Case-by-Case | PR-0009 | · · | ENERGY ANSWERS ARECIRO LLC | 4/10/2014 | 670 | hP | None | 0.15 | g/hn-hr | BACT-PSD |
| NV-0047 Nellis Air Force Base USAF 2/26/2008 1,350 hP Turbocharger 0.20 g/hp-hr Other Case-by-Case TX-0728 Peony Chemical Manufacturing Facility BASF 4/1/2015 1,500 HP NSPS Compliance 0.21 g/hp-hr Other Case-by-Case | 110005 | nenewasie Energy i roject | | 7, 10, 2014 | 370 | | 110110 | 0.13 | ייי איי יט | 5.101135 |
| | NV-0047 | Nellis Air Force Base | = | 2/26/2008 | 1,350 | hP | Turbocharger | 0.20 | g/hp-hr | Other Case-by-Case |
| | | | | | | | | | | · |
| | TX-0728 | Peony Chemical Manufacturing Facility | BASF | 4/1/2015 | 1,500 | HP | NSPS Compliance | 0.21 | g/hp-hr | Other Case-by-Case |
| | IN-0158 | St. Joseph Energy Center, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 2,012 | HP | GCP | | | BACT-PSD |

Emergency Generator Table D-5 - RBLC Results for Emergency-Fire Pump

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|-----------|--|----------------------------------|--------------------|------------|-------|-----------------|---------------|------------|----------------------|
| | Moundsville Combined Cycle Power | | | | | | | | |
| WV-0025 | Plant | MOUNDSVILLE POWER, LLC | 11/21/2014 | 2,016 | HP | None | 0.28 | g/hp-hr | BACT-PSD |
| PA-0291 | Hickory Run Energy Station | HICKORY RUN ENERGY LLC | 4/23/2013 | 1,135 | hP | None | | g/hp-hr | Other Case-by-Case |
| | | | | | | | | | |
| LA-0292 | Holbrook Compressor Station | CAMERON INTERSTATE PIPELINE LLC | 1/22/2016 | 1,341 | HP | GCP | 0.28 | g/hp-hr | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | 2,922 | hP | GCP | 0.29 | g/hp-hr | BACT-PSD |
| | | MID AMERICAN STEEL AND WIRE | | | | | | | |
| OK-0128 | Mid American Steel Rolling Mill | COMPANY | 9/8/2008 | | | None | | g/hp-hr | BACT-PSD |
| VA-0327 | Perdue Grain And Oilseed, LLC | PERDUE AGRIBUSINESS, LLC | 7/12/2017 | 760 | hP | None | 0.29 | g/hp-hr | BACT-PSD |
| 0470 | | | 6/4/2044 | 2.500 | | | 0.04 | , , | D 4 CT DCD |
| IN-0173 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | 3,600 | | GCP | | g/hp-hr | BACT-PSD |
| IN-0179 | Ohio Valley Resources, LLC | OHIO VALLEY RESOURCES, LLC | 9/25/2013 | 4,690 | НР | GCP | 0.31 | g/hp-hr | BACT-PSD |
| IN-0180 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | 3,600 | ШΒ | GCP | 0.21 | g/hp-hr | BACT-PSD |
| 114-0190 | Wildwest Fertilizer Corporation | WIDWEST FERTILIZER CORPORATION | 0/4/2014 | 3,600 | пг | GCP | 0.51 | g/IIp-III | DACI-P3D |
| NV-0049 | Harrah's Operating Company, Inc. | HARRAH'S OPERATING COMPANY, INC. | 8/20/2009 | 1,232 | НР | Turbocharger | 0.32 | g/hp-hr | Other Case-by-Case |
| AK-0082 | Point Thomson Production Facility | EXXON MOBIL CORPORATION | 1/23/2015 | 2,695 | | None | | g/hp-hr | BACT-PSD |
| 7.11 0002 | | WESTERN FARMERS ELECTRIC | 2,20,2010 | 2,033 | | | 0.02 | 876 | 27.01.02 |
| OK-0154 | Mooreland Generating Sta | COOPERATIVE | 7/2/2013 | 1,341 | HP | GCP | 0.32 | g/hp-hr | BACT-PSD |
| | | ASSOCIATED ELECTRIC COOPERATIVE | , , | ,- | | | | O/ - | |
| OK-0129 | Chouteau Power Plant | INC | 1/23/2009 | 2,200 | HP | GCP | 0.32 | g/hp-hr | BACT-PSD |
| | | | | | | | | | |
| IN-0263 | Midwest Fertilizer Company LLC | MIDWEST FERTILIZER COMPANY LLC | 3/23/2017 | 3,600 | HP | GCP | 0.35 | g/hp-hr | BACT-PSD |
| IN-0158 | St. Joseph Energy Center, LLC | ST. JOSEPH ENERGY CENTER, LLC | 12/3/2012 | 1,006 | HP | GCP | 0.47 | g/hp-hr | BACT-PSD |
| OH-0352 | Oregon Clean Energy Center | ARCADIS, US, INC. | 6/18/2013 | 2,250 | kW | NSPS Compliance | 0.79 | g/hp-hr | BACT-PSD |
| | | | | | | | | | |
| LA-0254 | Ÿ | ENTERGY LOUISIANA LLC | 8/16/2011 | 1,250 | | GCP, Clean Fuel | | g/hp-hr | BACT-PSD |
| OK-0175 | Wildhorse Terminal | WILDHORSE TERMINAL LLC | 6/29/2017 | 500 | | GCP | | g/hp-hr | BACT-PSD |
| LA-0313 | St. Charles Power Station | ENTERGY LOUISIANA, LLC | 8/31/2016 | 2,584 | | GCP | | g/hp-hr | BACT-PSD |
| MD-0044 | Cove Point LNG Terminal | DOMINION COVE POINT LNG, LP | 6/9/2014 | 1,550 | HP | GCP, Clean Fuel | 4.80 | g/hp-hr | LAER |
| | | | 0 /40 /0000 | 700 | | | 0.00 | // // / | |
| IA-0095 | Tate & Lyle Ingredients Americas, Inc. | LOVAVA FEDTILIZED COMMONNY | 9/19/2008 | 700 | - | None GCP | | g/kW-hr | BACT-PSD |
| IA-0105 | lowa Fertilizer Company | IOWA FERTILIZER COMPANY | 10/26/2012 | 2,000 | kW | | | g/kW-hr | BACT-PSD |
| IL-0114 | Cronus Chemicals, LLC CF Industries Nitrogen, LLC - Port Neal | CRONUS CHEMICALS, LLC | 9/5/2014 | 3,755 | нР | NSPS Compliance | 0.40 | g/kW-hr | BACT-PSD |
| IA-0106 | Nitrogen Complex | CF INDUSTRIES NITROGEN, LLC | 7/12/2013 | | | GCP | 4.00 | g/kW-hr | BACT-PSD |
| SC-0113 | Pyramax Ceramics, LLC | PYRAMAX CERAMICS, LLC | 2/8/2012 | 757 | ЦΒ | NSPS Compliance | | g/kW-hr | BACT-PSD BACT-PSD |
| OH-0317 | Ohio River Clean Fuels, LLC | OHIO RIVER CLEAN FUELS, LLC | 11/20/2008 | | | GCP | | g/kW-hr | BACT-PSD BACT-PSD |
| SC-0159 | US10 Facility | MICHELIN NORTH AMERICA, INC. | 7/9/2012 | 1,000 | | NSPS Compliance | | g/kW-hr | BACT-PSD BACT-PSD |
| ID-0018 | Langley Gulch Power Plant | IDAHO POWER COMPANY | 6/25/2012 | 750 | | GCP | | g/kW-hr | BACT-PSD |
| .5 0010 | | DYNO NOBEL LOUISIANA AMMONIA, | 3,23,2310 | , 50 | | | 0.40 | 0/ 1/4 1/1 | 2 |
| LA-0272 | Ammonia Production Facility | LLC | 3/27/2013 | 1,200 | НР | GCP | 6.40 | g/kW-hr | BACT-PSD |
| NY-0104 | CPV Valley Energy Center | CPV VALLEY LLC | 8/1/2013 | 2,200 | ļ | GCP | | lb/MMBtu | |

Table D-5 Addendum: RBLC Results for Emergency Generator Updated Data: November 2018 to October 2021

| | I | | | L I | | А | | | _ |
|--------------------|---|--------------------------------------|--------------------------|---------------|-----------|-------------------------------------|----------------|--------------------|------|
| RBLC ID | Facility Name | Company Name | Permit Date | | Units | Controls ^A | Emission Limit | Units | Туре |
| AD 0171 | NUICOR CTEFL ARVANCAC | NUICOR CORRODATION | Nitrogen Oxi | | L | loca | 1 3 | C/KIA/ LID | BACT |
| AR-0171 KY-0110 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 1073 | bhp HP | GCP GCP | | G/KW-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG NUCOR STEEL BRANDENBURG | NUCOR NUCOR | 07/23/2020 07/23/2020 | 920 700 | HP | GCP | | G/HP-HR G/HP-HR | BACT |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 1500 | HP | GCP | | 3/HP-HK G/KW-H | BACT |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | 1341 | HP | GCP | 14.96 | | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | HR/YR | GCP/high efficiency design/CBF | | G/HP-HR | BACT |
| VA-0332 | CHICKAHOWINT FOWER LEC | CHICKAHOWINT FOWER LEC | Carbon Mono | | TIII TIX | der / High emiciency design/ cbi | 1 31 | 3/111-1110 | DACI |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 1073 | bhp | GCP | 4 | G/KW-HR | BACT |
| IL-0130 | JACKSON ENERGY CENTER | JACKSON GENERATION, LLC | 12/31/2018 | 1500 | kW | 00. | | G/KW-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 920 | HP | GCP | | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 700 | HP | GCP | | G/HP-HR | BACT |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 1500 | HP | GCP | | G/KW-H | BACT |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 4474.2 | KW | GCP | | G/KW-H | BACT |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | 1341 | HP | GCP | 7.7 | | BACT |
| *PA-0326 | | SHELL CHEMICAL APPALACHIA LLC | 02/18/2021 | 0 | | GCP/engine design | 0.5 | G | BACT |
| *PA-0326 | | SHELL CHEMICAL APPALACHIA LLC | 02/18/2021 | 0 | | GCP/engine design | 0.5 | G . | BACT |
| *PA-0326 | | SHELL CHEMICAL APPALACHIA LLC | 02/18/2021 | 0 | | GCP/engine design | | GRAM | BACT |
| TX-0889 | SWEENY OLD OCEAN FACILITIES | CHEVRON PHILLIPS CHEMICAL COMPANY LP | 08/08/2020 | 0 | | GCP/engine design | | HR/YR | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | HR/YR | GCP/high efficiency design/CBF | | G/HP-H | BACT |
| | | | tile Organic Co | | | 1 | | | |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 1073 | bhp | GCP | 1 | G/KW-HR | BACT |
| LA-0366 | HOLDEN WOOD PRODUCTS MILL | WEYERHAEUSER NR COMPANY | 02/03/2021 | 0 | | GCP | 804.6 | HP | BACT |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | 1341 | HP | GCP | 14.96 | LB/H | BACT |
| OK-0181 | WILDHORSE TERMINAL | KEYERA ENERGY INC | 09/11/2019 | 0 | | GCP | 3 | GM/HP-HR | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | HR/YR | GCP/high efficiency design/CBF | 0.11 | G/HP-HR | BACT |
| | | | PM ₁₀ (tota | I) | | | | | |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 1073 | bhp | GCP | 0.2 | G/KW-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 920 | HP | GCP | 0.15 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 700 | HP | GCP | 0.15 | G/HP-HR | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 700 | HP | GCP | 0.15 | G/HP-HR | BACT |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 1500 | HP | GCP/CBF | 0.69 | LB/H | BACT |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 4474.2 | KW | GCP/CBF | 1 | LB/H | BACT |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | 1341 | HP | GCP | 0.44 | LB/H | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | HR/YR | GCP/high efficiency design/CBF | 0.15 | G/HP-HR | BACT |
| | | | PM _{2.5} (tota | I) | | | | | |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 1073 | bhp | GCP | 0.2 | G/KW-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 920 | HP | GCP | | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 700 | HP | GCP | 0.15 | G/HP-HR | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 700 | HP | GCP | 0.15 | G/HP-HR | BACT |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 1500 | HP | CBF | 0.69 | LB/H | BACT |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 4474.2 | KW | CBF | 1 | LB/H | BACT |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | 1341 | HP | GCP | 0.44 | LB/H | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | HR/YR | GCP/high efficiency design/CBF | 0.15 | G/HP-HR | BACT |
| | | Greenho | use Gases - CO | 2 Equivalents | | | | | |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 1073 | bhp | GCP | 163 | LB/MMBTU | BACT |
| IL-0130 | JACKSON ENERGY CENTER | JACKSON GENERATION, LLC | 12/31/2018 | 1500 | kW | | 225 | TONS/YEAR | BACT |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 1500 | HP | GCP/energy efficiency measures. | 406 | | BACT |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 4474.2 | KW | GCP/CBF/energy efficiency measures. | 590 | • | BACT |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | 1341 | HP | GCP | 80 | | BACT |
| *PA-0326 | SHELL POLYMERS MONACA SITE | SHELL CHEMICAL APPALACHIA LLC | 02/18/2021 | 0 | | GCP | | TONS | BACT |
| *PA-0326 | SHELL POLYMERS MONACA SITE | SHELL CHEMICAL APPALACHIA LLC | 02/18/2021 | 0 | | GCP | 10 | TONS | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | HR/YR | GCP/high efficiency design/CBF | 106 | Γ/YR | BACT |
| | | | Sulfuric Acid I | | | | | | |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | HR/YR | GCP/high efficiency design/CBF | 0.0001 | LB/MMBTU | BACT |
| | | | Opacity | | | | | | |
| AR-0171 | NUCOR STEEL ARKANSAS | NUCOR CORPORATION | 02/14/2019 | 1073 | bhp | GCP | 20 | % | BACT |
| | | | | | | | | | |

(a) GCP = good combustion practices, CBF = clean burning fuels

Emergency Fire Pump Table D-6 - RBLC Results for Emergency Generator

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Type |
|-----------|--|------------------------|-------------|------------|-------|---------------------------------------|---------------|-----------------------|---------------|
| - | , | | | Monoxide | | | | | 71. |
| | | AVENAL POWER CENTER | | | | | | | |
| CA-1192 | Avenal Energy Project | LLC | 6/21/2011 | 288 | НР | Turbocharger, aftercooler | 0.45 | g/HP-hr | BACT-PSD |
| | , , | CRICKET VALLEY ENERGY | -, , - | | | , , , , , , , , , , , , , , , , , , , | | O, | |
| NY-0103 | Cricket Valley Energy Center | CENTER LLC | 2/3/2016 | 460 | НР | GCP | 0.53 | g/HP-hr | BACT-PSD |
| | Flopam Inc. Facility | FLOPAM INC. | 4/26/2011 | 444 | | GCP | | g/HP-hr | BACT-PSD |
| | | GRAIN PROCESSING | , -, - | | | | | U/ | |
| IN-0234 | Grain Processing Corporation | CORPORATION | 12/8/2015 | 425 | НР | GCP | 2.01 | g/HP-hr | BACT-PSD |
| | Oregon Clean Energy Center | ARCADIS, US, INC. | 6/18/2013 | 300 | | NSPS | 2.57 | , | BACT-PSD |
| | and the second second | | 5, 25, 2525 | | 1 11 | | | <i>8,</i> · · · · · · | 1 |
| NI-0085 | Middlesex Energy Center, LLC | STONEGATE POWER, LLC | 7/19/2016 | 327 | НР | Clean Fuels | 2.59 | g/HP-hr | BACT-PSD |
| 143 0003 | initializate Energy center, EEC | ASSOCIATED ELECTRIC | 7/13/2010 | 32, | | Cicari racis | 2.33 | 6/ 111 111 | - D/(C) 13D |
| OK-0129 | Chouteau Power Plant | COOPERATIVE INC | 1/23/2009 | 267 | НР | None | 2 60 | g/HP-hr | BACT-PSD |
| OK OILS | endited i over i lant | COMPETITIVE POWER | 1/23/2003 | 207 | | Tronc | 2.00 | 6/ 111 111 | - Dr. (C. 135 |
| | | VENTURES, INC./CPV | | | | | | | · |
| MD-0040 | CPV St Charles | MARYLAND, LLC | 11/12/2008 | 300 | нр | None | 2 60 | g/HP-hr | BACT-PSD |
| | CPV St. Charles | CPV MARYLAND, LLC | 4/23/2014 | 300 | | GCP, Clean Fuels | 2.60 | Ū. | BACT-PSD |
| IVID-0041 | Energy Answers Arecibo Puerto Rico | ENERGY ANSWERS | 4/23/2014 | 300 | 111 | Ger, clearrides | 2.00 | 8/111-111 | DACI-13D |
| DD-0000 | Renewable Energy Project | ARECIBO, LLC | 4/10/2014 | 335 | HD | None | 2 60 | g/HP-hr | BACT-PSD |
| | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | 260 | | GCP, NSPS | 2.60 | | BACT-PSD |
| 1011-0423 | Lake Charles Chemical Complex Ethylene 2 | SASOL CHEMICALS (USA) | 1/4/2017 | 200 | TIF | GCF, NSF3 | 2.00 | g/11F-111 | BACI-F3D |
| LA-0301 | 1 | LLC | 5/23/2014 | 500 | ШΒ | GCP, NSPS | 2.60 | g/HP-hr | BACT-PSD |
| LA-0301 | Offic | MIDWEST FERTILIZER | 3/23/2014 | 300 | ПР | GCF, N3F3 | 2.00 | g/ nr-iii | BAC1-P3D |
| INI 0172 | Midwest Fertilizer Corporation | CORPORATION | C/4/2014 | 500 | LID | GCP | 2.00 | ~/UD ha | BACT-PSD |
| IIV-01/3 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER | 6/4/2014 | 500 | пР | GCP | 2.00 | g/HP-hr | BACT-P3D |
| INI 0172 | Midwest Fortilizer Corneration | CORPORATION | C/4/2014 | F00 | LID | CCD | 2.00 | ~/UD ha | DACT DCD |
| IN-0173 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER | 6/4/2014 | 500 | пР | GCP | 2.00 | g/HP-hr | BACT-PSD |
| INI 0100 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | LID | GCP | 2.00 | ~/UD ha | DACT DCD |
| IIV-0180 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER | 6/4/2014 | 500 | ПР | GCP | 2.60 | g/HP-hr | BACT-PSD |
| INI 0100 | Midwest Fortilizer Corneration | CORPORATION | C/4/2014 | F00 | LID | GCP | 2.00 | ~/UD ha | DACT DCD |
| IN-0180 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | HP | GCP | 2.60 | g/HP-hr | BACT-PSD |
| 14 0354 | Nice and I - Beint Electric Consenting Blant | ENTERCYLOUIGIANIA II C | 0/46/2044 | 250 | | CCD Class Finals | 2.00 | -/UD b | DACT DCD |
| LA-0254 | Ninemile Point Electric Generating Plant | ENTERGY LOUISIANA LLC | 8/16/2011 | 350 | нР | GCP, Clean Fuels | 2.60 | g/HP-hr | BACT-PSD |
| 011 0247 | Ohia Bissa Class Fuels III C | OHIO RIVER CLEAN | 44/20/2000 | 200 | | CCD | 2.00 | -/UD b | DACT DCD |
| OH-0317 | Ohio River Clean Fuels, LLC | FUELS, LLC | 11/20/2008 | 300 | HP | GCP | 2.60 | g/HP-hr | BACT-PSD |
| 101 04 70 | | OHIO VALLEY | 0/25/2042 | 404 | | COD | 2.50 | /115.1 | DAGT BCD |
| IN-0179 | Ohio Valley Resources, LLC | RESOURCES, LLC | 9/25/2013 | 481 | НР | GCP | 2.60 | g/HP-hr | BACT-PSD |
| | | | 0/=/004 | 0-0 | | | | | |
| NJ-0081 | PSEG Fossil LLC Sewaren Generating Station | PSEG FOSSIL LLC | 3/7/2014 | 250 | НР | None | 2.60 | g/HP-hr | BACT-PSD |
| | | | 0/04/0046 | | | | | | |
| LA-0313 | St. Charles Power Station | ENTERGY LOUISIANA, LLC | 8/31/2016 | 282 | НР | GCP, NSPS | 2.60 | g/HP-hr | BACT-PSD |
| | | ST. JOSEPH ENERGY | | | | | | | |
| IN-0158 | St. Joseph Energy Center, LLC | CENTER, LLC | 12/3/2012 | 371 | HP | GCP | 2.60 | g/HP-hr | BACT-PSD |
| | | | | | | | | | |
| | Sweet Sorghum-To-Ethanol Advanced | SOUTHEAST RENEWABLE | | | | | | | |
| FL-0322 | Biorefinery | FUELS (SRF), LLC | 12/23/2010 | 600 | ΗP | None | 2.60 | g/HP-hr | BACT-PSD |

Emergency Fire Pump Table D-6 - RBLC Results for Emergency Generator

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|-----------|--|--------------------------|--------------------|------------|----------|------------------|---------------|--|-----------|
| | | CONSUMERS ENERGY | | | | | | | |
| MI-0410 | Thetford Generating Station | COMPANY | 7/25/2013 | 315 | HP | GCP, Clean Fuels | 2.60 | g/HP-hr | BACT-PSD |
| | | MOUNDSVILLE POWER, | | | | | | | |
| WV-0025 | Moundsville Combined Cycle Power Plant | LLC | 11/21/2014 | 251 | HP | None | 2.60 | g/HP-hr | BACT-PSD |
| | | DOMINION COVE POINT | | | | | | | |
| MD-0044 | Cove Point LNG Terminal | LNG, LP | 6/9/2014 | 350 | HP | GCP | 3.00 | g/HP-hr | BACT-PSD |
| | | SOUTHWEST ELECTRIC | | | | | | | |
| | | POWER COMPANY | | | | | | | |
| LA-0224 | Arsenal Hill Power Plant | (SWEPCO) | 3/20/2008 | 310 | НР | GCP, Clean Fuels | 3.03 | g/HP-hr | BACT-PSD |
| | Holland Board Of Public Works - East 5th | HOLLAND BOARD OF | | | | | | <u>. </u> | |
| MI-0412 | Street | PUBLIC WORKS | 12/4/2013 | 165 | HP | GCP | 3.70 | g/HP-hr | BACT-PSD |
| | Holland Board Of Public Works - East 5th | HOLLAND BOARD OF | , , | | | | | <i>.</i> | |
| MI-0424 | | PUBLIC WORKS | 12/5/2016 | 165 | HP | GCP | 3.70 | g/HP-hr | BACT-PSD |
| | | | , , , , , | | | | | O, | |
| IL-0114 | Cronus Chemicals, LLC | CRONUS CHEMICALS, LLC | 9/5/2014 | 373 | НР | GCP, NSPS | 3.50 | g/kW-hr | BACT-PSD |
| | Flopam Inc. Facility | FLOPAM INC. | 4/26/2011 | 193 | | None | 3.50 | g/kW-hr | BACT-PSD |
| 27.0201 | , repair me recincy | IOWA FERTILIZER | ., 20, 2011 | | | | 0.00 | 6/ | 27.61.102 |
| IA-0105 | lowa Fertilizer Company | COMPANY | 10/26/2012 | 235 | kW/ | GCP | 3 50 | g/kW-hr | BACT-PSD |
| 171 0103 | iowa i citilizar company | KEYS ENERGY CENTER, | 10/20/2012 | 233 | 1.00 | | 3.30 | 6/ 111 | B/(C) 13B |
| MD-0046 | Keys Energy Center | LLC | 10/31/2014 | 300 | HP | GCP, Clean Fuels | 3 50 | g/kW-hr | BACT-PSD |
| 1010-0040 | Reys Energy Center | KEYS ENERGY CENTER, | 10/31/2014 | 300 | 111 | der, clearr ders | 3.30 | 8/ KVV-111 | BACT-13D |
| MD-0046 | Keys Energy Center | LLC | 10/31/2014 | 1500 | KW | GCP, Clean Fuels | 3 50 | g/kW-hr | BACT-PSD |
| 1010-0040 | Reys Ellergy Celiter | LLC | 10/31/2014 | 1300 | KVV | GCF, Clean Fuels | 3.30 | g/KVV-III | BACT-P3D |
| EL 0246 | Lauderdale Plant | FLORIDA POWER & LIGHT | 4/22/2014 | 200 | шъ | GCP | 2.50 | a/1011 br | DACT DCD |
| FL-0346 | Lauderdale Plant | FLORIDA POWER & LIGHT | 4/22/2014 | 300 | ПР | GCP | 3.50 | g/kW-hr | BACT-PSD |
| EL 03E4 | Laudardala Diant | FLORIDA POWER & LIGHT | 0/25/2015 | 200 | LID | Class Fuels | 2.50 | ~/IdA/ ha | DACT DCD |
| FL-0354 | Lauderdale Plant | MATTAWOMAN ENERGY, | 8/25/2015 | 300 | ПР | Clean Fuels | 3.50 | g/kW-hr | BACT-PSD |
| NAD 0045 | Matter Conton | • | 44/42/2045 | 205 | LIB | CCD Class Fuels | 2.50 | -/134/ | DACT DCD |
| MD-0045 | Mattawoman Energy Center | LLC | 11/13/2015 | 305 | НР | GCP, Clean Fuels | 3.50 | g/kW-hr | BACT-PSD |
| EL 0256 | Oles albahas Class Francis Cantan | ELODIDA DOMED O LICUT | 2 /2 /204 6 | 422 | | COD | 2.50 | /134/1 | DAGT DCD |
| FL-0356 | Okeechobee Clean Energy Center | FLORIDA POWER & LIGHT | 3/9/2016 | 422 | НР | GCP | 3.50 | g/kW-hr | BACT-PSD |
| | | SOLID WASTE | | | | | | | |
| EL 0224 | | AUTHORITY OF PALM | 42/22/2040 | 250 | | COD CL . F . I | 2.50 | /134/1 | DAGT DCD |
| | Palm Beach Renewable Energy Park | BEACH COUNTY | 12/23/2010 | 250 | | GCP, Clean Fuels | | g/kW-hr | BACT-PSD |
| CA-1212 | Palmdale Hybrid Power Project | CITY OF PALMDALE | 10/18/2011 | 182 | HP | None | 3.50 | g/kW-hr | BACT-PSD |
| | | | - 1- 1 | | | | | | |
| | Pyramax Ceramics, LLC | PYRAMAX CERAMICS, LLC | 2/8/2012 | 500 | | NSPS | | g/kW-hr | BACT-PSD |
| | Victorville 2 Hybrid Power Project | CITY OF VICTORVILLE | 3/11/2010 | | KW | None | | Ċ. | BACT-PSD |
| MI-0389 | Karn Weadock Generating Complex | CONSUMERS ENERGY | 12/29/2009 | 40 | KW | GCP, Clean Fuels | 5.00 | g/kW-hr | BACT-PSD |
| | | | | | | | | | |
| SC-0113 | Pyramax Ceramics, LLC | PYRAMAX CERAMICS, LLC | 2/8/2012 | 29 | HP | GCP | 5.50 | g/kW-hr | BACT-PSD |
| | | | | | | | | | |
| TX-0799 | Beaumont Terminal | PHILLIPS 66 PIPELINE LLC | 6/8/2016 | | | GCP | 0.01 | lb/HP-hr | BACT-PSD |
| | | | | | | | | | |
| | PSEG Fossil LLC Sewaren Generating Station | PSEG FOSSIL LLC | 3/10/2016 | 2.6 | MMBtu/hr | Clean Fuels | | lb/MMBtu | |
| NY-0104 | CPV Valley Energy Center | CPV VALLEY LLC | 8/1/2013 | | | GCP | 0.75 | lb/MMBtu | BACT-PSD |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|---------|--|------------------------|-----------------|----------------|-------------|------------------|---------------|------------|----------|
| AK-0083 | Kenai Nitrogen Operations | AGRIUM U.S. INC. | 1/6/2015 | 2.7 | MMBtu/hr | None | 0.95 | lb/MMBtu | BACT-PSD |
| | | | | | | | | | |
| LA-0204 | Plaquemine PVC Plant | SHINTECH LOUISIANA LLC | | 420 | | GCP, Clean Fuels | 0.95 | lb/MMBtu | BACT-PSD |
| | | _ | eenhouse Gas | es - Carbon Di | oxide | | 1 | 1 | |
| | | MIDWEST FERTILIZER | | | | | | | |
| IN-0173 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | HP | GCP | 527.40 | g/HP-hr | BACT-PSD |
| | | MIDWEST FERTILIZER | | | | | | | |
| IN-0173 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | HP | GCP | 527.40 | g/HP-hr | BACT-PSD |
| | | MIDWEST FERTILIZER | | | | | | | |
| IN-0180 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | HP | GCP | 527.40 | g/HP-hr | BACT-PSD |
| | | MIDWEST FERTILIZER | | | | | | | |
| IN-0180 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | HP | GCP | 527.40 | g/HP-hr | BACT-PSD |
| | | OHIO VALLEY | | | | | | | |
| IN-0179 | Ohio Valley Resources, LLC | RESOURCES, LLC | 9/25/2013 | 481 | HP | GCP | 527.40 | g/HP-hr | BACT-PSD |
| | | IOWA FERTILIZER | | | | | | | |
| IA-0105 | Iowa Fertilizer Company | COMPANY | 10/26/2012 | 235 | kW | GCP | 1.55 | g/kW-hr | BACT-PSD |
| | | | | | | | | | |
| LA-0254 | Ninemile Point Electric Generating Plant | ENTERGY LOUISIANA LLC | 8/16/2011 | 350 | | GCP | 163.00 | lb/MMBtu | BACT-PSD |
| | | | ouse Gases - Ca | rbon Dioxide | Equivalents | | T | 1 | |
| | | MOUNDSVILLE POWER, | | | | | | | |
| WV-0025 | Moundsville Combined Cycle Power Plant | LLC | 11/21/2014 | 251 | HP | None | 558.41 | g/HP-hr | BACT-PSD |
| | | LOWER COLORADO | | | | | | | |
| TX-0612 | Thomas C. Ferguson Power Plant | RIVER AUTHORITY | 11/10/2011 | 617 | HP | GCP | 5,166.54 | g/HP-hr | BACT-PSD |
| | | FOOTPRINT POWER | | | | | | | |
| | | SALEM HARBOR | | | | | | | |
| MA-0039 | Salem Harbor Station Redevelopment | DEVELOPMENT LP | 1/30/2014 | | MMBtu/hr | None | 162.85 | lb/MMBtu | BACT-PSD |
| | | T | | Acid Mist | ı | | • | ı | T |
| | | MATTAWOMAN ENERGY, | | | | | | | |
| | Mattawoman Energy Center | LLC | 11/13/2015 | 305 | HP | GCP, Clean Fuels | 7.00E-03 | ŭ. | BACT-PSD |
| NY-0104 | CPV Valley Energy Center | CPV VALLEY LLC | 8/1/2013 | | | Clean Fuels | 3.00E-05 | lb/MMBtu | BACT-PSD |
| | | CRICKET VALLEY ENERGY | | | | | | | |
| NY-0103 | Cricket Valley Energy Center | CENTER LLC | 2/3/2016 | 460 | HP | Clean Fuels | 1.00E-04 | lb/MMBtu | BACT-PSD |
| | | FOOTPRINT POWER | | | | | | | |
| | | SALEM HARBOR | | | | | | | |
| MA-0039 | Salem Harbor Station Redevelopment | DEVELOPMENT LP | 1/30/2014 | 2.7 | MMBtu/hr | None | 1.11E-04 | lb/MMBtu | BACT-PSD |
| | | | | | | | | | |
| FL-0354 | Lauderdale Plant | FLORIDA POWER & LIGHT | 8/25/2015 | 300 | HP | Clean Fuels | 15.00 | ppm Sulfur | BACT-PSD |
| | | LOUISIANA ENERGY CO | Nitroge | en Dioxide | | | | 1 | |
| | | LOUISIANA ENERGY AND | | | | | | | |
| | | POWER AUTHORITY | 0.10 = 1=== | | | | | | |
| | Morgan City Power Plant | (LEPA) | 9/26/2013 | 380 | | GCP | | | BACT-PSD |
| OH-0352 | Oregon Clean Energy Center | ARCADIS, US, INC. | 6/18/2013 | 300 | HP | NSPS | 2.57 | g/HP-hr | BACT-PSD |
| | | MIDWEST FERTILIZER | 01-1 | | | | | | |
| IN-0173 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | HP | GCP | 2.83 | g/HP-hr | BACT-PSD |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|---------|--|------------------------|-------------|------------|-------|---------------------------|---------------|---------|----------|
| | | MIDWEST FERTILIZER | | | | | | | |
| IN-0173 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | HP | GCP | 2.83 | g/HP-hr | BACT-PSD |
| | | MIDWEST FERTILIZER | | | | | | | |
| IN-0180 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | HP | GCP | 2.83 | g/HP-hr | BACT-PSD |
| | | MIDWEST FERTILIZER | | | | | | | |
| IN-0180 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | HP | GCP | 2.83 | g/HP-hr | BACT-PSD |
| | Energy Answers Arecibo Puerto Rico | ENERGY ANSWERS | | | | | | | |
| PR-0009 | Renewable Energy Project | ARECIBO, LLC | 4/10/2014 | 335 | HP | None | 2.85 | g/HP-hr | BACT-PSD |
| | | OHIO VALLEY | | | | | | | |
| IN-0179 | Ohio Valley Resources, LLC | RESOURCES, LLC | 9/25/2013 | 481 | HP | GCP | 2.86 | g/HP-hr | BACT-PSD |
| | Lake Charles Chemical Complex Ethylene 2 | SASOL CHEMICALS (USA) | | | | | | | |
| LA-0301 | Unit | LLC | 5/23/2014 | 500 | HP | GCP, NSPS | 2.91 | g/HP-hr | BACT-PSD |
| | | | | | | | | | |
| | Sweet Sorghum-To-Ethanol Advanced | SOUTHEAST RENEWABLE | | | | | | | |
| FL-0322 | Biorefinery | FUELS (SRF), LLC | 12/23/2010 | 600 | HP | None | 3.00 | g/HP-hr | BACT-PSD |
| | | BENTELER STEEL / TUBE | | | | | | | |
| | | MANUFACTURING | | | | | | | |
| LA-0309 | Benteler Steel Tube Facility | CORPORATION | 6/4/2015 | 288 | HP | NSPS | 3.00 | g/HP-hr | BACT-PSD |
| | | COMPETITIVE POWER | | | | | | | |
| | | VENTURES, INC./CPV | | | | | | | |
| MD-0040 | CPV St Charles | MARYLAND, LLC | 11/12/2008 | 300 | HP | None | 3.00 | g/HP-hr | BACT-PSD |
| LA-0251 | Flopam Inc. Facility | FLOPAM INC. | 4/26/2011 | 444 | HP | None | 3.00 | g/HP-hr | BACT-PSD |
| | Holland Board Of Public Works - East 5th | HOLLAND BOARD OF | | | | | | | |
| MI-0412 | Street | PUBLIC WORKS | 12/4/2013 | 165 | HP | GCP | 3.00 | g/HP-hr | BACT-PSD |
| | Holland Board Of Public Works - East 5th | HOLLAND BOARD OF | | | | | | | |
| MI-0424 | Street | PUBLIC WORKS | 12/5/2016 | 165 | | GCP | | g/HP-hr | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | 260 | HP | GCP, NSPS | 3.00 | g/HP-hr | BACT-PSD |
| | | MOUNDSVILLE POWER, | | | | | | | |
| WV-0025 | Moundsville Combined Cycle Power Plant | LLC | 11/21/2014 | 251 | HP | None | 3.00 | g/HP-hr | BACT-PSD |
| | | | | | | | | | |
| LA-0313 | St. Charles Power Station | ENTERGY LOUISIANA, LLC | 8/31/2016 | 282 | HP | GCP, NSPS | 3.00 | g/HP-hr | BACT-PSD |
| | | ST. JOSEPH ENERGY | | | | | | | |
| IN-0158 | St. Joseph Energy Center, LLC | CENTER, LLC | 12/3/2012 | 371 | HP | GCP | 3.00 | g/HP-hr | BACT-PSD |
| | | CONSUMERS ENERGY | | | | | | | |
| MI-0410 | Thetford Generating Station | COMPANY | 7/25/2013 | 315 | HP | GCP, Clean Fuels | 3.00 | g/HP-hr | BACT-PSD |
| | | WOLVERINE POWER | | | | | | | |
| | | SUPPLY COOPERATIVE, | | | | | | | |
| MI-0400 | Wolverine Power | INC. | 6/29/2011 | 420 | HP | None | 3.00 | g/HP-hr | BACT-PSD |
| | | AVENAL POWER CENTER | | | | | | | |
| CA-1192 | Avenal Energy Project | LLC | 6/21/2011 | 288 | HP | Turbocharger, aftercooler | 3.40 | g/HP-hr | BACT-PSD |
| | | 99 CIVIL ENGINEER | | | | | | | |
| NV-0047 | Nellis Air Force Base | SQUADRON OF USAF | 2/26/2008 | 500 | HP | GCP, NSPS | 3.88 | g/HP-hr | BACT-PSD |
| | | ASSOCIATED ELECTRIC | | | | | | | |
| OK-0129 | Chouteau Power Plant | COOPERATIVE INC | 1/23/2009 | 267 | HP | None | 7.80 | g/HP-hr | BACT-PSD |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|----------|------------------------------------|--------------------------------|-------------|-------------|---------|-------------------------------------|---------------|----------|----------|
| | | OHIO RIVER CLEAN | | <u> </u> | | | | | , |
| OH-0317 | Ohio River Clean Fuels, LLC | FUELS, LLC | 11/20/2008 | 300 | HP | GCP, ITR, Turbocharger, aftercooler | 7.80 | g/HP-hr | BACT-PSD |
| | | GRAIN PROCESSING | | | | | | | |
| IN-0234 | Grain Processing Corporation | CORPORATION | 12/8/2015 | 425 | НР | GCP | 9.50 | g/HP-hr | BACT-PSD |
| | | SOUTHWEST ELECTRIC | | | | | | | |
| | | POWER COMPANY | | | | | | | |
| LA-0224 | Arsenal Hill Power Plant | (SWEPCO) | 3/20/2008 | 310 | НР | GCP, Clean Fuels | 14.06 | g/HP-hr | BACT-PSD |
| IL-0114 | Cronus Chemicals, LLC | CRONUS CHEMICALS, LLC | 9/5/2014 | 373 | НР | GCP, NSPS | 3.50 | g/kW-hr | BACT-PSD |
| | | IOWA FERTILIZER | | | | | | | |
| | Iowa Fertilizer Company | COMPANY | 10/26/2012 | 235 | | GCP | | g/kW-hr | BACT-PSD |
| | Victorville 2 Hybrid Power Project | CITY OF VICTORVILLE | 3/11/2010 | 135 | | None | | g/kW-hr | BACT-PSD |
| LA-0251 | Flopam Inc. Facility | FLOPAM INC. | 4/26/2011 | 193 | HP | None | 4.00 | g/kW-hr | BACT-PSD |
| | | KEYS ENERGY CENTER, | | | | | | | |
| MD-0046 | Keys Energy Center | LLC | 10/31/2014 | 300 | HP | GCP, Clean Fuels | 4.00 | g/kW-hr | BACT-PSD |
| | | IDAHO POWER | | | | | | | |
| ID-0018 | Langley Gulch Power Plant | COMPANY | 6/25/2010 | 235 | KW | GCP, NSPS | 4.00 | g/kW-hr | BACT-PSD |
| FL-0354 | Lauderdale Plant | FLORIDA POWER & LIGHT | 8/25/2015 | 300 | НР | Clean Fuels | 4.00 | g/kW-hr | BACT-PSD |
| | | SOLID WASTE AUTHORITY OF PALM | | | | | | | |
| FL-0324 | Palm Beach Renewable Energy Park | BEACH COUNTY | 12/23/2010 | 250 | kW | GCP, Clean Fuels | 4.00 | g/kW-hr | BACT-PSD |
| CA-1212 | Palmdale Hybrid Power Project | CITY OF PALMDALE | 10/18/2011 | 182 | HP | None | 4.00 | g/kW-hr | BACT-PSD |
| SC-0113 | Pyramax Ceramics, LLC | PYRAMAX CERAMICS, LLC | 2/8/2012 | 500 | НР | NSPS | 4.00 | g/kW-hr | BACT-PSD |
| | | KEYS ENERGY CENTER, | | | | | | | |
| MD-0046 | Keys Energy Center | LLC | 10/31/2014 | 1500 | KW | GCP, Clean Fuels | 6.40 | g/kW-hr | BACT-PSD |
| SC-0113 | Pyramax Ceramics, LLC | PYRAMAX CERAMICS, LLC | 2/8/2012 | 29 | НР | GCP | 7 50 | g/kW-hr | BACT-PSD |
| | Kenai Nitrogen Operations | AGRIUM U.S. INC. | 1/6/2015 | | MMBtu/h | | | | BACT-PSD |
| | | | | | , | | | , | |
| LA-0204 | Plaquemine PVC Plant | SHINTECH LOUISIANA LLC | | | HP | GCP, Clean Fuels | 4.41 | lb/MMBtu | BACT-PSD |
| | | 122.002 | PM10 | - Filerable | I | | | | |
| | | COMPETITIVE POWER | | | | | | | |
| NAD 0040 | CDV Ct Charles | VENTURES, INC./CPV | 44/42/2000 | 200 | | News | 0.45 | -/UD b | DACT DCD |
| | CPV St Charles | MARYLAND, LLC | 11/12/2008 | | | None | | g/HP-hr | BACT-PSD |
| LA-0251 | Flopam Inc. Facility | FLOPAM INC. | 4/26/2011 | 444 | пР | None | 0.15 | g/HP-hr | BACT-PSD |
| LA-0313 | St. Charles Power Station | ENTERGY LOUISIANA, LLC | 8/31/2016 | 282 | НР | GCP, NSPS | 0.15 | g/HP-hr | BACT-PSD |
| | | ST. JOSEPH ENERGY | | | | | | | |
| IN-0158 | St. Joseph Energy Center, LLC | CENTER, LLC | 12/3/2012 | 371 | HP | GCP | 0.15 | g/HP-hr | BACT-PSD |
| OH-0317 | Ohio River Clean Fuels 11 C | OHIO RIVER CLEAN | 11/20/2009 | 300 | НР | GCP | 0.40 | g/HP-hr | BACT-PSD |
| OH-0317 | Ohio River Clean Fuels, LLC | OHIO RIVER CLEAN FUELS, LLC | 11/20/2008 | 300 | НР | GCP | 0.40 | g/HP-hr | |

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|----------|--|---------------------------|-------------|------------|-------------|--------------------|---------------|-----------|----------|
| | <u> </u> | SOUTHWEST ELECTRIC | | | | | | | 1 |
| | | POWER COMPANY | | | | | | | |
| LA-0224 | Arsenal Hill Power Plant | (SWEPCO) | 3/20/2008 | 310 | HP | GCP, Clean Fuels | 0.99 | g/HP-hr | BACT-PSD |
| LA-0251 | Flopam Inc. Facility | FLOPAM INC. | 4/26/2011 | 193 | HP | None | 0.20 | g/kW-hr | BACT-PSD |
| | | | PM1 | 0 - Total | | | <u> </u> | | |
| | | | | | | | | t | |
| NJ-0085 | Middlesex Energy Center, LLC | STONEGATE POWER, LLC | 7/19/2016 | 327 | HP | Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| | | BENTELER STEEL / TUBE | | | | | | | |
| | D . I C. IT I F | MANUFACTURING | 6/4/2045 | 200 | | Nege | 0.45 | /up.l | DACT DCD |
| | Benteler Steel Tube Facility | CORPORATION | 6/4/2015 | 288 | | NSPS | | g/HP-hr | BACT-PSD |
| MD-0041 | CPV St. Charles | CPV MARYLAND, LLC | 4/23/2014 | 300 | НР | GCP, Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| DD 0000 | Energy Answers Arecibo Puerto Rico | ENERGY ANSWERS | 4/40/2044 | 225 | | | 0.45 | / | DACT DCD |
| PR-0009 | Renewable Energy Project | ARECIBO, LLC | 4/10/2014 | 335 | HP | None | 0.15 | g/HP-hr | BACT-PSD |
| V/A 0240 | Gateway Cogeneration 1, LLC - Smart Water | GATEWAY GREEN | 0/27/2012 | 1.00 | N 40 4D4 /l | CCD Class Finals | 0.45 | -/UD b | DACT DCD |
| VA-0319 | , | ENERGY | 8/27/2012 | 1.86 | MMBtu/nr | r GCP, Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| 1 4 0201 | Lake Charles Chemical Complex Ethylene 2 | SASOL CHEMICALS (USA) | E /22 /2014 | 500 | LID | CCD NCDC | 0.15 | ~/UD b~ | DACT DCD |
| LA-0301 | Unit | LLC MIDWEST FERTILIZER | 5/23/2014 | 500 | HP | GCP, NSPS | 0.15 | g/HP-hr | BACT-PSD |
| IN 0172 | Midwood Foutilines Composation | CORPORATION | C/4/2014 | F00 | LID | GCP | 0.15 | ~/UD ha | BACT-PSD |
| IIN-U1/3 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER | 6/4/2014 | 500 | ПР | GCP | 0.15 | g/HP-hr | BACT-PSD |
| IN 0172 | Midwest Fortilizer Corneration | CORPORATION | 6/4/2014 | 500 | шъ | GCP | 0.15 | g/HP-hr | DACT DED |
| IIV-U1/3 | Midwest Fertilizer Corporation | MIDWEST FERTILIZER | 6/4/2014 | 500 | пР | GCP | 0.15 | g/nP-III | BACT-PSD |
| INI_0190 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | ыD | GCP | 0.15 | g/HP-hr | BACT-PSD |
| 114-0100 | Wildwest Fertilizer corporation | MIDWEST FERTILIZER | 0/4/2014 | 300 | IIF | der | 0.13 | 8/115-111 | BACT-F3D |
| IN-0180 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | HD | GCP | 0.15 | g/HP-hr | BACT-PSD |
| 114-0100 | Wildwest Fertilizer corporation | CONTONATION | 0/4/2014 | 300 | 111 | GCI | 0.13 | 8/111-111 | BACT-13B |
| Ι Δ-0254 | Ninemile Point Electric Generating Plant | ENTERGY LOUISIANA LLC | 8/16/2011 | 350 | HP | GCP, Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| 27.020. | | OHIO VALLEY | 0, 10, 1011 | | | 00.70.00 | 0.23 | 6/ | 27101102 |
| IN-0179 | Ohio Valley Resources, LLC | RESOURCES, LLC | 9/25/2013 | 481 | НР | GCP | 0.15 | g/HP-hr | BACT-PSD |
| 02/3 | | | 3,23,2323 | .01 | | | 0.23 | 6/ | 27101102 |
| NJ-0081 | PSEG Fossil LLC Sewaren Generating Station | PSEG FOSSIL LLC | 3/7/2014 | 250 | HP | Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| | <u> </u> | FOOTPRINT POWER | | | | | | Ŭ, | + |
| | | SALEM HARBOR | | | | | | | |
| MA-0039 | Salem Harbor Station Redevelopment | DEVELOPMENT LP | 1/30/2014 | 2.7 | MMBtu/hr | None | 0.15 | g/HP-hr | BACT-PSD |
| | | THE EMPIRE DISTRICT | | | | | | <u> </u> | |
| KS-0029 | The Empire District Electric Company | ELECTRIC COMPANY | 7/14/2015 | 750 | KW | Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| OH-0352 | Oregon Clean Energy Center | ARCADIS, US, INC. | 6/18/2013 | 300 | HP | NSPS | 0.15 | g/HP-hr | BACT-PSD |
| | | WOLVERINE POWER | | | | | | | |
| | | SUPPLY COOPERATIVE, | | | | | | | |
| MI-0400 | Wolverine Power | INC. | 6/29/2011 | 420 | HP | None | 0.15 | g/HP-hr | BACT-PSD |
| | | GRAIN PROCESSING | | | | | | | |
| IN-0234 | Grain Processing Corporation | CORPORATION | 12/8/2015 | 425 | HP | GCP | 0.16 | g/HP-hr | BACT-PSD |
| | | DOMINION COVE POINT | | | | | | | |
| MD-0044 | Cove Point LNG Terminal | LNG, LP | 6/9/2014 | 350 | HP | GCP, Clean Fuels | 0.17 | g/HP-hr | BACT-PSD |

Emergency Fire Pump Table D-6 - RBLC Results for Emergency-Generator

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|----------|---|-----------------------------|--------------------------|------------|---------------|------------------|---------------|--------------------|----------------------|
| | | LOUISIANA ENERGY AND | | | | | | | |
| | | POWER AUTHORITY | | | | | | | |
| LA-0308 | Morgan City Power Plant | (LEPA) | 9/26/2013 | 380 | HP | GCP | 0.18 | g/HP-hr | BACT-PSD |
| | | KEYS ENERGY CENTER, | | | | | | | |
| MD-0046 | Keys Energy Center | LLC | 10/31/2014 | 300 | HP | GCP, Clean Fuels | 0.18 | g/HP-hr | BACT-PSD |
| | | KEYS ENERGY CENTER, | | | | | | | |
| MD-0046 | Keys Energy Center | LLC | 10/31/2014 | 1500 | KW | GCP, Clean Fuels | 0.18 | g/HP-hr | BACT-PSD |
| | | MATTAWOMAN ENERGY, | | | | | | | |
| MD-0045 | Mattawoman Energy Center | LLC | 11/13/2015 | 305 | HP | GCP, Clean Fuels | 0.18 | g/HP-hr | BACT-PSD |
| | | ASSOCIATED ELECTRIC | | | | | | | |
| OK-0129 | Chouteau Power Plant | COOPERATIVE INC | 1/23/2009 | 267 | HP | None | 0.40 | g/HP-hr | BACT-PSD |
| | | CONSUMERS ENERGY | | _ | | | | | |
| | Thetford Generating Station | COMPANY | 7/25/2013 | 315 | | GCP, Clean Fuels | | g/HP-hr | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | 260 | HP | GCP | 0.99 | g/HP-hr | BACT-PSD |
| 0444 | | CDONIUS CUENTIONIS II C | 0/5/2044 | 272 | | CCD NCDC | 0.40 | /1.55/ | DACT DCD |
| IL-0114 | Cronus Chemicals, LLC | CRONUS CHEMICALS, LLC | 9/5/2014 | 373 | HP | GCP, NSPS | 0.10 | g/kW-hr | BACT-PSD |
| 14 0105 | Janua Fantiliaan Canananu | IOWA FERTILIZER | 10/20/2012 | 225 | LAAZ | GCP | 0.20 | ~/I-\A/ b | DACT DCD |
| | Iowa Fertilizer Company Palmdale Hybrid Power Project | COMPANY CITY OF PALMDALE | 10/26/2012 10/18/2011 | 235 182 | | Clean Fuels | | g/kW-hr g/kW-hr | BACT-PSD BACT-PSD |
| CA-1212 | Fairidale Hybrid Fower Froject | CITTOF PALIVIDALE | 10/16/2011 | 102 | ПР | Clean Fuels | 0.20 | g/KVV-III | DACT-P3D |
| NIL-0084 | PSEG Fossil LLC Sewaren Generating Station | PSEG FOSSIL LLC | 3/10/2016 | 2.6 | MMARtu/hr | r Clean Fuels | 0.04 | lb/MMBtu | BACT-DSD |
| 143-0004 | Holland Board Of Public Works - East 5th | HOLLAND BOARD OF | 3/10/2010 | 2.0 | IVIIVIDEA/III | Cicaii i deis | 0.04 | ib/ iviivibtu | DACI-13D |
| MI-0412 | | PUBLIC WORKS | 12/4/2013 | 165 | НР | GCP | 0.09 | lb/MMBtu | BACT-PSD |
| 0 | Holland Board Of Public Works - East 5th | HOLLAND BOARD OF | 12, 1, 2010 | | | 00. | 0.03 | , | 27101 102 |
| MI-0424 | | PUBLIC WORKS | 12/5/2016 | 165 | НР | GCP | 0.09 | lb/MMBtu | BACT-PSD |
| | Karn Weadock Generating Complex | CONSUMERS ENERGY | 12/29/2009 | | KW | GCP, Clean Fuels | | lb/MMBtu | |
| AK-0083 | Kenai Nitrogen Operations | AGRIUM U.S. INC. | 1/6/2015 | 2.7 | MMBtu/hr | • | | lb/MMBtu | |
| | | | | | | | | | |
| LA-0204 | Plaquemine PVC Plant | SHINTECH LOUISIANA LLC | 2/27/2009 | 420 | HP | GCP, Clean Fuels | 0.31 | lb/MMBtu | BACT-PSD |
| | | | PM2. | 5 - Total | | | | | • |
| | | | | | | | | | |
| NJ-0085 | Middlesex Energy Center, LLC | STONEGATE POWER, LLC | 7/19/2016 | 327 | HP | Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| | | BENTELER STEEL / TUBE | | | | | | | |
| | | MANUFACTURING | | | | | | | |
| LA-0309 | Benteler Steel Tube Facility | CORPORATION | 6/4/2015 | 288 | HP | NSPS | 0.15 | g/HP-hr | BACT-PSD |
| | Energy Answers Arecibo Puerto Rico | ENERGY ANSWERS | | | | | | | |
| PR-0009 | Renewable Energy Project | ARECIBO, LLC | 4/10/2014 | 335 | HP | None | 0.15 | g/HP-hr | BACT-PSD |
| | Gateway Cogeneration 1, LLC - Smart Water | GATEWAY GREEN | | | | | | | |
| VA-0319 | | ENERGY | 8/27/2012 | 1.86 | MMBtu/hr | GCP, Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| 14.0003 | Lake Charles Chemical Complex Ethylene 2 | SASOL CHEMICALS (USA) | E /22 /224 | | Lub | CCD NCDC | 0.1- | -/UD ! | DACT DCD |
| LA-0301 | Unit | LLC | 5/23/2014 | 500 | HP | GCP, NSPS | 0.15 | g/HP-hr | BACT-PSD |
| INI 0472 | Midwoot Foutilines Courses | MIDWEST FERTILIZER | C / 4 / 2004 4 | 500 | LID | CCD | 0.15 | ~/UD 5:: | DACT DCD |
| IIV-U1/3 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | пР | GCP | 0.15 | g/HP-hr | BACT-PSD |
| IN 0172 | Midwest Fortilizer Corneration | MIDWEST FERTILIZER | 6/4/2014 | 500 | шь | GCP | 0.15 | a/UD br | BACT-PSD |
| IIN-U1/3 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | וחץ | שנר | 0.15 | g/HP-hr | BAC1-PSD |

Emergency Fire Pump Table D-6 - RBLC Results for Emergency Generator

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|---------|--|------------------------|-------------|--------------|----------|------------------|---------------|----------|----------|
| | | MIDWEST FERTILIZER | | | | | | | |
| IN-0180 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | HP | GCP | 0.15 | g/HP-hr | BACT-PSD |
| | | MIDWEST FERTILIZER | | | | | | | |
| IN-0180 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | НР | GCP | 0.15 | g/HP-hr | BACT-PSD |
| | | | | | | | | | |
| LA-0254 | Ninemile Point Electric Generating Plant | ENTERGY LOUISIANA LLC | 8/16/2011 | 350 | HP | GCP, Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| | | OHIO VALLEY | | | | | | | |
| IN-0179 | Ohio Valley Resources, LLC | RESOURCES, LLC | 9/25/2013 | 481 | HP | GCP | 0.15 | g/HP-hr | BACT-PSD |
| | | FOOTPRINT POWER | | | | | | | |
| | | SALEM HARBOR | | | | | | | |
| MA-0039 | Salem Harbor Station Redevelopment | DEVELOPMENT LP | 1/30/2014 | 2.7 | MMBtu/hr | None | 0.15 | g/HP-hr | BACT-PSD |
| | | THE EMPIRE DISTRICT | | | | | | | |
| KS-0029 | The Empire District Electric Company | ELECTRIC COMPANY | 7/14/2015 | 750 | KW | Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| | | WOLVERINE POWER | | | | | | | |
| | | SUPPLY COOPERATIVE, | | | | | | | |
| MI-0400 | Wolverine Power | INC. | 6/29/2011 | 420 | HP | None | 0.15 | g/HP-hr | BACT-PSD |
| | | DOMINION COVE POINT | | | | | | | |
| MD-0044 | Cove Point LNG Terminal | LNG, LP | 6/9/2014 | 350 | HP | GCP, Clean Fuels | 0.17 | g/HP-hr | BACT-PSD |
| | | MATTAWOMAN ENERGY, | | | | | | | |
| MD-0045 | Mattawoman Energy Center | LLC | 11/13/2015 | 305 | HP | GCP, Clean Fuels | 0.18 | g/HP-hr | BACT-PSD |
| | | CONSUMERS ENERGY | | | | | | | |
| MI-0410 | Thetford Generating Station | COMPANY | 7/25/2013 | 315 | HP | GCP, Clean Fuels | 0.86 | g/HP-hr | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | 260 | HP | GCP | 0.99 | g/HP-hr | BACT-PSD |
| | | | | | | | | | |
| IL-0114 | Cronus Chemicals, LLC | CRONUS CHEMICALS, LLC | 9/5/2014 | 373 | HP | GCP, NSPS | 0.10 | g/kW-hr | BACT-PSD |
| | | IOWA FERTILIZER | | | | | | | |
| IA-0105 | Iowa Fertilizer Company | COMPANY | 10/26/2012 | 235 | kW | GCP | 0.20 | g/kW-hr | BACT-PSD |
| CA-1212 | Palmdale Hybrid Power Project | CITY OF PALMDALE | 10/18/2011 | 182 | HP | Clean Fuels | 0.20 | g/kW-hr | BACT-PSD |
| CA-1191 | Victorville 2 Hybrid Power Project | CITY OF VICTORVILLE | 3/11/2010 | 135 | KW | None | 0.20 | g/kW-hr | BACT-PSD |
| | | | | | | | | | |
| NJ-0084 | PSEG Fossil LLC Sewaren Generating Station | PSEG FOSSIL LLC | 3/10/2016 | 2.6 | MMBtu/hr | Clean Fuels | 0.04 | lb/MMBtu | BACT-PSD |
| | Holland Board Of Public Works - East 5th | HOLLAND BOARD OF | | | | | | | |
| MI-0412 | Street | PUBLIC WORKS | 12/4/2013 | 165 | HP | GCP | 0.09 | lb/MMBtu | BACT-PSD |
| | Holland Board Of Public Works - East 5th | HOLLAND BOARD OF | | | | | | | |
| MI-0424 | Street | PUBLIC WORKS | 12/5/2016 | 165 | HP | GCP | 0.09 | lb/MMBtu | BACT-PSD |
| AK-0083 | Kenai Nitrogen Operations | AGRIUM U.S. INC. | 1/6/2015 | 2.7 | MMBtu/hr | None | 0.31 | lb/MMBtu | BACT-PSD |
| | | | PM2.5 | - filterable | | | | | |
| | | | | | | | | | 1 |
| LA-0313 | St. Charles Power Station | ENTERGY LOUISIANA, LLC | 8/31/2016 | 282 | HP | GCP, NSPS | 0.14 | g/HP-hr | BACT-PSD |
| | | MOUNDSVILLE POWER, | | | | | | | |
| WV-0025 | Moundsville Combined Cycle Power Plant | LLC | 11/21/2014 | 251 | НР | None | 0.15 | g/HP-hr | BACT-PSD |
| | | ST. JOSEPH ENERGY | | | | | | | |
| IN-0158 | St. Joseph Energy Center, LLC | CENTER, LLC | 12/3/2012 | 371 | HP | GCP | 0.15 | g/HP-hr | BACT-PSD |

Emergency Fire Pump Table D-6 - RBLC Results for Emergency Generator

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|-----------|--|-----------------------------------|-----------------------|------------|-------|-------------------|---------------|------------------------|----------------------|
| | • | LOUISIANA ENERGY AND | | | | | | | |
| | | POWER AUTHORITY | | | | | | | |
| LA-0308 | Morgan City Power Plant | (LEPA) | 9/26/2013 | 380 | HP | GCP | 0.18 | g/HP-hr | BACT-PSD |
| | | | PM - 1 | filterable | | • | | | |
| | | CRICKET VALLEY ENERGY | | | | | | | |
| NY-0103 | Cricket Valley Energy Center | CENTER LLC | 2/3/2016 | 460 | HP | GCP | 0.09 | g/HP-hr | BACT-PSD |
| | | | | | | | | | |
| NJ-0085 | Middlesex Energy Center, LLC | STONEGATE POWER, LLC | 7/19/2016 | 327 | HP | Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| | | DOMINION COVE POINT | | | | | | | |
| MD-0044 | Cove Point LNG Terminal | LNG, LP | 6/9/2014 | 350 | HP | GCP, Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| | | COMPETITIVE POWER | | | | | | | |
| | | VENTURES, INC./CPV | / / | | | | 0.15 | // · · · · · | |
| | CPV St Charles | MARYLAND, LLC | 11/12/2008 | | | None | | g/HP-hr | BACT-PSD |
| MD-0041 | CPV St. Charles | CPV MARYLAND, LLC | 4/23/2014 | 300 | НР | GCP, Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| DD 0000 | Energy Answers Arecibo Puerto Rico | ENERGY ANSWERS | 4/10/2014 | 225 | LID | Nana | 0.15 | ~/UD b~ | DACT DCD |
| | Renewable Energy Project Indeck Niles, LLC | ARECIBO, LLC INDECK NILES, LLC | 4/10/2014 1/4/2017 | 335 260 | | None GCP, NSPS | | g/HP-hr g/HP-hr | BACT-PSD BACT-PSD |
| IVII-0423 | Indeck Miles, LLC | MIDWEST FERTILIZER | 1/4/2017 | 260 | пР | GCP, NSPS | 0.15 | g/nP-III | BACT-P3D |
| INI_0173 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | HD | GCP | 0.15 | g/HP-hr | BACT-PSD |
| 114-0173 | widwest rertilizer corporation | MIDWEST FERTILIZER | 0/4/2014 | 300 | 111 | GCI | 0.13 | 8/111-111 | DACI-13D |
| IN-0173 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | НР | GCP | 0.15 | g/HP-hr | BACT-PSD |
| 11 01/3 | who west refunded corporation | MIDWEST FERTILIZER | 0, 1,2011 | 300 | | ge. | 0.13 | 6/ 111 111 | B/(C1 13B |
| IN-0180 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | НР | GCP | 0.15 | g/HP-hr | BACT-PSD |
| | | MIDWEST FERTILIZER | 5, 1, 2221 | | | | | <i>6</i> / · · · · · · | |
| IN-0180 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | НР | GCP | 0.15 | g/HP-hr | BACT-PSD |
| | · | OHIO VALLEY | | | | | | O, | |
| IN-0179 | Ohio Valley Resources, LLC | RESOURCES, LLC | 9/25/2013 | 481 | НР | GCP | 0.15 | g/HP-hr | BACT-PSD |
| | | | | | | | | | |
| NJ-0081 | PSEG Fossil LLC Sewaren Generating Station | PSEG FOSSIL LLC | 3/7/2014 | 250 | HP | Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| | | ST. JOSEPH ENERGY | | | | | | | |
| IN-0158 | St. Joseph Energy Center, LLC | CENTER, LLC | 12/3/2012 | 371 | HP | GCP | 0.15 | g/HP-hr | BACT-PSD |
| | | CONSUMERS ENERGY | | | | | | | |
| MI-0410 | Thetford Generating Station | COMPANY | 7/25/2013 | 315 | HP | GCP, Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| | | WOLVERINE POWER | | | | | | | |
| | | SUPPLY COOPERATIVE, | | | | | | | |
| MI-0400 | Wolverine Power | INC. | 6/29/2011 | 420 | HP | None | 0.15 | g/HP-hr | BACT-PSD |
| | | GRAIN PROCESSING | | | | | | | |
| IN-0234 | Grain Processing Corporation | CORPORATION | 12/8/2015 | 425 | HP | GCP | 0.16 | g/HP-hr | BACT-PSD |
| | Holland Board Of Public Works - East 5th | HOLLAND BOARD OF | 40/1/2015 | | | | 2 | (115.1 | DAGE SGS |
| MI-0412 | | PUBLIC WORKS | 12/4/2013 | 165 | HP | GCP | 0.22 | g/HP-hr | BACT-PSD |
| NAL 0424 | Holland Board Of Public Works - East 5th | HOLLAND BOARD OF | 12/5/2016 | 4.05 | LID | CCD | 0.00 | ~/UD 5 ·· | DACT DCD |
| MI-0424 | Street | PUBLIC WORKS | 12/5/2016 | 165 | н | GCP | 0.22 | g/HP-hr | BACT-PSD |
| II 0114 | Cronus Chamicals II.C | CDONILIS CHEMICALS 110 | 9/5/2014 | 272 | μп | CCD NSDS | 0.10 | a/k/M br | BACT-PSD |
| 1L-U114 | Cronus Chemicals, LLC | CRONUS CHEMICALS, LLC | 9/5/2014 | 373 | IUL | GCP, NSPS | 0.10 | g/kW-hr | DAC1-P3D |

Emergency Fire Pump Table D-6 - RBLC Results for Emergency-Generator

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|-----------|---|--------------------------------------|---------------|---------------|----------|------------------|---------------|-----------|----------|
| | , | KEYS ENERGY CENTER, | | | | | | | 71. |
| MD-0046 | Keys Energy Center | LLC | 10/31/2014 | 300 | НР | GCP, Clean Fuels | 0.20 | g/kW-hr | BACT-PSD |
| | | KEYS ENERGY CENTER, | | | | | | <u> </u> | |
| MD-0046 | Keys Energy Center | LLC | 10/31/2014 | 1500 | KW | GCP, Clean Fuels | 0.20 | g/kW-hr | BACT-PSD |
| | | IDAHO POWER | | | | | | | |
| ID-0018 | Langley Gulch Power Plant | COMPANY | 6/25/2010 | 235 | KW | GCP, NSPS | 0.20 | g/kW-hr | BACT-PSD |
| | | MATTAWOMAN ENERGY, | | | | | | | |
| MD-0045 | Mattawoman Energy Center | LLC | 11/13/2015 | 305 | HP | GCP, Clean Fuels | 0.20 | g/kW-hr | BACT-PSD |
| | | | | | | | | | |
| | PSEG Fossil LLC Sewaren Generating Station | PSEG FOSSIL LLC | 3/10/2016 | 2.6 | MMBtu/hi | r Clean Fuels | | lb/MMBtu | |
| NY-0104 | CPV Valley Energy Center | CPV VALLEY LLC | 8/1/2013 | | | Clean Fuels | 0.04 | lb/MMBtu | BACT-PSD |
| | | T | PM | - total | | 1 | | | |
| | Sweet Sarahum To Ethanal Advanced | COLITHEACT DENEWARD E | | | | | | | |
| בו חפפפ | Sweet Sorghum-To-Ethanol Advanced Biorefinery | SOUTHEAST RENEWABLE | 12/22/2010 | 600 | ШΒ | None | 0.15 | a/UD br | BACT-PSD |
| FL-0322 | Бюгеппегу | FUELS (SRF), LLC THE EMPIRE DISTRICT | 12/23/2010 | 600 | пР | None | 0.15 | g/HP-hr | BACT-P3D |
| KS-0029 | The Empire District Electric Company | ELECTRIC COMPANY | 7/14/2015 | 750 | ΚW | Clean Fuels | 0.15 | g/HP-hr | BACT-PSD |
| 13 0023 | The Empire District Electric company | ELECTRIC CONTENT | 7/14/2013 | 730 | 1000 | Cicarr acis | 0.13 | 6/111 111 | DACT 13D |
| FL-0346 | Lauderdale Plant | FLORIDA POWER & LIGHT | 4/22/2014 | 300 | НР | GCP | 0.20 | g/HP-hr | BACT-PSD |
| | | IOWA FERTILIZER | , , , | | | | | , | |
| IA-0105 | Iowa Fertilizer Company | COMPANY | 10/26/2012 | 235 | kW | GCP | 0.20 | g/kW-hr | BACT-PSD |
| | · | | | | | | | | |
| FL-0354 | Lauderdale Plant | FLORIDA POWER & LIGHT | 8/25/2015 | 300 | HP | Clean Fuels | 0.20 | g/kW-hr | BACT-PSD |
| | | | | | | | | | |
| FL-0356 | Okeechobee Clean Energy Center | FLORIDA POWER & LIGHT | 3/9/2016 | 422 | HP | Clean Fuels | 0.20 | g/kW-hr | BACT-PSD |
| | | SOLID WASTE | | | | | | | |
| | | AUTHORITY OF PALM | | | | | | | |
| | Palm Beach Renewable Energy Park | BEACH COUNTY | 12/23/2010 | | | GCP, Clean Fuels | | g/kW-hr | BACT-PSD |
| | Palmdale Hybrid Power Project | CITY OF PALMDALE | 10/18/2011 | 182 | | Clean Fuels | | g/kW-hr | BACT-PSD |
| | Victorville 2 Hybrid Power Project | CITY OF VICTORVILLE | 3/11/2010 | | | None | | g/kW-hr | BACT-PSD |
| | Karn Weadock Generating Complex | CONSUMERS ENERGY | 12/29/2009 | | KW | GCP, Clean Fuels | | g/kW-hr | BACT-PSD |
| AK-0083 | Kenai Nitrogen Operations | AGRIUM U.S. INC. | 1/6/2015 | nic Compound | MMBtu/hı | rinone | 0.31 | lb/MMBtu | BAC1-PSD |
| | Holland Board Of Public Works - East 5th | HOLLAND BOARD OF | voiatile Orga | inic Compound | 15 | | | | |
| MI-0412 | | PUBLIC WORKS | 12/4/2013 | 165 | нр | GCP | 2.75E-03 | g/HD_hr | BACT-PSD |
| 1011-0412 | Street | GRAIN PROCESSING | 12/4/2013 | 103 | IIF | der | 2.73L-03 | g/11F-111 | DACIFOD |
| IN-0234 | Grain Processing Corporation | CORPORATION | 12/8/2015 | 425 | НР | GCP | 0.05 | g/HP-hr | BACT-PSD |
| 114 0254 | Lake Charles Chemical Complex Ethylene 2 | SASOL CHEMICALS (USA) | 12/0/2013 | 723 | | GCI | 0.03 | 6/111 111 | DACT 13D |
| LA-0301 | Unit | LLC | 5/23/2014 | 500 | НР | GCP, NSPS | 0.09 | g/HP-hr | BACT-PSD |
| | - | MIDWEST FERTILIZER | -,-5,2011 | 200 | - | 7 - 7 - 7 - 7 | 3.33 | J | |
| IN-0173 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | НР | GCP | 0.14 | g/HP-hr | BACT-PSD |
| | 1 | MIDWEST FERTILIZER | ,, | | | | | <i>-</i> | |
| IN-0173 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | НР | GCP | 0.14 | g/HP-hr | BACT-PSD |
| | | MIDWEST FERTILIZER | | | | | | | |
| IN-0180 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | HP | GCP | 0.14 | g/HP-hr | BACT-PSD |

Emergency Fire Pump Table D-6 - RBLC Results for Emergency Generator

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls | EmissionLimit | Units | Туре |
|---------|--|--|-------------|------------|---------|------------------|---------------|----------|------------|
| | - | MIDWEST FERTILIZER | | | | | | | , |
| IN-0180 | Midwest Fertilizer Corporation | CORPORATION | 6/4/2014 | 500 | НР | GCP | 0.14 | g/HP-hr | BACT-PSD |
| | | OHIO VALLEY | | | | | | | |
| IN-0179 | Ohio Valley Resources, LLC | RESOURCES, LLC | 9/25/2013 | 481 | HP | GCP | 0.14 | g/HP-hr | BACT-PSD |
| | Energy Answers Arecibo Puerto Rico | ENERGY ANSWERS | | | | | | | |
| PR-0009 | Renewable Energy Project | ARECIBO, LLC | 4/10/2014 | 335 | HP | None | 0.15 | g/HP-hr | BACT-PSD |
| | | ST. JOSEPH ENERGY | | | | | | | |
| IN-0158 | St. Joseph Energy Center, LLC | CENTER, LLC | 12/3/2012 | 371 | HP | GCP | 0.20 | g/HP-hr | BACT-PSD |
| | | MOUNDSVILLE POWER, | | | | | | | |
| WV-0025 | Moundsville Combined Cycle Power Plant | LLC | 11/21/2014 | 251 | HP | None | 0.31 | g/HP-hr | BACT-PSD |
| OH-0352 | Oregon Clean Energy Center | ARCADIS, US, INC. | 6/18/2013 | 300 | HP | NSPS | 0.38 | g/HP-hr | BACT-PSD |
| | | | | | | | | | |
| LA-0254 | Ninemile Point Electric Generating Plant | ENTERGY LOUISIANA LLC | 8/16/2011 | 350 | HP | GCP, Clean Fuels | 1.00 | g/HP-hr | BACT-PSD |
| MI-0423 | Indeck Niles, LLC | INDECK NILES, LLC | 1/4/2017 | 260 | HP | GCP | 1.12 | g/HP-hr | BACT-PSD |
| | | ASSOCIATED ELECTRIC | | | | | | | |
| OK-0129 | Chouteau Power Plant | COOPERATIVE INC | 1/23/2009 | 267 | HP | GCP | 1.12 | g/HP-hr | BACT-PSD |
| | | SOUTHWEST ELECTRIC | | | | | | | |
| | | POWER COMPANY | | | | | | | |
| LA-0224 | Arsenal Hill Power Plant | (SWEPCO) | 3/20/2008 | 310 | HP | GCP, Clean Fuels | 1.13 | g/HP-hr | BACT-PSD |
| | Holland Board Of Public Works - East 5th | HOLLAND BOARD OF | | | | | | | |
| MI-0424 | Street | PUBLIC WORKS | 12/5/2016 | 165 | HP | GCP | 1.29 | g/HP-hr | BACT-PSD |
| | | WILDHORSE TERMINAL | | | | | | | |
| OK-0175 | Wildhorse Terminal | LLC | 6/29/2017 | 500 | HP | GCP, NSPS | 3.00 | g/HP-hr | BACT-PSD |
| | | | | | | | | | |
| LA-0313 | St. Charles Power Station | ENTERGY LOUISIANA, LLC | 8/31/2016 | 282 | HP | GCP | 3.01 | g/HP-hr | BACT-PSD |
| | | OHIO RIVER CLEAN | | | | | | | |
| OH-0317 | Ohio River Clean Fuels, LLC | FUELS, LLC | 11/20/2008 | 300 | HP | GCP | 7.80 | g/HP-hr | BACT-PSD |
| | | | | | | | | | |
| | | TINKER AIR FORCE BASE | | | | | | | |
| OK-0164 | Midwest City Air Depot | LOGISTICS CENTER | 1/8/2015 | 300 | HP | GCP | 0.15 | g/kW-hr | BACT-PSD |
| | | IOWA FERTILIZER | | | | | | | |
| IA-0105 | Iowa Fertilizer Company | COMPANY | 10/26/2012 | 235 | kW | GCP | 0.25 | g/kW-hr | BACT-PSD |
| | | | | | | | | | |
| IL-0114 | Cronus Chemicals, LLC | CRONUS CHEMICALS, LLC | 9/5/2014 | 373 | HP | GCP, NSPS | 0.40 | g/kW-hr | BACT-PSD |
| | | IDAHO POWER | | | | | | | |
| ID-0018 | Langley Gulch Power Plant | COMPANY | 6/25/2010 | 235 | KW | GCP, NSPS | 4.00 | g/kW-hr | BACT-PSD |
| | | | | | | | | | |
| SC-0113 | Pyramax Ceramics, LLC | PYRAMAX CERAMICS, LLC | 2/8/2012 | 500 | HP | GCP, NSPS | 4.00 | g/kW-hr | BACT-PSD |
| | | MICHELIN NORTH | | | | | | | |
| SC-0159 | US10 Facility | AMERICA, INC. | 7/9/2012 | 211 | KW | NSPS | 4.00 | g/kW-hr | BACT-PSD |
| | | | 0/-/ | | | | | | |
| SC-0113 | Pyramax Ceramics, LLC | PYRAMAX CERAMICS, LLC | 2/8/2012 | 29 | HP | GCP | 7.50 | g/kW-hr | BACT-PSD |
| TV 6705 | | DI III I I I I I I I I I I I I I I I I | 6/0/20:- | | | COD | 2 - 2 - 2 - 2 | | D 4 CT 222 |
| | Beaumont Terminal | PHILLIPS 66 PIPELINE LLC | 6/8/2016 | ~ = | | GCP | | lb/HP-hr | BACT-PSD |
| AK-0083 | Kenai Nitrogen Operations | AGRIUM U.S. INC. | 1/6/2015 | 2.7 | MMBtu/h | rjivone | 0.36 | In/MMRt | BACT-PSD |

Table D-6 Addendum: RBLC Results for Emergency Diesel Fire Pump Updated Data: November 2018 to October 2021

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls ^A | Emission Limit | Units | Туре |
|-----------|---|---|----------------------|------------|------------|-------------------------------------|----------------|-----------|------|
| NDEC ID | ruency rune | Company Nume | Nitrogen Dioxide | | Omes | 55.11.55 | | | Турс |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 19.4 | gph | GCP | 3.6 | G/HP-HR | BACT |
| *AK-0086 | KENAI NITROGEN OPERATIONS | AGRIUM U.S. INC. | 03/26/2021 | 2.7 | MMBtu/hr | GCP | 4.41 | LB/MMBTU | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 260 | HP | GCP | 2.98 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 190 | HP | GCP | 2.98 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 440 | HP | GCP | 2.98 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 190 | HP | GCP | 2.98 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 61 | HP | GCP | 3.5 | G/HP-HR | BACT |
| *LA-0370 | WASHINGTON PARISH ENERGY CENTER | WASHINGTON PARISH ENERGY CENTER LLC | 04/27/2020 | 1.1 | MM BTU/hr | CBF | 1.15 | LB/HR | BACT |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 1.66 | MMBTU/H | GCP | 3 | G/BHP-H | BACT |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | 402 | HP | GCP | 2.64 | LB/H | BACT |
| OH-0379 | PETMIN USA INCORPORATED | PETMIN USA INCORPORATED | 02/06/2019 | 158 | HP | | 0.104 | LB/H | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | H/YR | GCP/high efficiency design/CBF | 4.8 | G/HP-H | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | HR/YR | GCP/high efficiency design/CBF | 3 | G/HP-HR | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | 0.22 | mmBTU/hr | GCP | 4.7 | G/KWH | BACT |
| | | | Carbon Monoxid | e | | | | | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 19.4 | gph | GCP | 3.3 | G/HP-HR | BACT |
| *AK-0086 | KENAI NITROGEN OPERATIONS | AGRIUM U.S. INC. | 03/26/2021 | 2.7 | MMBtu/hr | GCP | 0.95 | LB/MMBTU | BACT |
| IL-0130 | JACKSON ENERGY CENTER | JACKSON GENERATION, LLC | 12/31/2018 | 420 | horsepower | | 3.5 | G/KW-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 260 | HP | GCP | 2.61 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 190 | HP | GCP | 2.61 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 440 | HP | GCP | 2.61 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 190 | HP | GCP | 2.61 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 61 | HP | GCP | 3.73 | G/HP-HR | BACT |
| *LA-0370 | WASHINGTON PARISH ENERGY CENTER | WASHINGTON PARISH ENERGY CENTER LLC | 04/27/2020 | 1.1 | MM BTU/hr | GCP | 0.4 | LB/HR | BACT |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 2.5 | MMBTU/H | GCP | 2.6 | G/HP-H | BACT |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 1.66 | MMBTU/H | GCP | 2.6 | G/BHP-H | BACT |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 2.5 | MMBTU/H | GCP | 2.6 | G/HP-H | BACT |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | 402 | HP | GCP | 2.31 | LB/H | BACT |
| *PA-0326 | SHELL POLYMERS MONACA SITE | SHELL CHEMICAL APPALACHIA LLC | 02/18/2021 | 0 | | GCP | 0.5 | G | BACT |
| *PA-0326 | SHELL POLYMERS MONACA SITE | SHELL CHEMICAL APPALACHIA LLC | 02/18/2021 | 0 | | GCP | 0.5 | G | BACT |
| *PA-0326 | SHELL POLYMERS MONACA SITE | SHELL CHEMICAL APPALACHIA LLC | 02/18/2021 | 0 | | GCP | 387 | GRAM | BACT |
| TX-0889 | SWEENY OLD OCEAN FACILITIES | CHEVRON PHILLIPS CHEMICAL COMPANY LP | 08/08/2020 | 0 | | GCP | 100 | HR/YR | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | H/YR | GCP/high efficiency design/CBF | 2.6 | G/HP-H | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | HR/YR | GCP/high efficiency design/CBF | 2.6 | G/HP-H | BACT |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | 0.22 | mmBTU/hr | GCP | 5 | G/KWH | BACT |
| | | | platile Organic Comp | | | | | | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 19.4 | gph | GCP/CBF | 0.19 | G/HP-HR | BACT |
| *AK-0086 | KENAI NITROGEN OPERATIONS | AGRIUM U.S. INC. | 03/26/2021 | 2.7 | MMBtu/hr | GCP | 0.36 | LB/MMBTU | BACT |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | 402 | HP | GCP | 2.64 | LB/H | BACT |
| OK-0181 | WILDHORSE TERMINAL | KEYERA ENERGY INC | 09/11/2019 | 0 | | GCP | 3 | GM/HP-HR | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | HR/YR | GCP/high efficiency design/CBF | 0.11 | G/HP-HR | BACT |
| *WI-0292 | GREEN BAY PACKAGING INC. â€"MILL DIVISION | GREEN BAY PACKAGING INC. â€"MILL DIVISION | 04/01/2019 | 0 | | | 200 | HOURS | BACT |
| **** 0005 | 0.05 TD5.4T4.514T D1.4.14T | | Gases - Carbon Dio | | | I | 162.6 | | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 19.4 | gph | GCP | 163.6 | LB/MMBTU | BACT |
| *AK-0086 | KENAI NITROGEN OPERATIONS | AGRIUM U.S. INC. | 03/26/2021 | 2.7 | MMBtu/hr | GCP | 164 | LB/MMBTU | BACT |
| IL-0130 | JACKSON ENERGY CENTER | JACKSON GENERATION, LLC | 12/31/2018 | 420 | horsepower | 000 | 241 | TONS/YEAR | BACT |
| *LA-0370 | WASHINGTON PARISH ENERGY CENTER | WASHINGTON PARISH ENERGY CENTER LLC | 04/27/2020 | 1.1 | MM BTU/hr | GCP | 9 | TPY | BACT |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 2.5 | MMBTU/H | GCP/energy efficiency measures. | 20 | T/YR | BACT |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 1.66 | MMBTU/H | GCP | 13.58 | T/YR | BACT |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 2.5 | MMBTU/H | CBF/GCP/energy efficiency measures. | 20 | T/YR | BACT |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | 402 | HP | GCP | 23 | T/YR | BACT |
| OH-0379 | PETMIN USA INCORPORATED | PETMIN USA INCORPORATED | 02/06/2019 | 158 | HP | GCP | 181.7 | LB/H | BACT |
| *PA-0326 | SHELL POLYMERS MONACA SITE | SHELL CHEMICAL APPALACHIA LLC | 02/18/2021 | 0 | - | GCP | 10 | TONS | BACT |
| *PA-0326 | SHELL POLYMERS MONACA SITE | SHELL CHEMICAL APPALACHIA LLC | 02/18/2021 | 0 | 1150 | GCP | 10 | TONS | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | H/YR | GCP/high efficiency design/CBF | 1203 | T/YR | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | HR/YR | GCP/high efficiency design/CBF | 106 | T/YR | BACT |
| *WI-0292 | GREEN BAY PACKAGING INC. â€"MILL DIVISION | GREEN BAY PACKAGING INC. â€"MILL DIVISION | 04/01/2019 | 0 | | | 200 | HOURS | BACT |

(a) GCP = good combustion practices, CBF = clean burning fuels

Table D-6 Addendum: RBLC Results for Emergency Diesel Fire Pump Updated Data: November 2018 to October 2021

| RBLC ID | Facility Name | Company Name | Permit Date | Throughput | Units | Controls ^A | Emission Limit | Units | Туре |
|----------|---------------------------------|--|---------------------------------|------------|-----------|--------------------------------|----------------|------------|------|
| | | | PM ₁₀ (total) | | | | • | | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 19.4 | gph | GCP/CBF | 0.19 | G/HP-HR | BACT |
| *AK-0086 | KENAI NITROGEN OPERATIONS | AGRIUM U.S. INC. | 03/26/2021 | 2.7 | MMBtu/hr | GCP | 0.31 | LB/MMBTU | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 260 | HP | GCP | 0.15 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 190 | HP | GCP | 0.15 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 440 | HP | GCP | 0.15 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 190 | HP | GCP | 0.15 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 61 | HP | GCP | 0.3 | G/HP-HR | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 350 | HP | GCP | 0.15 | G/HP-HR | BACT |
| *LA-0370 | WASHINGTON PARISH ENERGY CENTER | WASHINGTON PARISH ENERGY CENTER LLC | 04/27/2020 | 1.1 | MM BTU/hr | CBF | 0.04 | LB/HR | BACT |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 2.5 | MMBTU/H | CBF/GCP | 0.12 | LB/H | BACT |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 1.66 | MMBTU/H | GCP | 0.57 | LB/H | BACT |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 2.5 | MMBTU/H | CBF/GCP | 0.12 | LB/H | BACT |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | 402 | HP | GCP | 0.13 | LB/H | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | H/YR | GCP/high efficiency design/CBF | 0.15 | G/HP-HR | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | HR/YR | GCP/high efficiency design/CBF | 0.15 | G/HP-HR | BACT |
| | | | PM ₁₀ (filterable on | ly) | | | | | |
| OH-0379 | PETMIN USA INCORPORATED | PETMIN USA INCORPORATED | 02/06/2019 | 158 | HP | GCP | 5.22 | X10-3 LB/H | BACT |
| | | | PM _{2.5} (total) | | | | | | |
| *AK-0085 | GAS TREATMENT PLANT | ALASKA GASLINE DEVELOPMENT CORPORATION | 08/13/2020 | 19.4 | gph | GCP/CBF | 0.19 | G/HP-HR | BACT |
| *AK-0086 | KENAI NITROGEN OPERATIONS | AGRIUM U.S. INC. | 03/26/2021 | 2.7 | MMBtu/hr | GCP | 0.31 | LB/MMBTU | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 260 | HP | GCP | 0.15 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 190 | HP | GCP | 0.15 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 440 | HP | GCP | 0.15 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 190 | HP | GCP | 0.15 | G/HP-HR | BACT |
| KY-0110 | NUCOR STEEL BRANDENBURG | NUCOR | 07/23/2020 | 61 | HP | GCP | 0.3 | G/HP-HR | BACT |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | 350 | HP | GCP | 0.15 | G/HP-HR | BACT |
| *LA-0370 | WASHINGTON PARISH ENERGY CENTER | WASHINGTON PARISH ENERGY CENTER LLC | 04/27/2020 | 1.1 | MM BTU/hr | CBF | 0.04 | LB/HR | BACT |
| MI-0441 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 12/21/2018 | 2.5 | MMBTU/H | CBF/GCP | 0.12 | LB/H | BACT |
| *MI-0445 | INDECK NILES, LLC | INDECK NILES, LLC | 11/26/2019 | 1.66 | MMBTU/H | GCP | 0.57 | LB/H | BACT |
| MI-0447 | LBWLERICKSON STATION | LANSING BOARD OF WATER AND LIGHT | 01/07/2021 | 2.5 | MMBTU/H | CBF/GCP | 0.12 | LB/H | BACT |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | 402 | HP | GCP | 0.13 | LB/H | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | H/YR | GCP/high efficiency design/CBF | 0.15 | G/HP-HR | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | HR/YR | GCP/high efficiency design/CBF | 0.15 | G/HP-HR | BACT |
| | | | PM _{2.5} (Filterable |) | | | | | |
| OH-0379 | PETMIN USA INCORPORATED | PETMIN USA INCORPORATED | 02/06/2019 | 158 | HP | GCP | 5.22 | X10-3 LB/H | BACT |
| | | | Sulfuric Acid Mis | | | | | | |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | H/YR | GCP/high efficiency design/CBF | 0.0001 | LB/MMBTU | BACT |
| VA-0332 | CHICKAHOMINY POWER LLC | CHICKAHOMINY POWER LLC | 06/24/2019 | 500 | HR/YR | GCP/high efficiency design/CBF | 0.0001 | LB/MMBTU | BACT |
| | | | Opacity | ı | | | | 1 | |
| *WI-0291 | GRAYMONT WESTERN LIME-EDEN | GRAYMONT WESTERN LIME-EDEN | 01/28/2019 | 0.22 | mmBTU/hr | GCP | 10 | % OPACITY | BACT |

(a) GCP = good combustion practices, CBF = clean burning fuels

Table D-7

Table 2-4. RBLC Listings for Circuit Breaker Equipment Leaks

Best Available Control Technology Analysis

| RBLC ID | Facility Name | State | Permit Date | Pollutant | BACT Level | BACT Units | Control |
|----------|--|-------|----------------|-------------------|------------|-------------------------|---|
| *VA-0332 | Chickahominy Power LLC | VA | 6/24/2019 | CO ₂ e | 0.5 | % Leak Rate | Low-pressure detection system (with alarm) |
| TX-0748 | FGE Power, FGE Texas Project | TX | 4/28/2014 | CO ₂ e | 0.5 | % Leak Rate | Low pressure alarm and a low |
| VA-0319 | Gateway Cogeneration 1, LLC - Smart Water Project | VA | 8/27/2012 | CO ₂ e | 1.0 | % Leak Rate | Enclosed pressure circuit breaker. |
| VA-0328 | C4GT, LLC | VA | 4/26/2018 | CO ₂ e | 0.5 | % Leak Rate | Enclosed-pressure design with low-pressure detection system (with alarm). |
| *IL-0130 | Jackson Energy Center | IL | 12/31/2018 | SF ₆ | 0.5 | % Leak Rate | Not specified |
| FL-0355 | Fort Myers Plant | FL | 9/10/2015 | SF ₆ | 0.5 | % Leak Rate | Leakage detection systems and alarms. |
| FL-0356 | Okeechobee Clean Energy Center | FL | 3/9/2016 | SF ₆ | 0.5 | % Leak Rate | Leakage detection systems and alarms. |
| IA-0107 | Marshalltown Generating Station | IA | 4/14/2014 | SF ₆ | 0.5 | % Leak Rate | Not specified |
| IL-0129 | CPV Three Rivers Energy Center | IL | 7/30/2018 | SF ₆ | 0.5 | % Leak Rate | Not specified |
| IN-0158 | St. Joseph Energy Center, LLC | IN | 12/3/2012 | SF ₆ | 0.5 | % Leak Rate | A density alarm for leak detection and the use of totally enclosed and pressurized circuit breakers |
| MD-0041 | CPV St. Charles | MD | 4/23/2014 | SF ₆ | 0.5 | % Leak Rate | Designed to meet ANSI c37.013 or equivalent to detect and minimize SF6 leaks |
| TX-0612 | Thomas C. Ferguson Power Plant | TX | 11/10/2011 | SF ₆ | 0.006 | lb/hr | Not specified |
| CA-1212 | Palmdale Hybrid Power Project | CA | 10/18/2011 | CO ₂ e | 0.85 | lbs SF ₆ /yr | Not specified |
| CA-1223 | Pio Pico Energy Center | CA | 11/19/2012 | CO ₂ e | 3.56 | lbs SF ₆ /yr | Enclosed |
| KS-0029 | The Empire District Electric Company | KS | 7/14/2015 | CO ₂ e | 0.61 | lbs SF ₆ /yr | Density (leak detection) alarms |
| TX-0824 | Jackson County Generating Facility | TX | 6/30/2017 | CO ₂ e | 3.04 | lbs SF ₆ /yr | Totally enclosed insulation systems equipped with a low pressure alarm and low pressure lockout |
| PA-0309 | Lackawanna Energy Ctr/Jessup | PA | 12/23/2015 | SF ₆ | 6.00 | lbs SF ₆ /yr | State-of-the-art sealed enclosed- pressure circuit breakers with leak detection |
| PA-0310 | CPV Fairview Energy Center | PA | 9/2/2016 | SF ₆ | 1500 | ppm | Not specified |

| RBLC ID | Facility Name | State | Permit Date | Pollutant | BACT Level | BACT Units | Control | |
|--------------|---|-------|----------------|-------------------|--|--------------------------------|--|--|
| TX-0749 | Golden Spread Electric Cooperative, Antelope Station | TX | 6/2/2014 | CO ₂ e | Not s | specified | Pressure lockout. | |
| TX-0753 | Guadalupe Generating Station | TX | 12/2/2014 | CO ₂ e | Not s | specified | Low pressure alarm and a low pressure lockout | |
| TX-0757 | Indeck Wharton Energy Center | TX | 5/12/2014 | CO ₂ e | Not specified | | Low pressure alarm and a low pressure lockout | |
| TX-0758 | Ector County Energy Center | TX | 8/1/2014 | CO ₂ e | Not specified | | Low pressure alarm and a low pressure lockout | |
| *MD- 0042 | Wildcat Point Generation Facility | MD | 4/8/2014 | SF ₆ | | nufacturer Provided ak Rate | State-of-the-art circuit breakers | |
| MD-0045 | Mattawoman Energy Center | MD | 11/13/2015 | SF_6 | Unspecified Manufacturer Provided Leak Rate | | Designed to meet ANSI c37.013 or equivalent to detect and minimize SF6 leaks | |
| MD-0046 | Keys Energy Center | MD | 10/31/2014 | SF_6 | Unspecified Manufacturer Provided Leak Rate | | Designed to meet ANSI c37.013 or equivalent to detect and minimize SF6 leaks | |

Table D-7 Addendum: RBLC Listings for Circuit Breaker Equipment Leaks Updated Data: February 2020 to October 2021

| RBLC ID | Facility Name | State | Permit Date | Pollutant | BACT Level | BACT Units | Controls |
|---------|------------------------|-------|-------------|----------------------------------|------------|-------------------|---|
| IL-0130 | JACKSON ENERGY CENTER | IL | 12/31/2018 | Sulfur Hexafluoride | 0.5% Le | eak Rate | |
| VA-0332 | CHICKAHOMINY POWER LLC | VA | 06/24/2019 | Carbon Dioxide Equivalent (CO2e) | 0.5% Le | eak Rate | Enclosed-pressure design with low-pressure detection system (with alarm). |

| RBLC ID | Facility Name | Permit Date | Process Name | Pollutant | Control Method | Emission Limit | Limit Units |
|---------|------------------------------------|-------------|---|-----------|----------------|-----------------------|-------------|
| TX-0633 | CHANNEL ENERGY ENERGY CENTER, LLC | 11/29/2012 | Natural Gas Fugitives | CO2 | | 0.29 | tpy |
| TX-0753 | GUADALUPE GENERATING STATION | 12/2/2014 | Components Fugitive Leak Emissions | CO2e | AVO | | |
| TX-0757 | INDECK WHARTON ENERGY CENTER | 5/12/2014 | Components Fugitive Leak Emissions | CO2e | AVO | | |
| TX-0758 | ECTOR COUNTY ENERGY CENTER | 8/1/2014 | Components Fugitive Leaks | CO2e | AVO | | |
| MD-0042 | WILDCAT POINT GENERATION FACILITY | 4/8/2014 | Equipment Leaks | CO2e | AVO | | |
| MD-0045 | MATTAWOMAN ENERGY CENTER | 11/13/2015 | Equipment Leaks | CO2e | AVO | | |
| MD-0046 | KEYS ENERGY CENTER | 10/31/2014 | Equipment Leaks | CO2e | AVO | | |
| MD-0041 | CPV ST. CHARLES | 4/23/2014 | Fugitive Emissions | CO2e | AVO | 72.7 | tpy |
| TX-0824 | JACKSON COUNTY GENERATING FACILITY | 6/30/2017 | Natural Gas Fugitives | CO2e | AVO | 693.3 | tpy |
| VA-0328 | C4GT, LLC | 4/26/2018 | Equipment Leaks from Natural Gas Components | CO2e | LDAR | | |
| TX-0748 | FGE POWER, FGE TEXAS PROJECT | 4/28/2014 | Natural Gas Fugitive Emission Sources | CO2e | LDAR | | |
| TX-0633 | CHANNEL ENERGY ENERGY CENTER, LLC | 11/29/2012 | Natural Gas Fugitives | Methane | | 7.44 | tpy |
| IL-0130 | JACKSON ENERGY CENTER | 12/31/2018 | Natural Gas Piping and Components | Methane | LDAR | 4.3 | tpy |

Table D-8 Addendum: RBLC Results for Piping Fugitives Updated Data: February 2021 to October 2021

| RBLC ID | Facility Name | Permit Date | Process Name | Pollutant | Control Method | Emission Limit | Limit Units |
|----------|--|-------------|---|----------------------------------|--|-----------------------|--------------------|
| IL-0130 | JACKSON ENERGY CENTER | 12/31/2018 | Natural Gas Piping and Components | Methane | (LDAR)/, use of ''leakless'' components. | 4.3 | TONS/YEAR |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | Fugitive Emissions (P807) | Volatile Organic Compounds (VOC) | Enhanced connector monitoring requirements to the most stringent leak detection and repail | 99.38 | T/YR |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | Fugitive Emissions (P807) | Carbon Dioxide Equivalent (CO2e) | i.an LDAR program for leaks of methane from equipment and piping components in tail gas (f | 35 | T/YR |
| TX-0886 | MONT BELVIEU NGL FRACTIONATION UNIT | 03/31/2020 | EQUIPMENT LEAK FUGITIVES | Volatile Organic Compounds (VOC) | 28 LAER leak detection and repair (LDAR) program | 0 | |
| VA-0332 | CHICKAHOMINY POWER LLC | 06/24/2019 | Equipment Leaks from Natural Gas Components | Carbon Dioxide Equivalent (CO2e) | Best management practices to prevent, detect and repair leaks of natural gas from the piping | 0 | |
| *TX-0908 | NEWMAN POWER STATION | 08/27/2021 | Fugitives | Volatile Organic Compounds (VOC) | weekly AVO | 0 | |
| *TX-0908 | NEWMAN POWER STATION | 08/27/2021 | Fugitives | Carbon Dioxide Equivalent (CO2e) | weekly AVO | 0 | |
| TX-0864 | EQUISTAR CHEMICALS CHANNELVIEW COMPLEX | 09/09/2019 | Fugitive Components | Volatile Organic Compounds (VOC) | 28LAER & 28PI | 500 | PPMV |
| TX-0864 | EQUISTAR CHEMICALS CHANNELVIEW COMPLEX | 09/09/2019 | Fugitive Components | Carbon Dioxide Equivalent (CO2e) | LDAR | 500 | PPMV |

| RBLC ID | Facility Name | Permit Date | Process Name | Pollutant | Control Method | Emission Limit | Limit Units |
|---------|--|-------------|------------------------------|------------------|--|----------------|-------------|
| SC-0181 | RESOLUTE FP US INC CATAWBA LUMBER MILL | 11/3/2017 | Haul Roads | PM10-filterable | Good Housekeeping Practices | 0.03 | LB/VMT |
| OH-0376 | IRONUNITS LLC - TOLEDO HBI | 2/9/2018 | Haul Roads-Paved | PM10-filterable | Water Flushing and Sweeping | 0.63 | T/YR |
| IA-0105 | IOWA FERTILIZER COMPANY | 10/26/2012 | Haul Roads | PM10-total | Paving, wet/chemical suppression | | |
| IA-0106 | CF INDUSTRIES NITROGEN, LLC - PORT NEAL NITROGEN COMPLEX | 7/12/2013 | Haul Roads | PM10-total | Paving, wet/chemical suppression | | |
| IN-0263 | MIDWEST FERTILIZER COMPANY LLC | 3/23/2017 | Paved Roads and Parking Lots | PM10-total | Paving, wet/chemical suppression | | |
| MD-0046 | KEYS ENERGY CENTER | 10/31/2014 | Haul Roads-Paved and Unpaved | PM10-total | Water Flushing and Sweeping | | |
| IN-0166 | INDIANA GASIFICATION, LLC | 6/27/2012 | Haul Roads-Paved | PM10-total | Paving, wet/chemical suppression | 90 | % CONTROL |
| IN-0173 | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | Paved Roads and Parking Lots | PM10-total | Paving, wet/chemical suppression | 90 | % CONTROL |
| IN-0179 | OHIO VALLEY RESOURCES, LLC | 9/25/2013 | Paved Roads and Parking Lots | PM10-total | Paving, wet/chemical suppression | 90 | % CONTROL |
| IN-0180 | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | Paved Roads and Parking Lots | PM10-total | Paving, wet/chemical suppression | 90 | % CONTROL |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | Haul Roads | PM10-total | Paving, wet/chemical suppression, speed re | 0.38 | T/YR |
| OH-0368 | PALLAS NITROGEN LLC | 4/19/2017 | Haul Roads-Paved | PM10-total | Paving | 2.6 | T/YR |
| SC-0181 | RESOLUTE FP US INC CATAWBA LUMBER MILL | 11/3/2017 | Haul Roads | PM2.5-filterable | Good Housekeeping Practices | 0.01 | LB/VMT |
| OH-0376 | IRONUNITS LLC - TOLEDO HBI | 2/9/2018 | Haul Roads-Paved | PM2.5-filterable | Water Flushing and Sweeping | 0.15 | T/YR |
| IA-0105 | IOWA FERTILIZER COMPANY | 10/26/2012 | Haul Roads | PM2.5-total | Paving, wet/chemical suppression | | |
| IA-0106 | CF INDUSTRIES NITROGEN, LLC - PORT NEAL NITROGEN COMPLEX | 7/12/2013 | Haul Roads | PM2.5-total | Paving, wet/chemical suppression | | |
| IN-0263 | MIDWEST FERTILIZER COMPANY LLC | 3/23/2017 | Paved Roads and Parking Lots | PM2.5-total | Paving, wet/chemical suppression | | |
| IN-0166 | INDIANA GASIFICATION, LLC | 6/27/2012 | Haul Roads-Paved | PM2.5-total | Paving, wet/chemical suppression | 90 | % CONTROL |
| IN-0173 | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | Paved Roads and Parking Lots | PM2.5-total | Paving, wet/chemical suppression | 90 | % CONTROL |
| IN-0179 | OHIO VALLEY RESOURCES, LLC | 9/25/2013 | Paved Roads and Parking Lots | PM2.5-total | Paving, wet/chemical suppression | 90 | % CONTROL |
| IN-0180 | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | Paved Roads and Parking Lots | PM2.5-total | Paving, wet/chemical suppression | 90 | % CONTROL |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | Haul Roads | PM2.5-total | Paving, wet/chemical suppression, speed re | 0.09 | T/YR |
| MD-0046 | KEYS ENERGY CENTER | 10/31/2014 | Haul Roads-Paved and Unpaved | PM-filterable | Water Flushing and Sweeping | | |
| MO-0089 | OWENS CORNING INSULATION SYSTEMS, LLC | 5/12/2016 | Haul Roads | PM-filterable | Vacuum sweeping/washing | | |
| IN-0166 | INDIANA GASIFICATION, LLC | 6/27/2012 | Haul Roads-Paved | PM-filterable | Paving, wet/chemical suppression | 90 | % CONTROL |
| IN-0173 | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | Paved Roads and Parking Lots | PM-filterable | Paving, wet/chemical suppression | 90 | % CONTROL |
| IN-0179 | OHIO VALLEY RESOURCES, LLC | 9/25/2013 | Paved Roads and Parking Lots | PM-filterable | Paving, wet/chemical suppression | 90 | % CONTROL |
| IN-0180 | MIDWEST FERTILIZER CORPORATION | 6/4/2014 | Paved Roads and Parking Lots | PM-filterable | Paving, wet/chemical suppression | 90 | % CONTROL |
| SC-0181 | RESOLUTE FP US INC CATAWBA LUMBER MILL | 11/3/2017 | Haul Roads | PM-filterable | Good Housekeeping Practices | 0.13 | LB/VMT |
| KY-0100 | J.K. SMITH GENERATING STATION | 4/9/2010 | Haul Roads | PM-fugitive | Paving, wet/chemical suppression | | |
| MD-0041 | CPV ST. CHARLES | 4/23/2014 | Haul Roads | PM-fugitive | | | |
| OK-0156 | NORTHSTAR AGRI IND ENID | 7/31/2013 | Haul Roads | PM-fugitive | Paving | | |
| MD-0042 | WILDCAT POINT GENERATION FACILITY | 4/8/2014 | Haul Roads-Paved and Unpaved | PM-fugitive | Reasonable precautions | | |
| OH-0332 | MIDDLETOWN COKE COMPANY | 2/9/2010 | Paved Roads and Parking Lots | PM-fugitive | Watering | 1.08 | T/YR |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | Haul Roads | PM-fugitive | Paving, wet/chemical suppression, speed re | 1.88 | T/YR |
| OH-0368 | PALLAS NITROGEN LLC | 4/19/2017 | Haul Roads-Paved | PM-fugitive | Paving | 13.2 | T/YR |
| OH-0345 | DP&L J.M. STUART GENERATING STATION | 8/16/2011 | Haul Roads-Paved | PM-fugitive | Watering, speed restrictions | 110.96 | T/YR |
| IA-0105 | IOWA FERTILIZER COMPANY | 10/26/2012 | Haul Roads | PM-total | Paving, wet/chemical suppression | | |
| IA-0106 | CF INDUSTRIES NITROGEN, LLC - PORT NEAL NITROGEN COMPLEX | 7/12/2013 | Haul Roads | PM-total | Paving, wet/chemical suppression | | |
| IN-0263 | MIDWEST FERTILIZER COMPANY LLC | 3/23/2017 | Paved Roads and Parking Lots | PM-total | Paving, wet/chemical suppression | | |
| IL-0129 | CPV THREE RIVERS ENERGY CENTER | 7/30/2018 | Haul Roads | PM-total | Paving | 10 | % OPACITY |
| IL-0130 | JACKSON ENERGY CENTER | 12/31/2018 | Haul Roads | PM-total | | 10 | % OPACITY |

Table D-9 Addendum: RBLC Results for Haul Road Fugitives Updated Data: February 2021 to October 2021

| RBLC ID | Facility Name | Permit Date | Process Name | POLLUTANT | Control Method | Emission Limit | Limit Units |
|---------|------------------------------|-------------|---|---|--|----------------|-----------------|
| IL-0130 | JACKSON ENERGY CENTER | 12/31/2018 | Roadways | Particulate matter, total (TPM) | | 10 | PERCENT OPACITY |
| KY-0110 | NUCOR STEEL BRANDENBURG | 07/23/2020 | EP 14-01 - Paved Roadways | Particulate matter, fugitive | surface improvements/sweeping & watering | 0 | |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | Paved Roads & Datellite Coil Yard (EPs 04-01 & Damp; 04-04) | Particulate matter, filterable (FPM) | Sweeping & Watering | 0 | |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | Paved Roads & Datellite Coil Yard (EPs 04-01 & Damp; 04-04) | Particulate matter, total < 10 Âμ (TPM10) | Sweeping & Watering | 0 | |
| KY-0115 | NUCOR STEEL GALLATIN, LLC | 04/19/2021 | Paved Roads & Datellite Coil Yard (EPs 04-01 & Damp; 04-04) | Particulate matter, total < 2.5 Âμ (TPM2.5) | Sweeping & Watering | 0 | |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | Facility Roadways (F001) | Particulate matter, fugitive | Paving/Sweeping & Watering | 1.88 | T/YR |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | Facility Roadways (F001) | Particulate matter, total < 10 Âμ (TPM10) | Paving/Sweeping & Watering | 0.38 | T/YR |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | Facility Roadways (F001) | Particulate matter, total < 2.5 Âμ (TPM2.5) | Paving/Sweeping & Watering | 0.09 | T/YR |
| OH-0378 | PTTGCA PETROCHEMICAL COMPLEX | 12/21/2018 | Facility Roadways (F001) | Visible Emissions (VE) | Paving/Sweeping & Watering | 0 | |
| OH-0379 | PETMIN USA INCORPORATED | 02/06/2019 | Plant Roadways (F001) | Particulate matter, total < 10 Âμ (TPM10) | Watering | 0.21 | T/YR |
| OH-0379 | PETMIN USA INCORPORATED | 02/06/2019 | Plant Roadways (F001) | Particulate matter, total < 2.5 Âμ (TPM2.5) | Watering | 0.02 | T/YR |
| OH-0379 | PETMIN USA INCORPORATED | 02/06/2019 | Plant Roadways (F001) | Visible Emissions (VE) | Watering | 0 | |



Table E-1a SCR System Capital Cost Analysis - Auxiliary Boiler

| ltem | Value | Basis |
|--|-----------|---|
| Direct Costs | | |
| Purchased Equipment Cost | | |
| Equipment cost + auxiliaries [A] | \$350,000 | A = SCR system cost |
| Instrumentation | \$35,000 | 0.10 x (A) |
| Sales taxes | \$0 | Pollution Control Equipment Exempt |
| Freight | \$17,500 | 0.05 x (A) |
| Total Purchased Equipment Cost (PEC) [B] | \$402,500 | B = 1.15 x (A) |
| Direct Installation Costs | | |
| Total Direct Installation Cost | \$120,750 | 0.30 x B |
| Site Preparation (SP) | \$0 | As required |
| Buildings (Bldg.) | \$0 | As required |
| Total Direct Cost (DC) | \$523,250 | 1.30B + SP + Bldg. |
| Indirect Costs (Installation) | | |
| Engineering | \$40,250 | 0.10 x B |
| Construction and field expenses | \$20,125 | 0.05 x B |
| Contractor fees | \$40,250 | 0.10 x B |
| Start-up | \$8,050 | 0.02 x B |
| Performance test | \$7,500 | Stack Test Vendor Quote |
| Contingencies | \$20,125 | 0.05 x B |
| Other | \$0 | As required |
| Total Indirect Cost (IC) | \$136,300 | 0.32B + Other + Perf. Test |
| Total Capital Investment (TCI) = DC + IC | \$659,550 | 1.62B + Performance test + Other + SP + Bldg. |

Table E-1b SCR System Annual Cost Analysis - Auxiliary Boiler

| Item | | Auxiliary Boiler |
|---|-----------|--|
| | Value | Basis |
| Direct Annual Costs (DC) | | |
| Electricity | 2.0 | Dungarius dung nataliyat had |
| Press. Drop (in W.C.) | 3.0 | Pressure drop - catalyst bed |
| Power output of Gas Heater (kW) | 23,429 | ISO Rating |
| Power Loss Due to Pressure Drop (%) | 0.30% | 0.1% for every 1" pressure drop |
| Power Loss Due to Pressure Drop (kW) | 70.29 | |
| Unit cost (\$/kWh) | \$0.045 | Estimated market value |
| Cost of Power Loss (\$/yr) | \$27,707 | Based on operation 8760 hours/yr |
| Operating Labor | | |
| Catalyst labor req. | \$16,425 | 1/2 hr/shift @ \$30/hr |
| Ammonia delivery requirement (SCR) | \$720 | 24 hr/yr (3 deliveries per year) @ \$30/hr |
| Ammonia recordkeeping and reporting (SCR) | \$1,200 | 40 hours per year @ \$30/hr |
| Catalyst cleaning | \$1,200 | 40 hours per year @ \$30/hr |
| Supervisor | \$2,464 | 15% Operating labor |
| Total Cost (\$/yr) | \$22,009 | |
| Maintenance | | |
| Catalyst replacement labor | \$3,200 | 107 hr/yr (8 workers, 40 hr, every 3 years, \$30/hr) |
| Catalyst system maintenance labor req. | \$16,425 | 1/2 hr/shift @ \$30/hr |
| Ammonia system maintenance labor req. | \$10,950 | 1 hr/day @ \$30/hr |
| Material | \$27,375 | 100% of maintenance labor |
| Total Cost (\$/yr) | \$57,950 | |
| Ammonia | | |
| Requirement (tons/yr) | 33.7 | 29% aqueous ammonia @ \$375/ton |
| Unit Cost (\$/ton) | \$375 | Estimate |
| Total Cost (\$/yr) | \$12,654 | |
| Process Air | | |
| Requirement (scf/lb NH ₃) | 350 | |
| Requirement (mscf/yr) | 103,463 | |
| Unit Cost (\$/mscf) | \$0.20 | \$0.20 per 1000 scf |
| Total Cost (\$/yr) | \$20,693 | • |
| Catalyst | | |
| Catalyst Cost (\$) | \$35,000 | Catalyst modules |
| Catalyst Disposal Cost (\$) | \$38 | Disposal of catalyst modules |
| Sales Tax (\$) | \$0 | Pollution Control Equipment Exempt |
| Catalyst Life (yrs) | 3 | n |
| Interest Rate (%) | 7.0% | i |
| CRF | 0.381 | Amortization of catalyst for 3 yrs |
| Total Cost (\$/yr) | \$13,351 | (Volume) * (Unit Cost) * (CRF) |
| Indirect Annual Costs (IC) | . , | |
| Overhead | \$0 | OAQPS SCR Assumption |
| Administrative charges | \$0 | OAQPS SCR Assumption |
| Annual Contingency | \$0 | OAQPS SCR Assumption |
| Property taxes | \$0 | OAQPS SCR Assumption |
| Insurance | \$0 | OAQPS SCR Assumption |
| Capital Recovery | \$62,257 | CRF x TCI (20 yr life, 7.0% interest) |
| Total Indirect Costs (\$/yr) | \$62,257 | , |
| Total Annualized Costs (TAC) (\$) | \$216,620 | |
| Total NOx Controlled (ton/yr) | 14.2 | 90% reduction |
| Total 140x Controlled (toll/yl) | 14.2 | 30 /0 Teduction |
| COST EFFECTIVENESS (\$/ton) | \$15,264 | |
| | | |

Table E-2a
Ultra-Low NOx Burner System Capital Cost Analysis - Auxiliary Boiler

| ltem | Value | Basis |
|--|-----------|------------------------------------|
| Direct Costs | | |
| Purchased Equipment Cost | | |
| Equipment cost + auxiliaries [A] | \$115,000 | Α |
| Instrumentation | \$11,500 | 0.10 x A |
| Sales taxes | \$0 | Pollution Control Equipment Exempt |
| Freight | \$5,750 | 0.05 x A |
| Total Purchased Equipment Cost (PEC) [B] | \$132,250 | $B = 1.15 \times A$ |
| Direct Installation Costs | | |
| Electrical | \$5,290 | 0.04 x B |
| Insulation for ductwork | \$1,323 | 0.01 x B |
| Painting | \$1,323 | 0.01 x B |
| Total Direct Installation Cost | \$7,935 | 0.06 x B |
| Total Direct Cost (DC) | \$140,185 | 1.06B |
| Indirect Costs (Installation) | | |
| Start-up | \$2,645 | 0.02 x B |
| Performance test | \$1,323 | 0.01 x B |
| Contingencies | \$6,613 | 0.05 x B |
| Other | \$0 | As required |
| Total Indirect Cost (IC) | \$10,580 | 0.08B + Other |
| Total Capital Investment (TCI) = DC + IC | \$150,765 | 1.14B + Other |

Table E-2b
Ultra-Low Nox Burner System Annual Cost Analysis - Auxiliary Boiler

| Item | Value | Basis |
|---|-------------|--|
| Direct Annual Costs (DC) | | |
| Operating Labor | | |
| Operating Labor | \$19,163 | 1/2 hr/shift @ \$35/hr, 375 shifts/year |
| Supervisor | \$2,874 | 15% Operating labor |
| Total Cost (\$/yr) | \$22,037 | |
| Maintenance | | |
| Auxiliary boiler burner maintenance labor req. | \$3,210 | 107 hr/y (8 worker, 40 hr, every 3 years), \$30/hr |
| Material | \$3,210 | 100% of maintenance labor |
| Total Cost (\$/yr) | \$6,420 | |
| Indirect Annual Costs (IC) | | |
| Overhead | \$13,222.13 | 60% labor |
| Administrative charges | \$3,015 | 2% TCI |
| Annual Contingency | \$7,009 | 5% of DC |
| Property taxes | \$1,508 | 1% TCI |
| Insurance | \$1,508 | 1% TCI |
| Capital Recovery | \$12,150 | CRF x TCI (30 yr life, 7.0% interest) |
| Total Indirect Costs (\$/yr) | \$38,412 | |
| Total Annualized Costs (TAC) (\$) | \$66,868 | |
| Total Pollutant Controlled (ton/yr) (Natural Gas) | 11.3 | 30 ppm controlled to 9 ppm |
| COST EFFECTIVENESS (\$/ton) | \$5,895 | |
| | | |

Table E-3a
Oxidation Catalyst Capital Cost Analysis - Auxiliary Boiler

| Basis |
|---|
| |
| |
| A |
| |
| 0.10 x (A) |
| Pollution Control Equipment Exempt |
| 0.05 x (A) |
| B = 1.15 x (A) |
| |
| 0.08 x B |
| 0.14 x B |
| 0.04 x B |
| 0.02 x B |
| 0.01 x B |
| 0.01 x B |
| 0.30 x B |
| As required |
| As required (5-18% PEC) |
| 1.3B + SP + Bldg. |
| |
| 0.10 x B |
| 0.10 x B 0.05 x B |
| 0.03 x B 0.10 x B |
| 0.10 X B |
| Stack Test Vendor Quote |
| 0.05 x B |
| As required |
| 0.32B + Other + Perf. Test |
| 1.62B + Performance test + Other + SP + Bldg. |
| 1 |

Table E-3b
Oxidation Catalyst Annual Cost Analysis - Auxiliary Boiler

| Item | nnual Cost Analysis - Value | Basis |
|---------------------------------------|--------------------------------|---|
| itelli | vaiut | Dasis |
| Direct Annual Costs (DC) | | |
| | | |
| Steam | | |
| Press. Drop (in W.C.) | 3.0 | Pressure drop - catalyst bed |
| Power output of Gas Heater (kW) | 23,429 | ISO Rating |
| Output Loss Due to Pressure Drop (%) | 0.30% | 0.1% for every 1" pressure drop |
| Output Loss Due to Pressure Drop (kW) | 70.29 | |
| Unit cost (\$/kWh) | \$0.05 | Current Purchase Price |
| Cost of Heat Rate Loss (\$/yr) | \$27,707 | Based on operation 8,760 hours/yr |
| | | |
| Operating Labor | | Assumed \$30/hr |
| Catalyst labor req. | \$16,425 | 216 hr/yr (1/2 hr/shift. 1095 shifts/yr) |
| Supervisor | \$2,464 | 15% Operating labor |
| Total Cost (\$/yr) | \$18,889 | |
| Maintenance | | |
| Catalyst replacement labor | \$3,200 | 107 hr/yr(8 worker, 40 hr, every 3 years) |
| Material | \$3,200 | 100% of maintenance labor |
| Total Cost (\$/yr) | \$6,400 | 100 % of maintenance labor |
| Total Cost (\$791) | φ0,400 | |
| Catalyst | | |
| Catalyst Cost (\$) | \$35,000 | Catalyst modules |
| Catalyst Disposal Cost (\$) | \$1,500 | Disposal of catalyst modules |
| Sales Tax (\$) | \$0 | Assume exempt from taxes |
| Catalyst Life (yrs) | 3 | n |
| Interest Rate (%) | 7% | I |
| CRF | 0.381 | Amortization of catalyst over 3 yrs |
| Total Cost (\$/yr) | \$13,908 | (Volume)(Unit Cost)(CRF) |
| | | |
| Indirect Annual Costs (IC) | ФО | OAODS SCD Assumenting |
| Overhead | \$0 \$0 | OAQPS SCR Assumption |
| Administrative charges | \$0 | OAQPS SCR Assumption |
| Annual Contingency | \$0 | OAQPS SCR Assumption |
| Property taxes | \$0 | OAQPS SCR Assumption |
| Insurance | \$0 | OAQPS SCR Assumption |
| Capital Recovery | \$13,897 | CRF x TCI (20 yr life, 7.0% interest) |
| Total Indirect Costs (\$/yr) | \$13,897 | |
| Total Annualized Costs (TAC) (\$) | \$80,801 | |
| Total CO Controlled (ton/yr) | 14.6 | 90% removal |
| Total VOC Controlled (ton/yr) | 14.0 | 50% removal |
| COST EFFECTIVENESS (\$/ton) | \$5,125 | 00 /0 (GIIIOVA) |
| 333. I. 1 20111 Elite00 (\$7.011) | Ψ 0 , 120 | |

Table 1a
Ultra-Low NOx Burner System Capital Cost Analysis - Natural Gas Heater

| Item | Value | Basis |
|--|----------|------------------------------------|
| Direct Costs | | |
| Purchased Equipment Cost | | |
| Equipment cost + auxiliaries [A] | \$20,000 | А |
| Instrumentation | \$2,000 | 0.10 x A |
| Sales taxes | \$0 | Pollution Control Equipment Exempt |
| Freight | \$1,000 | 0.05 x A |
| Total Purchased Equipment Cost (PEC) [B] | \$23,000 | B = 1.15 x A |
| Direct Installation Costs | | |
| Electrical | \$920 | 0.04 x B |
| Insulation for ductwork | \$230 | 0.01 x B |
| Painting | \$230 | 0.01 x B |
| Total Direct Installation Cost | \$1,380 | 0.06 x B |
| Total Direct Cost (DC) | \$24,380 | 1.06 x B |
| Indirect Costs (Installation) | | |
| Start-up | \$460 | 0.02 x B |
| Performance test | \$0 | Assumed not required |
| Contingencies | \$1,150 | 0.05 x B |
| Other | \$0 | As required |
| Total Indirect Cost (IC) | \$1,610 | 0.07B + Other |
| Total Capital Investment (TCI) = DC + IC | \$25,990 | 1.13B + Other |

Table 1b

Ultra-Low NOx Burner System Annual Cost Analysis - Natural Gas Heater

| Item | Value | Basis |
|---|------------|--|
| Direct Annual Costs (DC) | | |
| Operating Labor | | |
| Operating Labor | \$6,388 | 1/2 hr/shift @ \$35/hr, 365 shifts/year |
| Supervisor | \$958 | 15% Operating labor |
| Total Cost (\$/yr) | \$7,346 | |
| Maintenance | | |
| Heater burner maintenance labor req. | \$3,210 | 107 hr/y (8 worker, 40 hr, every 3 years), \$30/hr |
| Material | \$3,210 | 100% of maintenance labor |
| Total Cost (\$/yr) | \$6,420 | |
| Indirect Annual Costs (IC) | | |
| Overhead | \$4,407.38 | 60% labor |
| Administrative charges | \$520 | 2% TCI |
| Annual Contingency | \$1,219 | 5% of DC |
| Property taxes | \$260 | 1% TCI |
| Insurance | \$260 | 1% TCI |
| Capital Recovery | \$2,094 | CRF x TCI (30 yr life, 7.0% interest) |
| Total Indirect Costs (\$/yr) | \$8,760 | |
| Total Annualized Costs (TAC) (\$) | \$22,526 | |
| Total Pollutant Controlled (ton/yr) (Natural Gas) | 1.7 | 80% Reduction |
| COST EFFECTIVENESS (\$/ton) | \$13,187 | |

Table E-3a SCR System Capital Cost Analysis - Gas Heater

| Item | Value | Basis |
|--|-----------|---|
| Direct Costs | | |
| Purchased Equipment Cost | | |
| Equipment cost + auxiliaries [A] | \$70,000 | A (SCR system cost) |
| Instrumentation | \$7,000 | 0.10 x (A) |
| Sales taxes | \$0 | Pollution Control Equipment Exempt |
| Freight | \$3,500 | 0.05 x (A) |
| Total Purchased Equipment Cost (PEC) [B] | \$80,500 | B = 1.15 x (A) |
| Direct Installation Costs | | |
| Total Direct Installation Cost | \$24,150 | 0.30 x B |
| Site Preparation (SP) | \$0 | As required |
| Buildings (Bldg.) | \$0 | As required |
| Total Direct Cost (DC) | \$104,650 | 1.30B + SP + Bldg. |
| Indirect Costs (Installation) | | |
| Engineering | \$8,050 | 0.10 x B |
| Construction and field expenses | \$4,025 | 0.05 x B |
| Contractor fees | \$8,050 | 0.10 x B |
| Start-up | \$1,610 | 0.02 x B |
| Performance test | \$7,500 | Stack Test Vendor Quote |
| Contingencies | \$4,025 | 0.05 x B |
| Other | \$0 | As required |
| Total Indirect Cost (IC) | \$33,260 | 0.32B + Other + Perf. Test |
| Total Capital Investment (TCI) = DC + IC | \$137,910 | 1.62B + Performance test + Other + SP + Bldg. |

Table E-3b SCR System Capital Cost Analysis - Gas Heater

| | oital Cost Analysis - 0 | |
|---|-------------------------|---|
| Item | Value | Basis |
| Direct Annual Costs (DC) | | |
| Electricity | | |
| Press. Drop (in W.C.) | 3.0 | Pressure drop - catalyst bed |
| Power output of Gas Heater (kW) | 2,343 | ISO Rating |
| Power Loss Due to Pressure Drop (%) | 0.30% | 0.1% for every 1" pressure drop |
| Power Loss Due to Pressure Drop (kW) | 7.03 | |
| Unit cost (\$/kWh) | \$0.045 | Estimated market value |
| Cost of Power Loss (\$/yr) | \$2,771 | Based on operation 8,760 hours/yr |
| Operating Labor | | |
| Catalyst labor req. | \$16,425 | 1/2 hr/shift @ \$30/hr |
| Ammonia delivery requirement (SCR) | \$720 | 24 hr/yr (3 deliveries per year) @ \$30/hr |
| Ammonia recordkeeping and reporting (SCR) | \$1,200 | 40 hours per year @ \$30/hr |
| Catalyst cleaning | \$1,200 | 40 hours per year @ \$30/hr |
| Supervisor | \$2,464 | 15% Operating labor |
| Total Cost (\$/yr) | \$22,009 | |
| Maintenance | | |
| Catalyst replacement labor | \$3,200 | 107 hr/yr (8 workers, 40 hr, every 3 years) |
| Catalyst system maintenance labor req. | \$16,425 | 1/2 hr/shift @ \$30/hr |
| Ammonia system maintenance labor req. | \$10,950 | 1 hr/day @ \$30/hr |
| Material | \$27,375 | 100% of maintenance labor |
| Total Cost (\$/yr) | \$57,950 | |
| Ammonia | | |
| Requirement (tons/yr) | 4.6 | 29% aqueous ammonia @ \$375/ton |
| Unit Cost (\$/ton) | \$375 | Estimate |
| Total Cost (\$/yr) | \$1,722 | |
| Process Air | | |
| Requirement (scf/lb NH ₃) | 350 | |
| Requirement (mscf/yr) | 14,082 | |
| Unit Cost (\$/mscf) | \$0.20 | \$0.20 per 1000 scf |
| Total Cost (\$/yr) | \$2,816 | |
| Catalyst | | |
| Catalyst Cost (\$) | \$8,500 | Catalyst modules |
| Catalyst Disposal Cost (\$) | \$38 | Disposal of catalyst modules |
| Sales Tax (\$) | \$0 | Pollution Control Equipment Exempt |
| Catalyst Life (yrs) | 3 | n |
| Interest Rate (%) | 7.0% | i |
| CRF | 0.381 | Amortization of catalyst for 3 yrs |
| Total Cost (\$/yr) | \$3,253 | (Volume) * (Unit Cost) * (CRF) |
| Indirect Annual Costs (IC) | | |
| Overhead | \$0 | OAQPS SCR Assumption |
| Administrative charges | \$0 | OAQPS SCR Assumption |
| Annual Contingency | \$0 | OAQPS SCR Assumption |
| Property taxes | \$0 | OAQPS SCR Assumption |
| Insurance | \$0 | OAQPS SCR Assumption |
| Capital Recovery | \$13,018 | CRF x TCI (20 yr life, 7.0% interest) |
| Total Indirect Costs (\$/yr) | \$13,018 | |
| Total Annualized Costs (TAC) (\$) | \$103,539 | |
| Total NOx Controlled (ton/yr) | 1.9 | 90% reduction |
| COST EFFECTIVENESS (\$/ton) | \$53,604 | _ |
| (4.44) | 7-2,52 | |
| , | | |

Table E-4a CO Catalyst Capital Cost Analysis - Gas Heater

| Item | Value | Basis |
|--|------------|---|
| Direct Costs | | |
| Purchased Equipment Cost | | |
| Equipment cost + auxiliaries [A] | \$14,000 | A |
| Instrumentation | \$1,400 | 0.10 x (A) |
| Sales taxes | \$0 | Pollution Control Equipment Exempt |
| Freight | \$700 | 0.05 x (A) |
| Total Purchased Equipment Cost (PEC) [B] | \$16,100 | B = 1.15 x (A) |
| Direct Installation Costs | | |
| Foundations and supports | \$1,288.00 | 0.08 x B |
| Handling and erection | \$2,254 | 0.14 x B |
| Electrical | \$644 | 0.04 x B |
| Piping | \$322 | 0.02 x B |
| Insulation for ductwork | \$161 | 0.01 x B |
| Painting | \$161 | 0.01 x B |
| Total Direct Installation Cost | \$4,830 | 0.30 x B |
| Site Preparation (SP) | \$0 | As required |
| Buildings (Bldg.) | \$0 | As required (5-18% PEC) |
| Total Direct Cost (DC) | \$20,930 | 1.3B + SP + Bldg. |
| Indirect Costs (Installation) | | |
| Engineering | \$1,610 | 0.10 x B |
| Construction and field expenses | \$805 | 0.05 x B |
| Contractor fees | \$1,610 | 0.10 x B |
| Start-up | \$322 | 0.02 x B |
| Performance test | \$7,500 | Stack Test Vendor Quote |
| Contingencies | \$805 | 0.05 x B |
| Other | \$0 | As required |
| Total Indirect Cost (IC) | \$12,652 | 0.32B + Other + Perf. Test |
| Total Capital Investment (TCI) = DC + IC | \$33,582 | 1.62B + Performance test + Other + SP + Bldg. |
| | | |

Table E-4b CO Catalyst Annual Cost Analysis - Gas Heater

| CO Catalyst Annual Cost Analysis - Gas Heater | | | |
|--|---------------------------|--|--|
| Item | Value | Basis | |
| Direct Annual Costs (DC) | | | |
| Steam | | | |
| Press. Drop (in W.C.) | 3.0 | Draggura drag actalyat had | |
| Power output of Gas Heater (kW) | 2,343 | Pressure drop - catalyst bed ISO Rating | |
| Output Loss Due to Pressure Drop (%) | 2,343 0.30% | 0.1% for every 1" pressure drop | |
| | 7.03 | 0.1% for every 1 pressure drop | |
| Output Loss Due to Pressure Drop (kW) Unit cost (\$/kWh) | \$0.05 | Current Purchase Price | |
| Cost of Heat Rate Loss (\$/yr) | \$0.05 \$2,771 | Based on operation 8,760 hours/yr | |
| Cost of Heat Rate Loss (\$/yr) | \$2,771 | based on operation 6,760 hours/yi | |
| Operating Labor | | Assumed \$30/hr | |
| Catalyst labor req. | \$16,425 | 216 hr/yr (1/2 hr/shift. 431 shifts/yr) | |
| Supervisor | \$2,464 | 15% Operating labor | |
| Total Cost (\$/yr) | \$18,889 | | |
| Maintenance | | | |
| Catalyst replacement labor | \$3,200 | 107 hr/yr(8 worker, 40 hr, every 3 years) | |
| Material | \$3,200 | 100% of maintenance labor | |
| Total Cost (\$/yr) | \$6,400 | | |
| Catalyst | | | |
| Catalyst Cost (\$) | \$8,000 | Catalyst modules | |
| Catalyst Disposal Cost (\$) | \$1,500 | Disposal of catalyst modules | |
| Sales Tax (\$) | \$0 | Assume exempt from taxes | |
| Catalyst Life (yrs) | 3 | n | |
| Interest Rate (%) | 7% | I | |
| CRF | 0.381 | Amortization of catalyst over 3 yrs | |
| Total Cost (\$/yr) | \$3,620 | (Volume)(Unit Cost)(CRF) | |
| Indirect Annual Costs (IC) | | | |
| Overhead | \$0 | OAQPS SCR Assumption | |
| Administrative charges | \$0 | OAQPS SCR Assumption | |
| Annual Contingency | \$0 | OAQPS SCR Assumption | |
| Property taxes | \$0 | OAQPS SCR Assumption | |
| Insurance | \$0 | OAQPS SCR Assumption | |
| Capital Recovery | \$3,170 | CRF x TCI (20 yr life, 7.0% interest) | |
| Total Indirect Costs (\$/yr) | \$3,170 | | |
| Total Annualized Costs (TAC) (\$) | \$34,849 | | |
| Total CO Controlled (ton/yr) | 434,049 3.2 | 90% removal | |
| Total CO Controlled (ton/yr) Total VOC Controlled (ton/yr) | 3.2 0.07 | 90% removal | |
| COST EFFECTIVENESS (\$/ton) | \$10,550 | | |
| (\$/(OII) | \$10,550 | | |
| | | | |

Table 1
Oxidation Catalyst Capital Cost Analysis - Emergency Fire Pump

| Item | Value | Basis |
|--|----------|--------------------------------------|
| Direct Costs | | |
| _ | | |
| Purchased Equipment Cost | | |
| Equipment cost + auxiliaries [A] | \$11,895 | Α |
| Instrumentation | \$1,190 | 0.10 x A |
| Sales taxes | \$0 | Pollution Control Equipment Exempt |
| Freight | \$595 | 0.05 x A |
| Total Purchased Equipment Cost (PEC) [B] | \$13,679 | B = 1.15 x A |
| Direct Installation Costs | | |
| Foundations and supports | \$1,094 | 0.08 x B |
| Handling and erection | \$1,915 | 0.14 x B |
| Electrical | \$547 | 0.04 x B |
| Piping | \$274 | 0.02 x B |
| Insulation for ductwork | \$137 | 0.01 x B |
| Painting | \$137 | 0.01 x B |
| Total Direct Installation Cost | \$4,104 | 0.30 x B |
| Site Preparation (SP) | \$0 | As required |
| Buildings (Bldg.) | \$0 | As required (5-18% PEC) |
| Total Direct Cost (DC) | \$17,783 | 1.3B + SP + Bldg. |
| Indirect Costs (Installation) | | |
| Engineering | \$1,368 | 0.10 x B |
| Engineering | | |
| Construction and field expenses | \$684 | 0.05 x B |
| Contractor fees | \$1,368 | 0.10 x B |
| Start-up | \$274 | 0.02 x B |
| Performance test | \$1,500 | Stack Test Vendor Quote |
| Contingencies | \$684 | 0.05 x B |
| Other | \$0 | As required |
| Total Indirect Cost (IC) | \$5,877 | 0.32B + Other + Performance Test |
| Total Capital Investment (TCI) = DC + IC | \$23,660 | 1.62B + Performance Test + SP + Bldg |

Table 2
Oxidation Catalyst Annual Cost Analysis - Emergency Fire Pump

| Oxidation Catalyst Annu Item | Value | Basis |
|---|------------|--|
| Kem | Value | Dusis |
| Direct Annual Costs (DC) | | |
| -1 | | |
| Electricity | 0.0 | December 1 and 1 and 1 and 1 |
| Press. Drop (in W.C.) | 3.0 | Pressure drop - catalyst bed |
| Power output of Black Start Engine (kW) | 450 | ISO Rating |
| Output Loss Due to Pressure Drop (%) | 0.30% | 0.1% for every 1" pressure drop |
| Output Loss Due to Pressure Drop (kW) | 1.35 | |
| Unit cost (\$/kWh) | \$0.059 | Current Purchase Price |
| Cost of Heat Rate Loss (\$/yr) | \$40 | Based on operation of 500 hours/yr |
| Operating Labor | | Assumed \$30/hr |
| Catalyst labor | \$938 | 1/2 hr per shift |
| Material | \$938 | 100% of maintenance labor |
| Supervisor | \$141 | 15% Operating labor |
| Total Cost (\$/yr) | \$2,016 | |
| νοια: Θουτ (ψ, γ, γ, | Ψ=,0:0 | |
| Catalyst | | |
| Catalyst Cost (\$) | \$827 | Catalyst modules |
| Catalyst Disposal Cost (\$) | \$38 | Disposal of catalyst modules |
| Catalyst replacement labor | \$3,200 | 107 hr/yr (8 worker, 40 hr, every 3 years) |
| Sales Tax (\$) | \$0 | Assume exempt from taxes |
| Catalyst Life (yrs) | 3 | n |
| Interest Rate (%) | 7% | I |
| CRF | 0.381 | Amortization of catalyst over 3 yrs |
| Total Cost (\$/yr) | \$1,549 | (Material + Labor Costs) * CRF |
| Indirect Annual Costs (IC) | | |
| Overhead | \$0 | OAQPS SCR Assumption |
| Administrative charges | \$0 | OAQPS SCR Assumption |
| Annual Contingency | \$0 | OAQPS SCR Assumption |
| Property taxes | \$0 | OAQPS SCR Assumption |
| Insurance | \$0 \$0 | OAQPS SCR Assumption |
| Capital Recovery | \$2,233 | CRF x TCI (20 yr life, 7.0% interest) |
| Total Indirect Costs (\$/yr) | \$2,233 | 311 X 131 (23)1 me, 7.370 merest) |
| Total muliect Gosts (\psi/yi) | ΨΖ,233 | |
| Total Annualized Costs (TAC) (\$) | \$5,838 | |
| Total CO Controlled (ton/yr) | 0.32 | 80% removal |
| Total VOC Controlled (ton/yr) | 0.09 | 50% removal |
| COST EFFECTIVENESS (\$/ton) | \$14,326 | |
| φιοπή | Ψ17,020 | |
| | | |

Table 3
SCR System Capital Cost Analysis - Emergency Generator

| ltem | Value | Basis |
|--|----------|---|
| Direct Costs | | |
| Purchased Equipment Cost | | |
| Equipment cost + auxiliaries [A] | \$42,601 | Α |
| Instrumentation | \$4,260 | 0.10 x (A) |
| Sales taxes | \$0 | Pollution Control Equipment Exempt |
| Freight | \$2,130 | 0.05 x (A) |
| Total Purchased Equipment Cost (PEC) [B] | \$48,991 | $B = 1.15 \times (A)$ |
| Direct Installation Costs | | |
| Total Direct Installation Cost | \$14,697 | 0.30 x B |
| Site Preparation (SP) | \$0 | As required |
| Buildings (Bldg.) | \$0 | As required |
| Total Direct Cost (DC) | \$63,688 | B + SP + Bldg. + Total Direct Install. Cost |
| Indirect Costs (Installation) | | |
| Engineering | \$4,899 | 0.10 x B |
| Construction and field expenses | \$2,450 | 0.05 x B |
| Contractor fees | \$4,899 | 0.10 x B |
| Start-up | \$980 | 0.02 x B |
| Performance test | \$1,500 | Stack Test Vendor Quote |
| Contingencies | \$2,450 | 0.05 x B |
| Other | \$0 | As required |
| Total Indirect Cost (IC) | \$17,177 | 0.32B + Other + Performance Test |
| Total Capital Investment (TCI) = DC + IC | \$80,866 | 1.32B + Perf. Test + SP + Bldg + DC |

Table 4
SCR System Annual Cost Analysis - Emergency Generator

| SCR System Annual Co | | |
|---|----------------|---|
| Item | Value | Basis |
| Direct Annual Costs (DC) | | |
| Electricity | | |
| Press. Drop (in W.C.) | 3.0 | Pressure drop - catalyst bed |
| Power output of Black Start (kW) | 450 | ISO Rating |
| Power Loss Due to Pressure Drop (%) | 0.30% | 0.1% for every 1" pressure drop |
| Power Loss Due to Pressure Drop (kW) | 1.35 | |
| Unit cost (\$/kWh) | \$0.059 | Estimated market value |
| Cost of Power Loss (\$/yr) | \$40 | Based on operation of 500 hours/yr |
| Operating Labor | | |
| Catalyst labor req. | \$938 | 1/2 hr/shift @ \$30/hr |
| Ammonia delivery requirement (SCR) | \$720 | 24 hr/yr (3 deliveries per year) @ \$30/hr |
| Ammonia recordkeeping and reporting (SCR) | \$1,200 | 10 hours per year @ \$30/hr |
| Catalyst cleaning | \$1,200 | 10 hours per year @ \$30/hr |
| Supervisor | \$141 | 15% Operating labor |
| Total Cost (\$/yr) | \$4,198 | , , |
| Maintenance | | |
| Catalyst replacement labor | \$3,210 | 107 hr/yr (8 workers, 40 hr, every 3 years) |
| Catalyst system maintenance labor req. | \$938 | 1/2 hr/shift @ \$30/hr |
| Ammonia system maintenance labor req. | \$10,950 | 1 hr/day @ \$30/hr |
| Material | \$11,888 | 100% of maintenance labor |
| Total Cost (\$/yr) | \$26,985 | |
| Ammonia | Ψ20,000 | |
| Requirement (tons/yr) | 7.9 | 29% aqueous ammonia @ \$375/ton |
| Unit Cost (\$/ton) | \$375 | Estimate |
| Total Cost (\$/yr) | \$2,975 | Loumato |
| Process Air | Ψ2,010 | |
| Requirement (scf/lb NH ₃) | 350 | |
| Requirement (mscf/yr) | 24,323 | |
| Unit Cost (\$/mscf) | \$0.20 | \$0.20 per 1000 scf |
| Total Cost (\$/yr) | \$4,865 | ψο.20 μει 1000 361 |
| Catalyst | ψ 1,000 | |
| Catalyst Cost (\$) | \$5,173 | Catalyst modules |
| Catalyst Disposal Cost (\$) | \$38 | Disposal of catalyst modules |
| Sales Tax (\$) | \$0 | Pollution Control Equipment Exempt |
| Catalyst Life (yrs) | 3 | n |
| Interest Rate (%) | 7.0% | i i |
| CRF | 0.381 | Amortization of catalyst for 3 yrs |
| Total Cost (\$/yr) | \$1,986 | (Volume) * (Unit Cost) * (CRF) |
| Indirect Annual Costs (IC) | φ1,900 | (Volume) (Onlit Cost) (CKF) |
| Overhead | \$0 | OAQPS SCR Assumption |
| Administrative charges | \$0 \$0 | OAQPS SCR Assumption |
| Annual Contingency | \$0 \$0 | OAQPS SCR Assumption |
| | | OAQPS SCR Assumption |
| Property taxes | \$0 \$0 | OAQPS SCR Assumption OAQPS SCR Assumption |
| Insurance | \$0 \$7.633 | · |
| Capital Recovery | \$7,633 | CRF x TCI (20 yr life, 7.0% interest) |
| Total Indirect Costs (\$/yr) | \$7,633 | |
| Total Annualized Costs (TAC) (\$) | \$48,681 | |
| Total Pollutant Controlled (ton/yr) (Natural gas) | 3.3 | 85% reduction (Based on 500 hrs/yr) |
| COST EFFECTIVENESS (\$/ton) | \$14,592 | |
| | C44 ED2 | |

State of Wisconsin DEPARTMENT OF NATURAL RESOURCES

Information Request

FID/Docket Number: 816127840 Date of Request: March 26, 2019

Requested From: WDNR Response Due: April 10, 2019

Contact Requesting Information: Megan Corrado, Air Management Engineer

If you feel your responses are trade secret or privileged, please indicate this on your response.

| Request No. | |
|----------------|--|
| | |

017 (3.)

For the diesel generator, please provide the cost difference between a Tier 2 and Tier 4 engine as well as the associated dollar per ton of controlled emissions.

Response:

017 (3.)

For the diesel generator, the cost difference between a Tier 2 and a Tier 4 engine is summarized below and shown in detail in Attachment 2.

| Parameter | Tier 2 Engine | Tier 4 Engine | Difference |
|---|---------------|---------------|---------------------|
| Initial Capital Cost | \$500,000 | \$950,000 | \$450,000 |
| Total Capital Investment | \$635,375 | \$1,207,213 | \$571,838 |
| Total Annualized Costs | \$105,368 | \$200,198 | \$94,831 |
| Emissions Sum of NOx, PM, and VOC) | 4.3 tons | 3.1 tons | 1.3 ton decrease |
| Cost per Ton for change from Tier 2 to Tier 4 | | | \$74,993 |

Due to the limited usage of the emergency generator and the cost of the Tier 4 engine, it is economically infeasible to install a Tier 4 engine.

| Response by: | Minda Nelson, P.E. | List Sources of Information: |
|--------------|----------------------------------|------------------------------|
| Title: | Associate Environmental Engineer | |
| Department: | Burns & McDonnell | |
| Telephone: | (816) 822-4208 | |

Table 2a
Tier 2 Generator Capital Cost Analysis

| | A 0.10 x A |
|-----------------|---|
| \$50,000 \$0 | • |
| \$50,000 \$0 | • |
| \$0 | 0.10 x A |
| | |
| A = | Pollution Control Equipment Exempt |
| \$25,000 | 0.05 x A |
| \$575,000 | B = 1.15 x A |
| | |
| | |
| \$575,000 | В |
| | |
| \$11,500 | 0.02 x B |
| \$0 | Assumed not required |
| \$28,750 | 0.05 x B |
| \$0 | As required |
| 0.5 | Years (n) |
| 7.0 | Percent (i) |
| \$20,125 | DCxixn |
| \$60,375 | 0.07B + Other + Int |
| \$635,375 | 1.07B + Other + Int. |
| | \$0 \$28,750 \$0 0.5 7.0 \$20,125 \$60,375 |

Tier 4 Generator Capital Cost Analysis

| Item | Value | Basis |
|--|-------------|------------------------------------|
| Direct Costs | | |
| Purchased Equipment Cost | | |
| Equipment cost + auxiliaries [A] | \$950,000 | А |
| Instrumentation | \$95,000 | 0.10 x A |
| Sales taxes | \$0 | Pollution Control Equipment Exempt |
| Freight | \$47,500 | 0.05 x A |
| Total Purchased Equipment Cost (PEC) [B] | \$1,092,500 | $B = 1.15 \times A$ |
| Direct Installation Costs | | |
| Not applicable | | |
| Total Direct Cost (DC) | \$1,092,500 | В |
| Indirect Costs (Installation) | | |
| Start-up | \$21.850 | 0 02 x B |
| Performance test | \$0 | Assumed not required |
| Contingencies | \$54,625 | 0.05 x B |
| Other | \$0 | As required |
| Construction Period | 0.5 | Years (n) |
| Interest Rate | 7.0 | Percent (i) |
| Interest during construction (Int.) | \$38,238 | DCxixn |
| Total Indirect Cost (IC) | \$114,713 | 0.07B + Other + Int |
| Total Capital Investment (TCI) = DC + IC | \$1,207,213 | 1.07B + Other + Int. |

Table 2b

| | enerator Annual Cost A | <u> </u> |
|-----------------------------------|------------------------|---------------------------------------|
| Item | Value | Basis |
| Direct Annual Costs (DC) | | |
| Operating Labor | | |
| Not applicable | | |
| Maintenance | | |
| | | |
| Not applicable | | |
| Indirect Annual Costs (IC) | | |
| Overhead | \$0 | 60% labor + materials |
| Administrative charges | \$12,708 | 2% TCI |
| Annual Contingency | \$28,750 | 5% of DC |
| Property taxes | \$6,354 | 1% TCI |
| Insurance | \$6,354 | 1% TCI |
| Capital Recovery | \$51,203 | CRF x TCI (30 yr life, 7.0% interest) |
| Total Indirect Costs (\$/yr) | \$105,368 | |
| Total Annualized Costs (TAC) (\$) | \$105,368 | |

| Tier 4 Generator Annual Cost Analysis | | | | |
|---------------------------------------|-----------|---------------------------------------|--|--|
| Item | Value | Basis | | |
| Direct Annual Costs (DC) | | | | |
| Operating Labor | | | | |
| Not applicable | | | | |
| Maintenance | | | | |
| Not applicable | | | | |
| | | | | |
| Indirect Annual Costs (IC) | | | | |
| Overhead | \$0 | 60% labor + materials | | |
| Administrative charges | \$24,144 | 2% TCI | | |
| Annual Contingency | \$54,625 | 5% of DC | | |
| Property taxes | \$12,072 | 1% TCI | | |
| Insurance | \$12,072 | 1% TCI | | |
| Capital Recovery | \$97,285 | CRF x TCI (30 yr life, 7.0% interest) | | |
| Total Indirect Costs (\$/yr) | \$200,198 | , | | |
| Total Annualized Costs (TAC) (\$) | \$200,198 | | | |

| Increase in Annualized Costs (Tier 2 vs Tier 4) | \$94,831 | | |
|---|-------------|-------------|--|
| Nitrogen Oxides (NOx) | 1.1 | % Reduction | |
| Particulate | 0.09 | % Reduction | |
| Volatile Organic Compounds (VOC) | 0.11 | % Reduction | |
| Total Pollutant Controlled (ton/yr) | 1.3 | Tier 4 | |
| COST EFFECTIVENESS (\$/ton) | \$74,993.24 | | |

Cost Evaluation for Natural Gas Piping Leak Detection and Repair (LDAR)

| LDAR Cost Item | 1992 [| Oolla | rs |
|--|-------------|-------|----------------|
| Annualized Capital Charges - Instrumental LDAR | | | |
| Control Equipment | | | |
| Monitoring instrument | \$1,495.00 | | |
| Compressor seal vent system | - | | |
| Rupture disk (i.e., pressure relief device) (Unit A model cost) | \$90.00 | 2 | disks |
| Rupture disk | \$360.00 | 8 | disks |
| Rupture disk assembly | \$1,256.00 | 2 | disks |
| Closed-loop sampling (assume none) | \$5,024.00 | 8 | disks |
| Subtotal Annualized Capital Charges (\$/year) | \$6,879.00 | | |
| Operating Costs | | | |
| Annual Maintenance Charges - Instrumental LDAR | | | |
| Monitoring instrument | \$4,280.00 | | |
| Compressor seal vent system | | | |
| Rupture disk (Unit A model cost) | \$8.00 | | |
| Rupture disk | \$32.00 | | |
| Rupture disk assembly (Unit A model cost) | \$385.00 | 2 | disks |
| Rupture disk assembly | \$1,540.00 | 8 | disks |
| Caps for open-ended lines (assume none) | \$0.00 | 2 | disks |
| Closed-loop sampling (assume none) | \$0.00 | 8 | disks |
| Replacement pump seals (assume none) | \$0.00 | | |
| Subtotal Annual Maintenance Charges (\$/year) | \$5,852.00 | | |
| Annual Miscellaneous Charges (taxes, insurance, administration) - Instru | umental LDA | R | |
| Monitoring instrument | \$260.00 | | |
| Compressor seal vent system | | | |
| Rupture disk assembly (Unit A model cost) | \$314.00 | 2 | disks |
| Rupture disk | \$1,256.00 | 8 | disks |
| Caps for open-ended lines (assume none) | \$0.00 | | |
| Closed-loop sampling (assume none) | \$0.00 | | |
| Replacement pump seals (assume none) | \$0.00 | | |
| Subtotal Annual Miscellaneous Charges (\$/year) | \$1,516.00 | | |
| Labor Charges - Instrumental LDAR | | | |
| LDAR monitoring | \$12,940 | | |
| Subsequent repair | \$7,369 | | |
| Administrative and support | \$8,124 | | |
| Subtotal Labor Charges (\$/year) | \$28,433 | | |
| Grand Total (\$/year) - Jan. 1992 dollars - Instrumental LDAR | \$42,680 | | |
| Total Annual Cost | 2020 [|)olla | s ^b |
| Grand Total Cost of Instrumental LDAR (\$/year) | \$79,726 | | |

⁽a) Cost information is from (Table 6-12) of Hazardous Air Pollutant Emissions from Process Units in the Synthetic Organic Chemical Manufacturing Industry – Background Information for Proposed Standards. Volume 1C: Model Emission Sources (EPA-453/D-92-016c). Nov. 1992. U.S. EPA. Unit A model facility costs utilized in the calculations. Costs are presented in 1992 dollars.

https://inflationdata.com/Inflation/Inflation_Calculators/Cumulative_Inflation_Calculator.aspx

⁽b) Annual costs converted from 1992 to January 2020 values using the consumer price index. Web site used to compute 2020 dollars is located at:

Cost Evaluation for Natural Gas Piping Leak Detection and Repair (LDAR)

| Cost Effectiveness Calculations | |
|--|-----------|
| Uncontrolled emission rate, CO₂e (ton/year) | 976.6 |
| Uncontrolled emission rate, mass greenhouse gas (GHG) (ton/year) [CO ₂ e/ GWP CH ₄] | 39.1 |
| Uncontrolled emission rate, VOC (ton/year) | 2.8 |
| Total Uncontrolled emission rate, VOC + mass greenhouse gas (GHG) (ton/year) ^a | 41.9 |
| Average assumed control efficiency of instrumental LDAR (range is 30-97%) | 56% |
| Mass GHG emission reduction from instrumental LDAR (ton/year) | 23.45 |
| Density of natural gas (pounds/standard cubic foot) ^b | 0.0420 |
| Volume GHG emission reduction from instrumental LDAR (standard cubic feet/year) | 1,116,037 |
| Value of natural gas (\$/1000 standard cubic feet - 2019) ^c | 2.99 |
| Instrumental LDAR Cost Effectiveness | |
| Natural gas recovery savings from instrumental LDAR (\$/year) | \$3,337 |
| Net annual cost of instrumental LDAR (grand total cost - savings) (\$/year) | \$76,389 |
| Cost effectiveness of instrumentation LDAR, mass basis (\$/ton GHG) | \$3,258 |
| Cost effectiveness of instrumental LDAR, carbon dioxide equivalent (CO ₂ e) basis (\$/ton CO ₂ e) ^d | \$130 |

- (a) Total emissions evaluated does not include fuel oil VOC. The overall natural gas emissions (41.9 tpy) is greater than fuel oil emissions (7.58 tpy).
- (b) Density of natural gas obtained from Compilation of Air Pollutant Emission Factors, Volume I: Stationary Point and Area Sources (AP-42). Appendix A. January 1995. U.S. EPA.
- (c) 2019 value of natural gas for electric power production obtained from the United States Energy Information Administration: https://www.eia.gov/dnav/ng/ng_pri_sum_dcu_nus_a.htm. Accessed on 15 January 2021
- (d) Global warming potential (GWP) for methane used to convert the cost effectiveness from a mass basis to a CO₂e basis by dividing the mass based cost effectiveness by the GWP of methane. The GWP of methane is 25 according to 40 Code of Federal Regulations Part 98, Subpart A, Table A-1.

From Post Application BACT evaluation on "leak-proof" Piping Components Cost Analysis

Table 1
VOC Capital Cost Analysis - Certified Low Leaking Valve

| Item | Value | Basis |
|--|-----------|------------------------------------|
| Direct Costs | | |
| Purchased Equipment Cost | | |
| Equipment cost + auxiliaries [A] | \$100,000 | A |
| Instrumentation | \$10,000 | 0.10 x (A) |
| Sales taxes | \$0 | Pollution Control Equipment Exempt |
| Freight | \$5,000 | 0.05 x (A) |
| Total Purchased Equipment Cost (PEC) [B] | \$115,000 | $B = 1.15 \times (A)$ |
| Direct Installation Costs | | |
| Total Direct Installation Cost | \$34,500 | 0.30 x B |
| Inspection access infrastructure | \$475,037 | |
| Total Direct Cost (DC) | \$624,537 | |
| Indirect Costs (Installation) | | |
| Engineering | \$11.500 | 0.10 x B |
| Construction and field expenses | \$5.750 | 0.10 x B |
| Contractor fees | \$11.500 | 0.03 X B |
| Start-up | \$2,300 | 0.02 x B |
| Contingencies | \$5.750 | 0.02 x B |
| Other | \$0 | As required |
| Construction Period | 0 | Years (n) |
| Interest Rate | 7.0 | Percent (i) |
| Interest during construction (Int.) | \$0 | DC x i x n |
| Total Indirect Cost (IC) | \$36,800 | 0.32B + Other |
| Total Capital Investment (TCI) = DC + IC | \$661,337 | 1.32B + SP + Bldg + DC |

Table 2 VOC Annual Cost Analysis - Certified Low Leaking Valve

| Item | Value | Basis |
|---------------------------------------|-----------|---|
| Direct Annual Costs (DC) | | |
| Operating Labor | | |
| Inspection labor req. | \$57,350 | 5 min to inspect a valve monthly @ \$50 /hr |
| Supervisor | \$8,603 | 15% Operating labor |
| Cost for inspection infrastructure | \$2,500 | lifts and temporary scaffolding |
| Total Cost \$/yr | \$68,453 | |
| Maintenance | | |
| Valve replacement labor | \$0 | All valves replaced over 5 years, 10 hr/replacement |
| Material | \$0 | \$2500 replacement cost/valve |
| Cost for replacement infrastructure | \$0 | lifts and temporary scaffolding |
| Total Cost \$/yr | \$0 | |
| Indirect Annual Costs (IC | | |
| Capital Recovery | \$161,294 | CRF x TCI 5 yr life, 7.0% interest |
| Total Indirect Costs \$/yr | \$161,294 | |
| Total Annualized Costs (TAC) (\$ | \$229,746 | |
| Total Pollutant Controlled ton/yr VOC | 7.7 | 80% reduction |
| COST EFFECTIVENESS \$/ton | \$29,826 | \$/ton VOC |

95.58 inspection hours/month
\$50 labor cost/hr
1,147 total valve count (NG and Oil)
229.40 valve/year replaced with 5 year life
5 year life
2,500 \$\text{\$\chi_{\text{N}}\$} valve total for replacements not needed on baseline valves

80% reduction 10 hr/replace a valve

| | Capital Recovery Factor | |
|----------|-------------------------|-------------|
| Interest | 7.0% | |
| Years | 5 | |
| | | |
| CRF = | i * (1+i)^n | |
| | 1+i)^n - 1 | |
| CRF = | , | 0.243890694 |

100 Low leak valve ppm guarantee 500 Standard valve ppm guarantee

From Post Application BACT evaluation on "leak-proof" Piping Components Cost Analysis

Table 1

Methane Capital Cost Analysis - Certified Low Leaking Valve

| Item | Value | Basis |
|--|-----------|------------------------------------|
| Direct Costs | | |
| Purchased Equipment Cost | | |
| Equipment cost + auxiliaries [A] | \$100,000 | A |
| Instrumentation | \$10,000 | 0.10 x (A) |
| Sales taxes | \$0 | Pollution Control Equipment Exempt |
| Freight | \$5,000 | 0.05 x (A) |
| Total Purchased Equipment Cost (PEC) [B] | \$115,000 | $B = 1.15 \times (A)$ |
| | | |
| Direct Installation Costs | | |
| Total Direct Installation Cost | \$34,500 | 0.30 x B |
| Inspection access infrastructure | \$475,037 | |
| Total Direct Cost (DC) | \$624,537 | |
| Indirect Costs (Installation) | | |
| Engineering | \$11,500 | 0.10 x B |
| Construction and field expenses | \$5.750 | 0.05 x B |
| Contractor fees | \$11,500 | 0.10 x B |
| Start-up | \$2,300 | 0.02 x B |
| Contingencies | \$5,750 | 0.05 x B |
| Other | \$0 | As required |
| Construction Period | 0 | Years (n) |
| Interest Rate | 7.0 | Percent (i) |
| Interest during construction (Int.) | \$0 | DC x i x n |
| Total Indirect Cost (IC) | \$36,800 | 0.32B + Other |
| Total Capital Investment (TCI) = DC + IC | \$661.337 | 1.32B + SP + Bldg + DC |

Table 2
Methane Annual Cost Analysis - Certified Low Leaking Valve

| Methane Annual Cost Analysis - Certified Low Leaking Valve | | | |
|--|---|--|--|
| Item | Value | Basis | |
| Direct Annual Costs (DC) | | | |
| Operating Labor | | | |
| Inspection labor req. | \$42,800 | 5 min to inspect a valve monthly @ \$50 /hr | |
| Supervisor | \$6,420 | 15% Operating labor | |
| Cost for inspection infrastructure | \$2,500 | lifts and temporary scaffolding | |
| Total Cost (\$/yr) | \$51,720 | | |
| Maintenance | | | |
| Valve replacement labor | \$0 A | Il valves replaced over 5 years, 10 hr/replacement | |
| Material | \$0 | \$2500 replacement cost/valve | |
| Cost for replacement infrastructure | \$0 | lifts and temporary scaffolding | |
| Total Cost (\$/yr) | \$0 | | |
| Indirect Annual Costs (IC | | | |
| Capital Recovery | \$161,294 | CRF x TCI (5 yr life, 7.0% interest | |
| Total Indirect Costs (\$/yr) | \$161,294 | | |
| Total Annualized Costs (TAC) (\$) | \$213,014 | | |
| Total Pollutant Controlled (ton/yr) Methane | 36.3 | 80% reduction | |
| COST EFFECTIVENESS \$/ton | T EFFECTIVENESS \$/ton \$5,874 \$/ton Methane | | |
| \$234.95 \$/ton CO2e | | | |

71.33 inspection hours/month \$50 labor cost/hr 856 total valve count (NG) 171.20 valve/year replaced with 5 year life 5 year life 2,500 \$/valve total for replacements not ne

80% reduction 10 hr/replace a valve

| Ca | apital Recovery Factor |
|----------|------------------------|
| Interest | 7.0% |
| Years | 5 |
| CRF = | i * (1+i)^n |
| 0 | 1+i)^n - 1 |
| CRF = | 0.243890694 |

100 Low leak valve ppm guarantee 500 Standard valve ppm guarantee





State of Wisconsin

DEPARTMENT OF NATURAL RESOURCES

Information Request

FID/Docket Number: 816127840 Date of Request: February 1, 2019

Requested From: WDNR Response Due: February 14, 2019

Contact Requesting Information: Megan Corrado, Air Management Engineer

If you feel your responses are trade secret or privileged, please indicate this on your response.

| Request No. | |
|----------------|--|
| 007 | Please propose allowable emission rates (lb/hr) of sulfur oxides for the |

Please propose allowable emission rates (lb/hr) of sulfur oxides for the relevant emissions units so that the department may determine whether or not the proposed project causes or exacerbates an exceedance of the Ambient Air Quality Standards [s. NR 404.04(2), Wis. Adm. Code] or increment [s. NR 404.05, Wis. Adm. Code].

Response:

007

The allowable emission rates of sulfur oxides (lb/hr and tpy) emitted for the relevant emissions units are listed in Table 1 below.

Table 1: SO₂ Emission Rates

| | | SO ₂ | |
|-----------|--------------------|-----------------|-------|
| Source ID | Source Description | (lb/hr) | (tpy) |
| S01_DBNG | Turbine NG DB | 6.4 | 28.2 |
| S01_100NG | Turbine NG 100 | 5.1 | 28.2 |
| S01_75NG | Turbine NG 75 | 4.0 | 28.2 |
| S01_LWNG | Turbine NG 35 | 2.4 | 28.2 |
| S01_SSNG | Turbine NG Starts | 5.1 | 28.2 |
| S01_DBFO | Turbine NG DB/FO | 6.1 | 28.2 |
| S01_100FO | Turbine FO 100 | 4.6 | 28.2 |
| S01_75FO | Turbine FO 75 | 3.6 | 28.2 |
| S01_LWFO | Turbine FO 46 | 2.8 | 28.2 |
| S01_SSFO | Turbine FO Starts | 4.6 | 28.2 |
| S02_AUXB | Auxiliary Boiler | 0.06 | 0.3 |
| S04_DPH1 | Natural Gas Heater | 5.9E-03 | 0.03 |
| S05_DPT2 | Natural Gas Heater | 5.9E-03 | 0.03 |

| Response by: | Minda Nelson, P.E. | List Sources of Information: |
|--------------|----------------------------------|------------------------------|
| Title: | Associate Environmental Engineer | |
| Department: | Burns & McDonnell | |
| Telephone: | (816) 822-4208 | |





September 1, 2020

Megan Corrado Air Management Engineer-Adv State of Wisconsin Department of Natural Resources 101 S. Webster Street Madison, WI 53707-7921

Re: Nemadji Trail Energy Center

Primary Site: FID No. 816127840 / Draft Permit 18-MMC-168 Alternate Site: FID No. 816121350 / Draft Permit 18-MMC-169

Air Pollution Control Construction Permit Request for Additional Information

Dear Ms. Corrado:

On behalf of South Shore Energy and Dairyland Power Cooperative ("Applicants," collectively), Burns & McDonnell Engineering Company hereby submits its response to the request for additional information for permits 18-MMC-168 and 18-MMC-169.

This response addresses WDNR's request for information confirming that the circuit breakers selected are consistent with the best that is presently available and are 'state of the art' and addresses why a 0.1% leakage rate is not achievable.

Circuit Breaker Performance Details

The below information presents data that supports the installation of three 345-kilovolt (kV) and two 19 kV low-side generator enclosed pressure SF₆ circuit breakers with a guaranteed loss rate of 0.5% by weight or less per year.

1) Circuit Breaker Industry Requirements

The current industry standard requirements of Institute of Electrical and Electronics Engineers (IEEE) is 0.5%. The requirements are listed in IEEE C37.122.3 "IEEE Guide for Sulphur Hexafluoride (SF₆) Gas Handling for High-Voltage Equipment."

IEEE C37.122.3-2011, Part 4.3.2

4.3.2 Closed-pressure systems

In closed-pressure systems, a volume is replenished only periodically by manual connection to an external gas source. High-voltage (above 72.5 kV) SF_6 single-pressure circuit breakers are examples of closed-pressure systems.

It is recommended that:

- The leakage rate be kept lower than 0.5% per annum (p.a.) per gas compartment.
- When SF_6 conditions are checked, that gas be recaptured from analysis equipment.
- Appropriate record-keeping procedures are used.



A leakage rate of 0.5% listed in the permit is in compliance with the IEEE industry standards.

2) Manufacturer Data

The contacted manufacturers indicated their lab tests demonstrated leakage rates below 0.1% per year. The manufacturers will guarantee this maximum leakage rate only during the warranty period of between 2 to 4 years, depending on the manufacturer.

This demonstrates that the best breakers presently available and 'state-of-the-art' breakers will be installed for the project and the installed breakers will meet permit conditions I.C.1.a.(1)(a) and I.C.1.c.(1)(b).

I.C.1.a.(1)(a) Circuit breakers containing SF_6 shall be pressurized and have a manufacturer guaranteed loss rate not to exceed 0.5%, by weight, per year: and

I.C.1.c.(1)(b) documentation from the manufacturer demonstrating that the circuit breakers installed are enclosed pressure SF_6 circuit breakers with a guaranteed loss rate of 0.5 percent by weight or less by year,

3) Leak Rates

EPA performed research on SF₆ leak rates from high voltage circuit breakers (See Attachment 1). The study evaluated a fleet of circuit breakers installed between 1998 and 2002 and found the average leakage range was between 0.2% to 2.5% per year over the study period.

The lower bound is overly optimistic relative to leakage over the life of fleet in that it did not include all leakage actually experienced in the fleet (only leakage that triggered the safety alarm) and further the study only evaluated breakers over a period of 2 to 7 years from initial installation versus a typical 30 year life. Even with these extremely optimistic characteristics, the average fleet leakage was found to be higher than the 0.1% per year levels.

It should also be noted that the upper bound (2.5%) is larger than the IEEC requirements (0.5%). The lower bound (0.2%) is higher than the manufacturer guarantees (0.1%), but lower than the IEEC requirement (0.5%).

While NTEC acknowledges that this study is slightly dated and it is possible that the circuit breakers for the project could perform better than those included in the study, it can also be concluded from the study that breakers leak more as they age. In the study, the 6 year old breakers exhibited more leakage than the younger breakers.

Based on this information, the 0.1% lifetime loss rate is not practical.



4) Measurements

Density analyzers will be used to determine compliance with condition I.C.1.c.(1)(i). Specifications for a density monitor is shown in Attachment 2, which shows an overall density measurement accuracy of 0.6% of its range.

This accuracy is not sufficient to measure the SF_6 gas loss of a single year with a permit limit at the 0.5% leakage loss rate and it would take more than 6 years of leakage for the accuracy of the instruments to measure the loss at a 0.1% level. As such, the instruments would not be suitable to provide an early indication of leaks to allow for preemptive maintenance to prevent exceedance of the permit limits if established at the 0.1% level.

Based on this information a 0.1% leakage loss rate limit is not practical.

5) Lifetime Performance

Manufacturer guarantees generally expire after 2 to 4 years of issuance. Manufacturers expect leakage rates will increase over the lifetime (30+ years) of the circuit breakers as components degrade, necessitating periodic overhauls to attempt to restore leakage levels. However, even with the overhauls, it is uncertain whether the leakage rates could be returned to the 0.1% per year level.

A leakage rate permit condition of 0.1% is not economically feasible as the circuit breakers will need to be overhauled and/or replaced more frequently to meet the permit condition.

Additionally, over the life of the equipment the leakage rate will not consistently meet the time-limited manufacturer guaranteed loss rate of 0.1% by weight per year value within the parameters of the permit condition presented in I.C.1.c.(1)(i).

I.C.1.c.(1)(i) an inventory of the initial SF_6 quantity and SF_6 replaced in the breakers each calendar year. The SF_6 replaced is assumed equal to the SF_6 that has lost to demonstrate compliance with I.C.1.a.(1)(a).

6) Economic

The economic impacts of installing circuit breakers with different loss rates was evaluated. For both the switchyard breakers (345 kV) and generator breakers (19 kV), a 0.1% loss rate is not maintainable over the 30-year life of the breakers. The cost analysis assumes that to meet a 0.1% loss rate, each breaker will need to be replaced every five years and for the 0.5% loss rate case the breakers will be replaced at the end of the 30-year life of the breakers.



Switchyard Breakers Economic Analysis

The initial capital costs associated with the switchyard breakers for both a 0.5% loss rate and a 0.1% loss rate is approximately \$250,000. This cost is also the cost to replace the breakers every five years to achieve a 0.1% loss rate. The difference in SF₆ losses from a 0.5% and 0.1% loss rate is 0.04 tons SF₆ over 30 years or 0.0014 tons SF₆ per year. On an annual basis, the 0.5% rate would cost approximately \$4,852,000 per ton SF₆ over a 30-year life and the 0.1% rate would cost approximately \$145,560,000 per ton SF₆ over a 30-year life.

Generator Breakers Economic Analysis

The initial capital costs associated with the generator breakers for both a 0.5% loss rate and a 0.1% loss rate is approximately \$700,000. This cost is also the cost to replace the breakers every five years to achieve a 0.1% loss rate. The difference in SF₆ losses from a 0.5% and 0.1% loss rate is 0.0014 tons SF₆ over 30 years or 0.000046 tons SF₆ per year. On an annual basis, the 0.5% rate would cost approximately \$405,797,000 per ton SF₆ over a 30-year life and the 0.1% rate would cost approximately \$12,173,913,000 per ton SF₆ over a 30-year life.

The details of the cost analysis is shown in Attachment 3. A 0.1% leakage rate results in costs that are economically infeasible due to the cost to replace the circuit breakers. BACT is a 0.5% leakage rate for the circuit breakers.

Conclusion

Based on the above information the conclusions are as follows:

- The circuit breakers will meet industry requirements (0.5% loss rate)
- The best circuit breakers available and 'State-of-the-art' breakers will be installed (Time-limited manufacturer guaranteed loss rate of 0.1% by weight per year.)
- Based on the EPA study the 0.1% lifetime loss rate is not practical.
- Due to density measurement accuracy limitations a 0.1% loss rate limit is not practical.
- Over the life of the equipment the leakage rate will not consistently meet the time-limited manufacturer guaranteed loss rate of 0.1% by weight per year value within the parameters of the permit condition presented in I.C.1.c.(1)(i).
- A leakage rate of 0.1% is not economically feasible due to the cost to continuously replace the circuit breakers over the plant lifetime.

Please note, a 0.1% leakage rate is unprecedented in WDNR permits and would drastically lower the BACT rate to a level that, as described in this response, is not demonstrated over the long term.

In conclusion, the circuit breakers selected are consistent with the best that is presently available and are 'state of the art' and a 0.1% leakage rate is not achievable.



Please contact me at (816) 822-4208 or email me at mnelson@burnsmcd.com if you have any questions.

Sincerely,

Minda Nelson, P.E.

Associate Environmental Engineer

Minda Nelson

cc: Tim Barton, Burns & McDonnell Robynn Andracsek, Burns & McDonnell Daniel McCourtney, Minnesota Power Melissa Weglarz, Minnesota Power Erik Hoven, Dairyland Power Cooperative Brad Foss, Dairyland Power Cooperative Josh Skelton, South Shore Energy, LLC



1

SF₆ Leak Rates from High Voltage Circuit Breakers - U.S. EPA Investigates Potential Greenhouse Gas Emissions Source

J. Blackman, *Program Manager, U.S. Environmental Protection Agency*, M. Averyt, *ICF Consulting*, and Z. Taylor, *ICF Consulting*

Abstract—This paper highlights a recent collaborative study between the EPA's SF_6 Emission Reduction Partnership for Electric Power Systems and the electric power industry to investigate SF_6 leak rates from high voltage circuit breakers manufactured and installed between 1998 and 2002. Information from over 2,300 circuit breakers were analyzed to quantify the frequency of leaks and to estimate the weighted average annual leak rate for this population of circuit breakers. The methodology, data, and results of this study are presented.

Index Terms-- SF_6 , annual leak rate, greenhouse gas emissions, circuit breaker.

I. INTRODUCTION

C ULFUR hexafluoride (SF₆) is a gaseous dielectric used in high voltage electrical equipment as an insulator and/or arc quenching medium. SF₆ is the most potent greenhouse gas with a global warming potential that is 23,900 times greater than that of carbon dioxide (CO_2) ; it is also very persistent in the atmosphere with a lifetime of 3,200 years [1]. Potential sources of SF₆ emissions occur from: 1) losses through poor gas handling practices during equipment installation, maintenance and decommissioning; and 2) leakage from SF₆containing equipment. The operation and maintenance of SF₆ gas carts, which are used to remove, store, clean, and re-fill SF₆ gas to high-voltage equipment, are considered a major source of handling-related losses. Equipment leakage, on the other hand, is the result of the deterioration of SF₆-containing equipment fittings and materials with time and use through chemical, hardening, and corrosion effects.

Equipment leakage is one of the two potential sources of SF_6 emissions. Leak detection surveys have noted that approximately 10 percent of circuit breaker populations may leak [2, 3], and of these leaking populations, 15 percent of the breaker leaks were minor, with repairs that could be conducted immediately, while the remaining 85 percent were considered significant and had to be referred to operations for scheduled repairs [3]. In terms of where these leaks typically

occur, studies have noted that the majority occurs at gas mechanisms (73 percent), 21 percent from worn or broken bushings, and 6 percent from gas tanks [4]. Typically, such losses can only be mitigated through equipment repair or replacement. As electrical equipment ages and reaches the end of its operational service life, replacement rather than equipment repair may provide the more attractive SF₆ mitigation strategy. Many equipment manufacturers now guarantee minimal to zero leak rates for new equipment. Additionally, industry standards recommend that new equipment be built to low leakage limits [5]. Since there is little published information on new equipment leak rates, in a study initiated in 2004, EPA sought to obtain an improved understanding of average leak rates associated with newly manufactured equipment (i.e., installed between 1998 and 2002).

This paper provides a brief review of the data and results of an equipment study funded by EPA [6]. The remainder of this paper is organized into four sections:

- <u>Section II</u> describes the methodology of the field study, including study scope and data parameters.
- <u>Section III</u> provides a summary of the data compiled from utilities participating in the study.
- Section IV presents the results of the equipment leak rate analyses.
- <u>Section V</u> summarizes the conclusions drawn from the study.

II. FIELD STUDY METHODOLOGY

Section II defines the scope of the study and describes the data collection and compilation process.

A. Study Scope and Data Parameters

The scope of the study was limited to data from three Partner utilities. Information was requested on high voltage circuit breakers manufactured and installed between 1998 and 2002. SF₆ equipment can take the form of sealed or closed pressure systems. Only closed pressure system breakers were included in the study; circuit breakers that are defined as "sealed-for-life" were not addressed by this study. The period in which equipment leakage was assessed was defined as from 1998 through 2005. For purposes of this study, a circuit breaker was classified as leaking if it had documented "topups" of SF₆, which occur after a density alarm is sounded, indicating that 10 percent of the circuit breaker gas volume

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has been emitted.

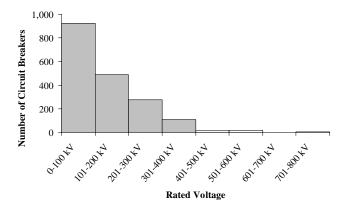
B. Data Collection and Compilation

The data collection was undertaken through a survey form via telephone and email correspondence. The form requested information on the utilities entire inventory of SF₆ breakers, defined by the study scope, including makes, models and installed quantities, number of breaker operations, and for leaking breakers, the quantity of SF₆ gas used during the "topup" operation.

III. DATA SUMMARY

To ensure confidentiality, the names of the utilities involved in the study are not listed. The data provided covered equipment ranging from 33kV to 800kV. In total, information was provided on 2,329 circuit breakers. Figure I illustrates the proportion of circuit breakers size by standard rated voltage. As shown, the majority of the equipment included in the study fell into the range of less than 100 kV. Only 148 breakers were greater 300 kV.

FIGURE I NUMBER OF CIRCUIT BREAKER BY RATED **VOLTAGE**



Of the 2,329 circuit breakers, 170 (7.3 percent) were reported as leaking.

Table I and Figure II present a summary of the number of circuit breakers, leaking and non-leaking, included in the study.

TABLE I SUMMARY OF LEAKING/NON-LEAKING CIRCUIT **BREAKERS**

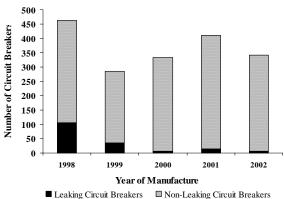
| | | | | | Leaking |
|-------------|-----------------|-----------------|--------------------|----------|---------|
| | | | | | as % of |
| | | Non- | | Leaking | Overall |
| Year of | Leaking | Leaking | Total | CB/Total | Total |
| Manufacture | CB ^a | CB ^b | CB | CB | Leaking |
| 1998 | 106 | 357 | 463 | 23% | 62% |
| 1999 | 35 | 250 | 285 | 12% | 21% |
| 2000 | 7 | 326 | 333 | 2% | 4% |
| 2001 | 15 | 396 | 411 | 4% | 9% |
| 2002 | 7 | 334 | 341 | 2% | 4% |
| Total | 170 | 1,663 | 1,833 ^c | | 100% |

^aCB – Circuit Breakers

^bNo alarm triggered

^cNumber of circuit breakers does not total 2,329 because year of CB manufacture data are not available for all non-leaking circuit breakers.

FIGURE II NUMBER OF CIRCUIT BREAKERS BY YEAR OF **MANUFACTURE**



For the circuit breakers in the data set that were manufactured in 1998, 23 percent were identified as leaking. These circuit breakers account for approximately 62 percent of the total number of leaking breakers. This result is intuitive considering the natural deterioration of seals and equipment over time.

Table II presents emissions data related to the leaking circuit breakers for each year of manufacture. Total emissions of SF_6 are indicated for the leaking circuit breakers manufactured in each year. Total emissions as a percent of total nameplate capacity associated with the leaking circuit breakers are also presented.

 $TABLE\ II \\ SF_6\ EMISSIONS\ FROM\ LEAKING\ CIRCUIT\ BREAKERS$

| Year | Total | No. | |
|----------|-------------------------|---------|---------------------------------|
| Manu- | Emissions | Leaking | Total Emissions as % of |
| factured | (lbs. SF ₆) | CBs | Nameplate Capacity ^a |
| 1998 | 2,859 | 106 | 6% |
| 1999 | 302 | 35 | 0.96% |
| 2000 | 24 | 7 | 0.07% |
| 2001 | 140 | 15 | 0.29% |
| 2002 | 81 | 7 | 0.12% |
| Total | 3,407 | 170 | |

^aNameplate capacity of leaking circuit breakers only.

Consistent with the observations in Table I, circuit breakers manufactured in 1998 were also the largest contributors to SF_6 emissions reported in the study. Their emissions as a function of total SF_6 -contained in the equipment (nameplate capacity), is approximately 6 percent, significantly larger than the values reported for leaking breakers manufactured in 1999 through 2002.

IV. LEAK RATE RESULTS AND ANALYSIS

Section IV presents the results of an analysis to define circuit breaker leak rates (as a percent of nameplate capacity) that are representative of the entire reported dataset. These estimates are referred to as the lower and upper bound leak rates, respectively, and are intended to illustrate potential industry trends. The key variables used to perform this analysis are 1) circuit breaker nameplate capacity, 2) total circuit breaker SF_6 leakage (lbs), and 3) the number of years that circuit breaker has been in operation.

Specifically, three leak rates (as a percent of nameplate capacity) were estimated. The first analysis generated a lower bound, or best case scenario, of an average circuit breaker leak rate estimate. The second two analyses both generated upper bound, or worst case scenario circuit breaker leak rate estimates, that are based on different methodologies and assumptions.

A. Lower Bound Weighted-Average Leak Rate

For the lower bound estimate, the weighted-average circuit breaker leak rate is approximately 0.2 percent per year. The lower bound leak rate was calculated by applying the raw reported data to Equation (1) and assuming that 1) through 2005, no additional "top-ups" have occurred after the last reported "top-up" (e.g., if the last reported "top-up was in 2003, it was assumed that no additional leakage occurred through 2005), and 2) for circuit breakers that have not reported any "top-ups" (i.e., they have not reached the 10 percent leakage threshold, and thus have not triggered a notification alarm), their emissions are zero.

This estimate is defined as the weighted average of circuit breaker annual leak rates as a percentage of SF_6 nameplate capacity, across all circuit breakers both leaking and non-leaking. The calculation for the weighted average annual leak rate per nameplate capacity is provided in Equation (1):

$$LC = \frac{\sum \frac{Q_{SF6_i}}{Y_i}}{\sum c_i} \quad (1)$$

Where:

LC = Weighted average annual leak rate per nameplate capacity (percent/year)

Q_{SF6i} = Total mass (i.e., lbs) of SF₆ for all top-up operations since installation for circuit breaker, i

 Y_i = Number of years the circuit breaker, i, has been in use C_i = Individual nameplate capacity for circuit breaker i (lbs SF_6)

B. Upper Bound Weighted-Average Leak Rate – Method 1

For the lower bound estimate, it was assumed that equipment that had not reported "top-ups" were not leaking; however, since "top-ups" are defined by density alarm triggers, it is possible that many more breakers had leaked, but had not reached the 10 percent density alarm leak threshold. To account for potential leakage under the density alarm threshold, an upper bound leak rate estimate was developed based on the following assumptions:

- (1) All circuit breakers that have not indicated an alarm trigger leaked slightly less than 10 percent of their capacity between their installation date and 2005. Thus, the 2,159 circuit breakers (93 percent) in the dataset which have no documented "top-ups" (and are assumed for the lower bound to have a leak rate of zero percent) are scaled to assume a leakage rate of 10 percent (this is an asymptotic upper bound).
- (2) The second adjustment assumed that for previously identified leaking breakers (those that have reported "top-ups"), an additional 10 percent of capacity (i.e., another "top-up") occurred between the last documented service call and 2005. For example, a circuit breaker with an annual leak rate of 5 percent whose last reported service call occurred one year before the company data submittal is assumed to have 10 percent additional leakage during that last year.

Based on these assumptions and the application of equation (1) the weighted-average upper bound estimate for circuit breaker leak rate is estimated to be 2.5 percent. This result represents a *worst case* upper bound leak rate.

C. Upper Bound Weighted-Average Leak Rate –Method 2

Since the second assumption listed in the prior section, may overestimate emissions from documented leaking circuit breakers, an additional upper bound estimate was calculated by redefining how additional "top-ups" for these circuit breakers are treated. That is, it was assumed that circuit breakers which are currently leaking will continue to leak at their current rate. That is, if a circuit breaker is calculated to have an existing leak rate of 2 percent per year per nameplate capacity between its installation and last reported top-up date, then it was assumed that this rate continues through the end of the study period. This alternative approach maintains the original assumptions for non-leaking circuit breakers by assuming a leakage of just under 10 percent has occurred since circuit breaker installation.

Based on these assumptions and the application of equation (1), the alternate weighted-average upper bound leak rate estimate is 2.4 percent.

V. CONCLUSION

For the study dataset, the lower and upper bound weighted-average leak rate estimates of 0.2 and 2.5 percent, respectively, represent the best and worst case scenarios for circuit breaker leakage. To put this into some context, NEMA's SF₆ management guidelines state, "...Over a 50 year service life the emission of SF₆ gas due to its use in electrical equipment will not exceed... 5% equipment leakage..." (i.e., 0.1 percent/year) [7]. Also, the IEC standard for new equipment leakage is 0.5 percent per year [5]. While the upper bound is significantly larger than both the NEMA and IEC guidelines, the lower bound leak rate estimate is comparable, and sits between the NEMA and IEC recommendations.

VI. ACKNOWLEDGMENT

The authors would like to acknowledge representatives from Eastern Research Group, Inc (ERG), the Electric Power Research Institute (EPRI), and the electric utilities, and original equipment manufacturers that assisted EPA in undertaking this study.

VII. REFERENCES

[1] IPCC, Climate Change 1995: The Science of Climate Change. Intergovernmental Panel on Climate Change; J.T. Houghton, L.G. Meira Filho, B.A. Callander, N. Harris, A. Kattenberg, and K. Maskell, eds; Cambridge University Press. Cambridge, U.K. [2] McCreary, J.D., "AEP: A Case Study," presented at the International Conference on SF₆ and the Environment: Emission Reduction Technologies, November 2-3, 2000, San Diego, CA. [Online]. Available: http://www.epa.gov/electricpower-sf6/pdf/mccrearyppt.pdf [3] D. Keith, J. Fisher, and T. McRae, "Experience with Infrared Leak Detection on FPL Switchgear," presented at the International Conference on SF₆ and the Environment: Emission Reduction Technologies, November 2-3, 2000, San Diego, CA. [Online]. Available: http://www.epa.gov/electricpower-sf6/pdf/fischerp.pdf [4] Salinas, A. and Flores, M., "Southern California Edison: SF₆ Gas Management Program Update," presented at the International Conference on SF₆ and the Environment: Emission Reduction Technologies, December 1-3, 2004, Scottsdale, AZ. [Online]. Available: http://www.epa.gov/electricpower-sf6/pdf/dec04/Salinas_ok2use.pdf [5] IEC, International Electrotechnical Commission Standard 62271-1, [6] EPA, "High Voltage Circuit Breakers Field Study," prepared by EPRI

[6] EPA, "High Voltage Circuit Breakers Field Study," prepared by EPRI and the Eastern Research Group, July, 2005.

[7] NEMA, "Management of SF₆ Gas for Use in Electrical Power Equipment," Ad-Hoc Task Group on SF₆, Switchgear Section (8-SG), February, 1998.

VIII. BIOGRAPHY

Jerome Blackman is Program Manager for EPA's SF_6 Emission Reduction Partnership for Electric Power Systems. Mr. Blackman joined EPA in 1995 and has work in several commercial/industrial non-regulatory voluntary pollution prevention programs within the Office of Atmospheric Programs.

Mollie Averyt is an Associate at ICF Consulting. Ms. Averyt specializes in environmental policy analyses related to climate change and ozone depletion issues; and provides support for EPA's SF_6 Emission Reduction Partnership.

Zephyr Taylor is a Research Assistant at ICF Consulting. Mr. Taylor specializes in quantitative modeling and analysis specifically related to climate change issues. Mr. Taylor provides technical support for EPA's SF₆ Emission Reduction Partnership.



Transmitter

For density, temperature, pressureand humidity of SF₆ gas Model GDHT-20, with MODBUS® output

WIKA data sheet SP 60.14



for further approvals see page 3

Applications

- Permanent monitoring of the relevant gas condition parameters in closed tanks
- For internal and external SF₆ gas-insulated equipment

Special features

- High-accuracy sensor technology
- MODBUS® output protocol via RS-485 interface
- Ingress protection IP65
- Very good long-term stability and EMC characteristics
- Compact dimensions



Transmitter, model GDHT-20

Description

The model GDHT-20 transmitter is a multi-sensor system with digital output for the measurands of pressure, temperature and humidity. Based on these measured values, the condition-related data can be determined.

Permanent monitoring

In order to prevent system failures in switchgear and, with that, network outages, the permanent monitoring of the gas density and moisture content is essential.

The GDHT-20 transmitter calculates the current gas density from the pressure and temperature using a complex virial equation in the transmitter's powerful microprocessor. Pressure changes resulting from thermal effects will be compensated by this and will not affect the output value.

In addition, the GDHT-20 transmitter delivers humidity or dew point information, which enables monitoring within the terms of the Cigré directives and IEC standards.

MODBUS® fieldbus

The RS-485 interface communicates using the MODBUS® RTU protocol. The instrument's output parameters and their units can be configured and read according to requirements. The GDHT-20 transmitter can be configured later by the customer for each defined SF₆ gas mixture with N₂ or CF₄.

Signal stability

Due to its high long-term stability, the transmitter is maintenance-free and requires no recalibration.

Due to the hermetically sealed weld seam and a measuring cell design without sealing elements, the permanent sealing of the measuring cell is ensured.

The EMC characteristics fulfil the IEC 61000-4-2 through to IEC 61000-4-6 standards and guarantee an interference-free data output.



Specifications

Measuring ranges

Dew point at ambient

pressure: -50 ... +30 °C

Density: 0 ... 60 g/litre (8.87 bar abs. SF₆ gas at

20 °C)

Temperature: -40 ... +80 °C

Pressure at 20 °C: 0 ... 8,87 bar abs. SF₆ gas

Pressure: 0 ...16 bar abs.

Burst pressure: 52 bar abs.

Overload safety: up to 30 bar abs.

Pressure reference: Absolute

Accuracy¹⁾

Specifications only valid for clean gaseous SF₆

Dew point: ±3 K

Density: ±0.60 %, ±0.35 g/litre (-40 ... 80 °C)

Temperature: ±1 K

Pressure: $\pm 0.20 \%$, $\pm 32 \text{ mbar } (-40 ... < 0 °C)$

±0.06 %, ±10 mbar (0 ... 80 °C)

Long-term stability at reference conditions 2)

Temperature: $\leq \pm 0.10 \%$ of span/year Pressure: $\leq \pm 0.05 \%$ of span/year Dew point: $\leq \pm 0.50 \%$ of span/year

Refresh rate

Density: 20 ms Temperature: 20 ms Pressure: 20 ms

Dew point: 2 s (typical), auto-adjustment cycle every 30 min.

Permissible ambient temperature

| Selectable versions | | |
|---------------------|---------------------------|---------------------------|
| Standard | -40 +80 °C -40 +176 °F | -40 +80 °C -40 +176 °F |
| Option | -60 +80 °C -76 +176 °F | -60 +80 °C -76 +176 °F |

Power supply UB+

DC 17 ... 30 V

Power consumption

max. 0.5 W (max. 3 W during the heating phase of the humidity sensor)

Electrical connection

Circular connector M12 x 1 (5-pin) MODBUS® RTU via RS-485 interface

| Circular connector M12 x 1 (5-pin) | | | |
|------------------------------------|---|------------------|---------------|
| | 1 | - | - |
| (20°01) | 2 | U_{B}^{+} | Power supply |
| ((30 5 04)) | 3 | U _B - | Ground |
| | 4 | Α | Signal RS-485 |
| | 5 | В | Signal RS-485 |

¹⁾ Following DIN EN 60770-2

Functionality MODBUS®

Mixture ratio of SF_6 to N_2 or CF_4 (default 100 % SF_6 gas)

Customer-specific sensor name

Measured values with alternative units can be retrieved directly in the MODBUS® registers.

- Density: g/litre, kg/m³
- Temperature: °C, °F, K
- Pressure: mbar, Pa, kPa, MPa, psi, N/cm², bar (at 20 °C)
- Humidity: ppmv, ppmw
- Dew point: °C
- Freezing point: °C
- Relative humidity: %

Process connections

| Selectable versions |
|-------------------------------------|
| G 1 B, male thread, stainless steel |
| DN20, female thread |
| G ½ B, male thread |
| Malmkvist® |
| G % JIS |
| Flange D40 |
| M10 x 0.5 |
| Via measuring chamber (see page 5) |
| DN8, female thread |
| Other connections on request |

Case

Stainless steel

Permissible air humidity

≤ 90 % r. h. (non-condensing)

Ingress protection

IP65, only when plugged in and using mating connectors with the corresponding ingress protection

Electrical safety

Protected against reverse polarity, protected against overvoltage

Dimensions

Diameter: 48 mm Height: 96 mm

Weight

approx. 0.40 kg

²⁾ per IEC 61298-2

EMC tests

For EMC, observe the installation instructions of the operating instructions.

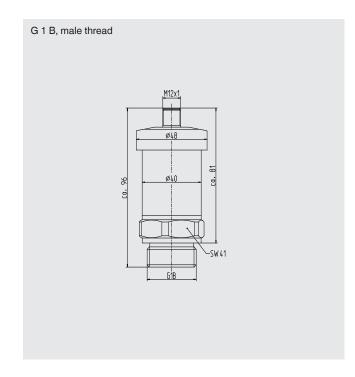
- Immunity per IEC 61000-4-3: 30 V/m (80 MHz ... 2.7 GHz)
- Burst per IEC 61000-4-4: 4 kV
- Surge immunity per IEC 61000-4-5: 1 kV conductor to ground, 1 kV conductor to conductor
- ESD per IEC 61000-4-2: 8 kV/15 kV, contact/air
- High-frequency fields per IEC 61000-4-6: 3 V

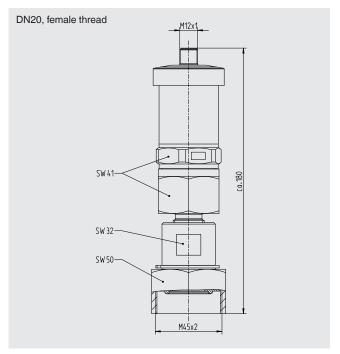
Approvals

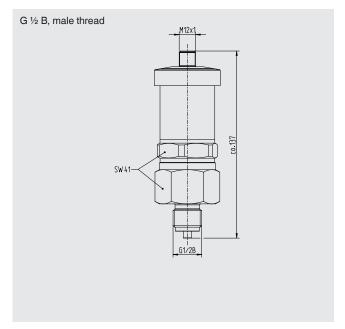
| Logo | Description | Country |
|------|---|--------------------------------|
| CE | EU declaration of conformity ■ EMC directive, EN 61326 emission (group 1, class B) and immunity (industrial application) ■ RoHS directive | European Union |
| EAC | EAC EMC directive | Eurasian Economic Community |

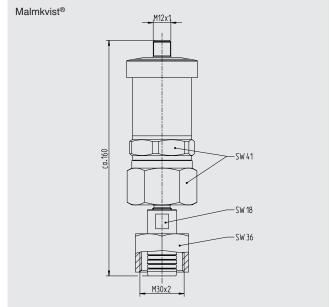
Approvals and certificates, see website

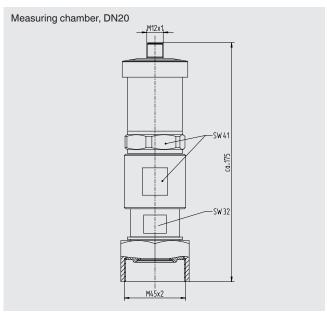
Dimensions in mm

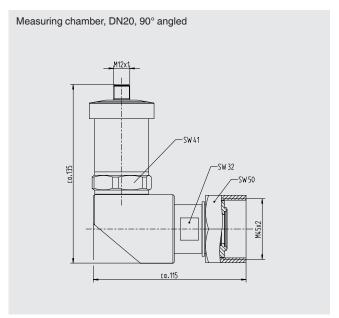


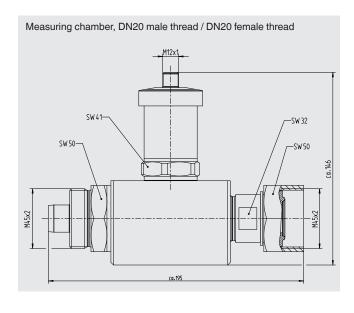


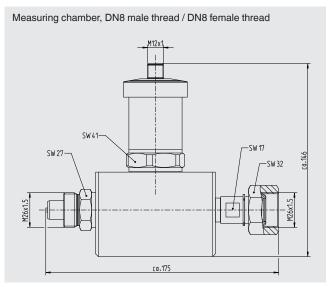


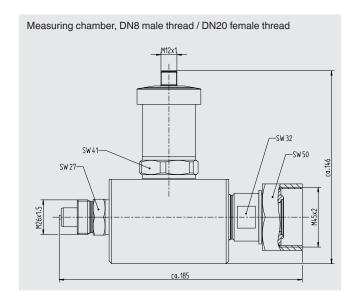


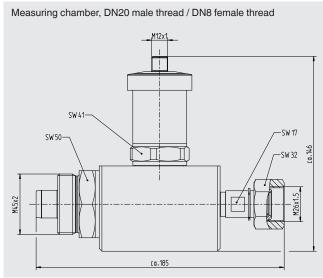


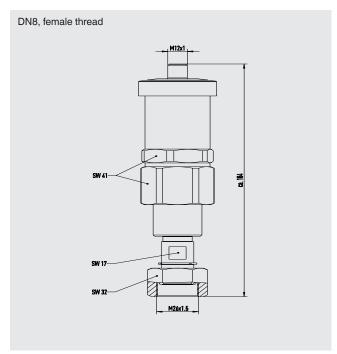












Accessories

| Designation | Order number |
|---|---|
| Modbus® startup kit for measured value recording and configuration, consisting of: ■ Power supply unit for transmitter ■ Cable with M12 x 1 connector ■ Interface converter (RS-485 to USB) ■ USB cable type A to type B ■ Modbus® tool software | 14075896 |
| WIKAsoft-GD for configuration and testing of the sensor | Free download from: www.wika.com/Download |

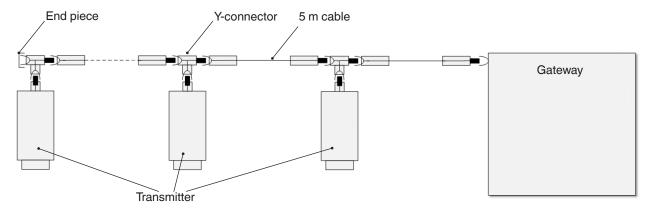
| Cable shielded, M12 x 1, AWG20 | Order number |
|--------------------------------|--------------|
| Length 1 m | 14372501 |
| Length 2 m | 14372502 |
| Length 3 m | 14372503 |
| Length 4 m | 14372504 |
| Length 5 m | 14372505 |
| Length 6 m | 14372506 |
| Length 7 m | 14372507 |
| Length 8 m | 14372500 |
| Length 9 m | 14372509 |
| Length 10 m | 14372510 |
| Length 15 m | 14372511 |
| Length 20 m | 14372513 |
| Length as required | on request |

| Conector | Shield | Order number |
|------------------------------|------------------------|--------------|
| Y-connector, M12 x 1 (5-pin) | Sensor side unshielded | 14294061 |
| T-connector, M12 x 1 (5-pin) | Sensor side unshielded | 14294063 |
| Y-connector, M12 x 1 (5-pin) | Sensor side shielded | 14271396 |
| T-connector, M12 x 1 (5-pin) | Sensor side shielded | 14109450 |
| End piece, M12 x 1 | - | 14299963 |

If no cable will be installed between connector and sensor, we recommend using connectors which are unshielded on the sensor side.

| Spare parts | Order number |
|--|--------------|
| Sealing for process connection G 1 B, male thread, (included in the standard scope of delivery.) | 14046738 |

Installation example



Ordering information

Model / Permissible ambient temperature / Process connection / Accessories

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The specifications given in this document represent the state of engineering at the time of publishing. We reserve the right to make modifications to the specifications and materials.

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Switchyard (345 kV) Breakers

| 0.5% Loss Rate | | |
|--|---------------|--|
| Cost | \$ 250,000.00 | |
| Replacement interval (yr) | 30.00 | |
| Replacements over life | 1.00 | |
| Life (years) | 30.00 | |
| Annual leak rate | 0.5% | |
| SF6 lb/yr | 3.44 | |
| SF6 lb/30 yr | 103.05 | |
| SF6 ton/30 yr | 0.05 | |
| Cost over 30 years/ton SF6 | \$ 4,852,014 | |
| Additional SF6 tons removed over 30 years | 0.04 | |
| Additional SF6 tons removed per year | 0.0014 | |
| | | |
| Global Warming Potential (SF6) | 22,800 | |
| CO2e lb/30 yr | 2,349,540.00 | |
| CO2e ton/30 yr | 1,174.77 | |
| Cost over 30 years/ton CO2e | \$ 213 | |
| Additional CO2e tons removed over 30 years | 939.82 | |
| Additional CO2e tons removed per year | 31.33 | |

| 0.1% Loss Rate | | |
|--------------------------------|----|-------------|
| Cost | \$ | 250,000.00 |
| Replacement interval (yr) | | 5.00 |
| Replacements over life | | 6.00 |
| Life years | | 30.00 |
| annual leak rate (low) | | 0.1% |
| SF6 lb/yr | | 0.69 |
| SF6 lb/30 yr | | 20.61 |
| SF6 ton/30 yr | | 0.01 |
| Cost over 30 years/ton SF6 | \$ | 145,560,408 |
| | | |
| | | |
| | | |
| Global Warming Potential (SF6) | | 22,800 |
| CO2e lb/30 yr | | 469,908.00 |
| CO2e ton/30 yr | | 234.95 |
| cost over 30 years/ton CO2e | \$ | 6,384 |
| | | |
| | | |

Generator (19 kV) Breakers

| 0.5% Loss Rate | | |
|--|----------------|--|
| Cost | \$ 700,000.00 | |
| Replacement interval (yr) | 30.00 | |
| Replacements over life | 1.00 | |
| Life (years) | 30.00 | |
| Annual leak rate | 0.5% | |
| SF6 lb/yr | 0.12 | |
| SF6 lb/30 yr | 3.45 | |
| SF6 ton/30 yr | 0.0017 | |
| Cost over 30 years/ton SF6 | \$ 405,797,101 | |
| Additional SF6 tons removed over 30 years | 0.0014 | |
| Additional SF6 tons removed per year | 0.000046 | |
| | | |
| Global Warming Potential (SF6) | 22,800 | |
| CO2e lb/30 yr | 78,660.00 | |
| CO2e ton/30 yr | 39.33 | |
| Cost over 30 years/ton CO2e | \$ 17,798 | |
| Additional CO2e tons removed over 30 years | 31.46 | |
| Additional CO2e tons removed per year | 1.05 | |

| 0.1% Loss Rate | | |
|--------------------------------|-------------------|--|
| cost | \$ 700,000.00 | |
| Replacement interval (yr) | 5.00 | |
| Replacements over life | 6.00 | |
| Life years | 30.00 | |
| Annual leak rate | 0.1% | |
| SF6 lb/yr | 0.023 | |
| SF6 lb/30 yr | 0.69 | |
| SF6 ton/30 yr | 0.0003 | |
| Cost over 30 years/ton SF6 | \$ 12,173,913,043 | |
| | | |
| | | |
| | | |
| Global Warming Potential (SF6) | 22,800 | |
| CO2e lb/30 yr | 15,732.00 | |
| CO2e ton/30 yr | 7.87 | |
| Cost over 30 years/ton CO2e | \$ 533,944 | |
| | | |
| | | |

Auxiliary Boiler Vendor Quote Post Application NTEC Response #3

From: Andracsek, Robynn
To: Nelson, Minda

Subject: FW: Cost for controls on an aux boiler Date: Friday, January 11, 2019 10:25:49 AM

Robynn Andracsek 816-822-3596 \ 816-377-1288 randracsek@burnsmcd.com

From: Clayton M. Young <cmyoung@rentechboilers.com>

Sent: Wednesday, October 31, 2018 9:11 AM

To: Andracsek, Robynn <RAndracsek@burnsmcd.com> **Cc:** Jason Hayes (jason@jchrep.com) <jason@jchrep.com>

Subject: RE: Cost for controls on an aux boiler

An oxidation catalyst (CO catalyst) would be in the around \$75,000 or so. We'd have to build the catalyst housing which adds the to the expense.

Clayton Young

Rentech Boiler Systems, Inc. Phone: (325) 794-5631

From: Andracsek, Robynn < <u>RAndracsek@burnsmcd.com</u>>

Sent: Wednesday, October 31, 2018 8:29 AM

To: Clayton M. Young cc: Jason Hayes (jason@jchrep.com) < jason@jchrep.com>

Subject: RE: Cost for controls on an aux boiler

Clayton

One more question. If we just put on a oxidation catalyst without an SCR, would it just be \$50,000 or would it be more?

Thank you.

Robynn Andracsek 816-822-3596 \ 816-377-1288 randracsek@burnsmcd.com

From: Clayton M. Young < cmyoung@rentechboilers.com>

Sent: Friday, October 19, 2018 4:22 PM

To: Andracsek, Robynn < <u>RAndracsek@burnsmcd.com</u>> **Cc:** Jason Hayes (<u>jason@jchrep.com</u>) < <u>jason@jchrep.com</u>>

Subject: RE: Cost for controls on an aux boiler

Individually, the SCR and CO catalyst run about \$35,000 (each).

Clayton Young

Rentech Boiler Systems, Inc. Phone: (325) 794-5631

From: Andracsek, Robynn < RAndracsek@burnsmcd.com>

Sent: Friday, October 19, 2018 1:50 PM

To: Clayton M. Young < cmyoung@rentechboilers.com cmyoung@rentechboilers.com cmyoung@rentechboilers.com cmyoung@rentechboilers.com cmy

Subject: RE: Cost for controls on an aux boiler

Clayton

A follow-up question. Do you have a rough cost for SCR and CO catalyst replacement?

Robynn Andracsek 816-822-3596 \ 816-377-1288 randracsek@burnsmcd.com

From: Clayton M. Young < cmyoung@rentechboilers.com>

Sent: Friday, October 19, 2018 11:38 AM

To: Andracsek, Robynn <<u>RAndracsek@burnsmcd.com</u>> **Cc:** Jason Hayes (<u>jason@jchrep.com</u>) <<u>jason@jchrep.com</u>>

Subject: RE: Cost for controls on an aux boiler

Robynn,

Here are the responses for the additional equipment as requested below. I added a little contingency to the oxidation catalyst number than what I stated on the phone to ensure coverage.

Adder to supply SCR / aqueous ammonia skids & manifold equipment, with a 90% reduction in NOx:

• \$350,000.00

Adder to supply CO / Oxidation Catalyst (90% reduction of CO & 50% reduction of VOC's):

• \$50,000.00

Thanks and hope you have a great weekend.

Clayton Young

Rentech Boiler Systems, Inc. Phone: (325) 794-5631

From: Craig Young

Sent: Thursday, October 18, 2018 1:20 PM

To: Clayton M. Young cmyoung@rentechboilers.com>

Subject: FW: Cost for controls on an aux boiler



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